### LES - Bartow Facility Drum Storage Building Certification Report

December 1997

**Prepared By** 



ViroGroup, Inc. 1445 Pisgah Church Road Lexington, SC 29072 Phone (803) 957-6270 FAX (803) 957-3845



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December 8, 1997

Denny Walton, Capital Projects Director Laidlaw Environmental Services, Inc. P.O. Box 11393 Columbia, SC 29211

Re: Drum Storage Building Quality Assurance Certification Report

ViroGroup Project No.12-32804.DO

Dear Mr. Walton:

ViroGroup, Inc. (ViroGroup) has been contracted by Laidlaw Environmental Services, Inc. to perform quality assurance services and RCRA certification for the above referenced project. The facility which consists of an enclosed drum storage building is designed to perform as secondary containment for storage of hazardous waste with primary containment consisting of storage drums. The design plans and specifications used for bidding and construction of the facility are dated December 5, 1996 and August 19, 1996 respectively. The plans were revised during construction to provide specific water stop details dated, May 21, 1997 and are presented in Appendix 1.

The construction of the structure was initiated in March 1997 and was completed in December 1997. During the construction ViroGroup made seven (7) site visits sporadically throughout the construction sequence to provide quality assurance inspections of inprogress and completed aspects of the facility structure. During these site visits ViroGroup project engineers observed the condition and methodology of completed and in progress work. LES contracted with Ardaman Associates (a local engineering materials testing company) either directly or through the general contractor (SEMCO) for quality control work during construction. LES also provided a construction manager on-site on a part time basis throughout the construction.

This report is separated into two main sections with the first section presenting ViroGroup's quality assurance documentation and certification that the facility was constructed in general accordance with project plans and specifications and the second section presenting the data ViroGroup has used in evaluating and providing a certification that the containment portion and other aspects of the structure meets the intent of RCRA regulations, specifically 40 CFR 264 Subpart I.

### Section I Quality Assurance Report

As indicated ViroGroup made seven visits to the facility during construction to document the procedures, methodologies and progress of construction. These visits were supplemented by data received from Ardaman and Associates with respect to soil, concrete, and reinforcing steel and data from the LES on-site construction manager with respect to other aspects of construction. During construction ViroGroup received the following shop drawing submittals and subsequently approved all final submittals:

- 1. Steel pre-engineered main structure by Whirlwind approved by Gene Amick, May 11, 1997
- Electrical system installation by RAYBRO approved by John Evans, March 17, 1997
- 3. Foundation system by SEMCO approved by John W. Bale
- 4. Fire suppression system by Wiginton Fire Sprinklers, Inc., approved by John D. Miles, July 16, 1997

The attached as-built drawings have been prepared by the following representatives for each primary section of the construction and have been used in our evaluation as to whether the facility was constructed in general accordance with the project plans and specifications:

- 1. Foundation plan John W. Bale Appendix 2
- 2. Floor plan John D. Miles Appendix 2
- 3. Electrical plan Horace Kirkland Appendix 2
- 4. Fire suppression system John D. Miles Appendix 3
- 5. Structural Steel John D. Nelson
- 6. Foam House John D. Miles Appendix 4

Based on the attached as-built plans (Appendices 2, 3, and 4), our periodic visits and data received from the LES construction manager and Ardaman Associates (Appendices 5 geotechnical report, 6 soils testing, 7 reinforcement inspections, 8 concrete testing, 9 concrete mix design) it is our professional opinion that the facility has been constructed in general accordance with the revised plans and specifications.

### Section 2 RCRA Certification

As indicated ViroGroup has also been retained to provide professional certification of the RCRA aspect of the facility. As outlined in 40CFR 264 Subpart I "Use and Management of Containers" RCRA requires that storage facilities of drums containing hazardous waste must meet the following criteria:

- 1. A container holding hazardous waste must always be closed during storage, except when it is necessary to add or remove waste.
- 2. At least weekly, the owner or operator must inspect areas where containers are stored, looking for leaking containers and for deterioration of containers and the containment system caused by corrosion or other factors.
- 3. Container storage areas must have a containment system that is designed and operated in accordance with the following,
  - (a) A base must underly the containers which is free of cracks or gaps and is sufficiently impervious to contain leaks, spills, and accumulated precipitation until the collected material is detected and removed;
  - (b) The base must be sloped or the containment system must be otherwise designed and operated to drain and remove liquids resulting from leaks, spills, or precipitation, unless the containers are elevated or are otherwise protected from contact with accumulated liquids;
  - (c) The containment system must have sufficient capacity to contain 10% of the volume of containers or the volume of the largest container, whichever is greater. Containers that do not contain free liquids need not be considered in this determination;
  - (d) Run-on into the containment system must be prevented unless the collection system has sufficient excess capacity in addition to that required in paragraph c above to contain any run-on which might enter the system; and

- (e) Spilled or leaked waste and accumulated precipitation must be removed from the sump or collection area in as timely a manner as is necessary to prevent overflow of the collection system.
- 4. containers holding ignitable or reactive waste must be located at least 15 meters (50 feet) from the facility's property line.
- 5. Incompatible wastes, or incompatible wastes and materials (see Appendix V for examples), must not be placed in the same container, unless §264.17(b) is complied with.
- 6. Hazardous waste must not be placed in an unwashed container that previously held an incompatible waste or material.

ViroGroup has based our evaluation of the constructed facility with respect to RCRA guidelines on the above mentioned criteria. Several of the items are operational procedures and not related to construction of the facility. This report addresses only those items which are construction oriented as discussed in the following paragraphs.

Items 1, 2, 3e, 6 and part of item 5 are operational procedures and therefore are not addressed in this report. Methodologies for verifying items 3a, 3b, 3c, 3d, 4, and part of 5 are as follows:

- 3a. ViroGroup has used the following mechanisms for evaluating the integrity of the base of the structure:
  - 1. Daily reports prepared by Ardaman Associates on inspections and observations they made on the following: foundation subgrade, floor slab subgrade, reinforcing steel, and concrete characteristics. Refer to appendix 6, 7 and 8 for daily reports on soils, concrete and reinforcing steel and Appendix 9 for concrete mix designs approved for the project. The geotechnical report outlining subsurface conditions and foundation design is included in appendix 5.
  - 2. Hydrostatic testing of the completed cells performed and documented by the Laidlaw Environmental Services Construction Manager. Test results of the hydrostatic testing are presented in appendix 10.
  - 3. Visual observations of the concrete for identifiable cracking.

- 3b. Visual observations were made to verify that the individual cells each sloped to a low spot to allow collection of spills. Refer to the attached as-built drawings (Appendix 2).
- 3c. Measurements were performed of each secondary containment cell after completion and the volume calculations are presented in appendix 11.
- 3d. The structure is constructed as a dock high facility which restricts all run -on.
- 5. The operational plan identifies internal methods of identifying individual waste streams. For physical separation once waste streams are identified, compatible and non compatible wastes can be separated because the facility is constructed with adjacent cells separated by an internal concrete dike (Appendix 1 and 2).

Based on our evaluations it is our professional opinion that the facility has been constructed in a manner which will allow it to function as intended in accordance with 40 CFR 264 Subpart I.

ViroGroup appreciates the opportunity to provide you with our professional services. Should you have any questions please call us.

Sincerely,

ViroGroup, Inc.

← John W. Bale, P.E.

Project Engineer

Reviewed by:

Charles S. Higgins, Jr., P.

Principal Engineer

FL # 0034452

JWB/lr

#### CERTIFICATION OF COMPLETION OF CONSTRUCTION

The hazardous waste container storage building for the Laidlaw Environmental Services of Bartow, Inc. facility located at 170 Bartow Municipal Airport, Bartow, Florida has been constructed in substantial accordance with the specific conditions of Construction Permit HC53-294150, as described in this certification report. Minor revisions are depicted in the attached As-Built Drawings. I certify that this document and the As-Built Drawings were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the persons or persons responsible for the construction of the building, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Laidlaw Environmental Services of Bartow, Inc. Facility EPA I.D. Number

#### FLD 980729610

**Facility** 

Charles S. Higgins, Jr., P.E. Principal Engineer FL# 0034452

Original Certification of December 8, 1997



#### CERTIFICATION OF COMPLETION OF CONSTRUCTION

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FLD 980 729 610

Facility EPA I.D. Number

Laidlaw Environmental Services of Bartow, Inc.

**Facility** 

Charles S. Higgias,

Principal Engineer FL# 0034452

12/9/97

### LES - Bartow Facility Drum Storage Building Certification Report

### **Appendices**

December 1997

Prepared By



ViroGroup, Inc. 1445 Pisgah Church Road Lexington, SC 29072 Phone (803) 957-6270 FAX (803) 957-3845

### **APPENDICES**

- 1. Revised Construction Plans
- 2. Building Foundation/Electrical As-Builts
- 3. Pre-Engineered Metal Building As-Builts
- 4. Fire Suppression System As-Builts
- 5. Geotechnical Exploration, Foundation Analysis and Design
- 6. Quality Control Data and Report for Foundation Preparation
- 7. Quality Control for Reinforcing Steel Inspection
- 8. Concrete Test Results
- 9. Concrete Mix Designs and Submittals
- 10. Secondary Containment Hydostatic Test Results
- 11. Secondary Containment Volume Calculations

### APPENDIX 1

**Revised Construction Plans** 

RECEIVED LEC 1 1 1997 DE P

### DRUM STORAGE BUILDING

PREPARED FOR

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ENVIRONMENTAL SERVICES OF BARTOW, INC.

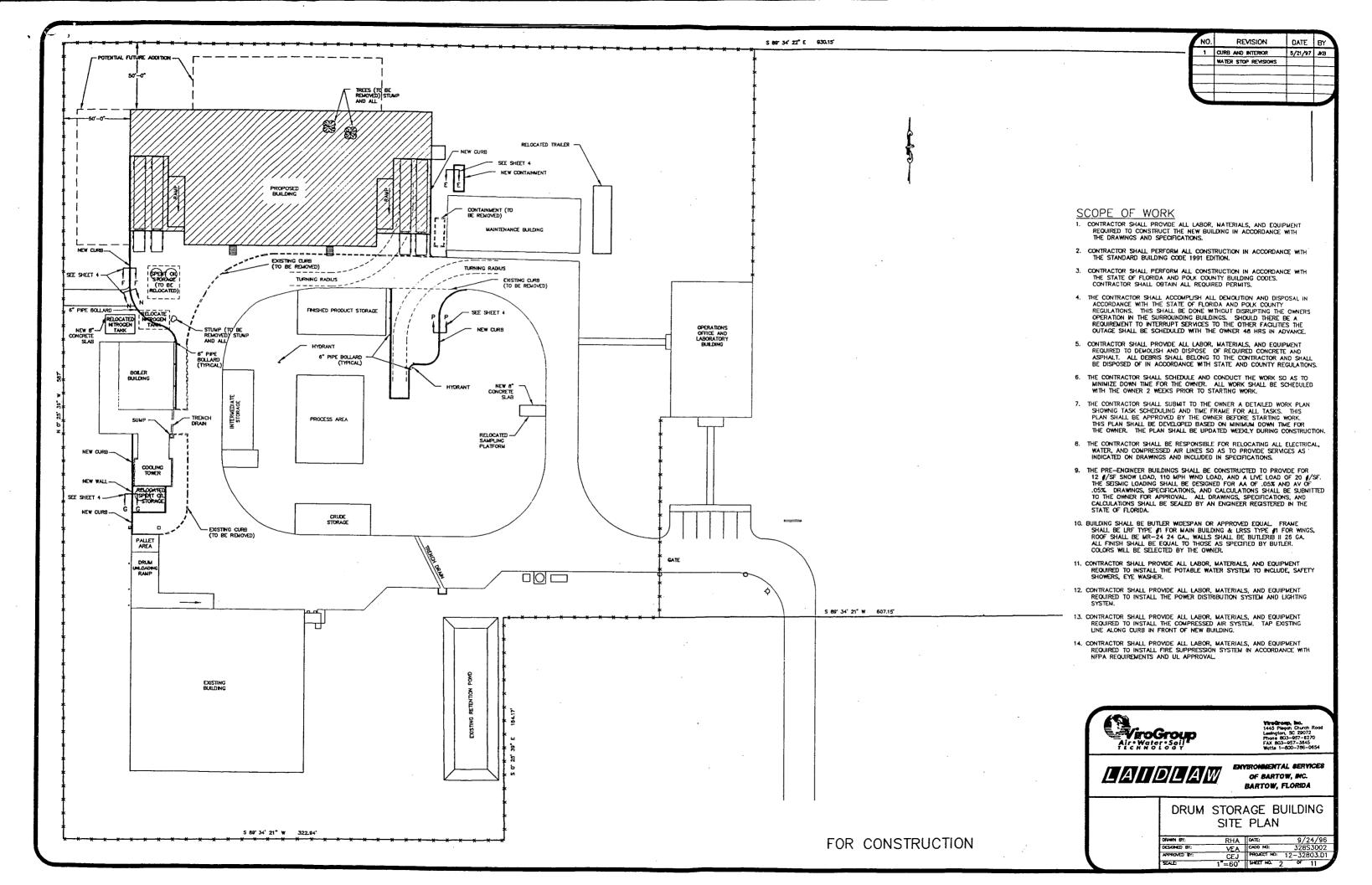
BARTOW, FLORIDA

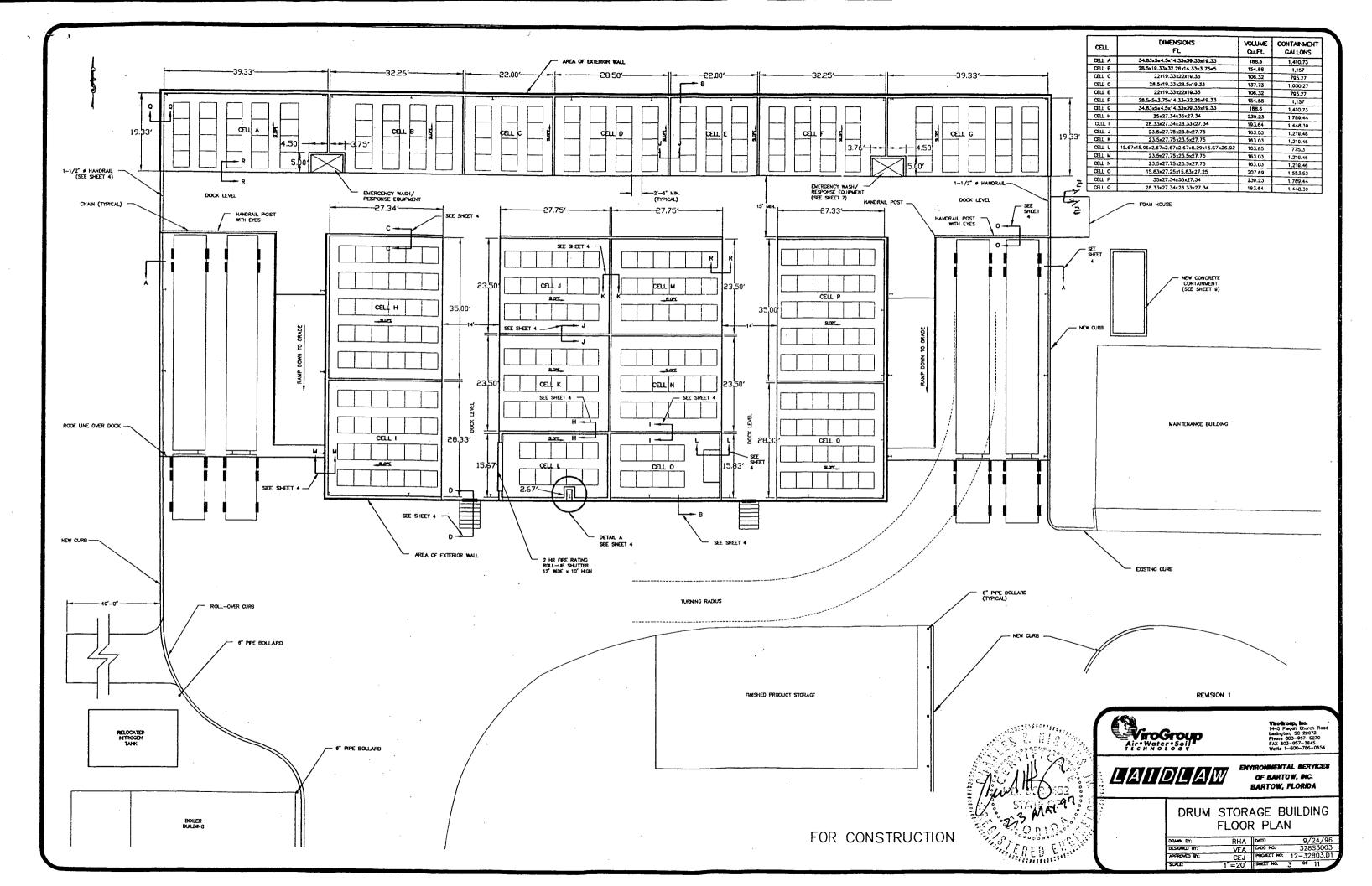
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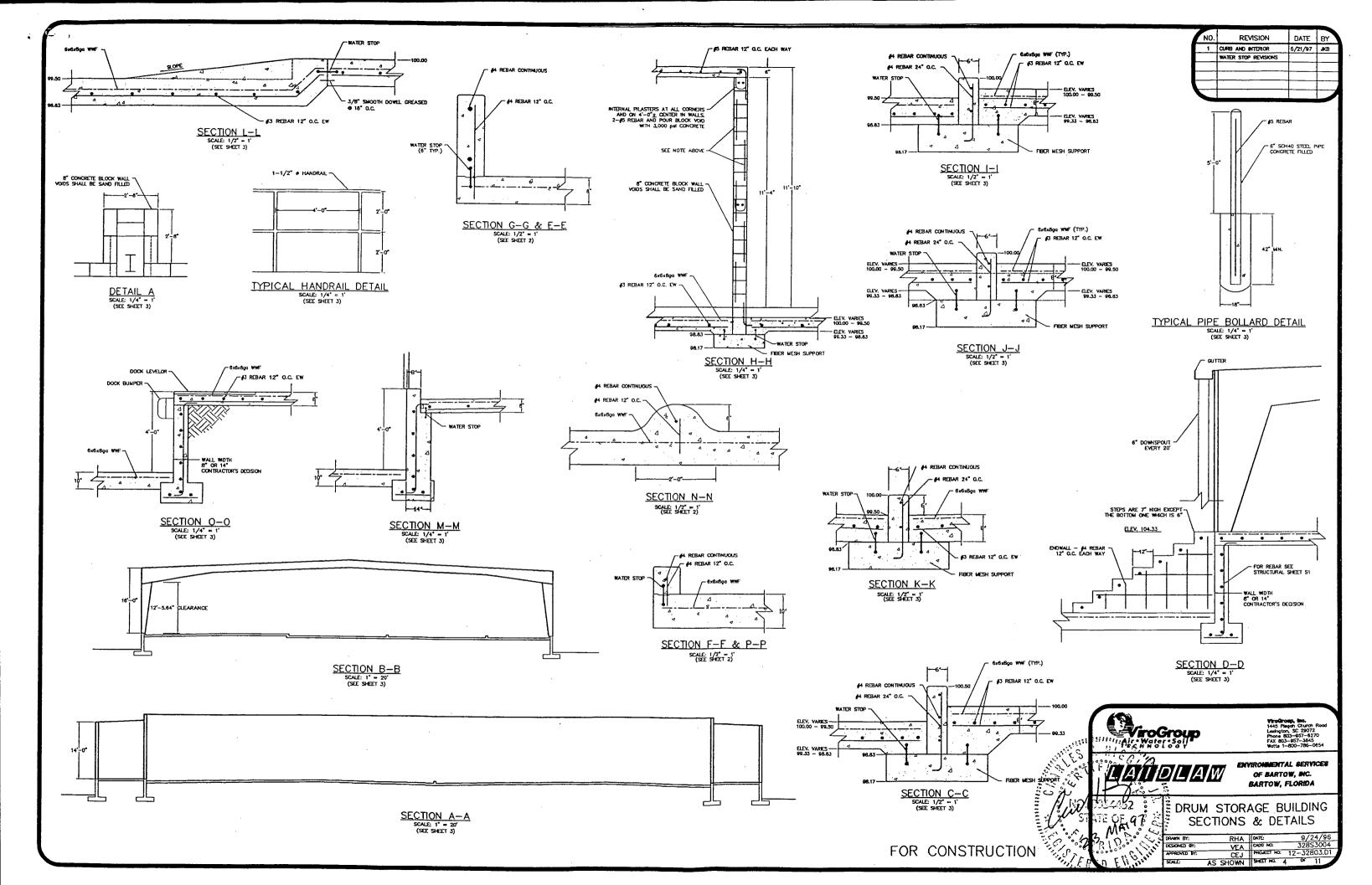


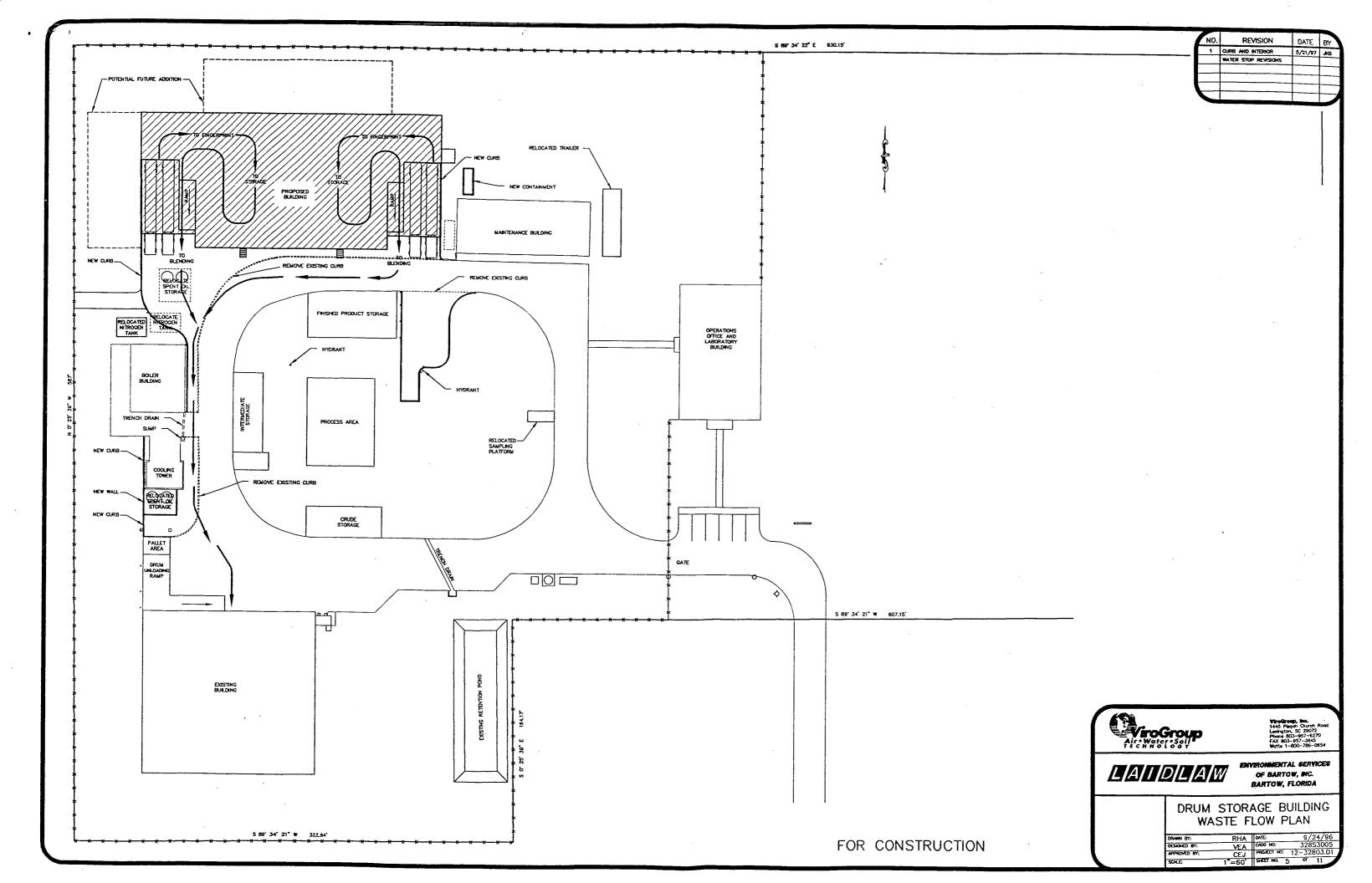
ETE Division

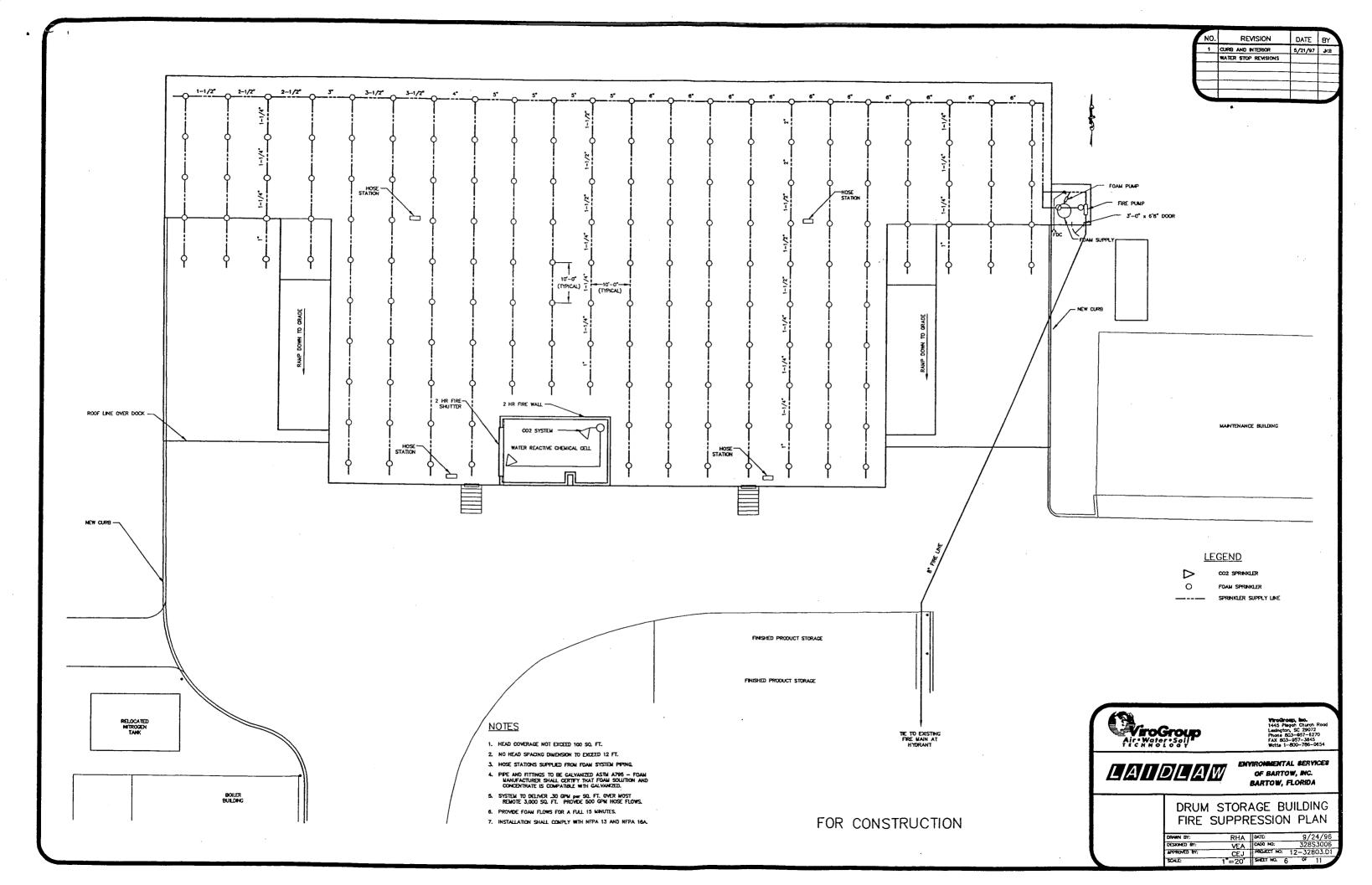
# LIST OF DRAWINGS SHEET NO. TITLE 1 COVER SHEET 2 SITE MAP 3 FLOOR PLAN 4 SECTIONS AND DETALS 5 WASTE PLAN PLAN 0 SPRINGLER SYSTEM PLAN 7 PIPMS SCHEMATC 8 ROOF PLAN 0 DEMOLITION & RELOCATION PLAN 10 GRADING PLAN 11 ELEVATION WE'MS 51 STRUCTURAL LAYOUT 52 STRUCTURAL LAYOUT 52 SLECTROAL SYSTEM PLAN 53 SLECTROAL SYSTEM PLAN

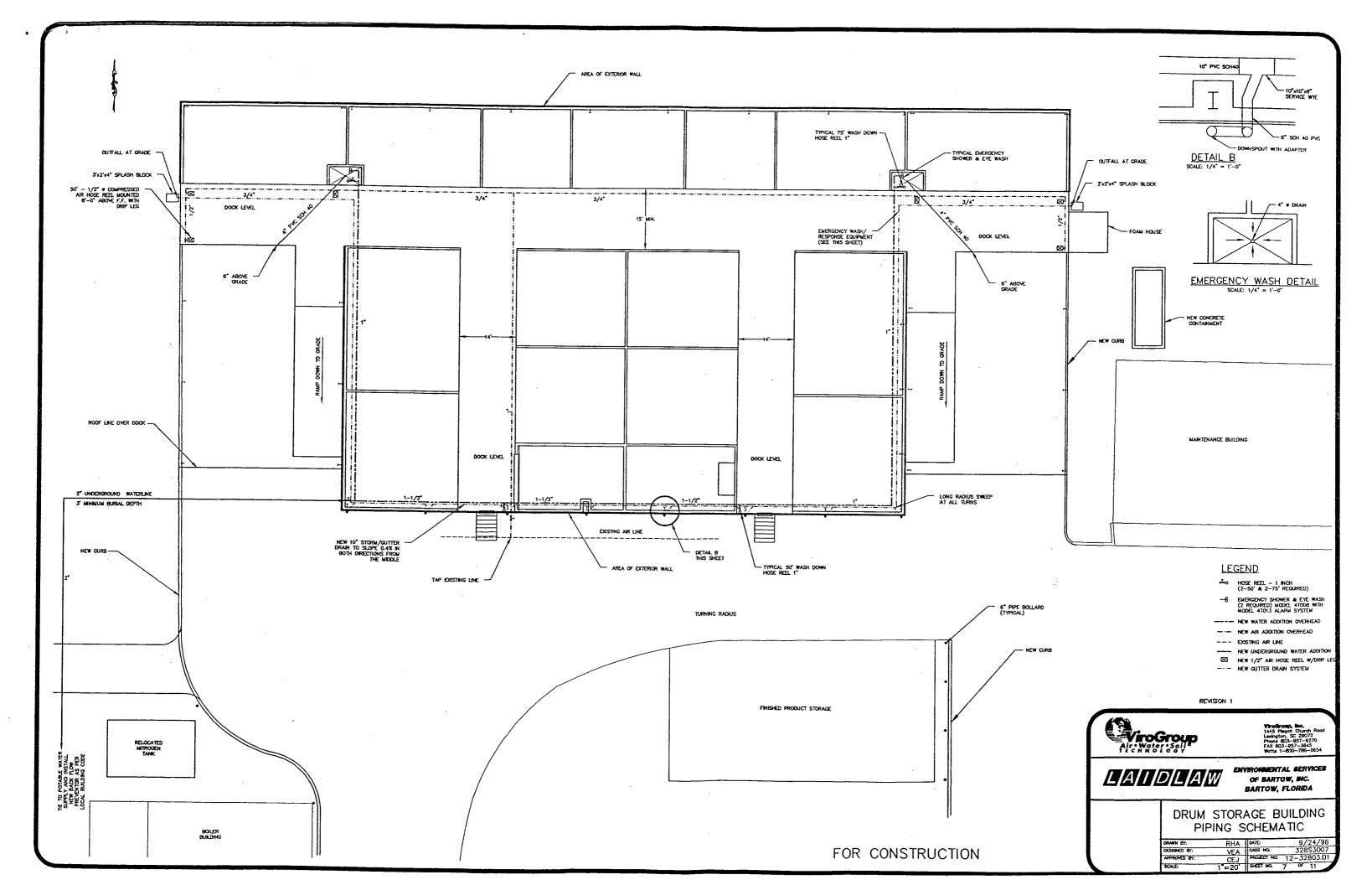


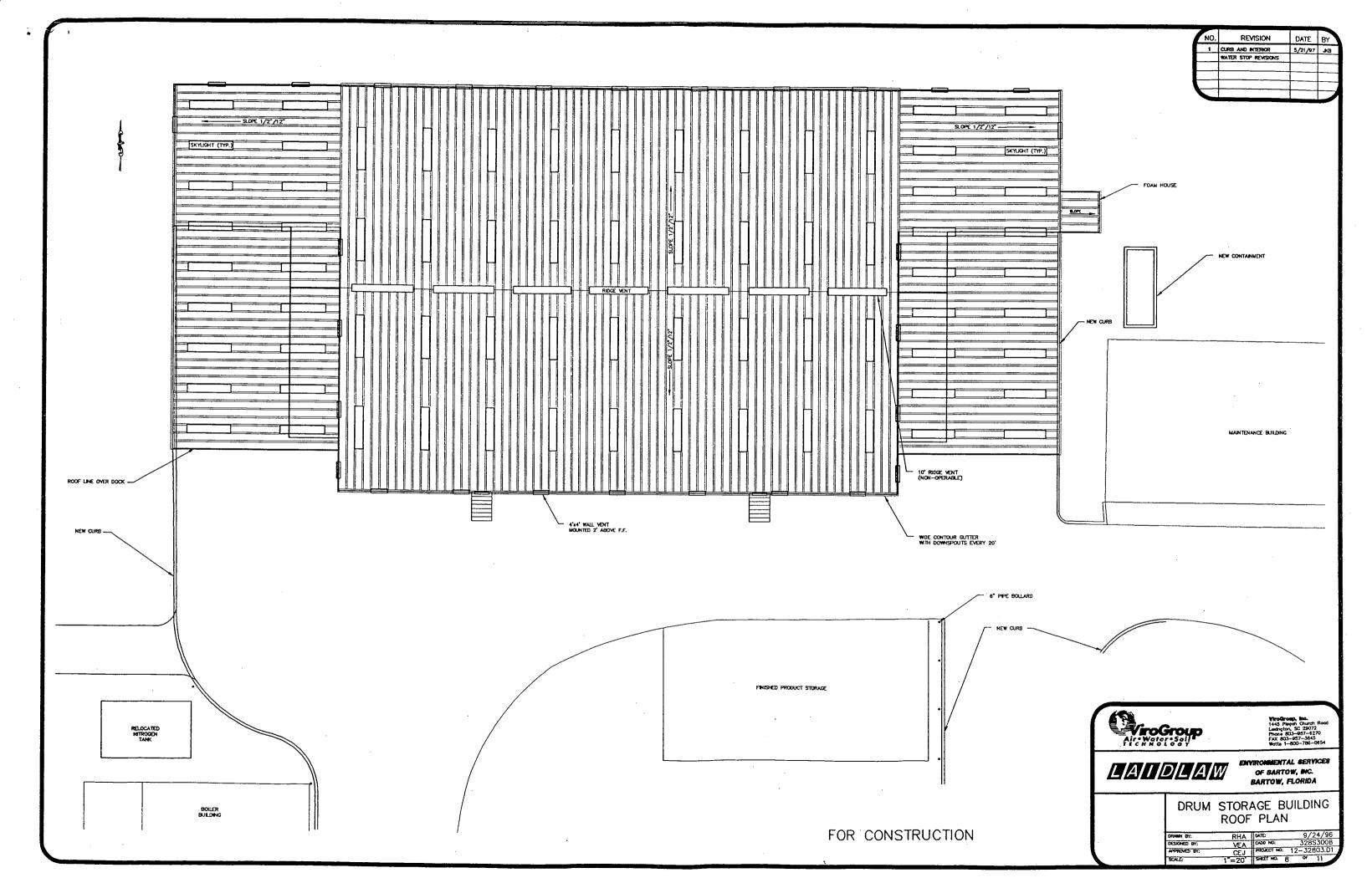


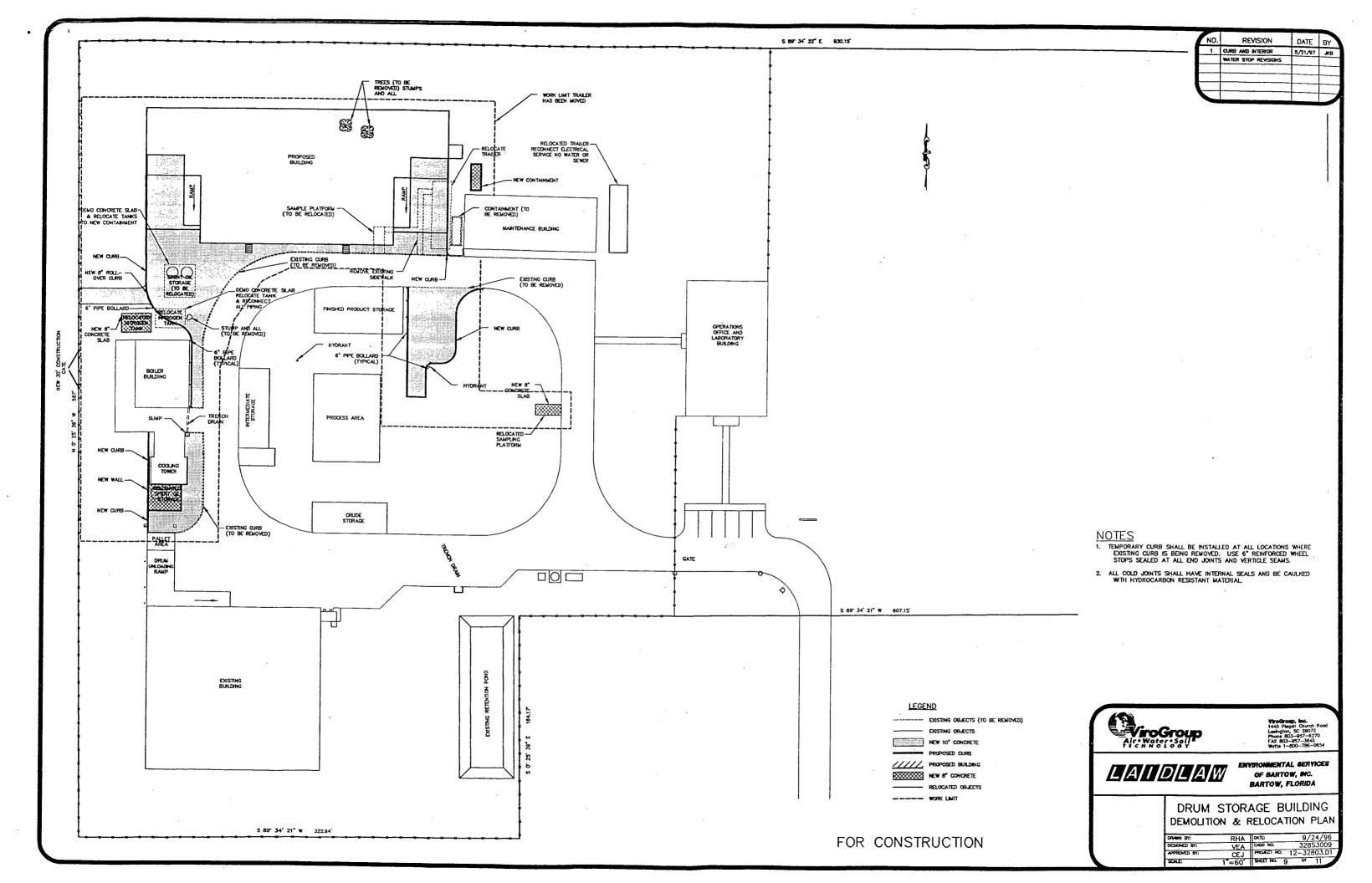


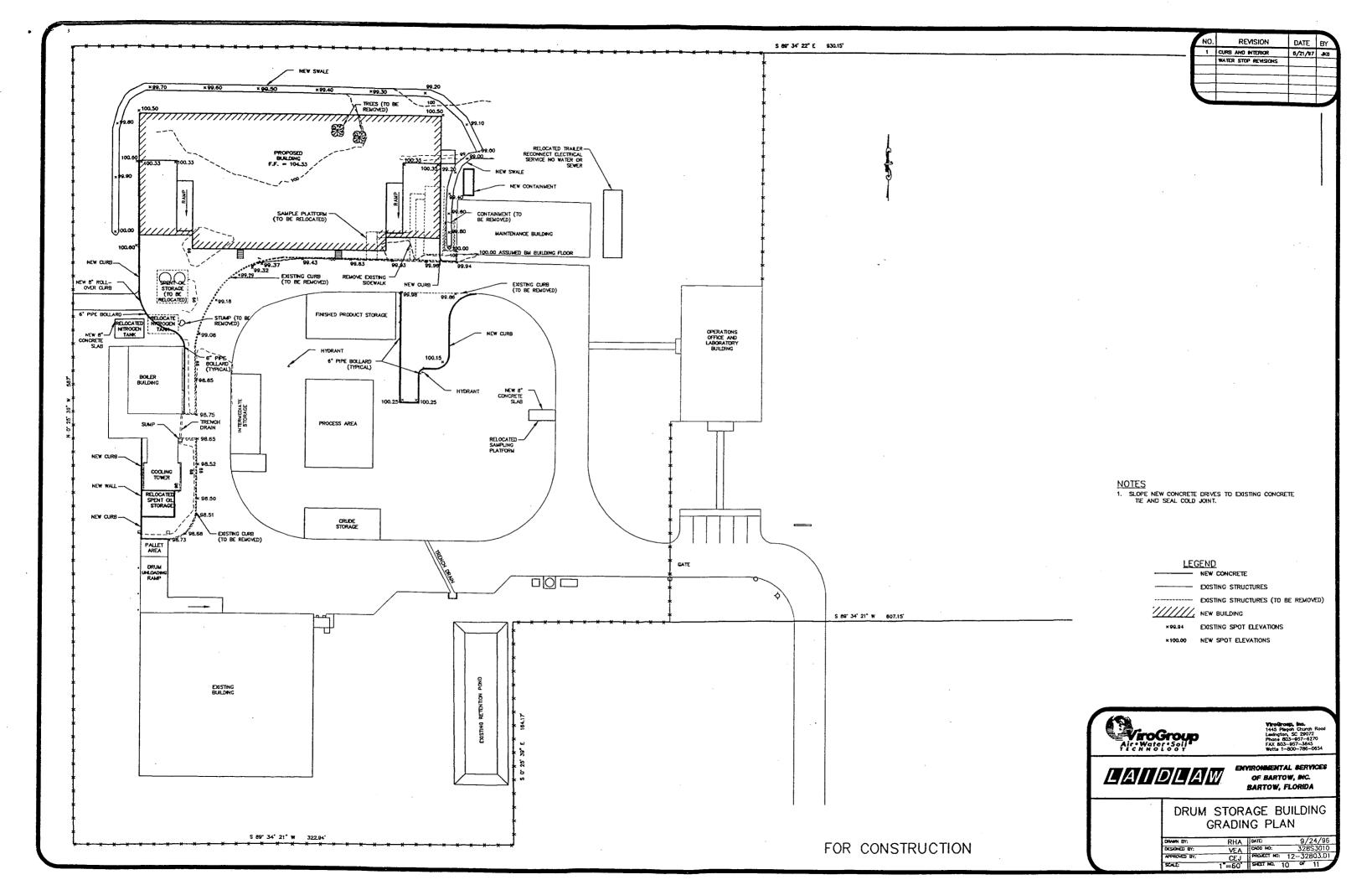




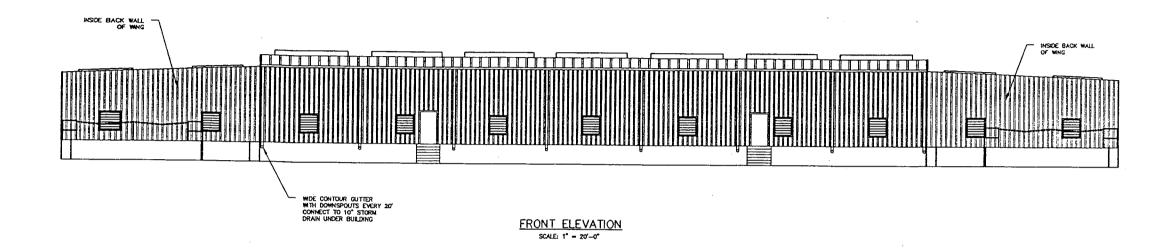


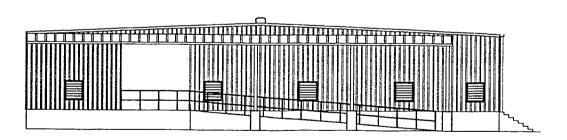






NO.	REVISION	DATE	BY
1	CURB AND INTERIOR	5/21/97	#GB
	WATER STOP REVISIONS		
		1	





SCALE: 1" = 20'-0"

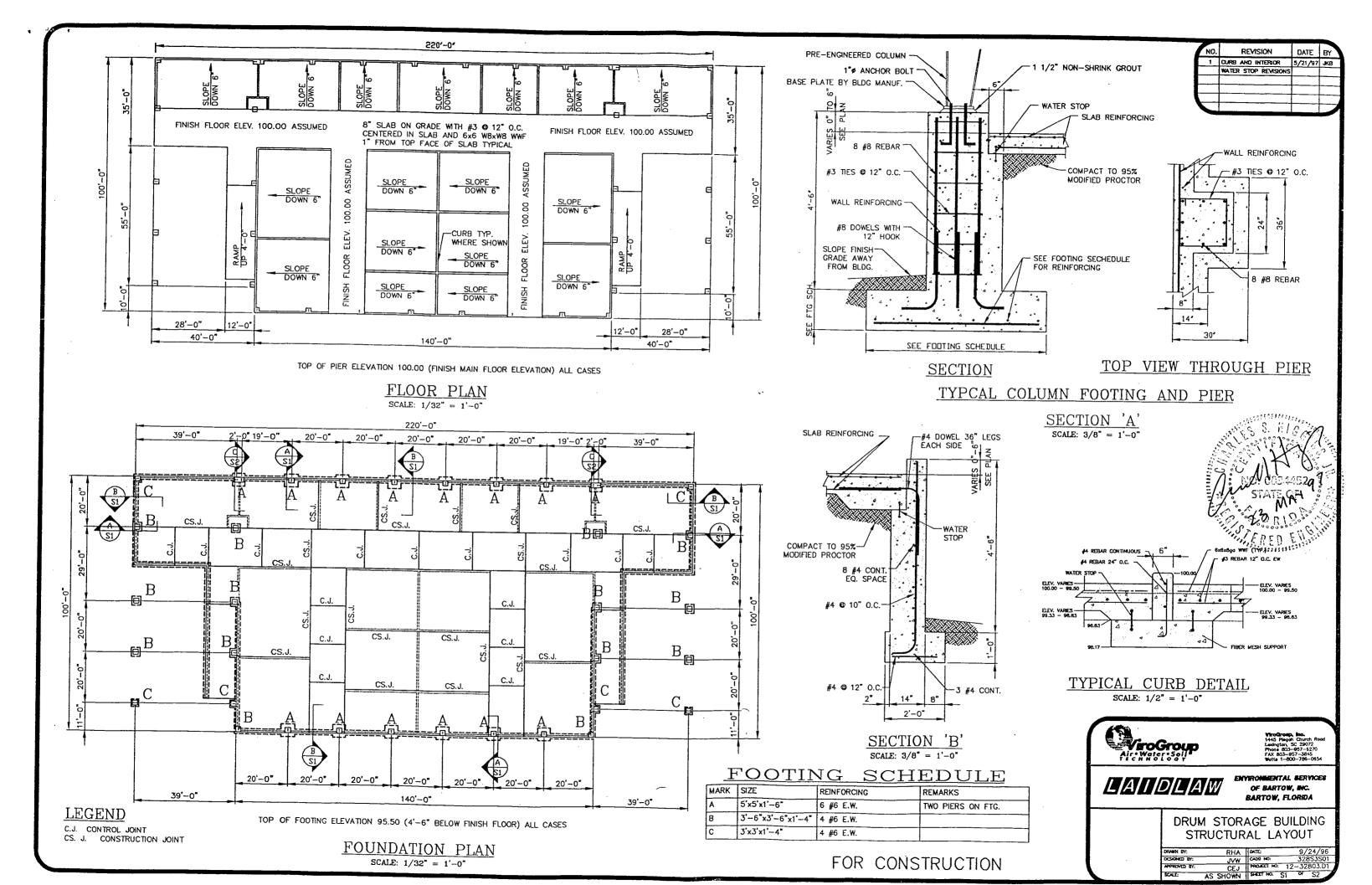


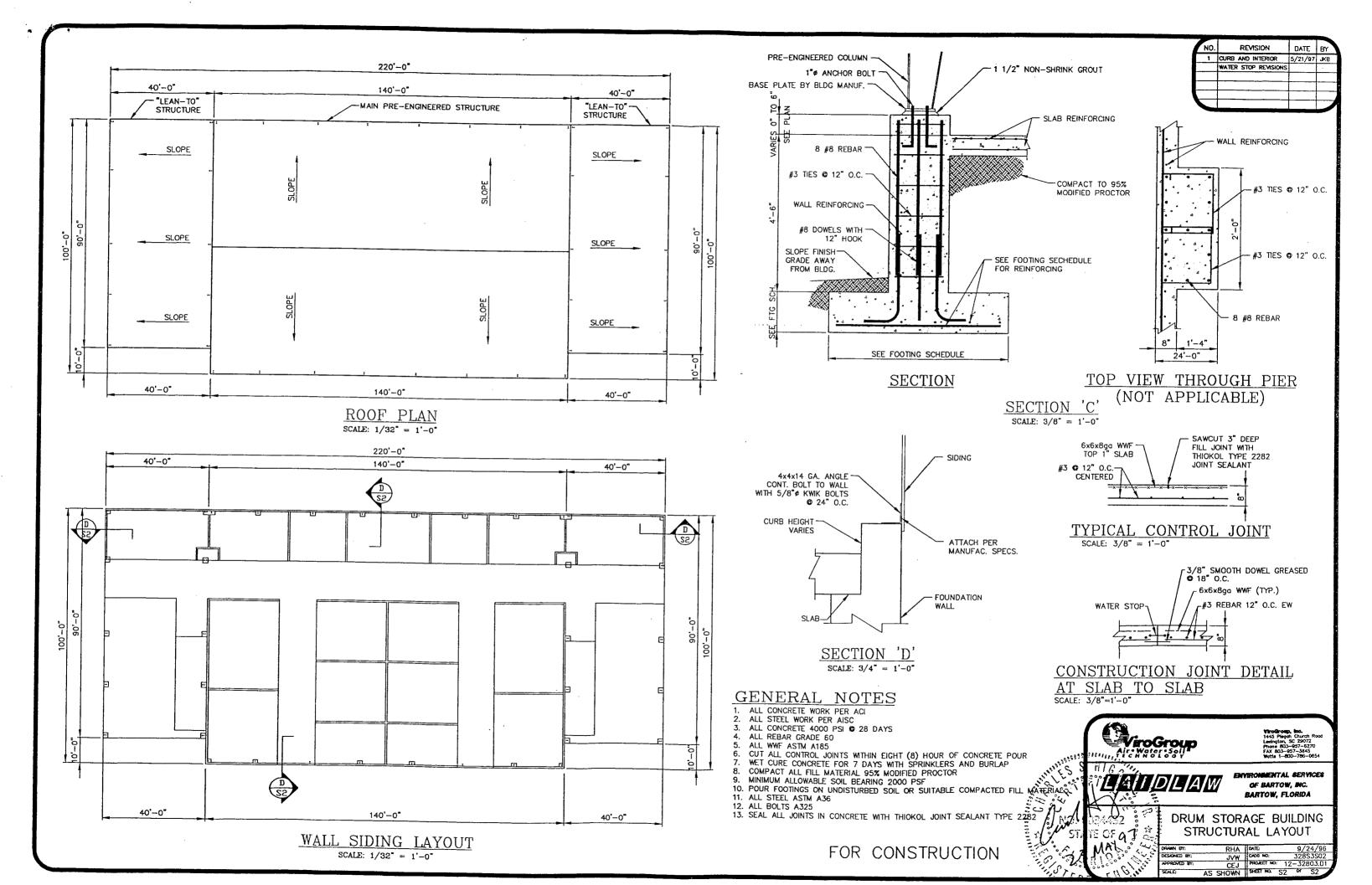
ViroGrosp, inc. 1445 Piegen Church Road Lashgton, SC 29072 Phone 803—957–8270 FAX 803–957–3845 Watta 1–800–786–0654

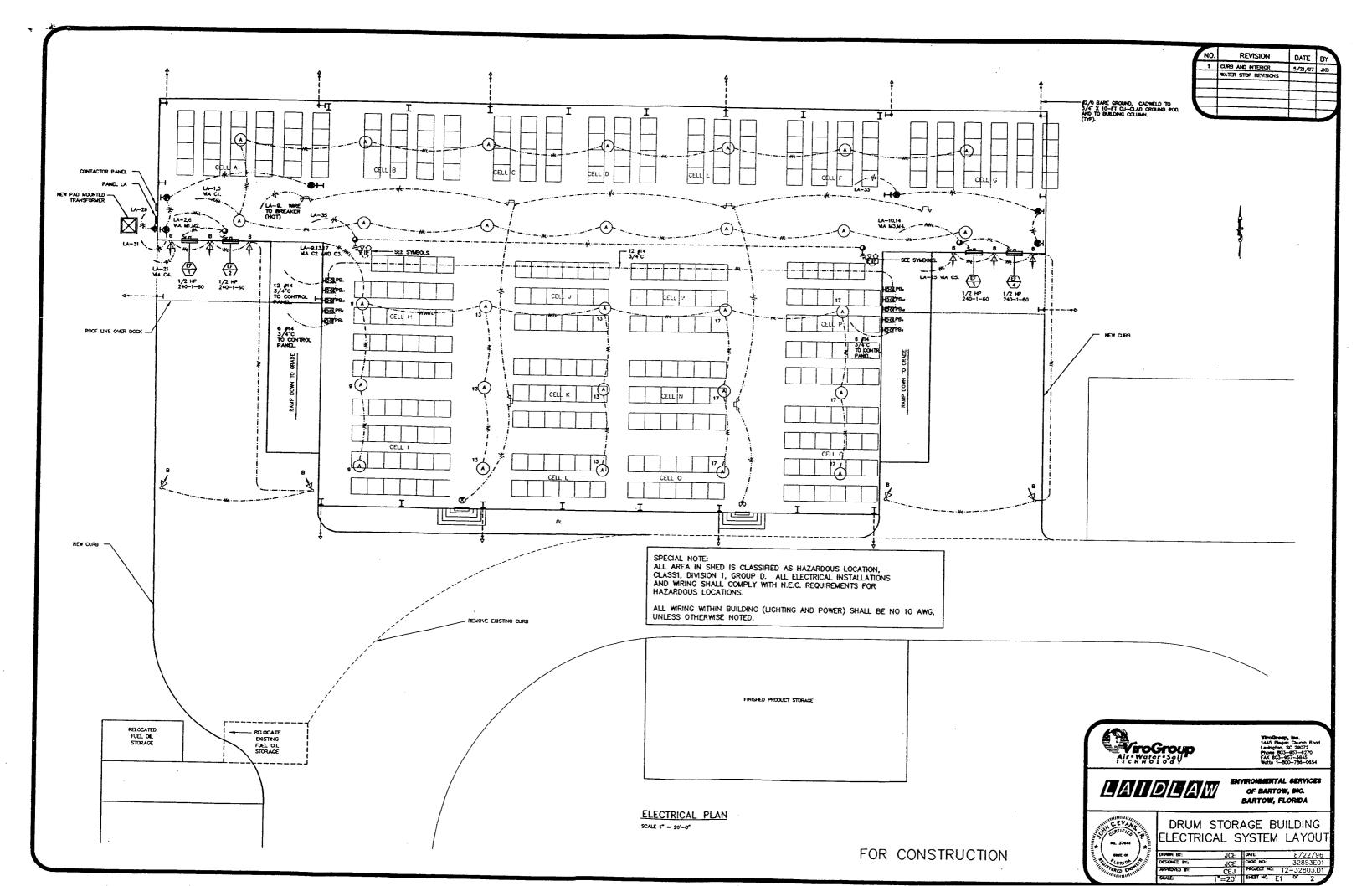


ENVIRONMENTAL SERVICES OF BARTOW, INC. BARTOW, FLORIDA

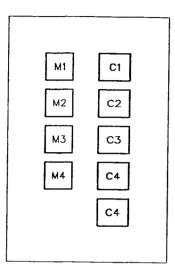
DRUM STORAGE BUILDING ELEVATION VIEWS

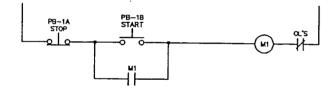






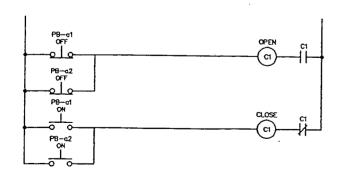
CONTROL SYSTEMS EQUIPMENT:		
TYPE	DESCRIPTION	
ENC	MEMA 4 ENCLOSED CABINET, 30-IN HIGH, 24-IN WIDE, 5-IN DEEP, WITH METAL BACK PANEL, HOFFMAN A-4 SERIES, OR EQUAL	
M1, M2 M3, M4	OPEN MOTOR STARTER, NEMA SIZE 0, 240-1-60, 1/2 HP WITH 120-VAC COIL AND HOLDING INTERLOCK. SQUARE D 8536/S80, OR APPROVED EQUAL.	
C1, C2 C3, C4 C5	MECHANICALLY HELD LIGHTING CONTACTOR, 30-AMP, 4-POLE, WITH 120-VAC COLS. SQUARE D 8903/LXQ, OR APPROVED EQUAL	
P81, P82 P83, P84	START-STOP PUSHBUTTON, SEALED, CLASS 1, DIVISION 1, CROUP D. SQUARE D 9001/BR214, OR APPROVED EQUAL	
P8a1, P8a2 P8b1, P8b2 P8c, P8d	ON-OFF PUSHBUTTON, SEALED, CLASS 1, DIVISION 1, GROUP D. SQUARE D 9001/BR214, OR APPROVED EQUAL	





#### CONTROL WIRING - FAN CIRCUIT

TYPICAL FOR EF-1, EF-2, EF-3, AND EF-4 NOT TO SCALE

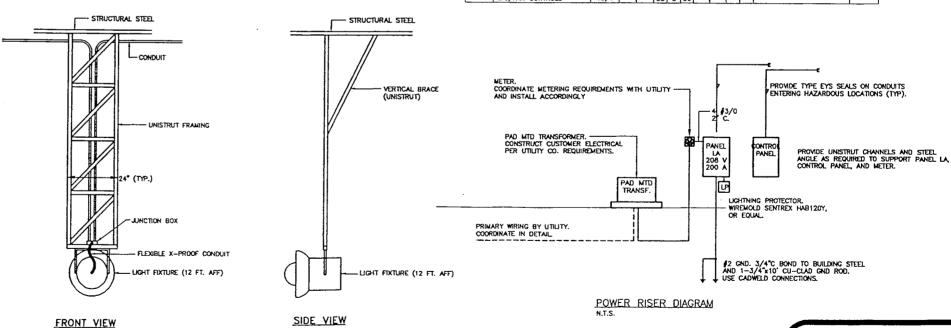


### LIGHTING CONTACTOR CONTROL WIRING

TYPICAL FOR C1, C2, AND C3.
SIMILAR FOR C4 AND C5, EXCEPT CONTROLLED BY ONE SET OF PB'S.
NOT TO SCALE

	ELECTRICAL SYMBOLS				
0	H.L.D. FIXTURE, PENDANT MOUNT.				
<b>\$</b>	SAME, EXCEPT WITH FLOODLIGHT TRUNNION BRACKET. SEE MOUNTING DETAIL				
⊗	EXIT SIGN.				
<b>↔</b>	EMERGENCY BATTERY LICHT.				
Sr	DISCONNECT SMITCH FOR FAM. MOUNT ADJACENT TO FAM. USE 20-AMP, 2-POLE EXPLOSION PROOF SMITCH, CROUSE HINDS, OR EQUAL.				
163	PUSHBUTTON FOR FAN STARTER OR LIGHTING CONTACTOR. SEE EQUIPMENT SCHEDULE. MOUNT ON COLUMN, 48-IN. ABOVE FIN. FLOOR.				
•	OFCI RECEPTACLE, 20A-120V-NEMA 5-20R. MOUNTING HEICHT 48" AFF. PROVIDE TYPE FD BOX AND WEATHERPROOF COVER PLATE.				
H	EXPLOSION PROOF RECEPTACLE, 20A-120V. MOUNTING HEIGHT 48" AFF. CROUSE HINDS CPS-152-201, OR APPROVED EQUAL.				
8	EMERGENCY LIGHT TO FLASH WHEN EMERGENCY SHOWER IS OPERATED. PROVIDE 120V EXPLOSION PROOF CONNECTION TO LIGHT AS REQUIRED.				
Ê	EMERGENCY SIGNAL HORN FOR EMERGENCY SHOWER, SAME AS ABOVE.				
Ю 0	WALL OR CEILING MOUNTED JUNCTION BOX.				
_	PANELBOARD.				
14: LA-1,	BRANCH CIRCUIT WIRING RUN EXPOSED AT WALLS OR CEILING. SLASH MARKS  MODICATE MUMBER OF #10 CONDUCTORS. WHERE MORE THAN TWO ARE  REQUIRED, SHORT SLASH DENOTES HOT OR SWITCH LEG, LONG SLASH DENOTES  NEUTRAL, "L" DENOTES GREEN GROUNDING WIRE. ARROW DENOTES HOME  RUN, NUMERAL DENOTES CIRCUIT NUMBER.				

FIXTURE SCHEDULE			
TYPE	VOLTAGE	DESCRIPTION	LAMP
^	MULTI-TAP 240V	EXPLOSION PROOF FIXTURE WITH MULTI-TAP BALLAST (SET AT 240-VOLT) AND STANDARO REFLECTOR, CLASS 1 DIVISION 1 GROUP 0, APPLETON AUBH SERIES, OR EQUAL OF CROUSE HINDS OR KILLARK. PROVIDE STEEL CHANNELS TO SUPPORT FIXTURE.	1/400W/MH SUPER 40K LUMENS
8	MULTI-TAP 240V	SAME AS TYPE A, EXCEPT WITH 30-DECREE REPLECTOR. FIXTURE MOUNTING HEIGHT TO BE 12-FT. ABOVE FINISHED FLOOR.	1/400W/MH "SUPER" 40K LUMENS
С	120V	EMERGENCY BATTERY LIGHT, EXPLOSION PROOF, CLASS 1, DIVISION 1, GROUP D. DUAL—LITE XPB—75P SERIES WITH (2) EX—1CD LIGHT HEADS.	INCLUDED
D	120V	EXIT SICN, EXPLOSION PROOF, CLASS 1, DIVISION 1, CROUP 0. DUAL-LITE XPB-75P SERIES WITH (1) EX-100 LIGHT HEAD AND EX-100 SIGN. FIXTURE MOUNTING HEIGHT TO BE 8 FT. ABOVE FINISHED FLOOR.	INCLUDED



TYPE B LIGHT FIXTURE MOUNTING DETAIL

CONTACTOR	CIRCUITS CONTROLLED	PUSHBUTTON CONTROLLER
CI	LA-1, LA-5	P8-a1, P8-a2
C2	LA-9, LA-13	PB-61, PB-62
C3	LA-17	PB-61, P8-62
C4	LA-21	P8-c
C5	LA~25	PB-d

#### GENERAL NOTES

- A. VISIT SITE TO DETERMINE EXISTING CONDITIONS PRIOR TO SUBMITTING BID.
- B. DO NOT SCALE THESE DRAWINGS. ROUGHING IN SHALL BE DONE FROM FIELD CONDITIONS AND DIMENSIONS ON ARCHITECTURAL DRAWINGS AND EQUIPMENT SHOP DRAWINGS.
- C. ELECTRICAL CONTRACTOR SHALL DO ALL CUITING AND PATCHING AS REQUIRED TO INSTALL HIS WORK. FINISH PATCHING AND PAINTING WILL BE DONE BY THE GENERAL CONTRACTOR.
- D. PRIOR TO DIGGING ANY TRENCHES, NOTIFY ALL UTILITIES (ELECTRIC, GAS, TELEPHONE, WATER, AND SEWER) AND OBTAIN LOCATIONS OF UNDERGROUND UTILITIES.
- E. ANY DAMAGES DONE TO UNDERGROUND UTILITIES OR PIPING BY THIS CONTRACTOR WILL BE REPAIRED BY THE OWNER OF THE LINE IN A SATISFACTORY MANNER. THIS CONTRACTOR WILL BEAR ALL COSTS FOR REPAIRS.
- F. ALL WORK SHALL COMPLY WITH THE 1996 NATIONAL ELECTRICAL CODE AND ALL LOCAL CODES.
- C. APPLY AND PAY FOR ALL PERMITS AND INSPECTIONS REQUIRED FOR THIS WORK.

  H. WIRING SHALL BE SOLID COPPER CONDUCTOR, SIZE NO. 10, UNLESS NOTED, WITH TYPE THHN-THWN-MTW, 90 C, 600V INSULATION. NO. 8 AND LARGER SHALL BE STRANDED COPPER CONDUCTOR WITH TYPE THHN-THWN, 75 C, 600V INSULATION. WIRING SHALL BE COLOR CODE. TO MATCH EXISTING COLOR CODE.
- I. ALL WIRING SHALL BE RUN IN GRC WITH THREADED FITTINGS.
- J. OUTLET BOXES IN SHED SHALL BE EXPLOSION PROOF.

K. SHED AREA IS CLASSIFIED AS A HAZARDOUS LOCATION, CLASS 1, DIMISION 1, GROUP D. ALL WORK IN SHED SHALL COMPLY WITH THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE FOR HAZARDOUS LOCATIONS. PROVIDE TYPE EYS SEALS WHERE RACEWAYS GO FROM HAZARDOUS LOCATION TO NON-HAZARDOUS LOCATIONS.

PANEI	"LA" SQUARE D TYPE 240/120 VOLT,	NOOD, NEW 1 PHASE, 3	SR CA WIRE, 2	BINE 00	T, V	WITH MAI	GROUND N BREAK	BUS, ER (BOT	TOM), 10K AIC RATED	
KVA	LOAD	BKR	TYPE	NO	æ	NO	TYPE	BKR	LOAD	KVA
3.5	LTG	20/2	QOB	1	A	2	Q08	20/2	FAN	0.7
				3	В	4				1
3.5	LTG	20/2		5	С	6	i	20/2	FAN	0.7
				7	Α	В				
3.5	LTG	20/2		9	В	10		20/2	FAN	0.7
				11	С	12				T
3.5	LTG	20/2		13	A	14		20/2	FAN	0.7
				15	В	16				
3.5	LTG	20/2		17	С	18		20/2	SPARE	
				19	A	20				I
2.5	LTG	20/2		21	В	22		20/2	SPARE	
				23	С	24		$\Box \Box \Box$		
2.5	LTG	20/2		25	Α	26		SPC	SPACE	]
				27	В	28				
	RECEPT	20/1		29	С	30				
	RECEPT	20/1		31	٨	32				1
	RECEPT	20/1		33	В	34		30/2	LIGHTNING PROTECTOR	T
	LTC/FAN CONTROLS	15/1	ŧ	35	C	36	-			1



ViroGroup, 3nd. 1445 Pisgoth Church Rood Lexington, SC 29072 Phone 803-957-5270 FAX 803-957-3845 W-41-1-900-796-0454

DATE BY

5/21/97 JKB

REVISION

WATER STOP REVISIONS

1 CURB AND INTERIOR



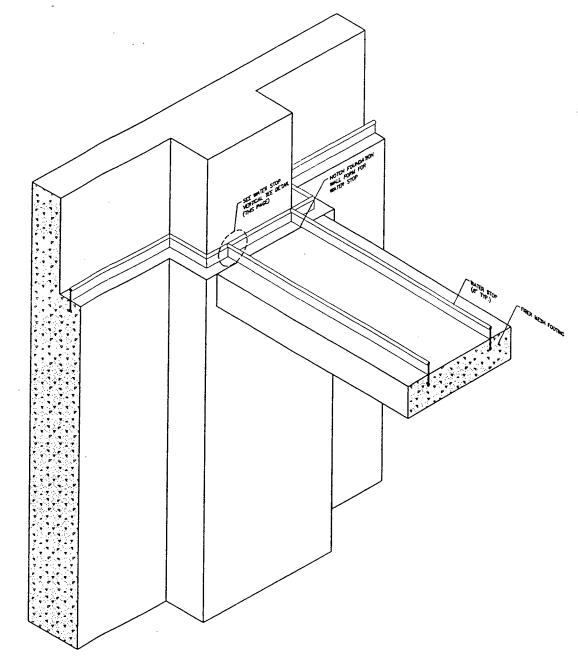
ENVIRONMENTAL SERVICES OF BARTOW, INC. BARTOW, FLORIDA



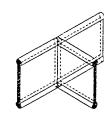
DRUM STORAGE BUILDING ELECTRICAL DETAILS

FOR CONSTRUCTION

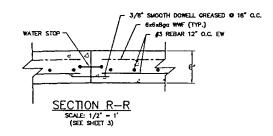
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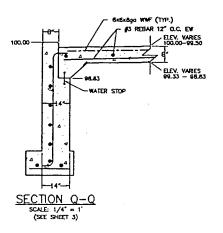


ISOMETRIC FOUNDATION WALL/INTERIOR SUPPORT DETAIL



WATER STOP VERTICAL TEE DETAIL
STATE 1"-1"-0"









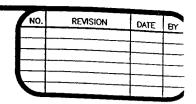
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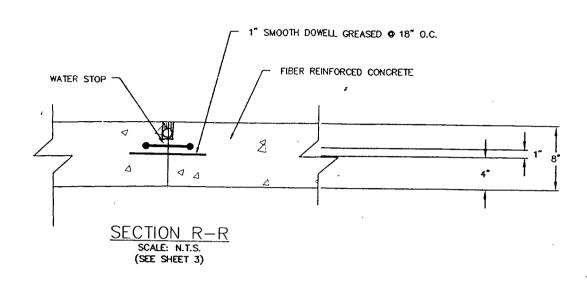
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ENVIRONMENTAL GERVICES OF BARTOW, INC. BARTOW, FLORIDA

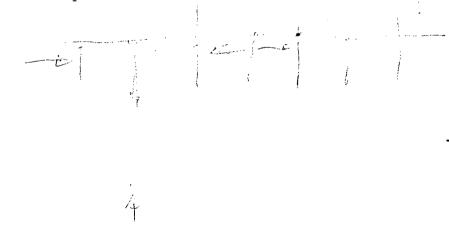
DRUM STORAGE BUILDING CHANGE ORDER #1

•			
DRAWN BY:	JKB	DATE:	5/21/97
DESIGNED BY:	JWB	C400 HO:	3285150
APPROVED BY:		PROJECT NO:	12-32803.D1
SCALE:	AS SHOWN	SHEET NO. 1	of 1





DETAILS SHOWN ON DRAWING 4 OF 11, REVISION 1, 5/27/97, VIROGROUP PROJECT # 12-32803.D1, CADD # 32803004 REFERENCED AS SECTIONS C-C, 0-0, M-M, H-H, J-J, K-K, L-L, I-I, & D-D SHOULD ALSO BE CONSIDERED REVISED. REFERENCE TO THE #3 REBAR 12" O.C. EACH WAY AND 6x6x8 WWF SHOULD BE DISREGARDED. ALSO DETAIL Q-Q ON WROGROUP PROJECT # 12-32803.D1, CADD # 328BISO (SHEET 1 OF 1) IS REVISED AS STATED ABOVE AND DETAIL R-R IS REVISED AS SHOWN ABOVE. IN ADDITION, SECTION A. B. AND THE CURB DETAIL PRESENTED ON VIROGROUP CADD # 32803S01 (SHEET S1 OF S2) AND SECTION C AND THE TYPICAL CONTROL JOINT AND CONSTRUCTION JOINT ON CADD # 32803S02 (SHEET S2 OF S2) ARE REVISED AS MENTIONED ABOVE.

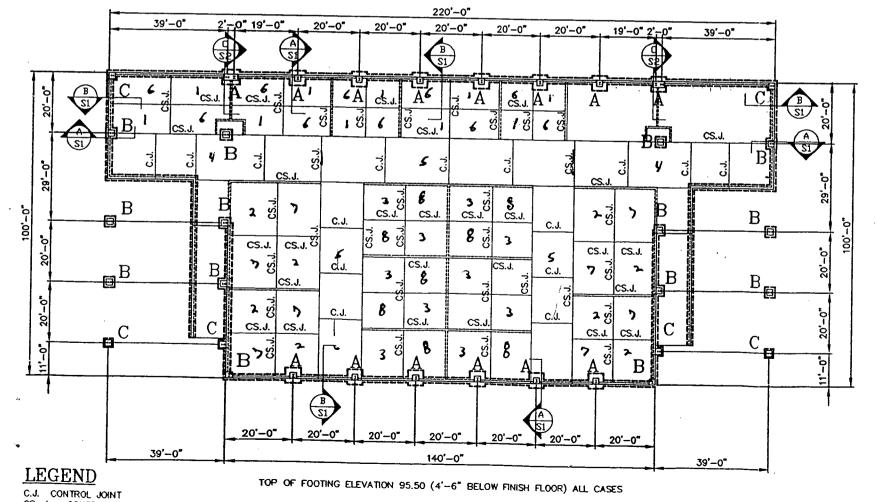


AC Builts Viro Group

LAIDLAW

OF BARTOW, SIC. BARTOW, FLORIDA

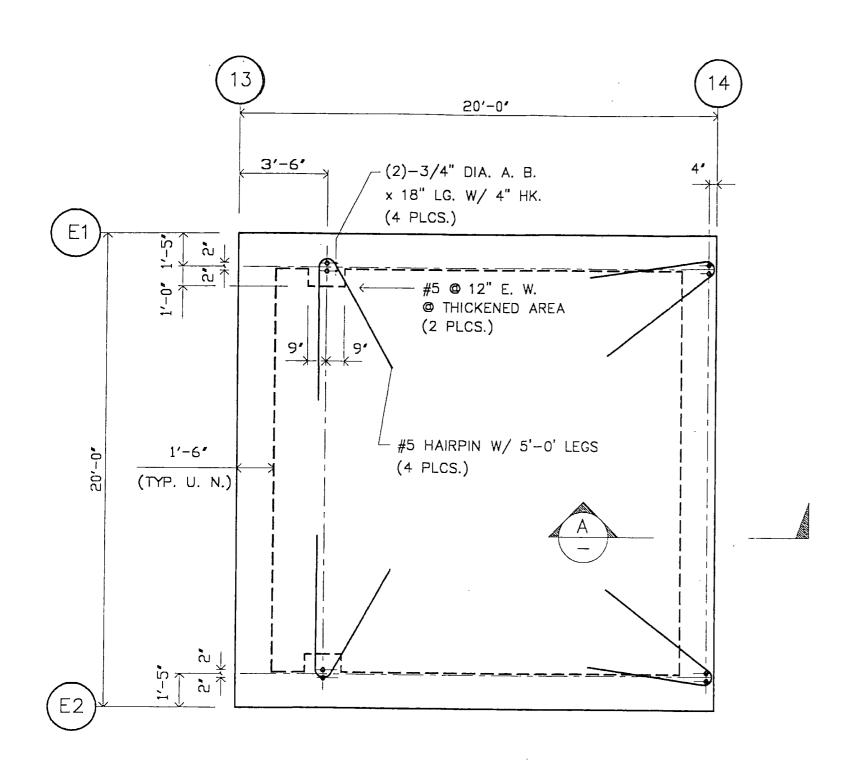
DRUM STORAGE BUILDING OPTION #2



FOUNDATION PLAN

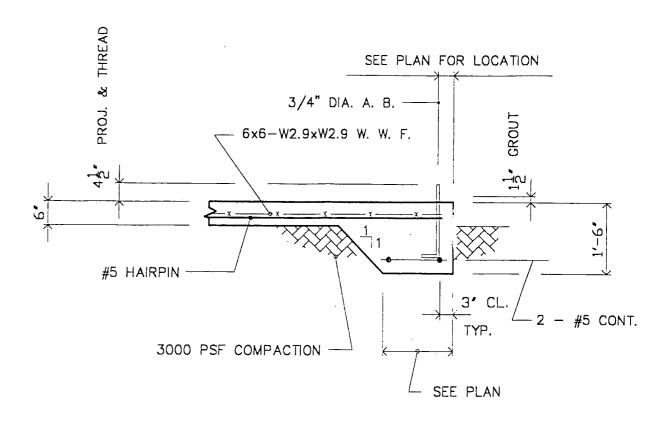
SCALE: 1/32" = 1'-0"

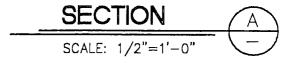
CS. J. CONSTRUCTION JOINT



### FOUNDATION PLAN

SCALE: 1/4"=1'-0"





### NOTE:

- 1. DESIGN CONFORMS WITH 1994 STANDARD BUILDING CODE SECTION 1606 100 MPH WIND LOADS.
- FIELD COORDINATE LAYOUT W/ METAL BLDG. VENDOR DWGS.
- 3. CONCRETE 3000 PSI
- 4. REBAR 60,000 PSI
- 5. ANCHOR BOLTS A-36

10-6-97

### LAIDLAW ENVIRONMENTAL SERVICES

BARTOW, FLORIDA

FOUNDATION PLAN AND SECTIONS

SHEET '1'

Madd. Palmer

### DRUM STORAGE BUILDING

PREPARED FOR

## 

ENVIRONMENTAL SERVICES OF BARTOW, INC.
BARTOW, FLORIDA

SEPTEMBER 24, 1996

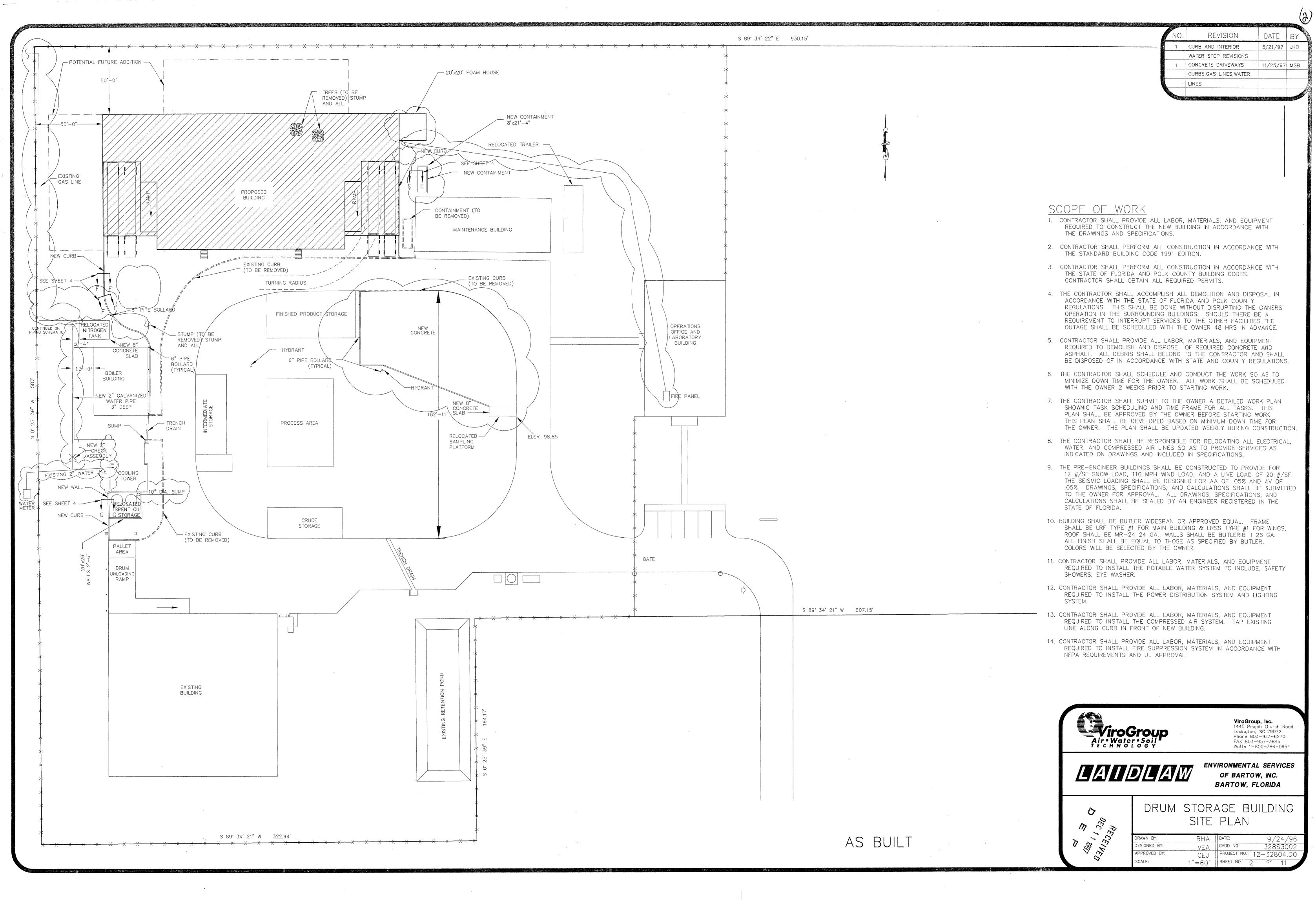


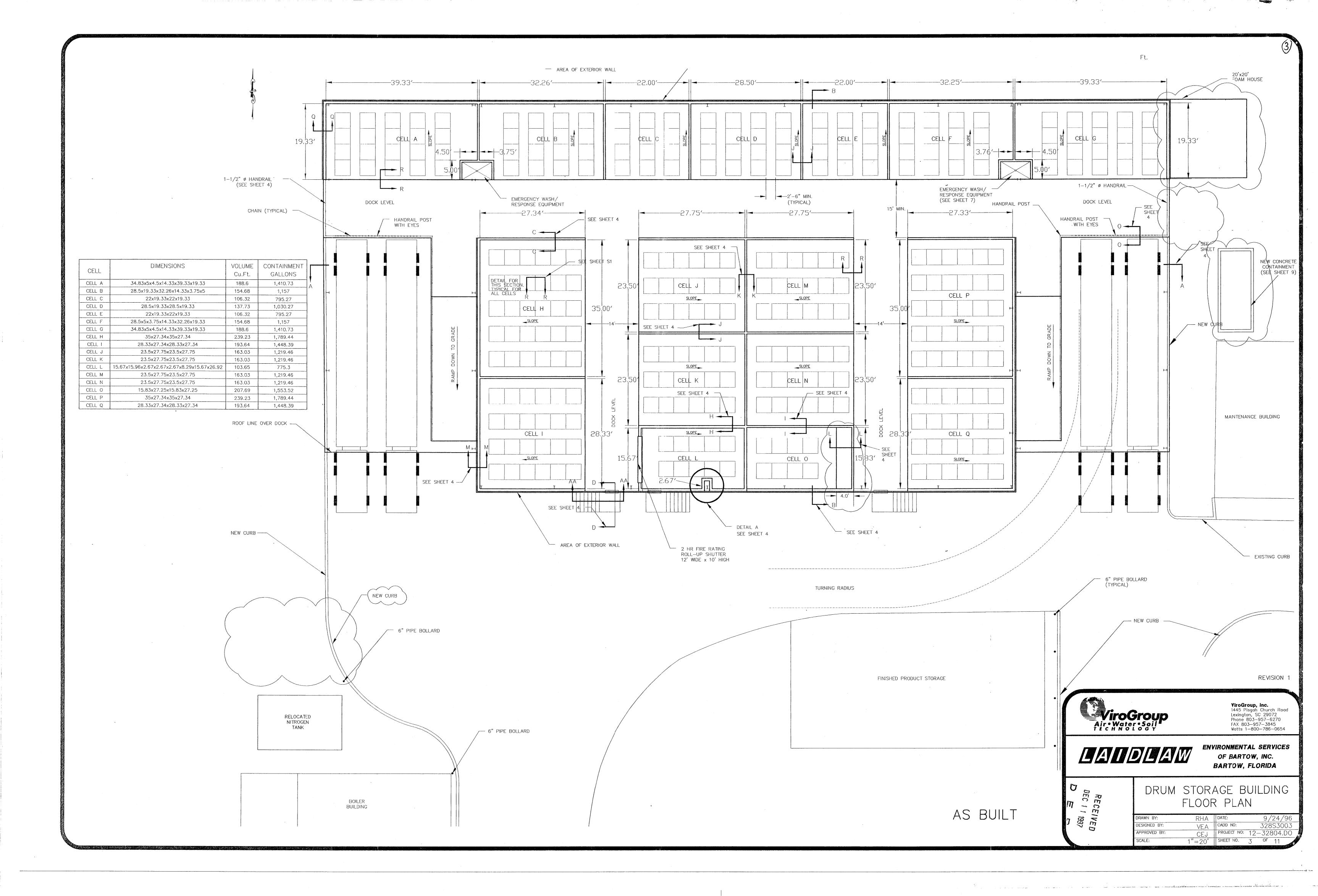
ETE Division

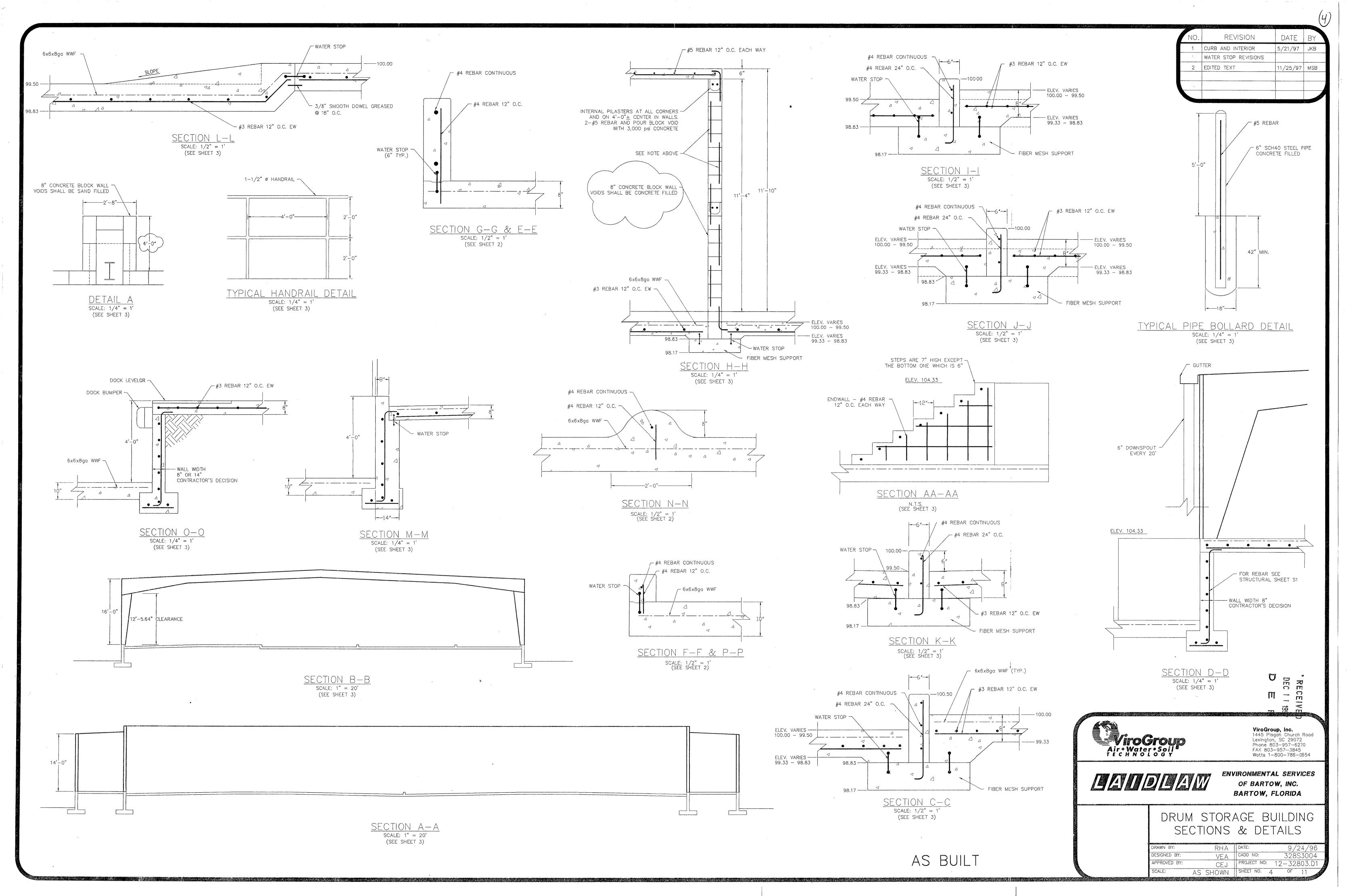
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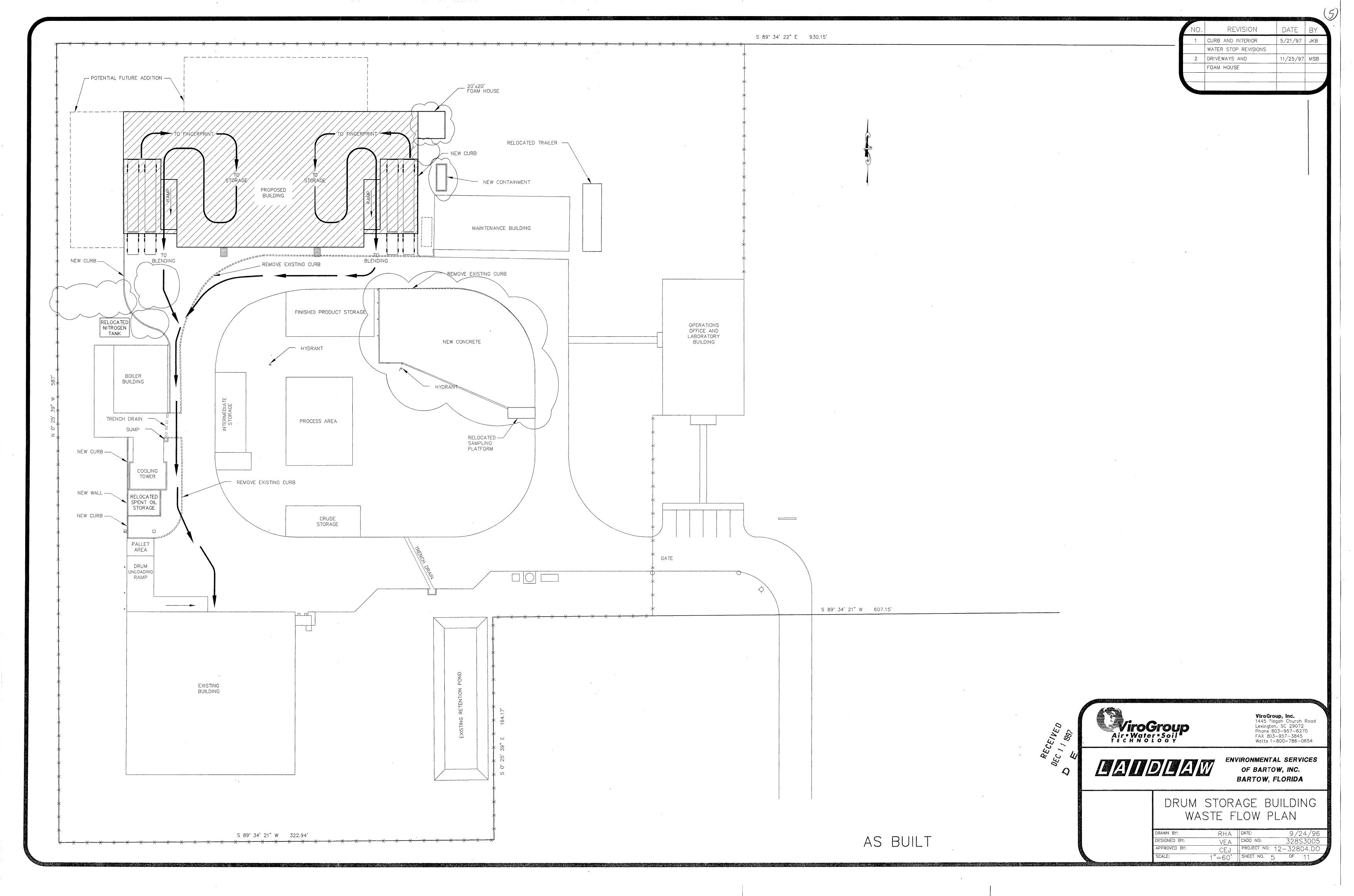
SHEET NO.	TITLE
1	COVER SHEET
2	SITE MAP
3	FLOOR PLAN
4	SECTIONS AND DETAILS
5	WASTE FLOW PLAN
6	SPRINKLER SYSTEM PLAN
7	PIPNG SCHEMATIC
8	ROOF PLAN
9	DEMOLITION & RELOCATION PLAN
10	GRADING PLAN
11	ELEVATION VIEWS
S1	STRUCTURAL LAYOUT
S2	STRUCTURAL LAYOUT
E1	ELECTRICAL SYSTEM PLAN
E2	ELECTRICAL SYSTEM PLAN

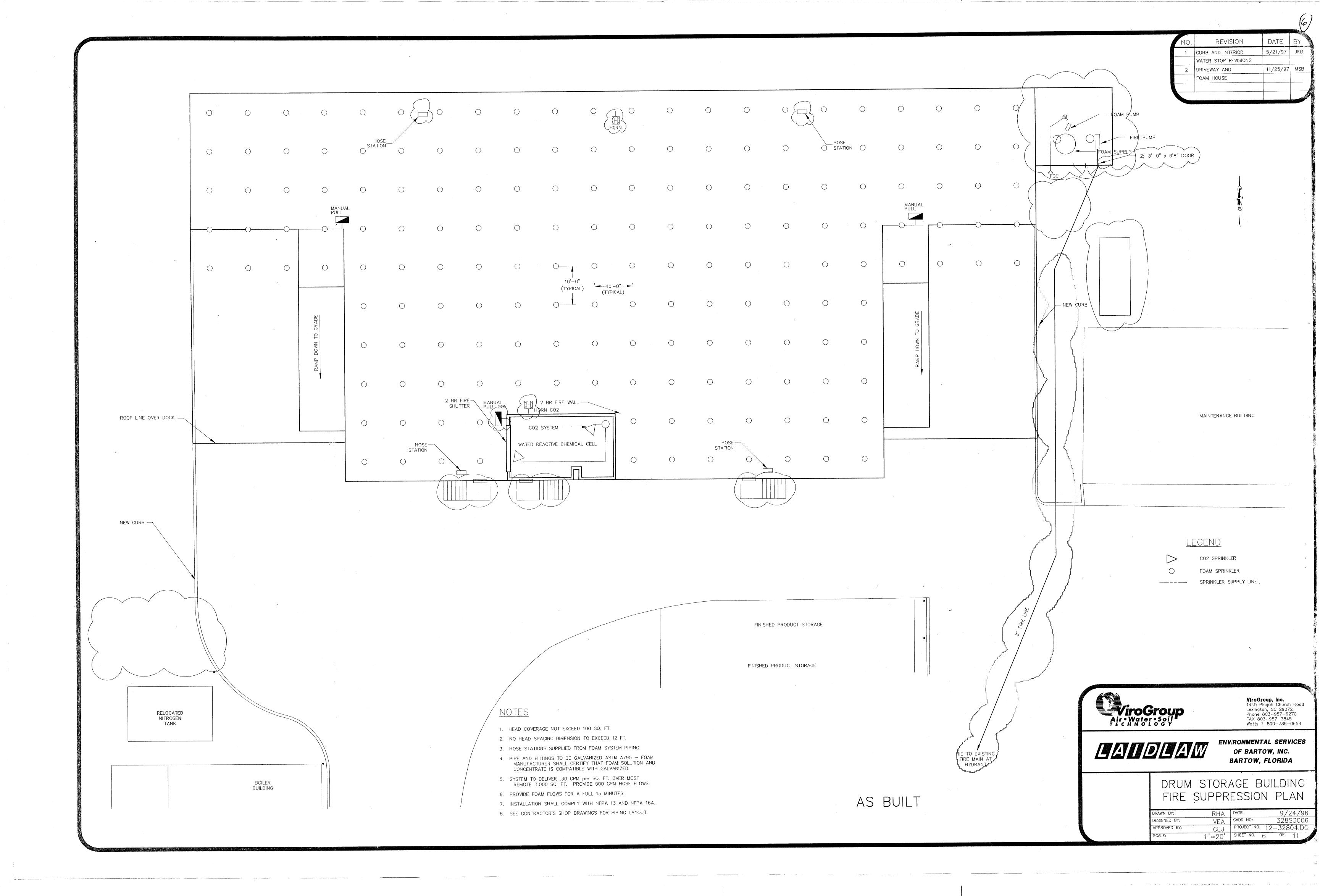
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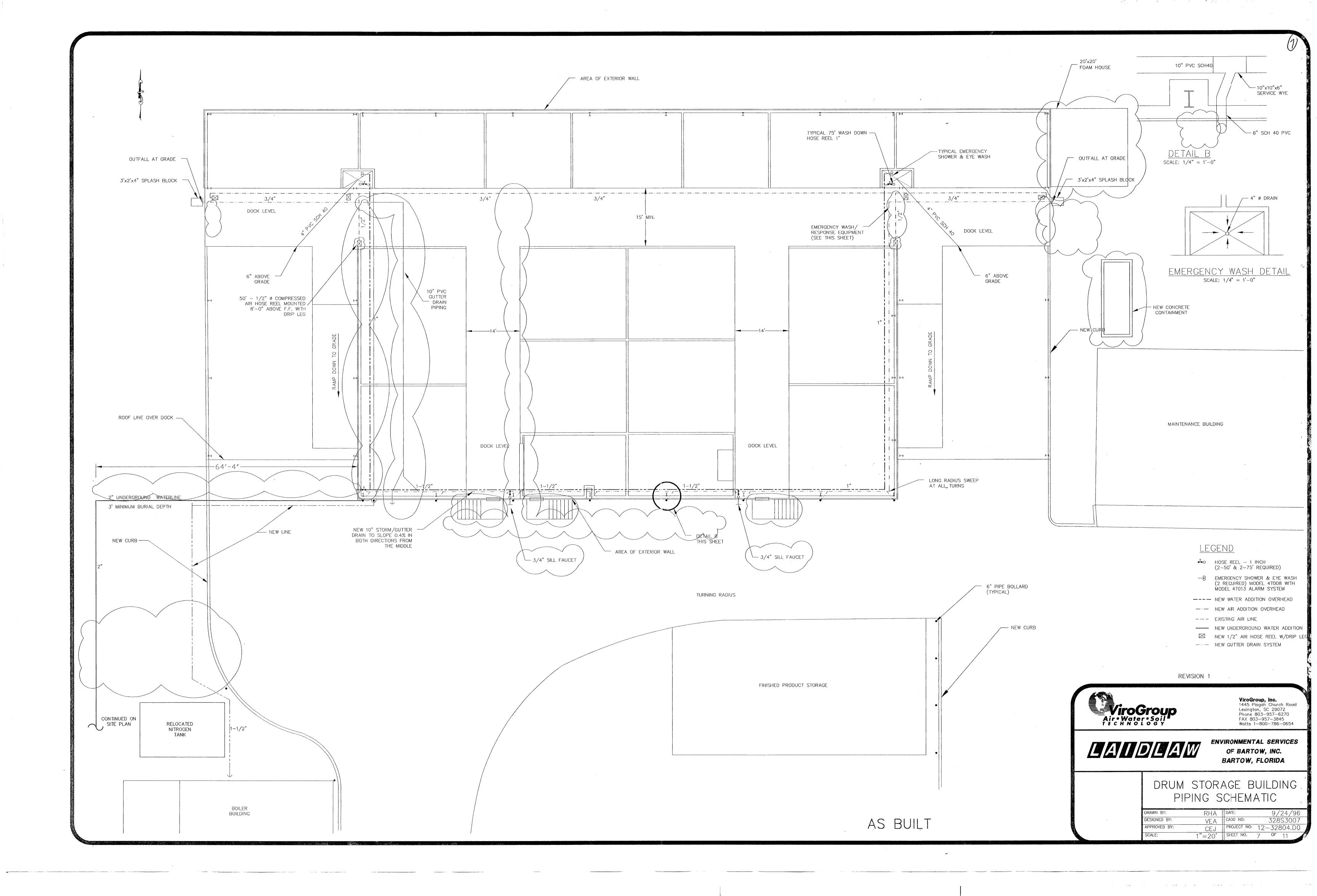


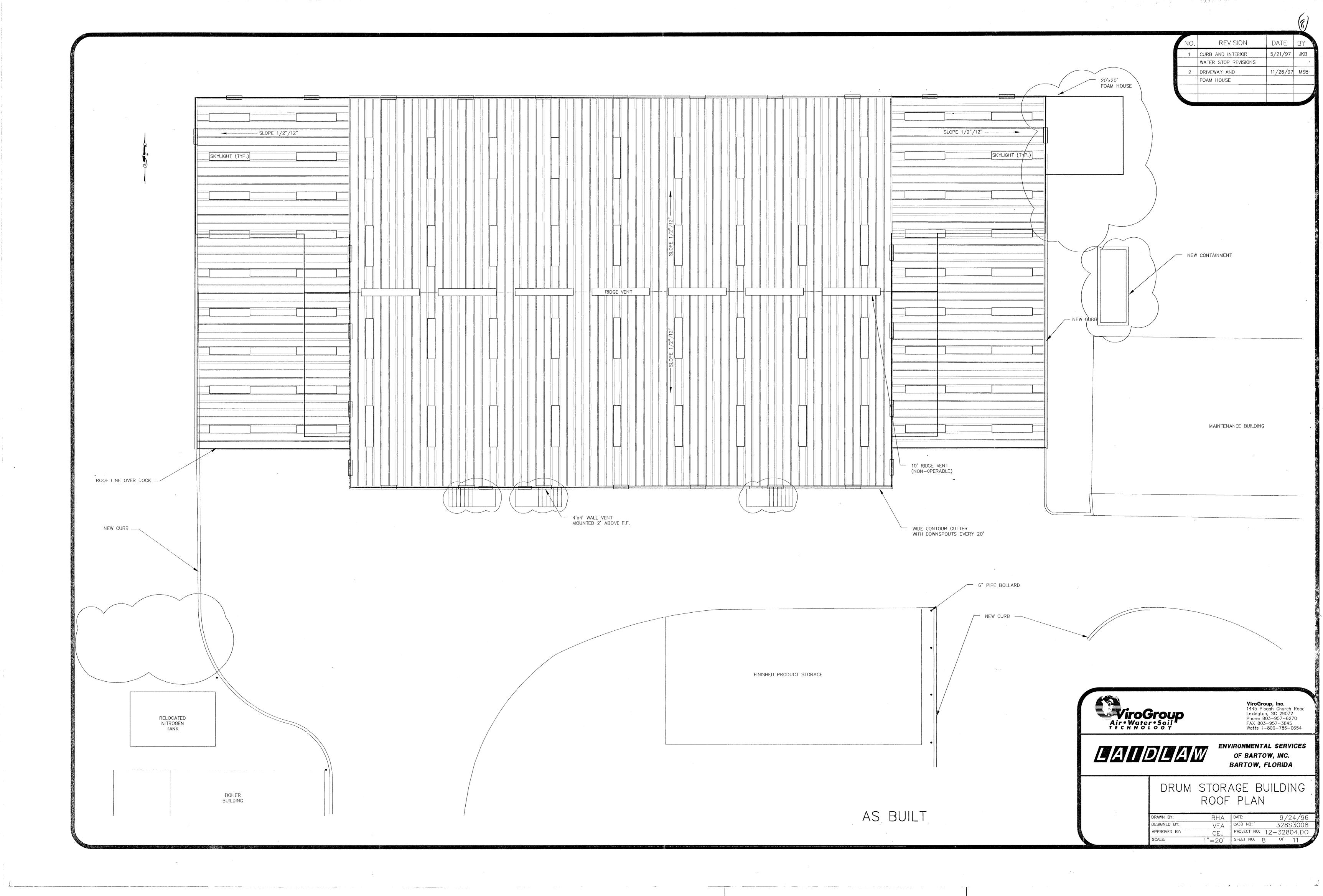


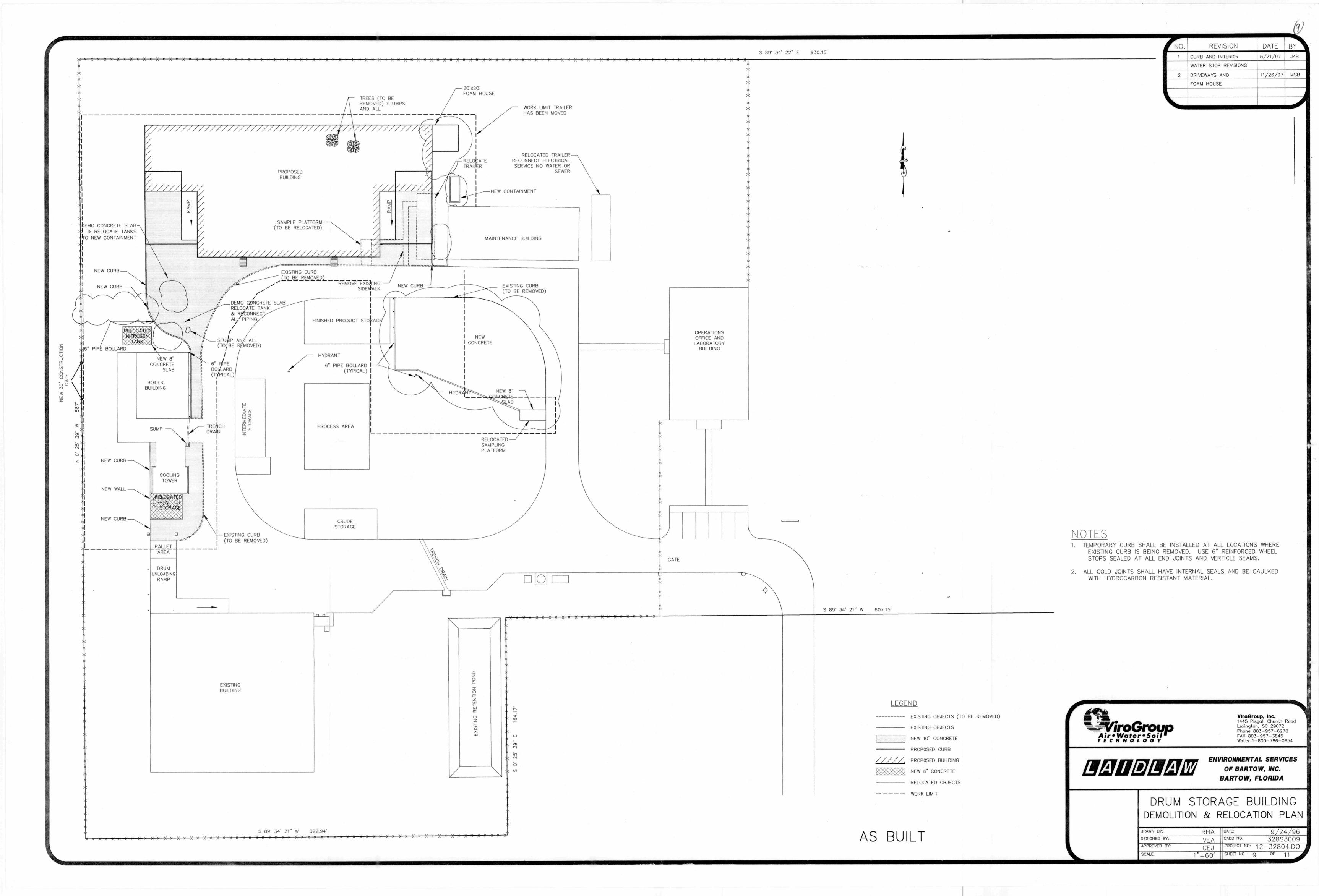


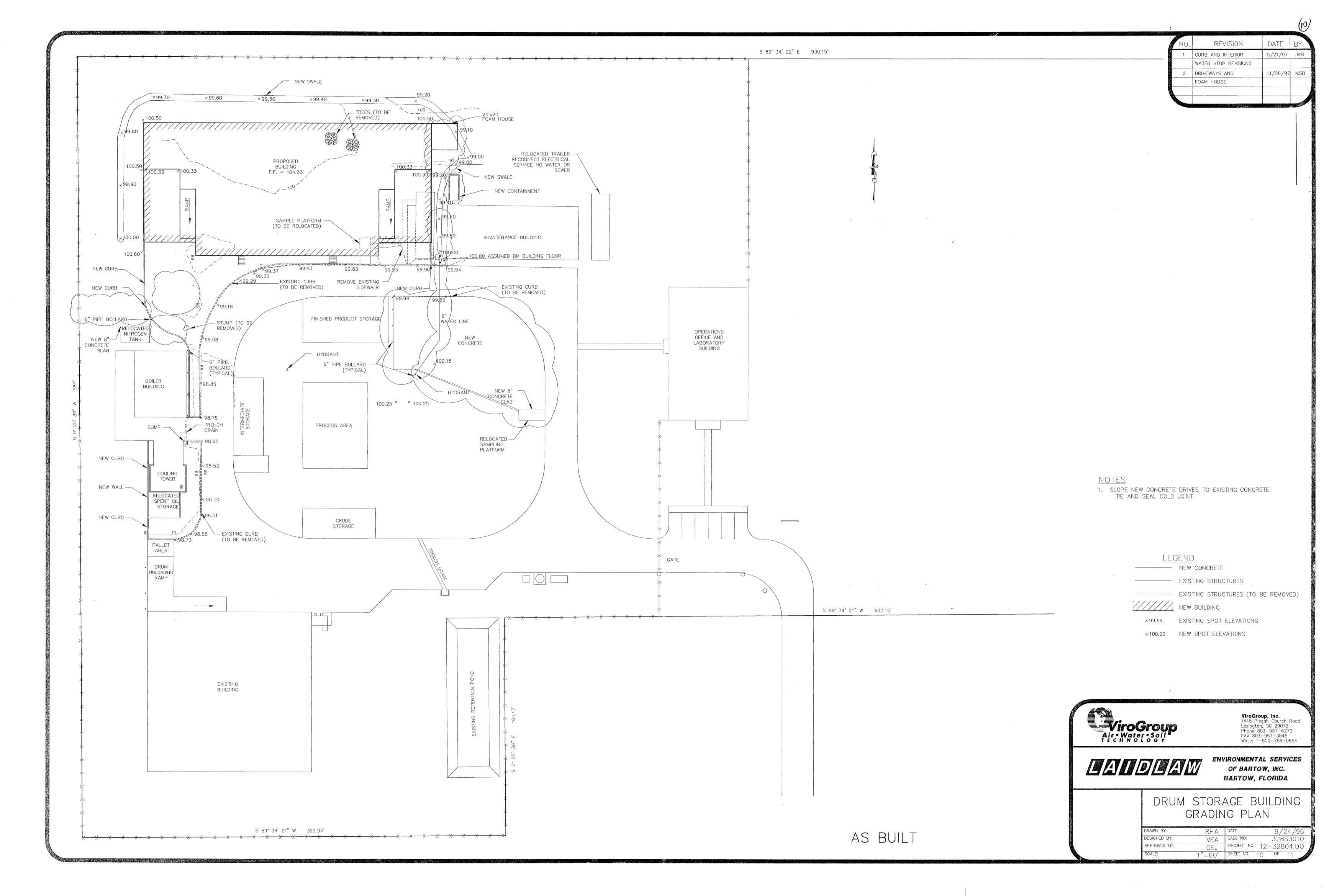




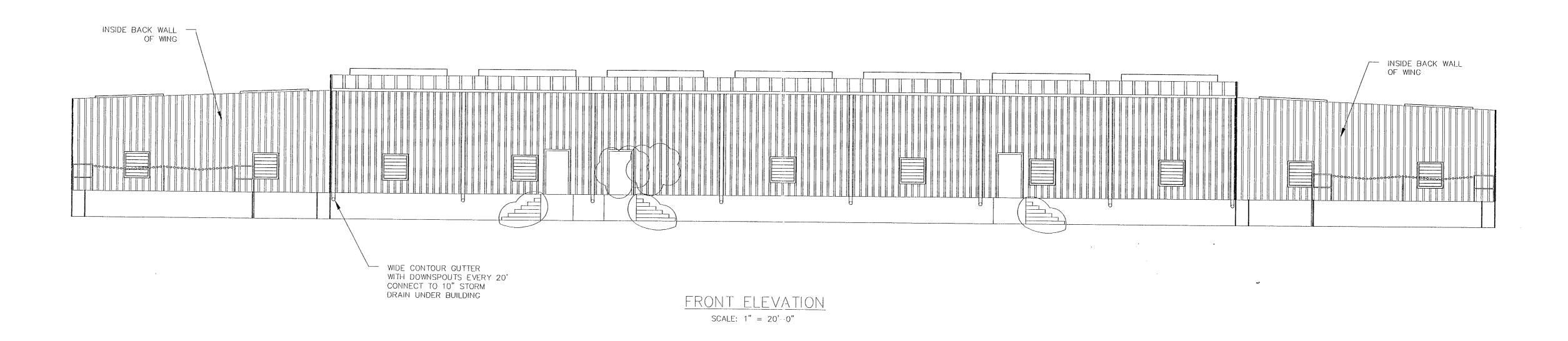


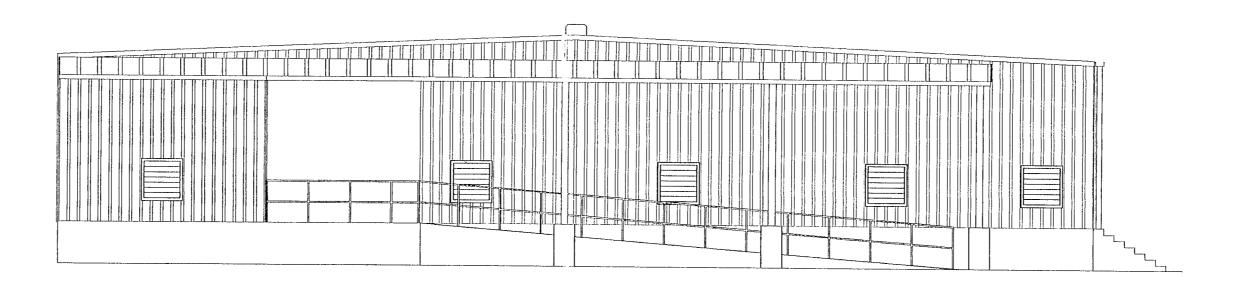






NO.	REVISION	DATE	BY
11	CURB AND INTERIOR	5/21/97	JKB
	WATER STOP REVISIONS		
2	VENT DELETED	11/26/97	MSB





SIDE ELEVATION

SCALE: 1" = 20'-0"



ViroGroup, Inc. 1445 Pisgah Church Road Lexington, SC 29072 Phone 803-957-6270 FAX 803-957-3845 Watts 1-800-786-0654

LAID LAW

OF BARTOW, INC.
BARTOW, FLORIDA

DRUM STORAGE BUILDING

ENVIRONMENTAL SERVICES

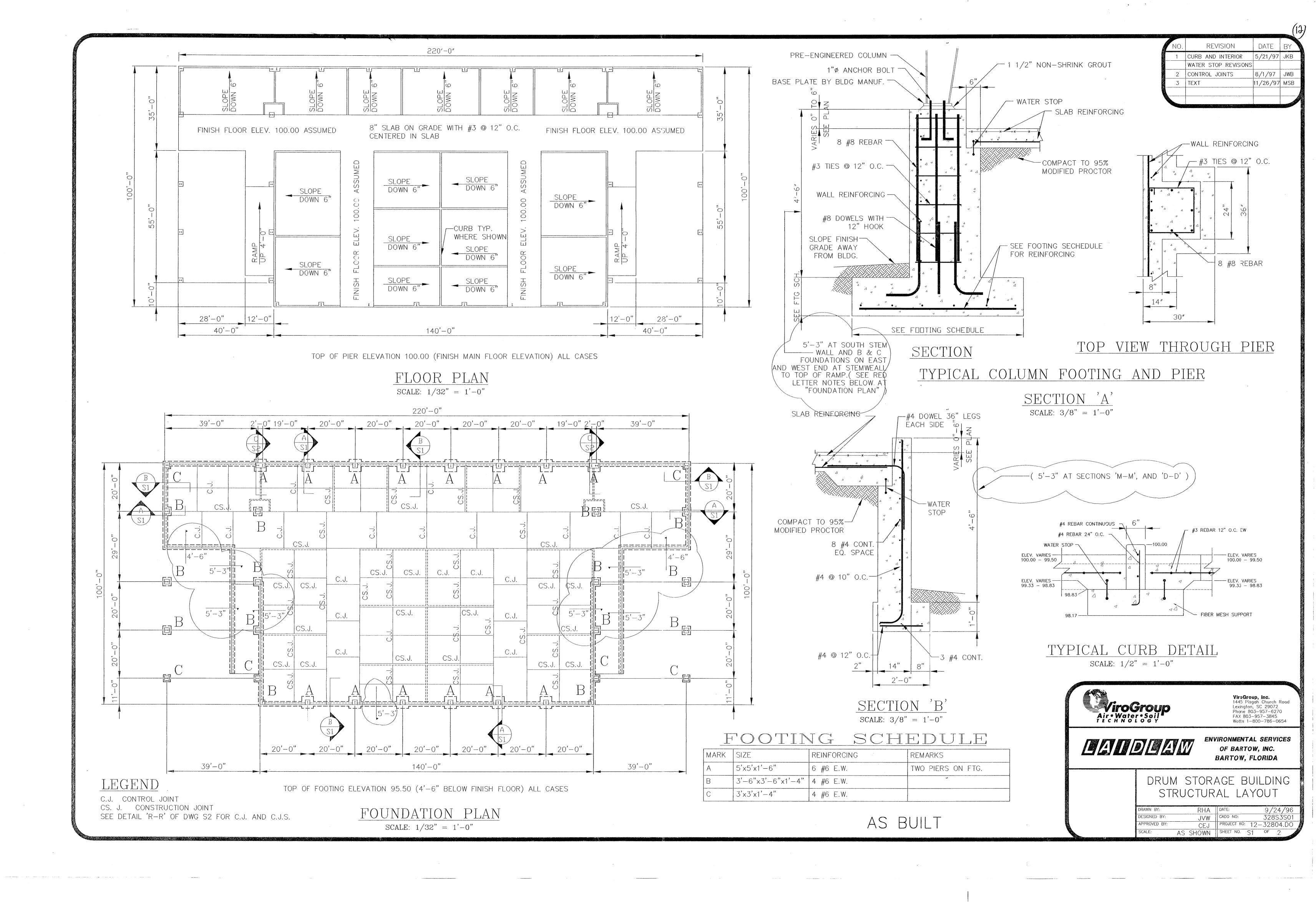
 DRAWN BY:
 RHA
 DATE:
 9/24/96

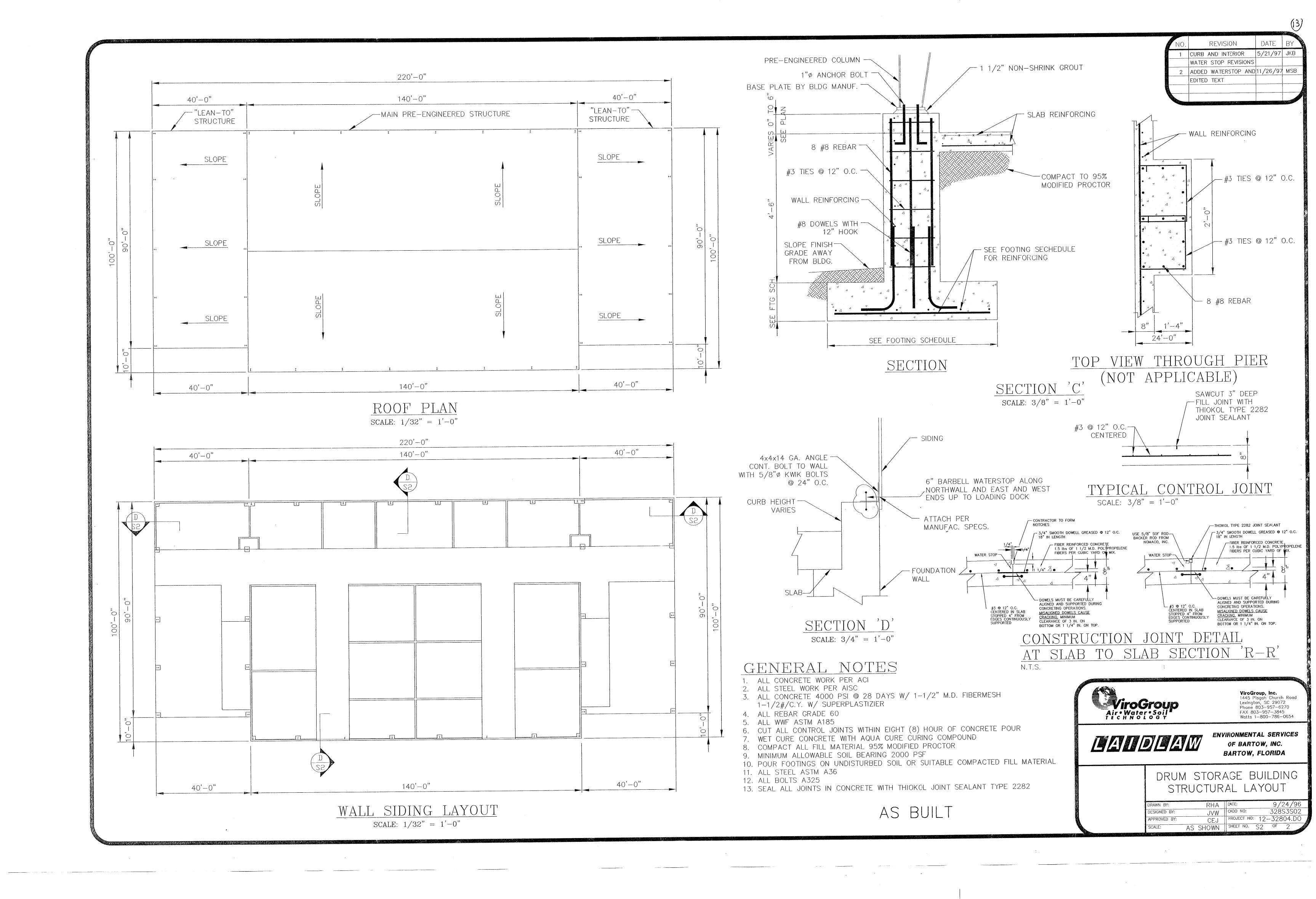
 DESIGNED BY:
 VEA
 CADD NO:
 328S3011

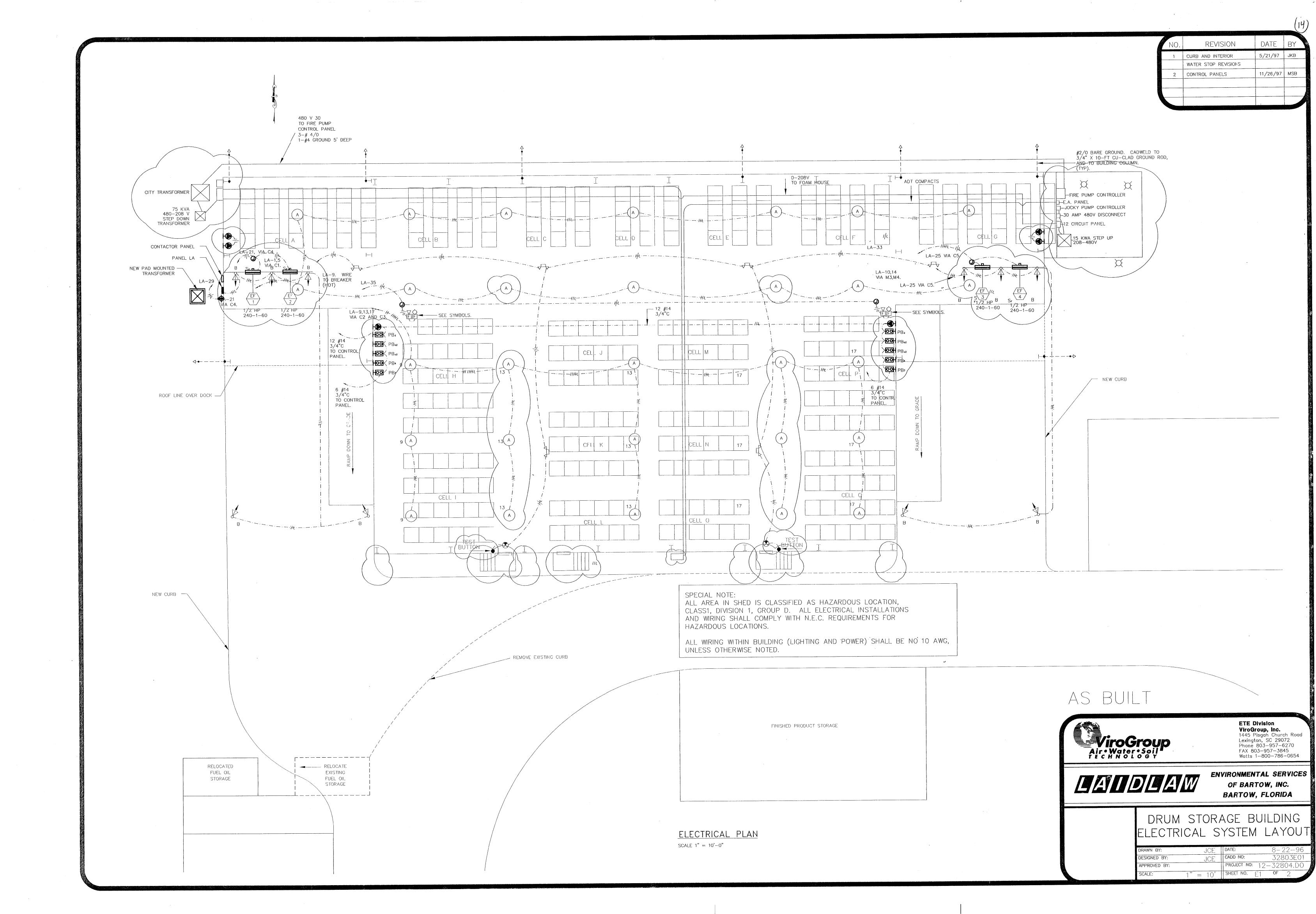
 APPROVED BY:
 CEJ
 PROJECT NO:
 12-32804.DO

 SCALE:
 1"=20'
 SHEET NO.
 11
 0F
 11

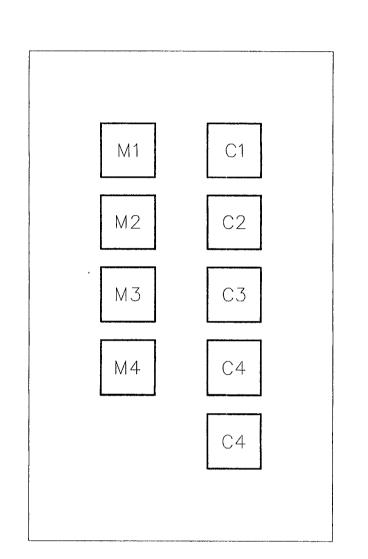
ELEVATION VIEWS

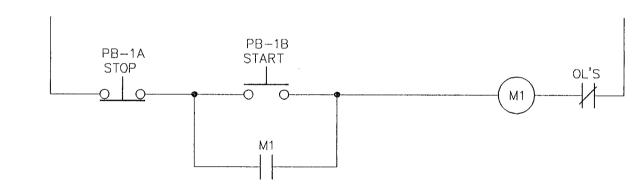






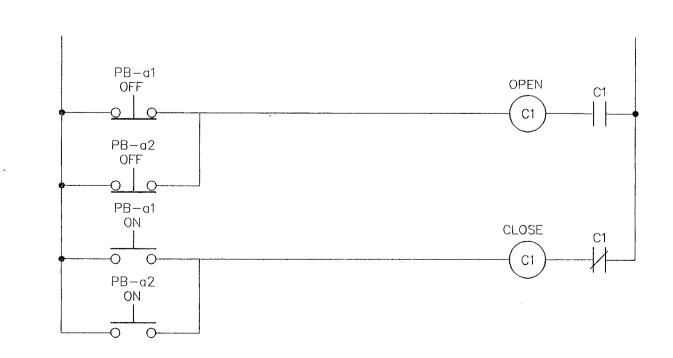
	CONTROL SYSTEMS EQUIPMENT:
TYPE	DESCRIPTION
ENC	NEMA 4 ENCLOSED CABINET, 30-IN HIGH, 24-IN WIDE, 6-IN DEEP, WITH METAL BACK PANEL, HOFFMAN A-4 SERIES, OR EQUAL.
M1, M2 M3, M4	OPEN MOTOR STARTER, NEMA SIZE 0, 240-1-60, 1/2 HP WITH 120-VAC COIL AND HOLDING INTERLOCK. SQUARE D 8536/SBO, OR APPROVED EQUAL.
C1, C2 C3, C4 C5	MECHANICALLY HELD LIGHTING CONTACTOR, 30-AMP, 4-POLE, WITH 120-VAC COILS. SQUARE D 8903/LXO, OR APPROVED EQUAL.
PB1, PB2 PB3, PB4	START-STOP PUSHBUTTON, SEALED, CLASS 1, DIVISION 1, GROUP D. SQUARE D 9001/BR214, OR APPROVED EQUAL.
PBa1, PBa2 PBb1, PBb2 PBc, PBd	ON-OFF PUSHBUTTON, SEALED, CLASS 1, DIVISION 1, GROUP D. SQUARE D 9001/BR214, OR APPROVED EQUAL.





## CONTROL WIRING - FAN CIRCUIT

TYPICAL FOR EF-1, EF-2, EF-3, AND EF-4 NOT TO SCALE



## LIGHTING CONTACTOR CONTROL WIRING

C1

C2

C3

C4

C5

LA-1, LA-5

LA-17

LA-21

LA-25

LA-9, LA-13

PB-a1, PB-a2

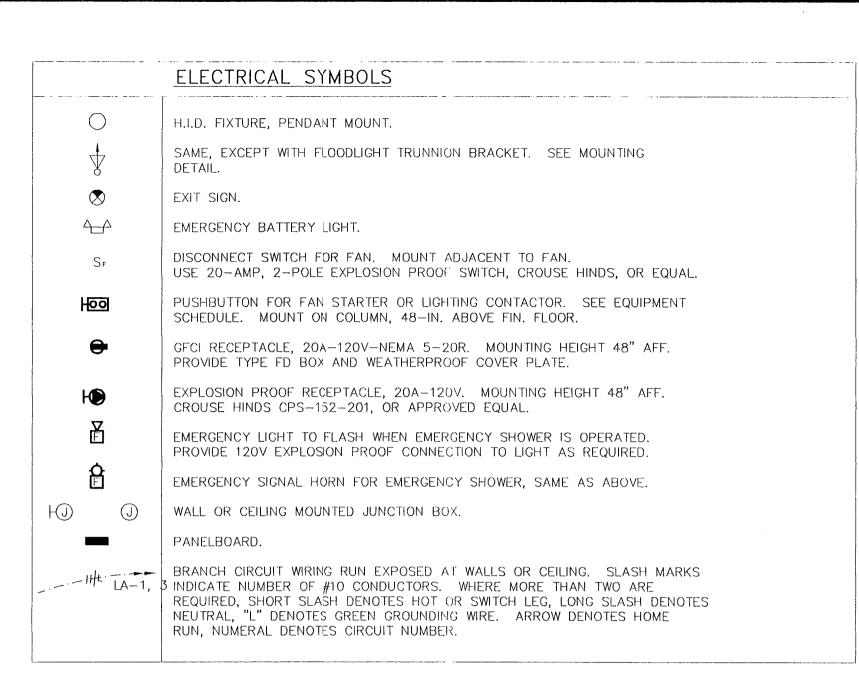
PB-b1, PB-b2

PB-b1, PB-b2

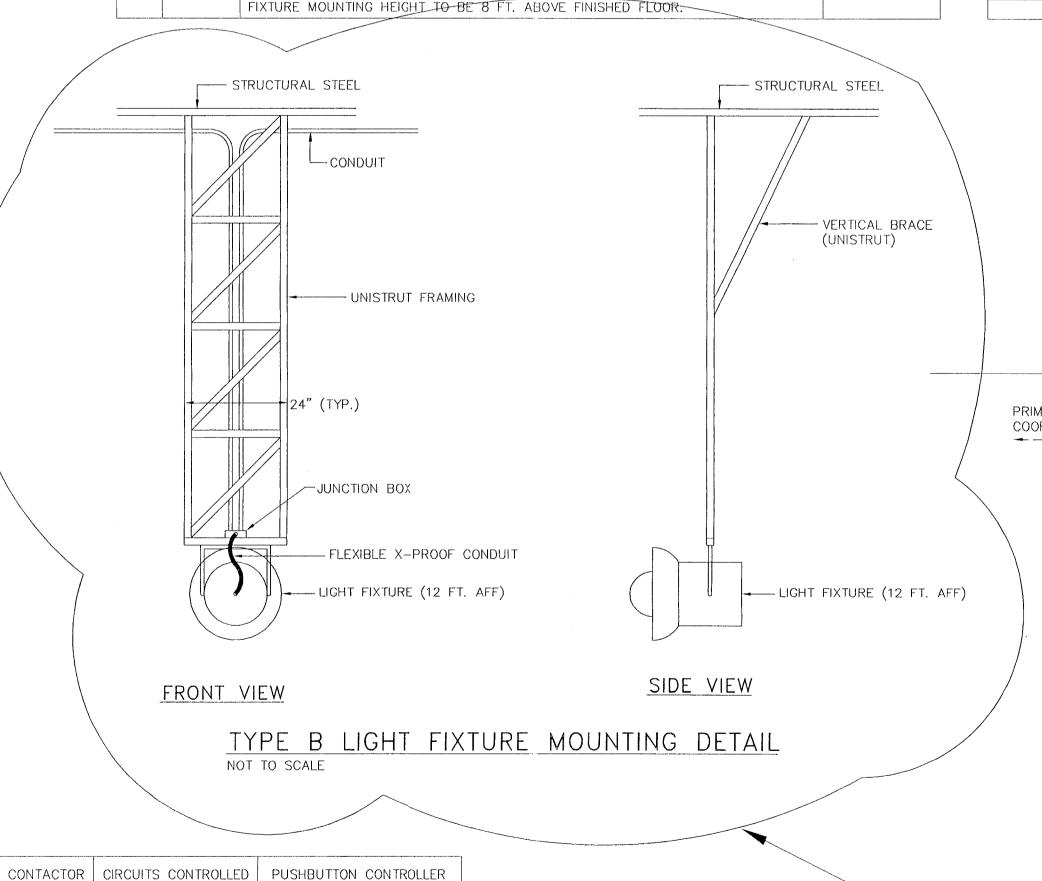
PB-c

PB-d

TYPICAL FOR C1, C2, AND C3. SIMILAR FOR C4 AND C5, EXCEPT CONTROLLED BY ONE SET OF PB'S. NOT TO SCALE



		FIXTURE SCHEDULE							
TYPE	VOLTAGE	DESCRIPTION							
Α	MULTI-TAP 240V	EXPLOSION PROOF FIXTURE WITH MULTI-TAP BALLAST (SET AT 240-VOLT) AND STANDARD REFLECTOR, CLASS 1 DIVISION 1 GROUP D. APPLETON AMBH SERIES, OR EQUAL OF CROUSE HINDS OR KILLARK. PROVIDE STEEL CHANNELS TO SUPPORT FIXTURE.	1/400W/MH "SUPER" 40K LUMENS						
В	MULTI-TAP 240V	SAME AS TYPE A, EXCEPT WITH 30-DEGREE REFLECTOR. FIXTURE MOUNTING HEIGHT TO BE 12-FT. ABOVE FINISHED FLOOR.	1/400W/MH "SUPER" 40K LUMENS						
С	120V	EMERGENCY BATTERY LIGHT, EXPLOSION PROOF, CLASS 1, DIVISION 1, GROUP D. DUAL—LITE XPB—75P SERIES WITH (2) EX—1CD LIGHT HEADS.	INCLUDED						
D	120V	EXIT SIGN, EXPLOSION PROOF, CLASS 1, DIVISION 1, GROUP D. DUAL-LITE XPB-75P SERIES WITH (1) EX-1CD LIGHT HEAD AND EX-100 SIGN. FIXTURE MOUNTING HEIGHT TO BE 8 FT. ABOVE FINISHED FLOOR.	INCLUDED						



#### GENERAL NOTES

A. VISIT SITE TO DETERMINE EXISTING CONDITIONS PRIOR TO SUBMITTING BID.

B. DO NOT SCALE THESE DRAWINGS. ROUGHING IN SHALL BE DONE FROM FIELD CONDITIONS AND DIMENSIONS ON ARCHITECTURAL DRAWINGS AND EQUIPMENT SHOP DRAWINGS.

C. ELECTRICAL CONTRACTOR SHALL DO ALL CUTTING AND PATCHING AS REQUIRED TO INSTALL HIS WORK. FINISH PATCHING AND PAINTING WILL BE DONE BY THE GENERAL CONTRACTOR.

D. PRIOR TO DIGGING ANY TRENCHES, NOTIFY ALL UTILITIES (ELECTRIC, GAS, TELEPHONE, WATER, AND SEWER) AND OBTAIN LOCATIONS OF UNDERGROUND UTILITIES.

E. ANY DAMAGES DONE TO UNDERGROUND UTILITIES OR PIPING BY THIS CONTRACTOR WILL BE REPAIRED BY

THE OWNER OF THE LINE IN A SATISFACTORY MANNER. THIS CONTRACTOR WILL BEAR ALL COSTS FOR REPAIRS.

F. ALL WORK SHALL COMPLY WITH THE 1996 NATIONAL ELECTRICAL CODE AND ALL LOCAL CODES.

H. WIRING SHALL BE SOLID COPPER CONDUCTOR, SIZE NO. 10, UNLESS NOTED, WITH TYPE THHN-THWN-MTW, 90 C, 500V INSULATION. NO. 8 AND LARGER SHALL BE STRANDED COPPER CONDUCTOR WITH TYPE THHN-THWN, 75 C, 600V INSULATION. WIRING SHALL BE COLOR CODED TO MATCH EXISTING COLOR CODE.

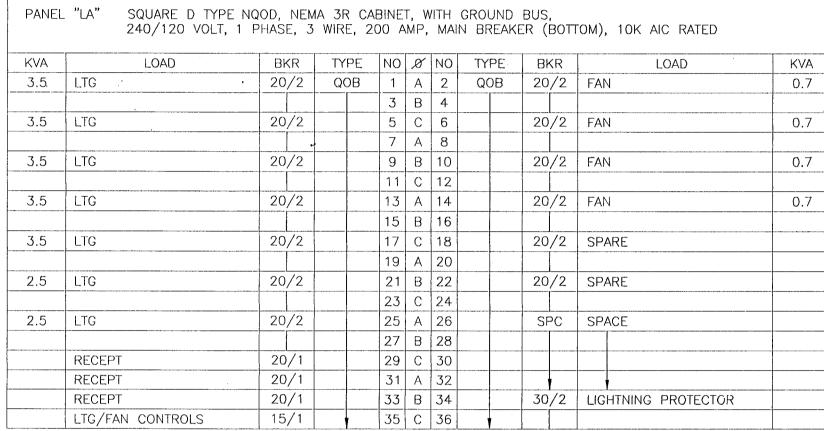
G. APPLY AND PAY FOR ALL PERMITS AND INSPECTIONS REQUIRED FOR THIS WORK.

I. ALL WIRING SHALL BE RUN IN GRC WITH THREADED FITTINGS.

J. OUTLET BOXES IN SHED SHALL BE EXPLOSION PROOF.

K. SHED AREA IS CLASSIFIED AS A HAZARDOUS LOCATION, CLASS 1, DIVISION 1, GROUP D. ALL WORK IN SHED SHALL COMPLY WITH THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE FOR HAZARDOUS LOCATIONS. PROVIDE TYPE EYS SEALS WHERE RACEWAYS GO FROM HAZARDOUS LOCATION TO NON-HAZARDOUS LOCATIONS.

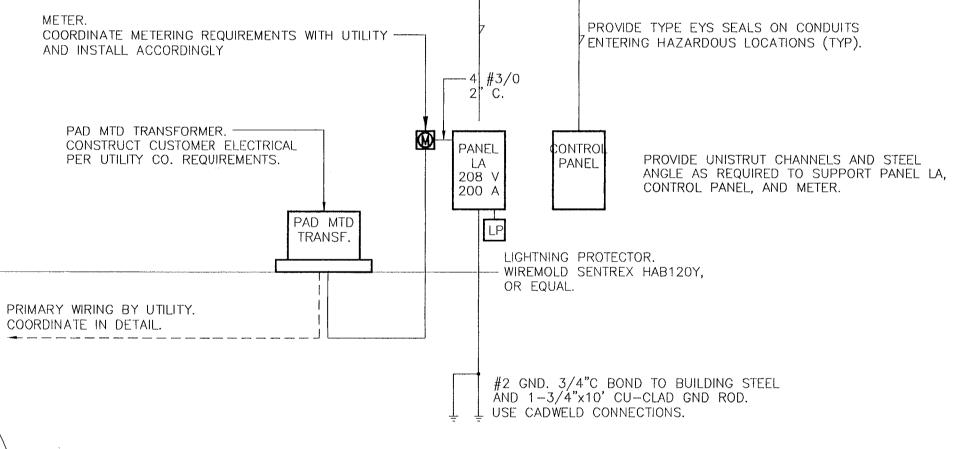
NO.	REVISION	DATE	BY
1	CURB AND INTERIOR	5/21/97	JKB
	WATER STOP REVISIONS		
2	DETAIL DELETED	11/26/97	MSB
			4



POWER RISER DIAGRAM

N.T.S.

DELETED



AS BUILT



ETE Division
ViroGroup, Inc.
1445 Pisgah Church Road
Lexington, SC 29072
Phone 803-957-6270
FAX 803-957-3845
Watts 1-800-786-0654

LAIDLAW

ENVIRONMENTAL SERVICES

OF BARTOW, INC.

BARTOW, FLORIDA

DRUM STORAGE BUILDING ELECTRICAL DETAILS

DRAWN BY:	JCE	DATE:		8/	/22/	91
DESIGNED BY:	JCE	CADD NO:		328	303E	0:
APPROVED BY:		PROJECT NO	12	-328	304.[	D(
SCALE:	NONE	SHEET NO.	E2	OF	2	

### APPENDIX 3

**Pre-Engineered Metal Building As-Builts** 

## GENERAL NOTES

1. Design and/or fabrication shall be in accordance with Whirlwind's standard practices and interpretation of the Ninth Edition AISC Steel Construction Manual ASD, 1986 AISI Cold—Formed Steel Design Manual, 1996 AWS D1.1 Structural Welding Code—Steel and any other code listed within the Design Information.

2. <u>Materials</u>	ASTM Designation	Minimum_Yield
Hot Rolled Mill Shapes	A36	FY=36 KSI
Steel Plate/Flat Bar	A572 or A529	FY=50 KSI
Structural Steel Sheets	A570	FY=50 KSI
Cold—Formed Light Gauge Shapes	A570	FY=55 KSI
Cable Bracing	A475	Extra High Strength
Rod Bracing	A36	FY=36 KSI
Roof and Wall Sheeting	A792	FY=50, 80 KSI
Machine Bolts	A307	•
High Strength Bolts	A325	1
Anchor Bolts (by others)	A36	FY=36 KSI

Whirlwind's standard Red-Oxide shop primer meets the end performance requirements of Federal Specification TT-P-636D and is intended for short term field protection from the elements. Whirlwind is not responsible for any deterioration of the shop primer paint as a result of improperly applied paint and/or coatings.

4. All Bolts are ½" x 0'-1¼" A307 Except:

A). Endwall rafter splice - 58" x 0'-1½" A325-N

B). Endwall column to rafter connection  $-\frac{5}{8}$ " x 0'-1\frac{1}{2}" A325 C). Main frame connections - SEE CROSS SECTION

5. A325 Bolt Tightening Requirements

All high strength bolts are A325 unless specifically noted otherwise. All structural A325 bolts with heavy hex nuts for the Rigid Frame are to be installed using the turn-of-nut method specified in the "Specification for Structural Joints Using ASTM A325 or A490 Bolts" in the AISC Manual. All boiled connections unless noted are designed as bearing type connections with bolt threads not excluded from the shear plane.

6. Closure Strips Furnished For Roof Application

INSIDE — under roof panels at eave

OUTSIDE — between endwall panels and rake trim and at the high side eave trim

**Erection Note:** 

All bracing shown and provided by Whirlwind for this building is required and shall be installed by the erector as a permanent part of the structure. ("Code of Standard Practice for Steel Buildings and Bridges" in the AISC Manual; Section 7.9)

Any claims or shortages by buyer must be made to Whirlwind within seven (7) working days after delivery, or such claims will be considered to have been waived by the customer and disallowed.

<u> Misfils</u>

Claims for correction of alleged misfits will be disallowed unless Whirlwind shall have received prior notice thereof and allowed reasonable inspection of such misfits. Ordinary inaccuracies of shop work shall not be construed as misfits. No part of the building may be returned or charges assessed for alleged misfits without prior approval from Whirlwind.



# STEEL BUILDINGS

## DRAWING PACKAGE FOR

CUSTOMER:

SEMCO CONSTRUCTION

JOB NUMBER:

OWNER:

LAIDLAW ENVIRONMENTAL SERVICES

JOBSITE: BARTOW, FL

970090

### DRAWING SCHEDULE

DRAWING NUMBER	ISSUE	DATE	DESCRIPTION
C-ONE	Α	02.26.97	COVER
E-ONE	Α	02.26.97	ROOF FRAMING PLAN
E-2	Α	02.26.97	FRAMING ELEVATIONS
E-3	Α	02.26.97	FRAMING ELEVATIONS
D-ONE	Α	02.26.97	GIRT/PURLIN LAPS
P-ONE	Α	02.26.97	FRAME X-SECTION
P-2	Α	02.26.97	FRAME X-SECTION
P-3	Α	02.26.97	FRAME X-SECTION
F-ONE	Α	02.26.97	ANCHOR BOLT FLAN
S & T-ONE	_	_	SHEETING/TRIM ELEV.
S & T-2	_	_	SHEETING/TRIM ELEV.

### RESPONSIBILITIES

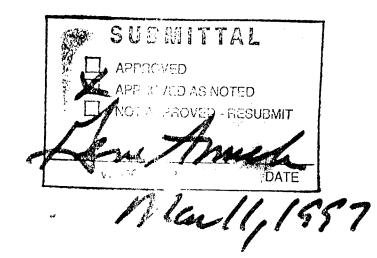
- 1. The Contractor obtains and pays for all building permits, licenses, public assessments, paving or utility pro rata, utility connections, occupancy fees and other fees required by any governmental authority or utility in connection with the work provided for in the Contract Documents. The Contractor provides at his expense all plans and specifications required to obtain a building permit. It is the Contractor's responsibility to ensure that all plans and specifications comply with the applicable requirements of any governing building authorities.
- 2. The End Customer is responsible for identifying all applicable building codes, zoning codes, or other regulations applicable to the Construction Project, including the metal building system.

It is the responsibility of the Contractor to interpret all aspects of the End Customer's specifications and incorporate the appropriate specifications, design criteria, and design loads into the Order Documents submitted to Whirlwind.

It is the responsibility of Whirlwind, through Whirlwind's Engineer, to design the metal building system to meet the specifications including the design criteria and design loads incorporated by the Contractor into the Order Documents. Whirlwind is not responsible for making an independent determination of any local codes or any other requirements not part of the Order Documents.

Whirlwind is responsible only for the structural design of the metal building system it provides. Whirlwind or Whirlwind's Engineer is not the Design Professional or Engineer of Record for the Construction Project. Whirlwind is not responsible for the design of any components or materials not provided by it or their interface and connection with the metal building system unless such design responsibility is specifically required by the Order Documents.

- 3. Whirlwind Steel Buildings' standard specifications apply unless stipulated otherwise in the Contract Documents. Whirlwind design, fabrication, quality criteria, standards, practice, methods and tolerances shall govern the work any other interpretations to the contrary not withstanding. It is understood by both parties that the Contractor is responsible for clarifications of inclusions or exclusions from the Architectural plans and/or specifications.
- 4. In case of discrepancies between Whirlwind's structural steel plans and plans for other trades, Whirlwind's shall govern ("Code of Standard Practice for Steel Buildings and Bridges" in the AISC Manual; Section 3.3)
- 5. Approval of Whirlwind drawings and/or calculations indicate that Whirlwind has correctly interpreted the contract requirements. This approval constitutes the Contractor acceptance of the Whirlwind design, concepts, assumptions and loadings ("Code of Standard Practice for Steel Buildings and Bridges" in the AISC Manual; Section 4.2)
- 6. Once the Contractor has signed Whirlwind's Approval Package and the project is released for fabrication, changes shall be billed to the Contractor including material, engineering and other cost. An additional fee may be charged if the project must be moved from fabrication and the shipping schedule.
- 7. The Contractor is responsible for overall project coordination. All interface, compatibility and design considerations concerning any materials not furnished by Whirlwind and Whirlwind's steel system are to be considered and coordinated by the Contractor. Specific design criteria concerning this interface between materials west be furnished before release for fabrication or Whirlwind's assumptions will
- 8. The Contractor is responsible for the setting of anchor bolts and erection of steel in accordance with Whirlwind's "For Construction" drawings only.
- 9. Temporary supports, such as guys, braces, falsework, cribbing or other elements required for the erection operation shall be determined and furnished by the erector ("Code of Standard Practice for Steel Buildings and Bridges in the AISC Manual; Section 7.9).
- 10. Normal erection operations include the correction of minor misfits by moderate amounts of reaming, chipping, welding or cutting and the drawing of elements into line through use of drift pins. Errors which require major changes in the member configuration are to be reported immediately to Whirlwind by the Contractor to enable whoever is responsible either to correct the error or to approve the most efficient and economic method of correction to be used by others ("Code of Standard Practice for Steel Buildings and Bridges" in the AISC Manual; Section 7.12).
- 11. Neither the fabricator nor the Contractor will cut, drill or otherwise alter their work, or the work of other trades to accommodate other trades unless such work is clearly specified in the contract documents. Whenever such work is specified the Contractor is responsible for furnishing complete information as to materials, size, location and number of alterations prior to preparation of shop drawings ("Code of Standard Practice for Steel Building and Bridges" in the AISC Manual; Section 7.13).
- 12. Whirlwind does not investigate the influence of the metal building system on existing buildings or structures. The End Customer assures that such buildings and structures are adequate to resist snow drifts, wind loads, or other conditions as a result of the presence of the metal building system.

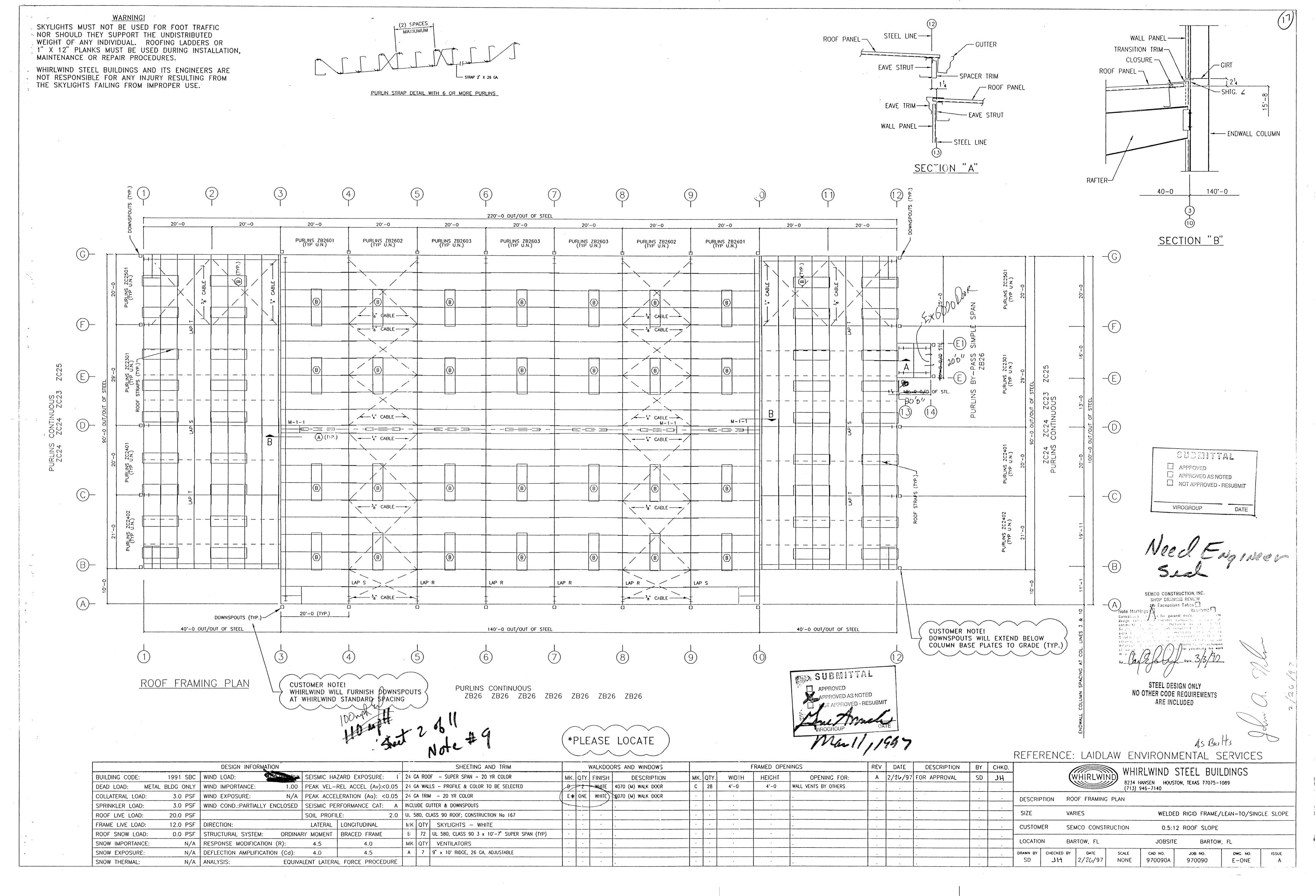


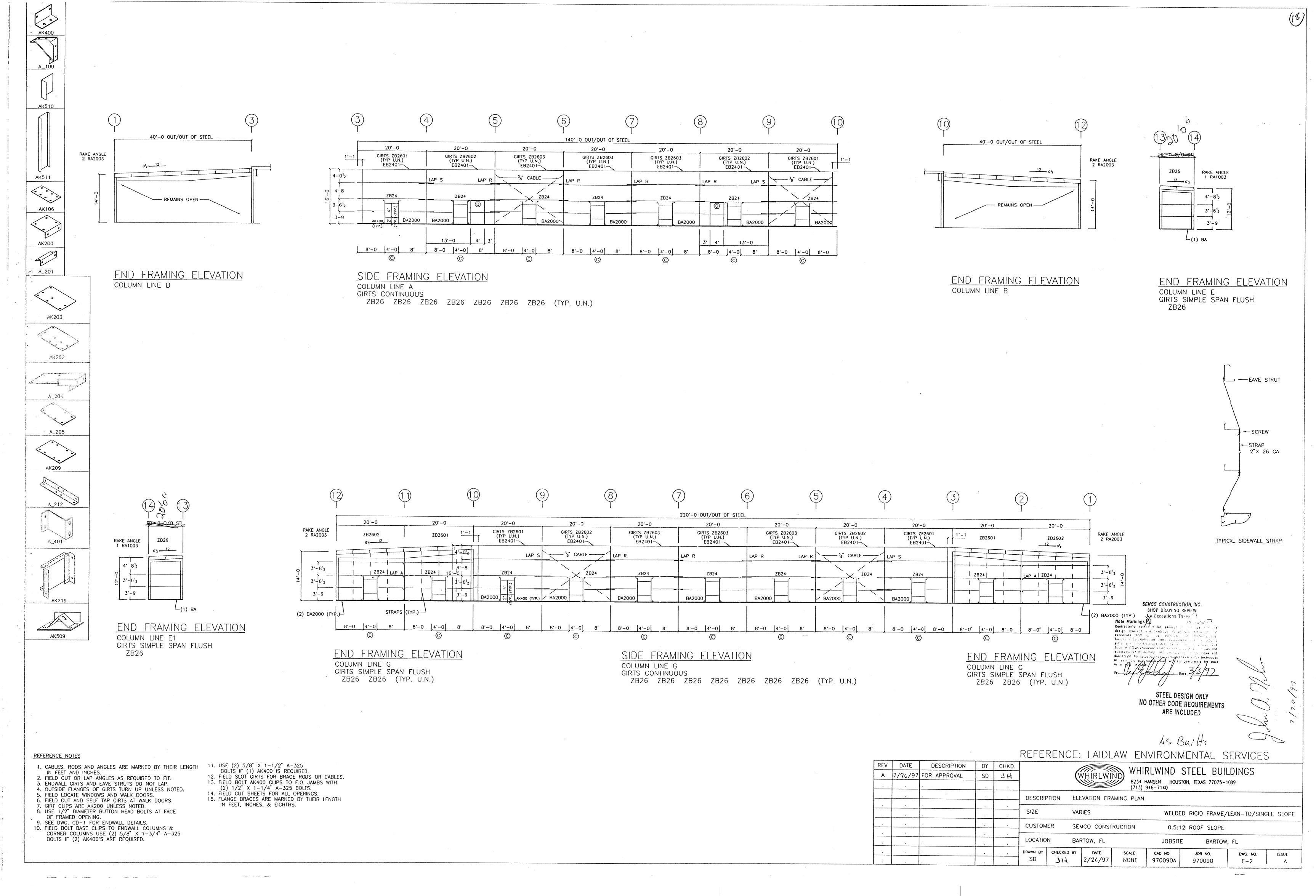
SEMOO CONSTRUCTION, INC. SHOP DRAWING REVIEW No Exceptions Taken [] Note Markings Contractor's review is for gandres that was all with the design convert and contract duri randients shat bat be comme. Supplier / Eucedhirocres Irah . plans sid apsolitoatring nor eg Supplier / Sale intractor Temples : eccuracy, for confirming and constitution, dimensions, for calacting for contracting provinces of continuous of assumpty and confitraction of the recommendate with the particular work

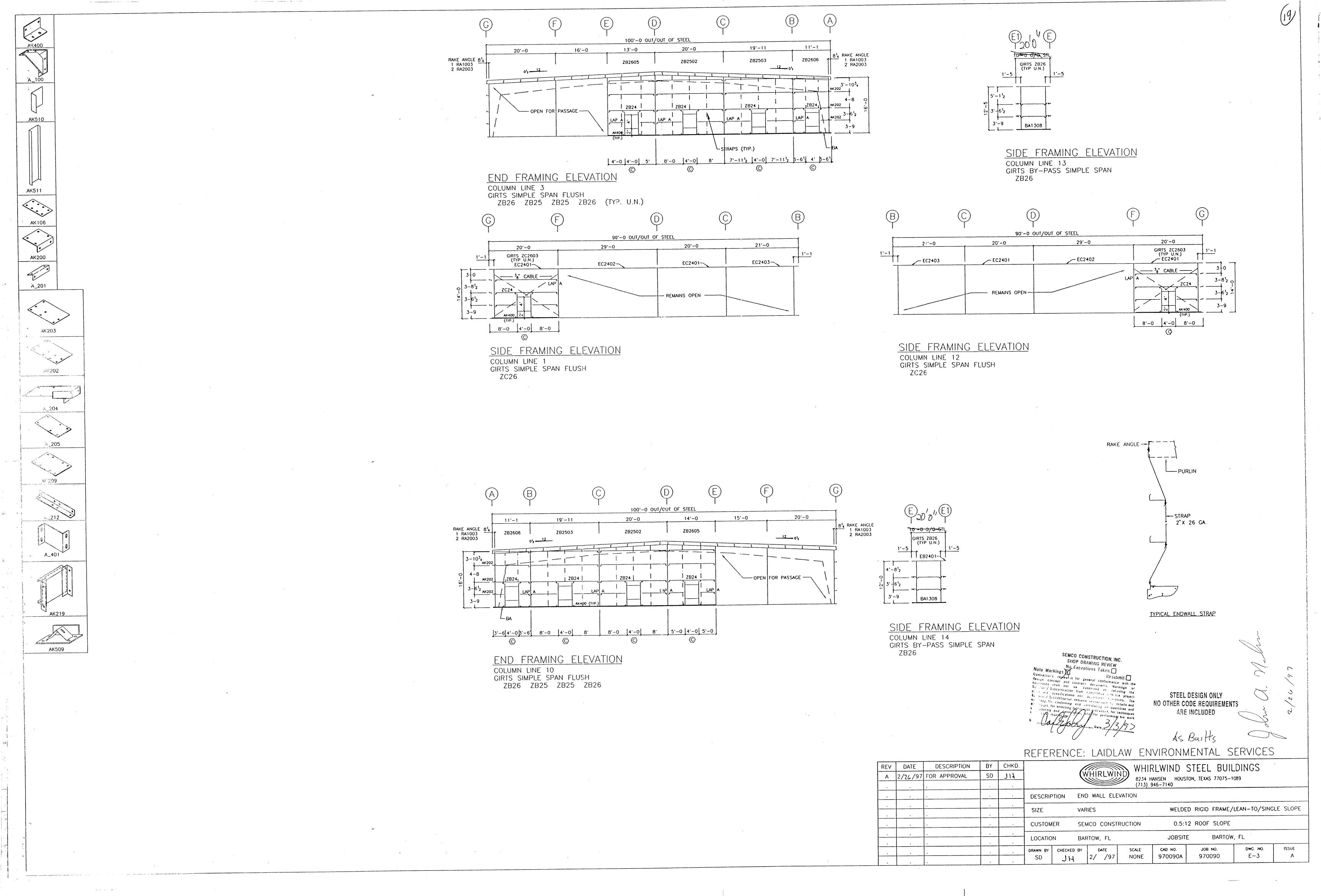
As Builts

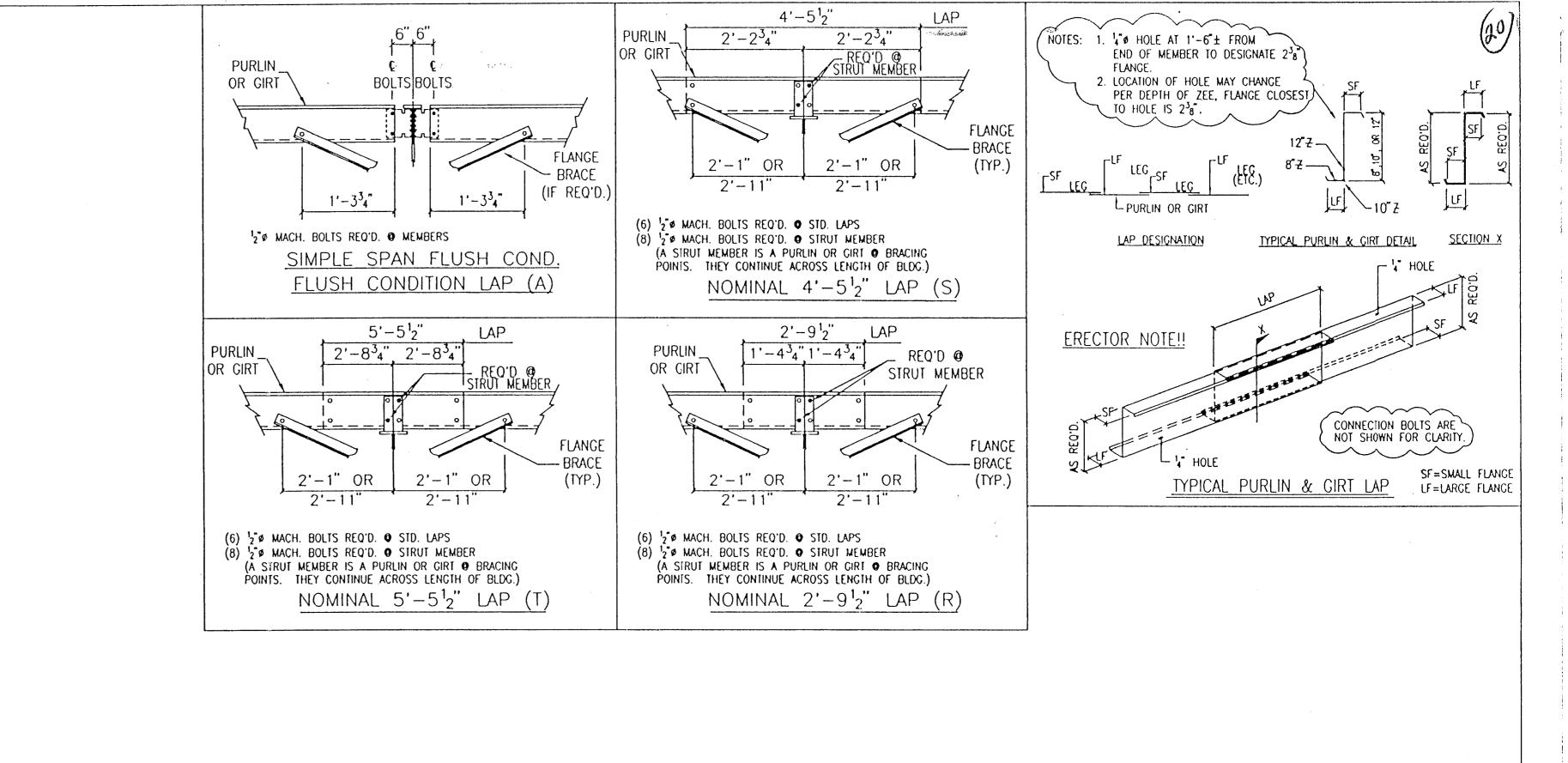
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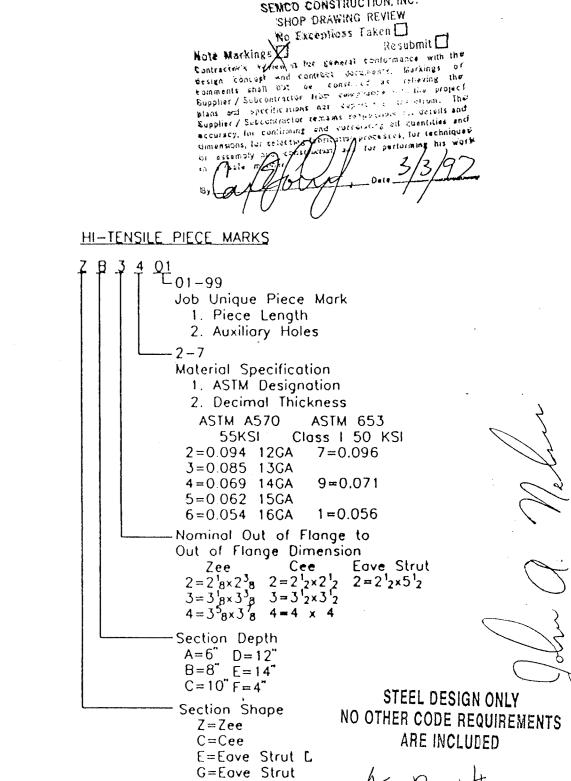
DWG. NO.: C-ONE











SEMOO CONSTRUCTION, INC.

Resubmit

REFERENCE: LAIDLAW ENVIRONMENTAL SERVICES

REV	DATE	DESCRIPTION	BY	CHKD.				NUIN	סואואום כ	STEEL BUI	LDINGS	
Α	2/26/97	FOR APPROVAL	SD	714		<b>(</b> Ý	v́Ң(RLW))	ND)				
									WNSEN HOUST( 946-7140	ON, TEXAS 77075-		
	•		· ·		DESCRIF	TION GIR	RT LAP DETA	JILS				
•	<u> </u>		ļ		SIZE	VAF	RIES		WELDED	RIGID FRAME,	/LEAN-TO/SING	SLE SLOPE
		•			CUSTOM	ER SEI	MCO CONSTI	RUCTION	0.5:12	ROOF SLOPE	· · · · · · · · · · · · · · · · · · ·	
			<u> </u>		LOCATIO	N BAI	RTOW, FL		JOBSITE	BARTOV	V, FL	
· ·					DRAWN BY	CHECKED BY	DATE	SCALE	CAD NO.	JOB NO.	DWG. NO.	ISSUE
			Ι,		SD	HL	2/26/97	NONE	970090A	970090	D-ONE	A

SKYLIGHTS MUST NOT BE USED FOR FOOT TRAFFIC

WEIGHT OF ANY INDIVIDUAL. ROOFING LADDERS OR

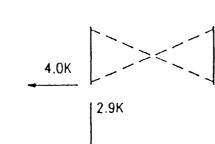
1" X 12" PLANKS MUST BE USED DURING INSTALLATION,

WHIRLWIND STEEL BUILDINGS AND ITS ENGINEERS ARE NOT RESPONSIBLE FOR ANY INJURY RESULTING FROM

NOR SHOULD THEY SUPPORT THE UNDISTRIBUTED

MAINTENANCE OR REPAIR PROCEDURES.

THE SKYLIGHTS FAILING FROM IMPROPER USE.



### REACTIONS AT WALL X-BRACING AT COLUMN LINES A & G

DEAD COLL LIVE SNOW WIND WIND WIND WIND WIND SEIS 
 LOAD
 LOAD
 LOAD
 LEFT1
 LEFT2
 RIGHT1
 RIGHT2
 LONG.
 LOAD
 LOAD

 4.1
 3.8
 15.0
 0.0
 -33.4
 -12.1
 0.0
 0.0
 -28.3
 0.0
 0.0
 MEMBERS LEFT COL. HOR LEFT COL. VER 3.8 | 3.0 | 12.0 | 0.0 | -28.2 | -9.1 | 0.0 | 0.0 | -27.5 | RIGT COL. HOR 
 -4.1
 -3.8
 -15.0
 0.0
 28.5
 7.2
 0.0
 0.0
 28.7
 0.0
 RIGT COL. VER 3.8 | 3.0 | 12.0 | 0.0 | -24.3 | -4.6 | 0.0 | 0.0 | -23.9 | 0.0

THE REACTIONS ARE STATED IN KIPS (1 KIP = 1000 POUNDS).

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OVER 4 DIAMETERS. BUT NOT EXCEEDING 8 DIAMETERS ...... 1/2 TURN OVER 8 DIAMETERS, BUT NOT EXCEEDING 12 DIAMETERS ..... 2/3 TURN

BEMCO CONSTRUCTION, INC. SHOP DRAWING REVIEW No Exceptions Taken Note Marking's Resemble Contractor's review is for Egeneral coording of the

> STEEL DESIGN ONLY NO OTHER CODE REQUIREMENTS ARE INCLUDED

As Builts

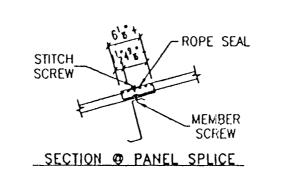
REFERENCE: LAIDLAW ENVIRONMENTAL SERVICES

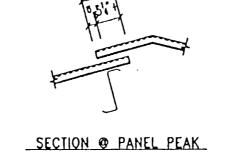
REV	DATE	DESCRIPTION	BY	CHKD.				> WILLI	חאואו וכ	STEEL BUII	DINCS	
Α	2/26/97	FOR APPROVAL	SD	711		<b>(</b> V	VÁ(RLW)	ND)				
									1445EN HOUS 946-7140	TON, TEXAS 77075-1	1089-	
•			ļ		DESCRI	PTION FRA	AME CROSS	SECTION				
			<del> </del>	<u> </u>	SIZE	1 4 \	חורכ	· • • • • • • • • • • • • • • • • • • •	WELDE	D DIOID FDANE	/1.5.1.1. TO /GING	
			<u> </u>	<u> </u>	SIZE	VAF	RIES 		WELDE	D RIGID FRAME/	LEAN-10/SINC	SLE SLOPE
			<u> </u>		CUSTON	IER SEI	MCO CONST	RUCTION	0.5:1	2 ROOF SLOPE		
•			<u> </u>									
					LOCATIO	N BAI	RTOW, FL		JOBSITE	E BARTOW	, FL	
	•				DRAWN BY	CHECKED BY	DATE	SCALE	CAD NO.	JOB NO.	DWG. NO.	ISSUE
					SD	714	2/ /97	NONE	970090A	970090	P-ONE	A

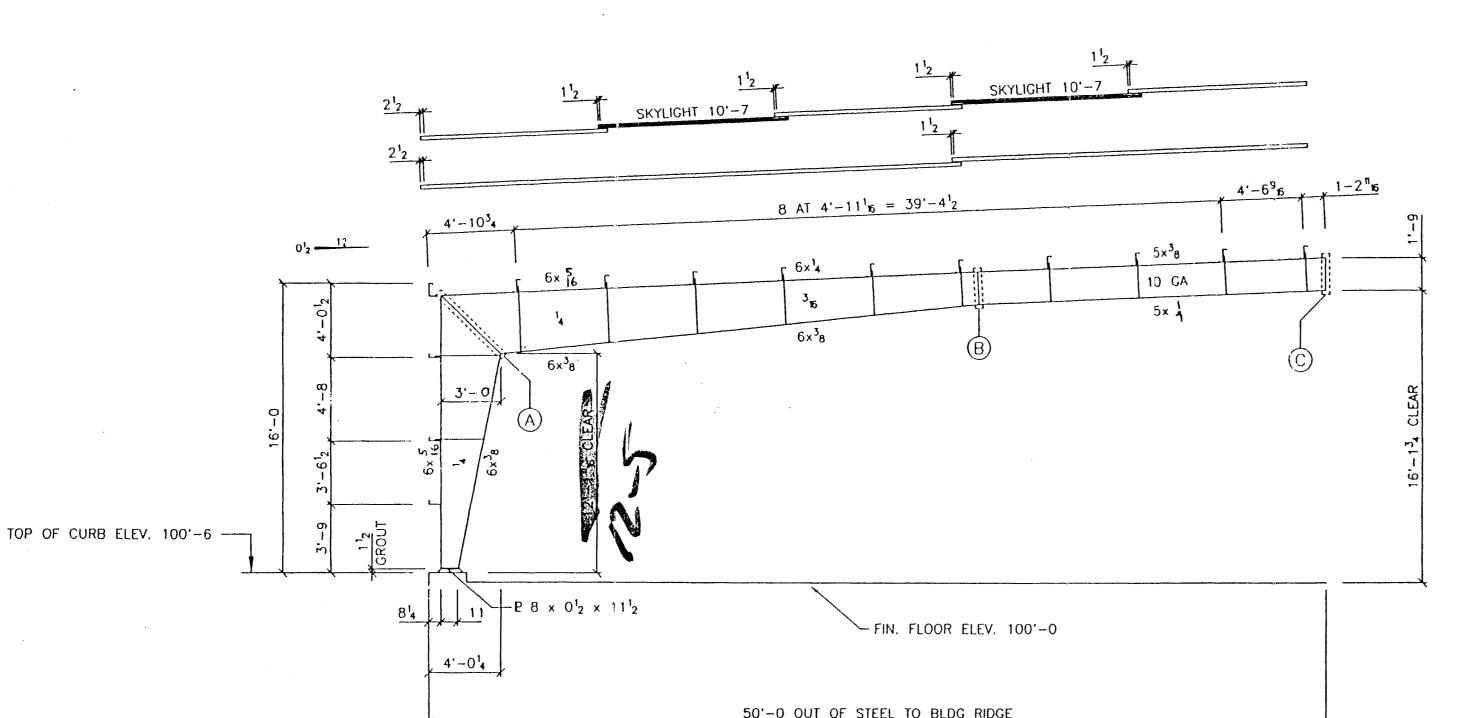
√-3" REINFORCEMENT PANEL

DETAIL @ SUPER SPAN UL 580, CLASS 90 SKYLIGHT PANEL

SECTION @ PANEL END







FRAME CROSS SECTION COLUMN LINES 3 - 10

SUBMITTAL

SPLICE BOLT TABLE

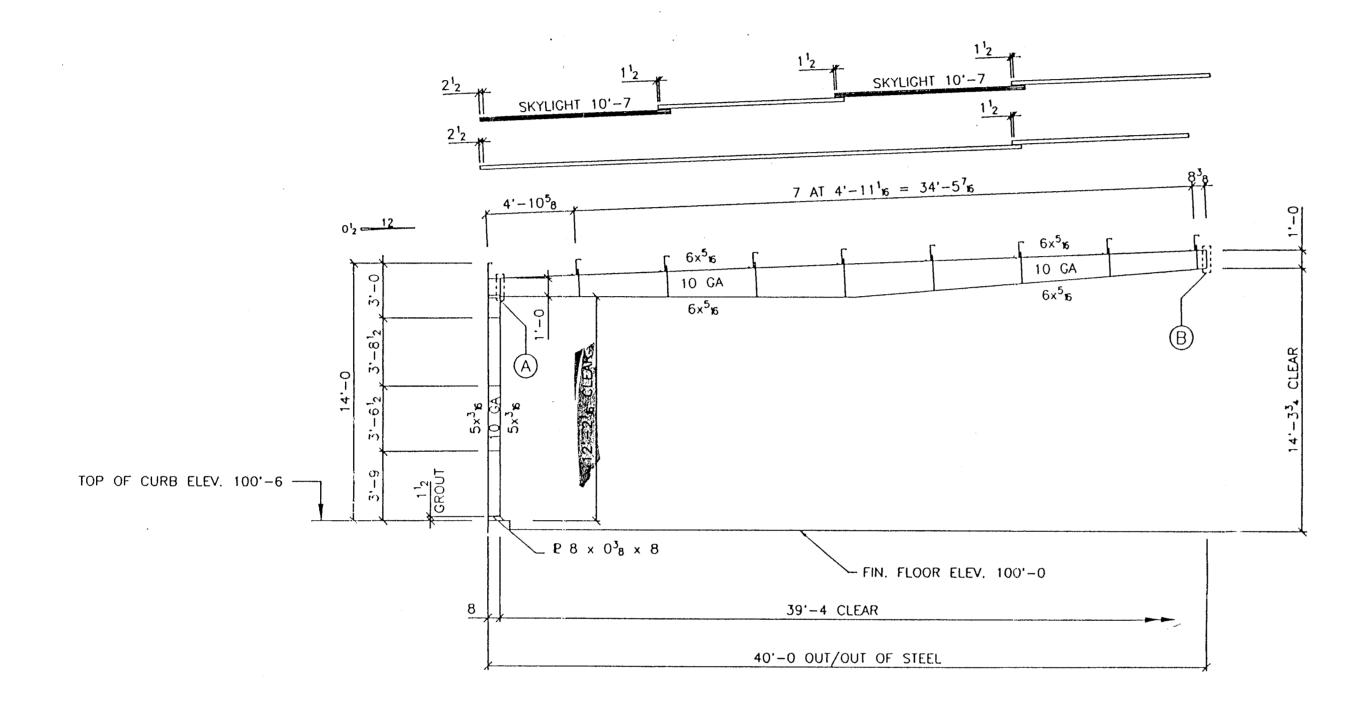
PLICE NO. SIZE

A 6 58" ø x 0-112"

WADNINGI

SKYLIGHTS MUST NOT BE USED FOR FOOT TRAFFIC NOR SHOULD THEY SUPPORT THE UNDISTRIBUTED WEIGHT OF ANY INDIVIDUAL. ROOFING LADDERS OR 1" X 12" PLANKS MUST BE USED DURING INSTALLATION, MAINTENANCE OR REPAIR PROCEDURES.

WHIRLWIND STEEL BUILDINGS AND ITS ENGINEERS ARE NOT RESPONSIBLE FOR ANY INJURY RESULTING FROM THE SKYLIGHTS FAILING FROM IMPROPER USE.



FRAME CROSS SECTION

COLUMN LINES B - G

REACTION DEAD COLL LIVE SNOW WIND WIND WIND WIND WIND SEIS MEMBERS LOAD LOAD LOAD LOAD LEFT1 LEFT2 RIGHT1 RIGHT2 LONG. LOAD EXT. COL. HOR 0.0 0.0 0.0 0.0 0.5 -2.4 3.1 0.2 3.5 0.0 EXT. COL. VER 1.6 1.5 5.9 0.0 -14.6 -5.1 -11.6 -1.6 -14.7 0.0 THE REACTIONS ARE STATED IN KIPS (1 KIP = 1000 POUNDS).

6.0K 3.9K

REACTIONS AT WALL X-BRACING

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SEMCO CONSTRUCTION, INC.

SHOP DRAWING REVIEW

No Exceptions Taken

Contractor's review is for general condesign concept and confrect

comments shall not confrect

Supplier / School not conf

STEEL DESIGN ONLY
NO OTHER CODE REQUIREMENTS
ARE INCLUDED

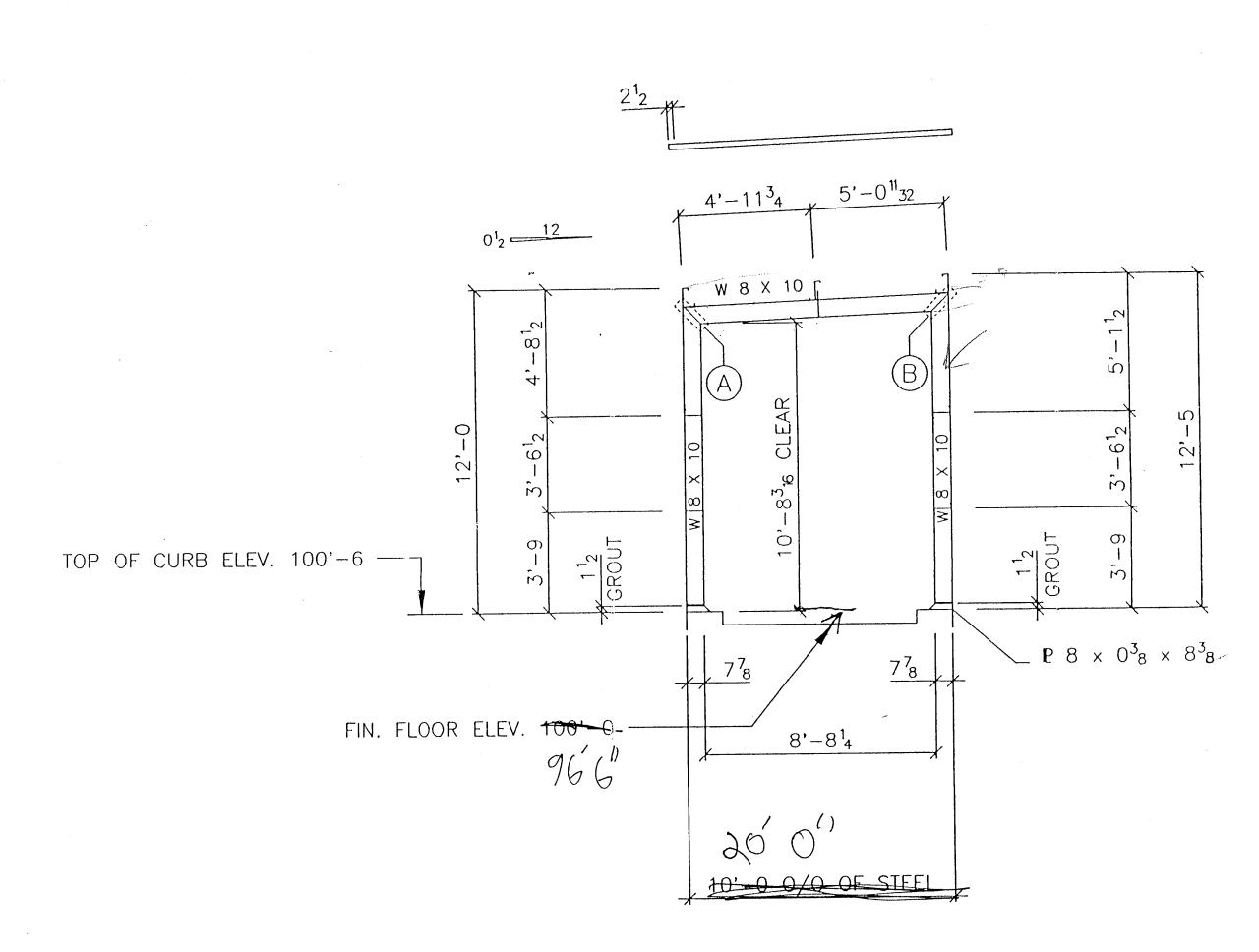
As Built

REFERENCE: LAIDLAW ENVIRONMENTAL SERVICES

REV	DATE	DESCRIPTION	BY	CHKD.				MLIIW «	טו אוואו וכ	STEEL BUIL	DINICS	
Α	2/26/97	FOR APPROVAL	SD	JH		<b>(</b> V	VÁÍRLWÌ	(UP)				
									IANSEN HOUS 946-7140	TON, TEXAS 77075-1	089	
<u>.</u>			ļ		DESCRIP	TION FRA	ME CROSS	SECTION				
	<u> </u>		<u> </u>	,								
					SIZE	40′	x 80.	X 14' E.H	I. LEAN-	10		
		•			CUSTOM	ER SEN	ACO CONST	RUCTION	0.5:1	2 ROOF SLOPE		
		•										
					LOCATION	N BAF	RTOW, FL		JOBSITE	E BARTOW	, FL	
					DRAWN BY	CHECKED BY	DATE	SCALE	CAD HO.	JOB NO:	DWG. NO.	ISSUE
					SD	JH	2/26/97	NONE	970090B	970090	P-2	A

	SPL	ICE BOLT TABLE	
SPLICE	NO.	SIZE	
- A	6	$\frac{3}{4}$ "ø × 0-2 $\frac{1}{2}$ "	
B	8	$^{3}_{4}$ "ø x $0-2^{1}_{2}$ "	
. C	6	$\frac{3}{4}$ "ø × 0-2 $\frac{1}{2}$ "	

and the second of the second o



FRAME CROSS SECTION

COLUMN LINES E - F

 REACTION
 DEAD
 COLL
 LIVE
 SNOW
 WIND
 SEIS

 MEMBERS
 LOAD
 LOAD
 LOAD
 LOAD
 LEFT1
 LEFT2
 RIGHT1
 RIGHT2
 LONG
 LOAD

 LEFT COL.
 HOR
 0.0
 0.0
 0.1
 0.0
 -2.2
 -2.6
 2.2
 1.7
 1.1
 0.0

 LEFT COL.
 VER
 0.3
 0.2
 1.0
 0.0
 -4.0
 -3.4
 1.7
 2.2
 -1.2
 0.0

 RIGT COL.
 HOR
 0.0
 0.0
 -0.1
 0.0
 -2.0
 -1.6
 2.2
 2.7
 -1.1
 0.0

 RIGT COL.
 VER
 0.3
 0.2
 1.0
 0.0
 1.4
 1.9
 -4.1
 -3.6
 -1.2
 0.0

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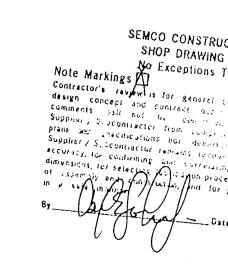
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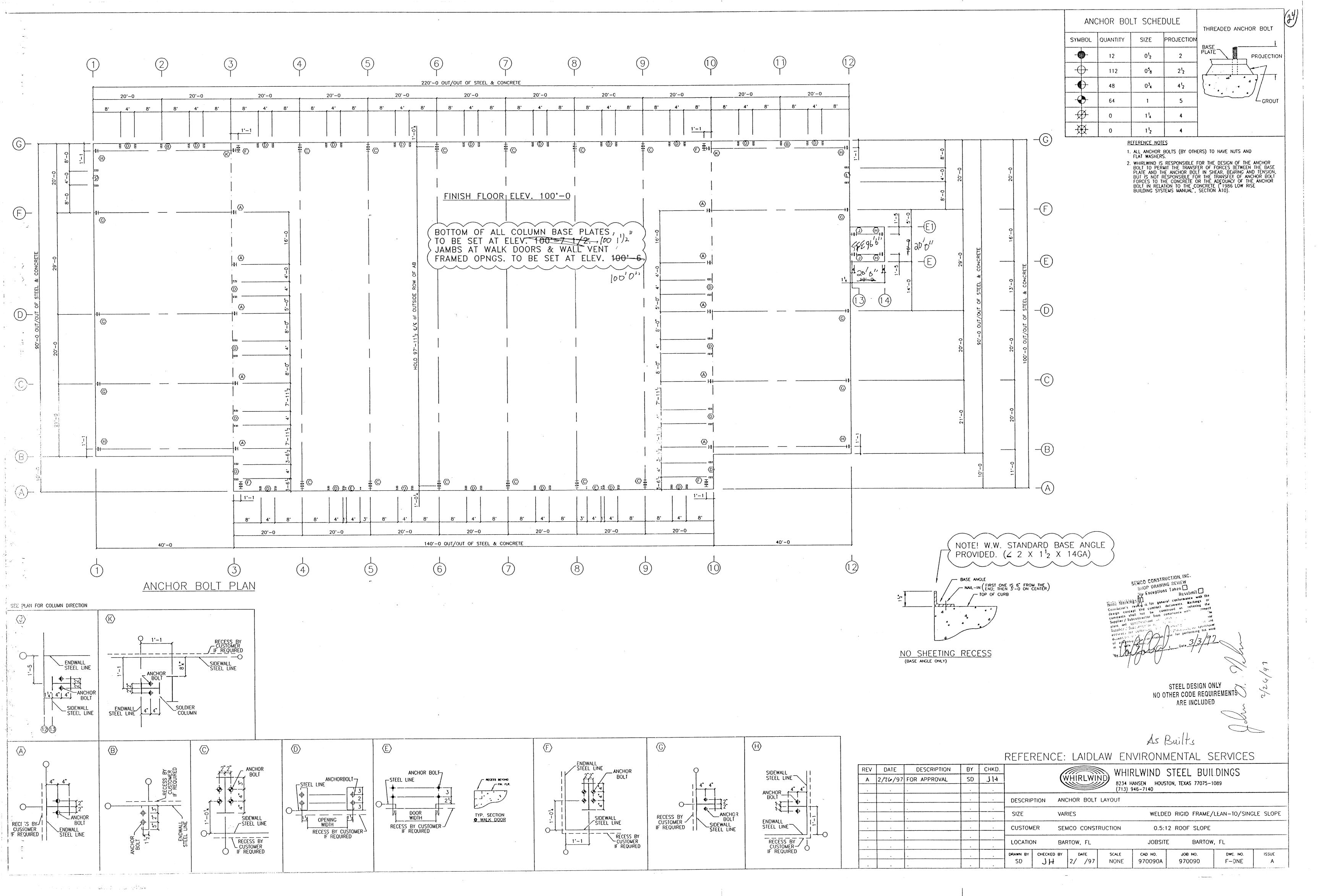


STEEL DESIGN ONLY
NO OTHER CODE REQUIREMENTS
ARE INCLUDED

As Bailts

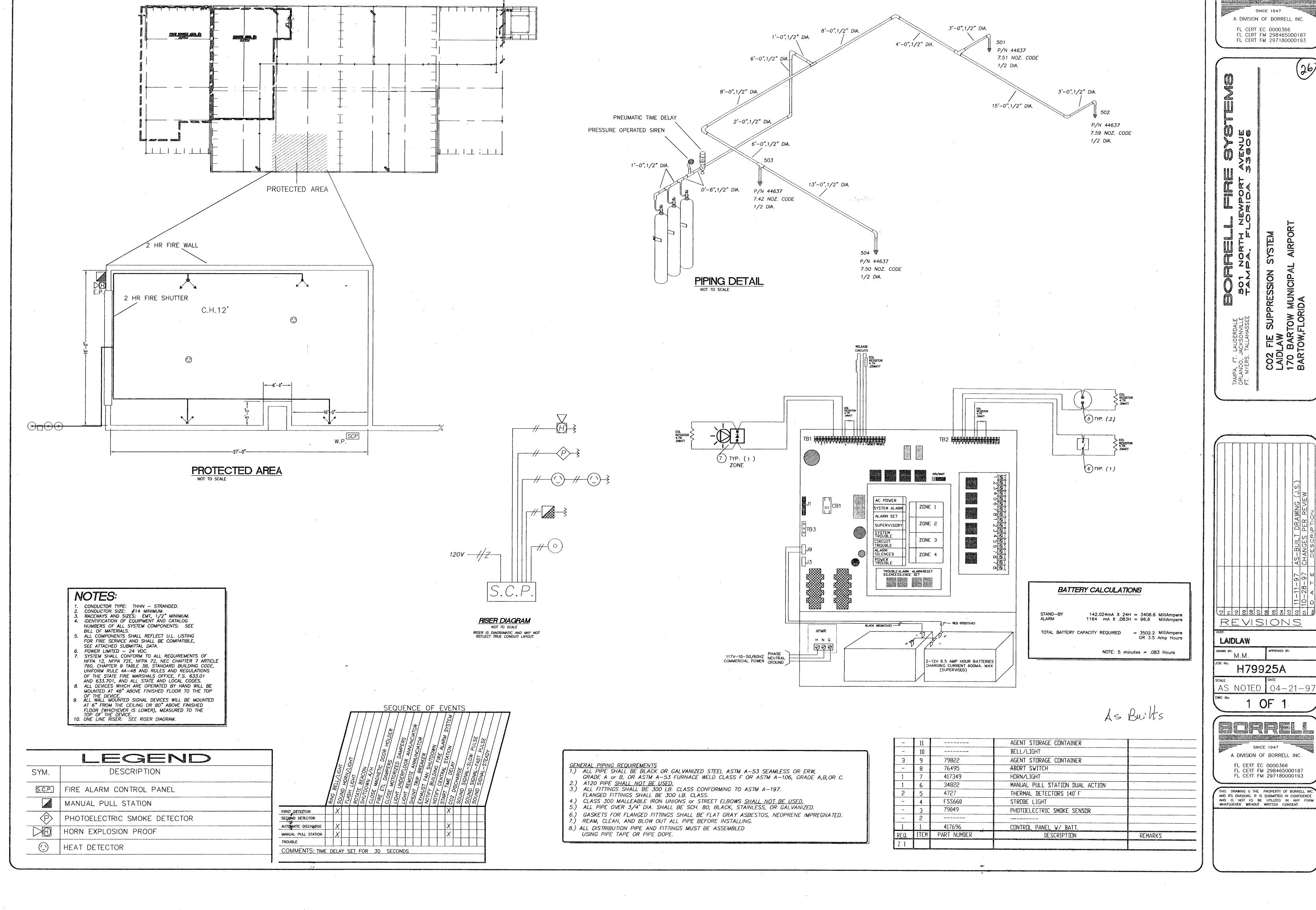
REFERENCE: LAIDLAW ENVIRONMENTAL SERVICES

REV	DATE	DESCRIPTION	BY	CHKD.				NHIF	NIWIND S	STEEL BUIL	DINGS	
A	2/26/97	FOR APPROVAL	SD	114		(v	VHÍRLWI	NDI		ON, TEXAS 77075-1		
									946-7140			
•					DESCRIPTION	ON FRA	ME CROSS	SECTION				
•			<u> </u>		SIZE	10'	X 10'	X 12' E.F	I. SINGLE	SLOPE		
					CUSTOMER	R SEM	MCO CONST	RUCTION	0.5:1:	2 ROOF SLOPE		
•			<u> </u>	· · · · · · · · · · · · · · · · · · ·	LOCATION	BAF	RTOW, FL		JOBSITE	BARTOW	/, FL	
•			_	<del>                                     </del>	DRAWN BY (	CHECKED BY	DATE	SCALE	CAD NO.	JOB NO.	DWC. NO.	ISSUE
	•	•	<del> </del>	· · · · · · · · · · · · · · · · · · ·	SD	HL	2/ /97	NONE	970090D	970090	P-3	А



## APPENDIX 4

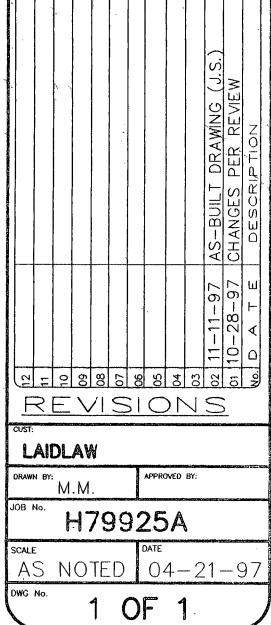
Fire Suppression Systems As-Builts

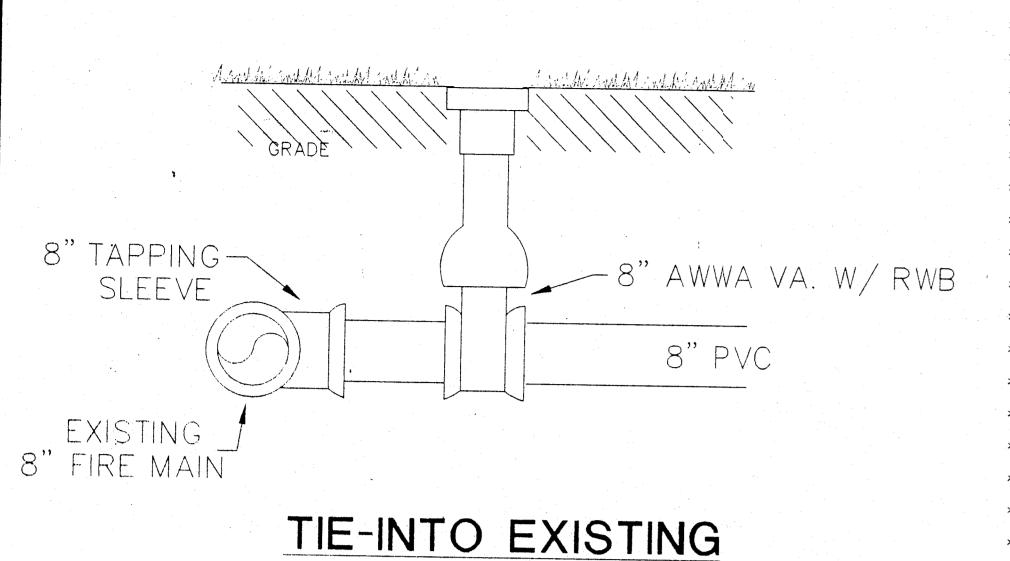


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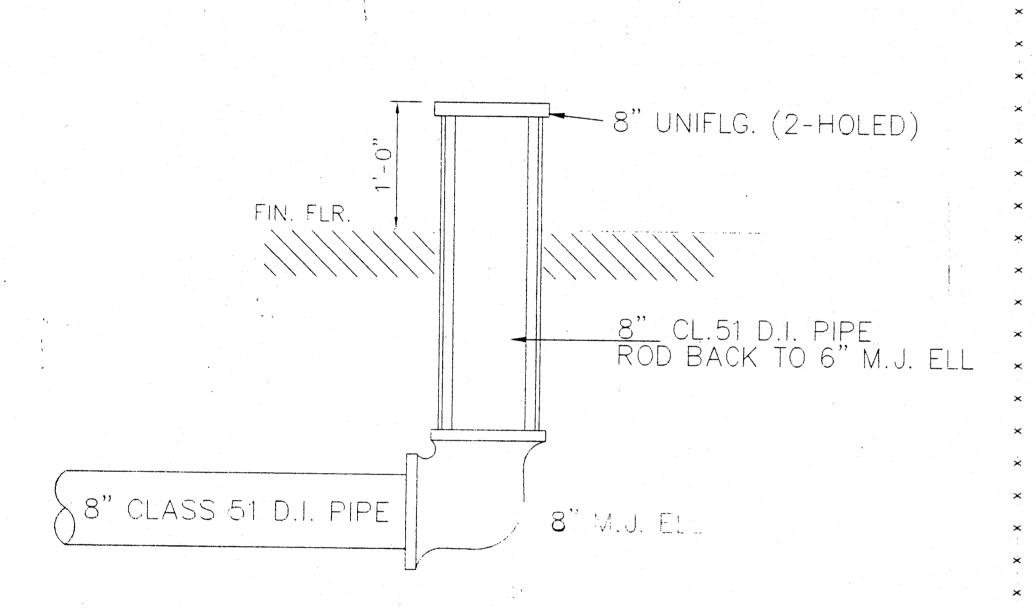
A DIVISION OF BORRELL INC. FL CERT EC 0000366 FL CERT FM 298465000187 FL CERT FM 297180000193

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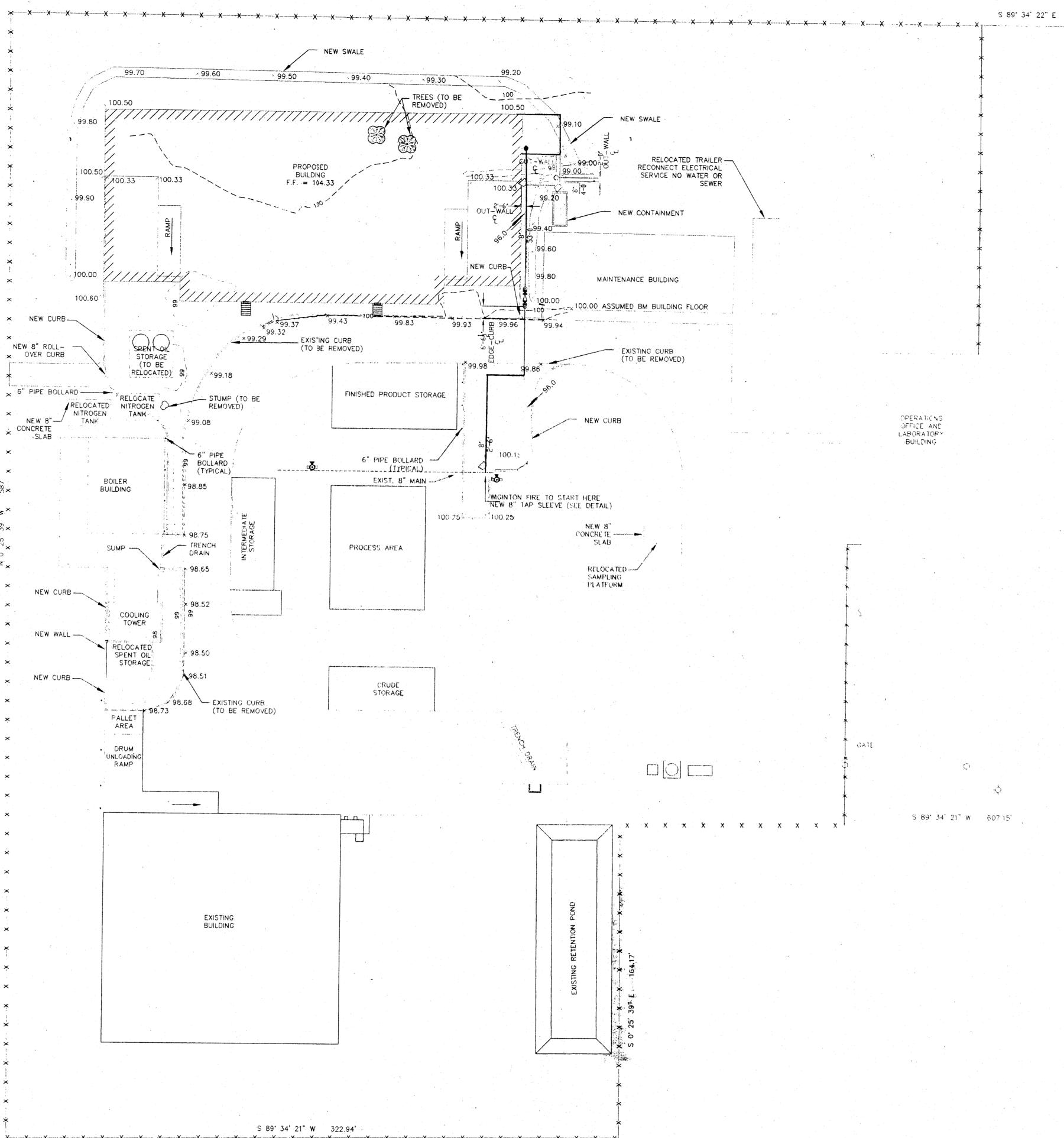
MAIN DETAIL



STUB DETAIL

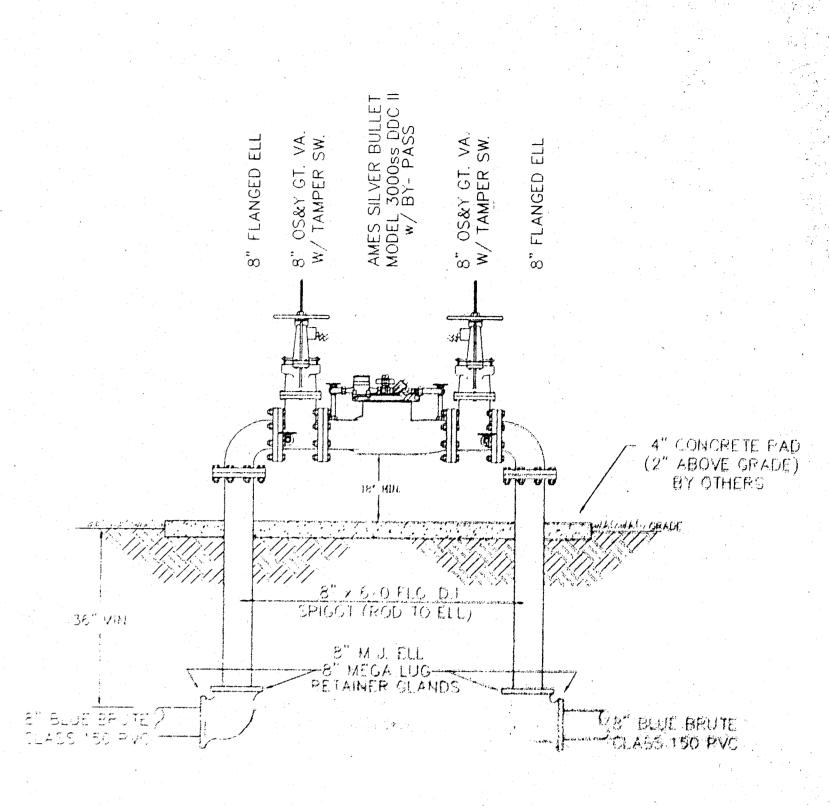
ABBREVIATIONS

WATER SUPPLY



## UNDERGROUND FIRE PROTECTION PIPING PLAN





## BACKFLOW PREVENTOR DETAIL

NEW CONCRETE

EXISTING STRUCTURES EXISTING STRUCTURES (TO BE REMOVED)

/////// NEW BUILDING EXISTING SPOT ELEVATIONS

100 00 NEW SPOT ELEVATIONS

## SYMBOLS LEGEND

NEW UNDERGROUND PIPE

----- EXIST. UNDERGROUND PIPE

SYSTEM RISER

GINDDIME BACKFLOW PREVENTOR

CHECK VALVE

AWWA VA. & ROADWAY BOX

EXISTIG HYDRANT

HYDRAULIC REFERENCE POINT

## GENERAL NOTES

- 1) NEW UNDERGROUND PIPE TO BE C-900 P.V.C. PIPE.
- 2) PIPE FOR NEW STUB-IN TO BE DUCTILE IRON.
- 3) ALL PIPE TO BE INSTALLED 36" MIN. BELOW GRADE.T.O.P.(GRADE TO BE FIELD VERIFIED)
- 4) UNDERGROUND PIPING INSTALLATION TO MEET REQUIREMENTS OF NFPA 24 & LOCAL CODES.

## AS BUILTS

UNDERGROUND PIPING PLAN

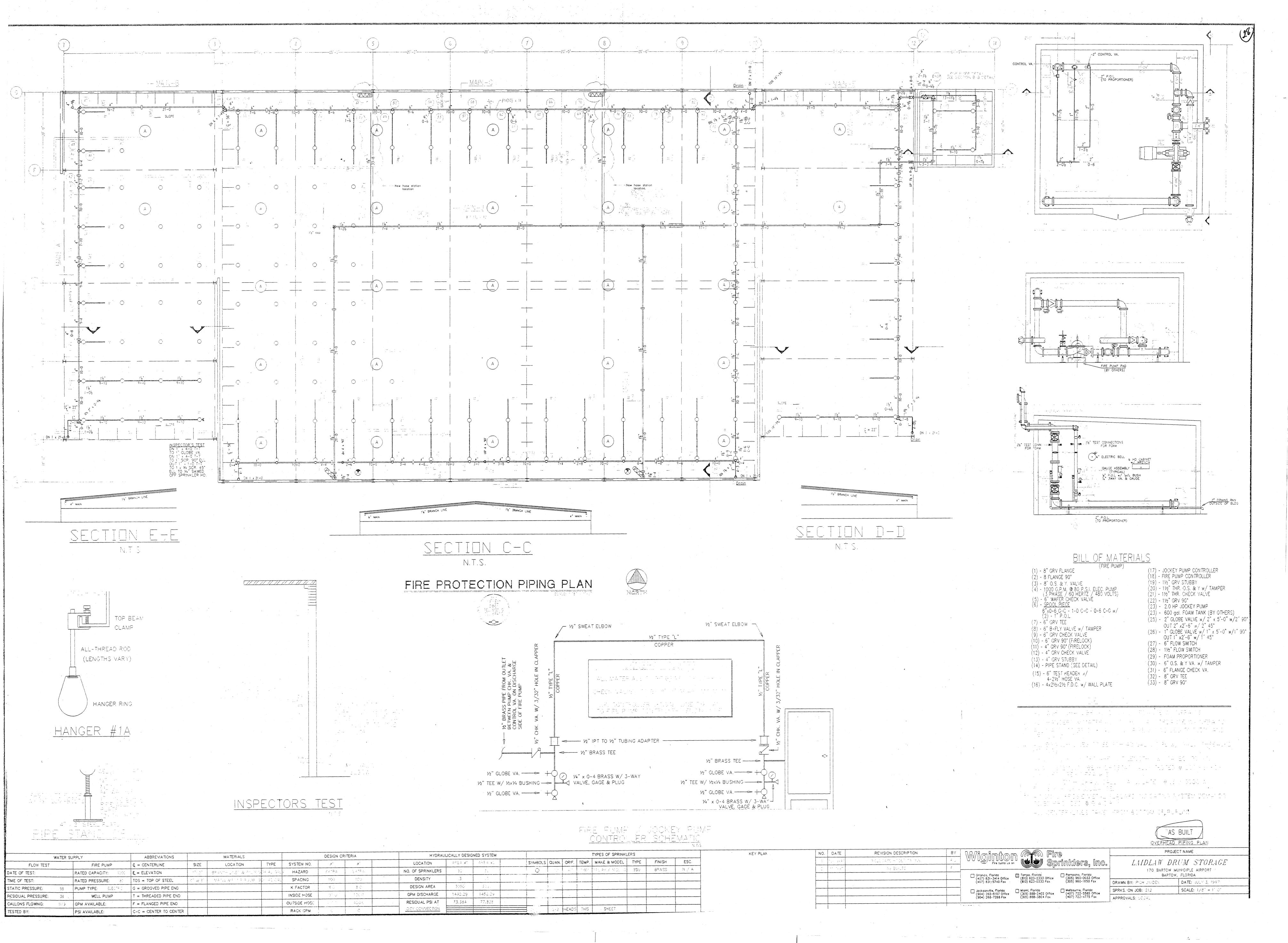
BARTOW, FLORIDA

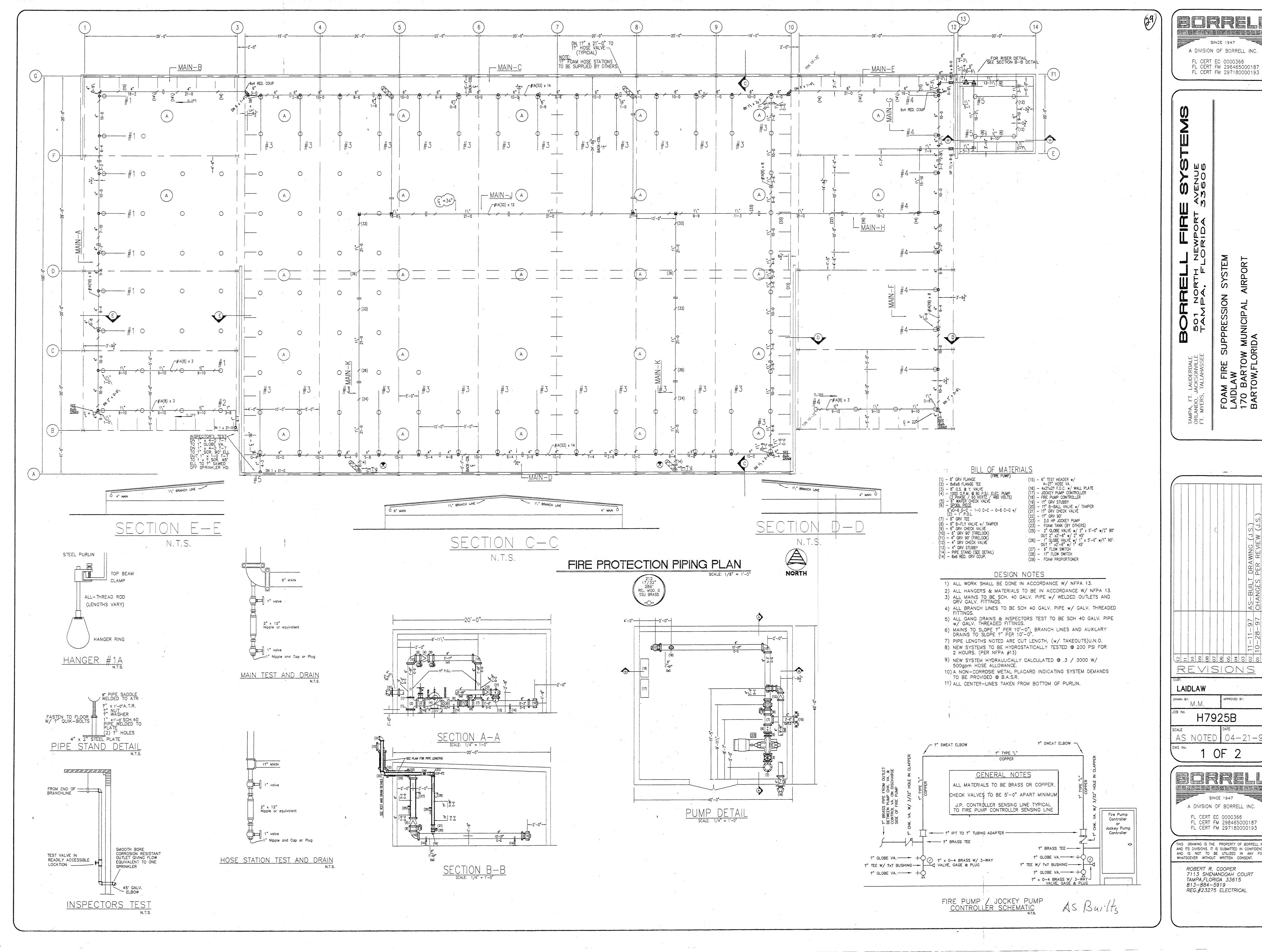
DATE: MARCH 26, 1997

MATERIALS DESIGN CRITERIA HYDRAULICALLY DESIGNED SYSTEM TYPES OF SPRINKLER'S FLOW TEST FIRE PUMP C = CENTERLINE LOCATION SYSTEM NO. LOCATION SYMBOLS QUAN. ORIF. TEMP. MAKE & MODEL DATE OF TEST: RATED CAPACITY: 1000 E = ELEVATION UNDERGROUND MAIN HAZARD NO. OF SPRINKLERS TIME OF TEST: RATED PRESSURE: 80 TOS = TOP OF STEEL UNDERGROUND MAIN SPACING DENSITY STATIC PRESSURE: G = GROOVED PIPE END DESIGN AREA T = THREADED PIPE END INSIDE HOSE GPM DISCHARGE GALLONS FLOWING: 1119 GPM AVAILABLE F = FLANGED PIPE END OUTSIDE HOSE RESIDUAL PSI AT PSI AVAILABLE: C-C = CENTER TO CENTER CITY CONNECTION

NO. DATE LAIDLAW DRUM STORAGE DRAWN BY: RICH JUDEN

CUSTOMER PROJECT NO



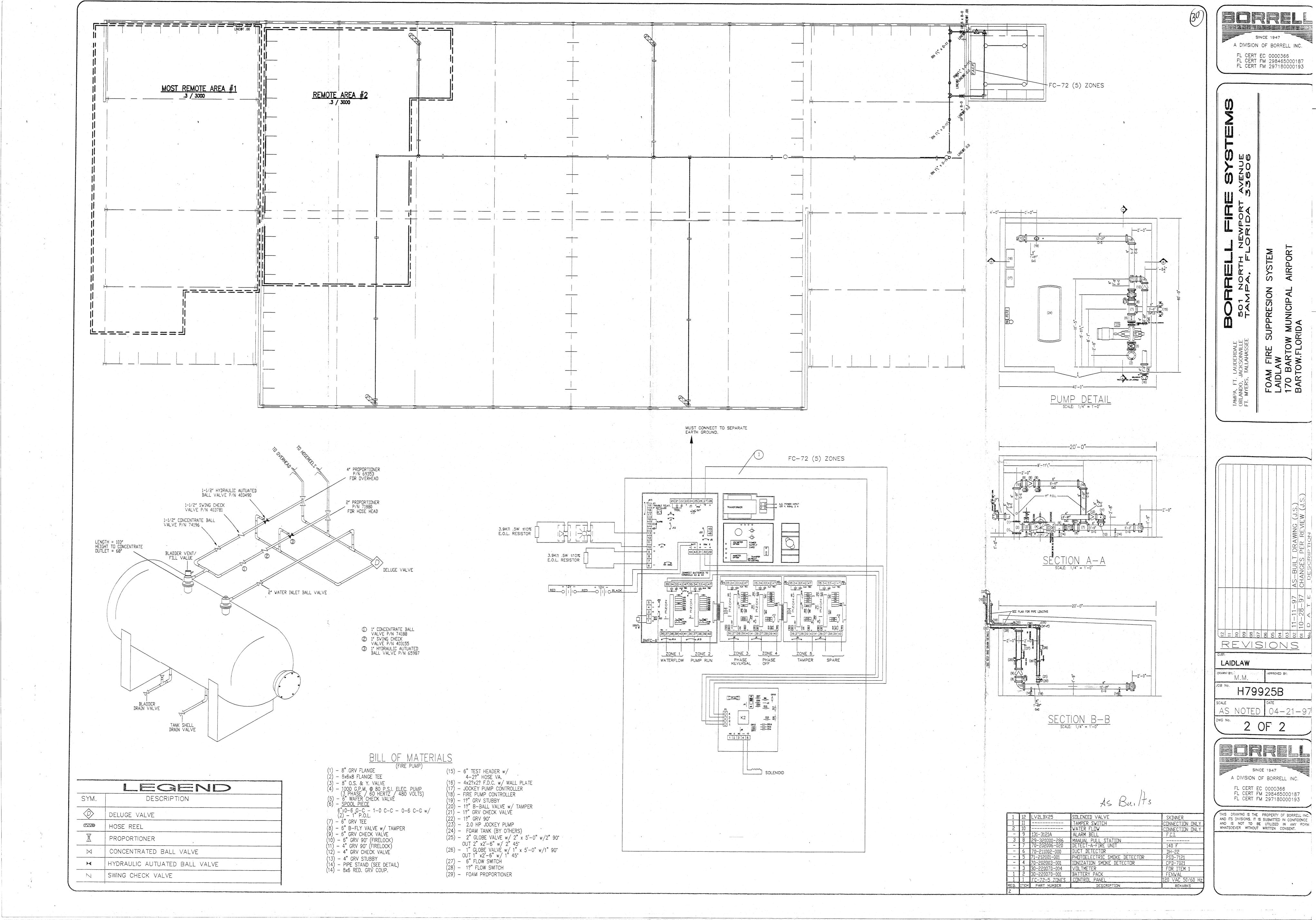


AS-BUILT DRAWING (J.S.) CHANGES PER REVIEW (J. 28-97

04-21-97

因共產黨國際等等調整指數國際與出國國際 A DIVISION OF BORRELL INC. FL CERT FM 298465000187

THIS DRAWING IS THE PROPERTY OF BORRELL IN AND ITS DIVISIONS. IT IS SUBMITTED IN CONFIDENCE
AND IS NOT TO BE UTILIZED IN ANY FORM
WHATSOEVER WITHOUT WRITTEN CONSENT.



## LAIDLAW ENVIRONMENTAL SERVICES OF BARTOW, INC.

Report of
Final Geotechnical Exploration
Proposed Drum Storage Building
Bartow, Florida



### Ardaman & Associates, Inc.

#### **OFFICES**

Orlando, 8008 S. Orange Avenue, Orlando. Florida 32809, Phone (407) 855-3860
Bartow, 1525 Centennial Drive, Bartow. Florida 33831, Phone (813) 533-0858
Cocoa, 1300 N. Cocoa Blvd., Cocoa. Florida 32922, Phone (407) 632-2503
Fort Lauderdale, 3665 Park Central Boulevard, North. Pompano Beach, Florida 33064, Phone (305) 969-8788
Fort Myers, 9970 Bavaria Road, Fort Myers. Florida 33913, Phone (813) 768-6600
Miami, 2608 W. 84th Street, Hialeah. Florida 33016, Phone (305) 825-2683
Port Charlotte, 740 Tamiami Trail, Unit 3, Port Charlotte, Florida 33954, Phone (813) 624-3393
Port St. Lucie, 1017 S.E. Holbrook Ct., Port St. Lucie, Florida 34952, Phone (407) 337-1200
Sarasota, 2500 Bee Ridge Road, Sarasota. Florida 34239, Phone (813) 922-3526
Tallahassee, 3175 West Tharpe Street, Tallahassee, Florida 32303, Phone (904) 576-6131
Tampa, 1406 Tech Boulevard, Tampa. Florida 33619, Phone (813) 620-3389
West Palm Beach, 2511 Westgate Avenue, Suite 10, West Palm Beach, Florida 33409, Phone (407) 687-8200

#### MEMBERS:

A.S.F.E.
American Concrete Institute
American Society for Testing and Materials
American Consulting Engineers Council
Florida Institute of Consulting Engineers
American Council of Independent Laboratories



March 25, 1997 File Number 97-51-9036

Laidlaw Environmental Services of Bartow, Inc. 17 Bartow Municipal Airport Bartow, FL 33830

Attention: Mr. Liam Munroe

Subject: Report of Final Geotechnical Exploration, Proposed Drum Storage Building, Bartow

Airport, Bartow, Polk County, Florida

Dear Mr. Munroe:

Ardaman & Associates, Inc. has completed the exploration of subsurface soil conditions beneath the proposed drum storage building at the referenced site, in general accordance with our Proposal Number 97-033, dated March 13, 1997. Authorization for the services in this study was verbally provided by you on March 13, 1997. The purposes of this exploration were to define the stratification and engineering properties of subsurface soils, to provide recommendations which address the design and installation of foundations, and to delineate recommended earthwork procedures and operations which should be implemented during the construction period. This study addresses foundation soils which are well within the influence of building loads, but this study does not address the condition of deep soil or bedrock strata.

This report was prepared for the exclusive use of Laidlaw Environmental Services of Bartow, Inc. and their consultants. The conclusions and recommendations are applicable only to those structures and facilities are described herein. This geotechnical study was performed in accordance with generally accepted geotechnical engineering practices. No other warranty, expressed or implied, is made.

#### **SCOPE**

The scope of our services has included the following items:

1. Flagging of proposed soil boring locations and discussion with your on-site contractor to determine if any existing underground utilities were present within the proposed building area. Resolution of any conflicts between the proposed location of the soil borings and the known location of buried utility lines, as necessary, to maintain a margin of at least 5 feet between marked utility lines and the soil boring locations.

- 2. Initial reconnaissance of the site by the drill crew chief to document the condition of the site, at the time of our exploration. The reconnaissance includes recording the type and condition of vegetation, the existence and general condition of any structures on the site and adjacent to the site, the inclination and direction of site topography, site drainage features, and other particulars about the site which may be pertinent to this study. Also, areas of the site which appear to have been physically or chemically altered are noted during the reconnaissance.
- Performance of seven (7) Standard Penetration Test (SPT) borings to determine the stratification and engineering properties of subsurface soils below the proposed drum storage building location.
- 4. Review of each soil sample obtained in our field testing program, by a soils engineer in our laboratory, for verification of classification and assignment of laboratory tests, if required.
- 5. Performance of laboratory soils classification tests, on selected soil samples, to confirm our visual soil classification of the site soils, and to provide pertinent test data to estimate soil engineering parameters.
- Analysis of the existing building site soil and ground water conditions as they relate to the proposed development.
- 7. Preparation of this report to document the results of our field testing program, engineering analysis, and foundation design and site earthwork recommendations.

#### SITE LOCATION AND CONDITIONS

The proposed building site is located within a tract of land situated in the southwest one-quarter of the southeast one-quarter of Section 14, Township 29 South, Range 25 East, Polk County. More specifically, the proposed construction area is within the Bartow Municipal Airport property. It lies immediately west of an existing maintenance area.

#### Topography

The site is relatively flat. There appeared to be a slight downward slop from west to east, based on ground water levels obtained within the soil borings.

#### **Vegetation**

Most existing ground vegetation had been stripped and removed prior to our field exploration. However, trace amounts of roots were encountered within the borings to depths of 15 to 18 inches below the ground surface.

#### FIELD EXPLORATION

#### Soil Borings

Our field operations consisted of conducting a series of seven (7) SPT borings using procedures similar to those outlined in ASTM D-1586. The borings were performed at the locations indicated on the attached Figure 1. The test locations and depths of the borings were determined by our firm, as described in Proposal No. 97-033, dated March 13, 1997. The borings were performed to determine the stratification and engineering properties of the subsurface soils below the proposed drum storage building. Borehole depths ranged from a minimum depth of 19 feet to a maximum depth of 19.5 feet below the existing ground surface. A continuous drilling and sampling procedure was performed within the upper 8 to 10.5 feet of the SPT boring to detect subtle changes in soil stratigraphy and pertinent engineering properties within this critical depth. Furthermore, the borings were located in the field by our drilling crew by visual reckoning using a site plan, provided by the General Contractor, Semco Construction, having a reduced scale of 1 inch = 22 feet, and by tape measurement from the northwest corner of the adjacent maintenance building. Land surface elevations at the soil boring locations were not determined.

The accuracy of the boring locations is that implied by the measurement method used. Upon completion, each borehole was filled in with local soil. A brief summary of the drilling and testing procedures utilized in the boring is included in the attached Appendix I.

#### LABORATORY TESTING

The field soil boring logs and recovered soil samples were transported to our Bartow office from the project site. Following the completion of the field exploration activities, each soil sample was examined by a geotechnical engineer in our soils laboratory to identify the apparent engineering classification of the soil samples retrieved in the field exploration, and to select representative soil samples for assignment of pertinent laboratory soil classification tests. The visual classification of the samples was performed in accordance with the current Unified Soil Classification System (ASTM D-2487).

#### Moisture Content and Percent Fines Tests

Five (5) moisture content and two (2) percent fines tests (the percent by dry weight finer than the U.S. No. 200 sieve) were performed on soil samples obtained from within borings TH-1, TH-2, and TH-4. These indices are useful in estimating compressibility and permeability characteristics of clayey soils, and in evaluating the applicability of soil improvement methods for granular soils. Furthermore, the results of these tests provide partial confirmation of our visual classification of the soils penetrated in this exploration. The results of the tests are plotted adjacent to the final soil boring profiles on the attached Figures 2 and 3 at the depth of the individually tested soil sample.

#### **Organic Content Tests**

Two (2) tests were performed and samples were selected, from those returned in our exploration, for determination of their percentage of organic constituents. Samples were selected from Borings TH-1 and TH-4. The results of these tests are useful in confirming our visual classification of these soils, and in evaluating their compressibility. The results of these organic content tests are plotted, at the appropriate depth, adjacent to the soil boring profiles on Figures 2 and 3.

#### SOIL CONDITIONS

The delineation of the vertical extent of individual soil strata, the identification of pertinent soil engineering properties, where applicable, and a description of each geologic layer discovered in the course of our exploration, is given in the final soil boring profiles illustrated on the attached Figures 2 and 3. The final soil boring profiles were prepared by a geotechnical engineer, based upon a combination of his technical review of the field soil boring logs, his visual classification of the recovered soil samples, and his review of the results of laboratory soils tests performed for this study, as described above. The stratification lines shown are used to indicate a transition from one soil type to another. The actual boundary between the illustrated soil layers may be gradual, or indistinct. Consequently, the stratification boundary lines, shown on the final soil boring profiles, represent our best estimate of the location of the transition between distinct soil strata. They are in no way intended to designate a depth of exact geological change. Furthermore, the recommendations contained in this report are based on the contents of the final soil boring profiles. While the borings are representative of subsurface conditions at their respective locations and vertical reaches, local variations which are characteristic of the subsurface materials of the region, or which may be due to man-made alteration of the native geologic conditions, may be encountered.

The subsurface soil profile, based on the data obtained from seven (7) SPT borings is generally described below:

DEPTH (	Feet)	
From	То	DESCRIPTION
Existing Ground Surface	4-6	Very loose to loose, find sands (SP). Trace amounts of root fragments were encountered within many of the samples.
4-6	7 - 9	Loose to very dense, very dark-colored sands with silt (SP-SM) containing trace amounts of organic fines (hardpan). Boring TH-4 encountered a 12-incl layer of organic sands (OL) at the top of this general stratum. A 6-inch layer of the material was encountered at a depth of 6 feet at TH-1. This general stratum was not encountered at Boring TH-5.
7 - 9	Term	Very dense, weakly cemented sands to sands with silt (SP, SP-SM).

#### **GROUND WATER CONDITIONS**

The ground water level readings were measured in the borehole upon completion of testing, where possible, and at the completion of each day's field work. The measured borehole ground water levels are plotted adjacent to the final logs. These water level readings may differ, somewhat, from the actual stable ground water table, due to variations in the permeability of various aquifer soils. The accuracy of the reported water levels is also related to the time allowed for the borehole water level to come to an equilibrium. Accurate determination of the ground water level is best obtained by use of a properly installed piezometer. It must be noted that fluctuations in the ground water level may occur due to variations in rainfall and other environmental or physical factors at the time measurements are made.

#### **Unconfined (Surficial) Aquifer Conditions**

The measured borehole, unconfined ground water table level ranged from 1' - 7" to 6' - 2" feet below land surface at the time of the field exploration. The range of fluctuation of the unconfined aquifer is largely dependent on the volume of water, which precipitates through the soil, at any given time, during the year. This water table will generally attain a peak level in the period from late August to mid-September, which is near the end of the three- to four-month period when 60 to 70 percent of the yearly precipitation falls. Conversely, the lowest water level is generally recorded in May, just prior to the commencement of the summer rains.

#### **EVALUATION AND RECOMMENDATIONS**

#### **Proposed Development**

The project plans we received, dated September 24, 1996, showed the proposed structure to be a single-story, metal-framed building, approximately 100 x 220 feet in plan area, with the floor slab-on-grade. Most of the building will be elevated about 4 to 4.5 feet above existing grade with structural fill contained within a masonry stem-wall foundation. Two truck loading and unloading areas are planned along the east and west sides of the structure. The pavement slab will be at existing grade. Steel columns are designed to bear on individual footings along the perimeter stem-wall. The continuous wall and isolated column footings are designed for an allowable soil bearing pressure of 2000 pounds per square foot. The plans show the wall footings to be 24 inches wide, and a maximum column footing size of 5 feet x 5 feet.

#### Soil Evaluation

The SPT borings encountered mostly clean sands to a depth of 4 to 6 feet below existing grade, underlain by very dark-colored, organically stained sands with silt (SP-SM), or hardpan. Boring TH-4 encountered 12 inches of organic sand beginning at a depth of 4 feet. Boring TH-1 encountered about 6 inches of the same material at a depth of about 6.5 feet. Below the hardpan soil were very dense sands through the end of the borings.

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#### Organic Soils

It is our opinion that the natural and fill soils encountered at the site, with the exception of buried organic strata, are capable of supporting the anticipated loads on a conventionally designed shallow foundation system, provided that surface re-working, organic soil removal and replacement, and compaction are performed.

Complete removal of the unsuitable organic strata and replacement with compacted granular fill in the buried organic areas will be necessary in order to allow safe building support by a conventional shallow foundation system. The organic material, as encountered, should be removed to its lateral and vertical extent within the building area, including the truck loading/unloading areas. This will reduce the potential of total and differential settlement caused by consolidation of the highly compressible organic layer under the weight of new fill and applied surface loads. Demucking limits should include a suitable margin beyond the perimeter of the foundation system that will be dependent upon the excavation depth. As a minimum, the excavation margin should extend 5 feet beyond the edge of structure or footing, or a horizontal distance of 1-foot for every foot of vertical cut below footing, as measured from the outer edge of the footing bottom, whichever is greater. The existing soil cover, except for the surface soils containing roots removed from above the organic stratum, may be stockpiled and reused as engineered fill under the direction of the soils engineer or his representative.

Once the organic soils have been removed where encountered, and the sand backfill placed and compacted to existing grade, the subgrade surfaces of both the floor slab-on-grade and the foundations should be densified. The purpose of the densification is to compress loose surficial soils, as well as subgrade soils disturbed by other site preparation procedures, thereby creating a more uniform and less yielding soil mass. The above-created conditions will promote uniform settlement of the structure, thereby, reducing the incidence and magnitude of differential settlement.

The following report subsection describes earthwork procedures which were found to be successful in achieving the required soil improvement, at similar sites. That section also includes target specifications for in-place soil densities. It has been our experience that the described procedures can be accomplished using conventional earthwork equipment and techniques.

#### Site Preparation Recommendations

The existing surficial soils should be prepared prior to placement of engineered fill and foundation construction on the soils, in accordance with the following site preparation recommendations. The recommended procedures should be covered in the project specifications, and completed prior to construction of the foundation system.



The building area, plus a margin of 5 feet beyond the perimeter of the foundation system, should be cleared and grubbed of any remaining vegetation, stumps, tree root systems, and sod. Organic topsoil should be excavated and removed. Strippings, debris, and organic soils should be disposed in accordance with the owner's instructions. Any hole larger than

- 3 feet in diameter resulting from the removal of any object should be ramped to allow compaction of the bottom and sides with mechanical equipment prior to filling.
- 2. The organic sands encountered at boring TH-4 must be removed to their full vertical and lateral extent within the construction area as defined above. A dewatering system, capable of lowering the water table below the excavation bottom, will be necessary to verify that the organic sands have been completed removed. Once it has been confirmed that the organic soils have been removed, backfilling of the excavation may commence. Backfill material should consist of sands as defined in Item 5 below, and be placed in 12-inch thick lifts. Each lift should be compacted to 95 percent of the soils Modified Proctor (ASTM D-1137) Maximum Dry Density. This operation should continue up to existing grade elevation.
- 3. After clearing, grubbing and organic topsoil removal, the exposed soils outside any excavated area but within the construction area plus the margin, should be proofrolled with appropriate compaction equipment. The soils should be compacted to a depth of 24 inches below existing grade to a minimum of 95 percent of the soil's Modified Proctor (ASTM D-1557) maximum dry density. This density level should be measured by a qualified soils technician using procedures described by ASTM D-2937 or approved equal, prior to commencement of subsequent procedures. In the event that initial rolling results in unstable, yielding or pumping conditions, the soils engineer shall be contacted to determine the cause of the problem and make recommendations for remediation. As a minimum, soft, yielding, excessively wet, or otherwise unsuitable material shall be cut out and replaced with compacted clean sand. In the event that applied water does not penetrate sufficiently deep into natural soils to act as a lubricant in the compaction process, it will be necessary to disk or otherwise break up the soils before and during application of water.

Care should be exercised to avoid damaging any neighboring structures during the compaction operation.

Continuous wall footing trenches and individual footing pits should be excavated to at least 4. 36 inches below footing line and bottom grade. This is to allow for visual verification of the presence of any organic soils. Therefore, a dewatering system will be necessary, as needed, to allow for visual inspection of the excavation bottom. If organic soils are encountered, they should be removed to their full vertical extent within the building area, plus a margin of 5 feet, and replaced with sand backfill as described above. Where organic soils are not encountered, the exposed undercut footing subgrade should be compacted with suitable mechanical equipment, to achieve the specified level of density, to the required depth. Exposed undercut foundation subgrade should be tested to confirm that a minimum density of 95 percent of the Modified Proctor maximum dry density exists to a depth of 12 inches below the undercut foundation subgrade. If necessary, the subgrade shall be excavated further, refilled, and recompacted with mechanical equipment to achieve the necessary minimum field density, to the required depth. Following confirmation of the above-stated soil density, the undercut foundation trench and/or pit should be backfilled using material defined in Item 5 below. It should be placed in level lifts of 12 inches or less and compacted to achieve 95 percent of the Modified Proctor maximum dry density.



Backfill density should be confirmed, as required, and the backfill should be constructed to the bottom of foundation subgrade, as necessary.

- 5. All fill and backfill soils should consist of clean sands containing less than 12 percent, non-plastic material passing the U.S. Sieve No. 200 (percent fines). These soils should be free of roots and debris. The existing soils above the dark-colored hardpan soils are suitable for use as backfill, except for the surficial sands containing roots.
- 6. After steps 1 through 4 are completed, fill necessary to raise the grade to finished floor subgrade, or any interim working grade, should then be placed in 12-inch thick layers, moisture-conditioned, and compacted to a minimum of 95 percent of the Modified Proctor maximum dry density. All fill should consist of clean sand as defined above.

Hand-held compactors should be used within five feet of any stem-wall to reduce the potential of over stressing the wall. Thinner lifts (6 inches or less) may be necessary to achieve required compaction in this area.

- 7. Foundation backfill on sides of formed footings, if any, and building slab subgrade fill should consist of clean sand, defined in Item 5 above, which is placed in 12-inch lifts and compacted to 95 percent of the Modified Proctor maximum dry density.
- 8. Ardaman & Associates, Inc., Bartow office, should be engaged by the owner prior to site preparation to provide field observation of site preparation steps, compaction operations on natural and fill soils, and conduct field in-place density testing to confirm that the specified requirements are met.

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#### Foundation Recommendations

For foundations placed on the soils prepared as previously recommended, the foundations may be proportioned for a maximum net allowable soil bearing pressure of 2000 pounds per square foot for design dead load plus sustained live load. This allowable pressure may be increased by one-third in the case where foundations will be exposed to transient live loads, such as wind.

A soil cover of 18 inches as measured from the bottom of the foundation system to lowest adjacent finished grade should be provided. Spread footings should be at least 2.5 feet wide. Also, for any continuous wall foundations, a minimum lateral dimension of 18 inches should be provided. The foundation should be designed for equal dead load distribution in accordance with Standard Building Code requirements.

#### Predicted Performance of Shallow Spread Footings

Selection of the recommended soil bearing pressure was based primarily on considerations of limiting the expected settlement to tolerable values. Considerations of overstress and general shear of the soils below the footings were found to not have a significant influence on the recommended soil bearing pressure. Based on the expected magnitude of the foundation loads,



we estimate that the maximum settlement will be on the order of 0.6 inches for the continuous wall footings, and 0.6 inches for the individual pad footings. The estimated differential settlement between adjacent footings is 0.4 inches. We also anticipate that most of the settlement will be distortional, in nature. That is, it will be the result of rearrangement of the soil particles which constitute the granular component of the soil and elastic compression of the soil particles which comprise the cohesive component of the soil, in response to the applied load. This distortional settlement would occur almost immediately following placement of dead load on the foundations. Furthermore, it is our judgment that the settlement would occur incrementally as the dead weight loads are applied due to the predominantly granular nature of the foundation soils. Further distortional settlement of the foundations due to the addition of sustained live loads during the useful life of the structure would also occur shortly following the application of those loads. Foundation settlement, which may be due to the application of transient live loads such as wind, is expected to be negligible.

#### Field Observations

Site earthwork procedures, including the removal and replacement of the organic soils, preparation of foundation bearing surfaces, and compaction of all fill and backfill, should be observed by a geotechnical engineer or his representative from Ardaman & Associates, Inc., to verify that subsurface conditions, revealed during the earthwork operations, are as anticipated in the design and that the earthwork procedures are completed in accordance with the recommendations contained in this report.



#### **TERMINOLOGY**

We have attached a Technical Glossary to this report, which defines certain phrases that may be incorporated into the test of this document. The reader is asked to review this Glossary to familiarize himself with these phrases and their definitions, as an aid to his understanding of the content, conclusions, and recommendations contained in this report.

#### Closure

The analyses and recommendations submitted in this report are based on the data obtained from seven (7) SPT borings performed at the locations indicated on the attached Figure 1. This report does not reflect any variation which may occur in-between the borings, the nature and extent of which may not become evident until during the course of construction. If variations then appear evident, it will be necessary for you to engage our firm to re-evaluate the recommendations of this report, on the basis of pertinent on-site observations made by us during the construction period, wherein the characteristics of any variations are noted.

When the final design and specifications are completed, we would like the opportunity to review them in order to determine whether changes in the original concept may have affected the validity of our recommendations, and whether these recommendations have been implemented in the design and specifications.



Laidlaw Environmental Services of Bartow, Inc. File Number 97-51-9036

The recovered soil samples are available for examination at our Bartow office. Unless otherwise instructed in writing, the soil samples will be discarded 60 days after the issuance of this report.

It has been a pleasure assisting you with this phase of your project. If there are any questions or when we may be of further assistance, please contact the undersigned at (941) 533-0858.

Very truly yours,

ARDAMAN & ASSOCIATES, INC

P. Rodney Mank, P.E. 3/27 /

Project Engineer

Florida Registration No. 41986

Thomas J. Leto, P.E. Vice President

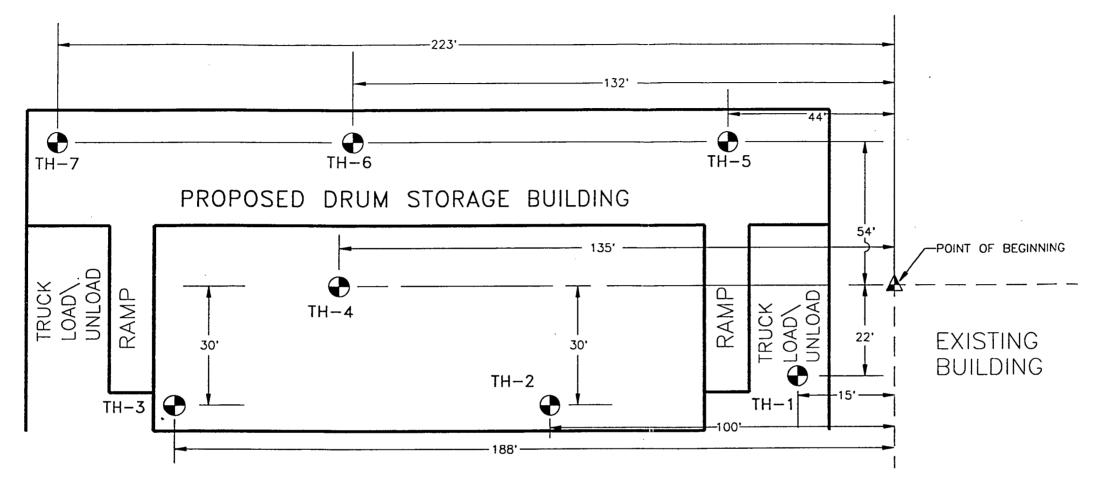
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# **FIGURES**

# SOIL BORING LOCATION PLAN



NOT TO SCALE

DRIVEWAY

LEGEND =



TH-1

STANDARD PENETRATION TEST BORING (ASTM D1586)

NOTICE:

THE PURPOSE OF THIS DRAWING IS TO PRESENT THE LOCATION OF THE SOIL BORINGS AND OTHER FIELD TESTS, AND TO PRESENT SPECIAL FEATURES RELATED TO THE SUBSURFACE CONDITIONS AT THE SITE. THE PROPOSED SITE MIPROVEWENTS SHOWN ON THIS DRAWING MAY HAVE BEEN RELOCATED, AND/OR REDESIGNED BETWEEN RECEIPT OF THE SITE PLAN AND ISSUANCE OF CONSTRUCTION BID DOCUMENTS. CONSEQUENTLY, THE SELECTED CONTRACTOR SHALL NOT USE OR RELY ON THIS DRAWING TO PLAN AND PERFORM THE CONSTRUCTION, INSOFAR AS IT RELATES TO THE PROPOSED SITE MIPROVEWENTS SHOWN HERCON, FURTHERMORE BECAUSE THIS DRAWING WAS PREPARED, USING A DOCUMENT WHICH WAS NOT RELEASED FOR CONSTRUCTION BIDS. THE CONTRACTOR SHALL BEAR IN MIND THAT ERRORS MAY EXIST ON THIS DRAWING WHICH MAY NOT HAVE BEEN CORRECTED, UNLESS THE BORING AND TEST LOCATIONS HAVE BEEN LOCATION BY A REGISTERED LAND SHALL REFLECT THE ACCURACY OF THE TEST LOCATION METHODS USED BY ARDAMAN & ASSOCIATES, INC.

WHILE THE BORINGS ARE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT THEIR RESPECTIVE LOCATIONS AND FOR THEIR RESPECTIVE VERTICAL REACHES, LOCAL VARATIONS CHARACTERISTIC OF THE SUBSURFACE MATERIALS OF THE RECION ARE ANTICIPATED AND MAY BE ENCOUNTERED. THE BORING LOCS AND RELATED INFORMATION ARE BASED ON THE DRILLERS LOCS AND VISUAL EXAMINATION OF SELECTED SAMPLES IN THE LABORATORY, THE DELINICATION BETWEEN SOIL TYPES SHOWN ON THE LABORATORY, THE DELINICATION BETWEEN SOIL TYPES SHOWN ON THE LOCS IS APPROXIMATE AND THE DESCRIPTION REPRESENTS OUR INTERPRETATION OF SUBSURFACE CONDITIONS AT THE DESCRIPTION REPORTS.

CROUNDWATER ELEVATIONS SHOWN ON THE BORING LOCS REPRESENT GROUNDWATER SURFACES ENCOUNTERED ON THE DATES SHOWN. FLUCTUATIONS IN WATER TABLE LEVELS SHOULD BE ANTICIPATED THROUGHOUT THE YEAR. ABSENCE OF WATER DATA ON CERTAIN BORINGS IMPUES THAT NO GROUNDWATER DATA IS AVAILABLE, BUT DOES NOT NECESSAFILY MEAN THAT GROUNDWATER WILL NOT BE ENCOUNTERED AT THOSE LOCATIONS OR WITHIN THE YERTICAL REACHES OF THESE BORINGS IN THE FUTURE

DATE DRILLED:

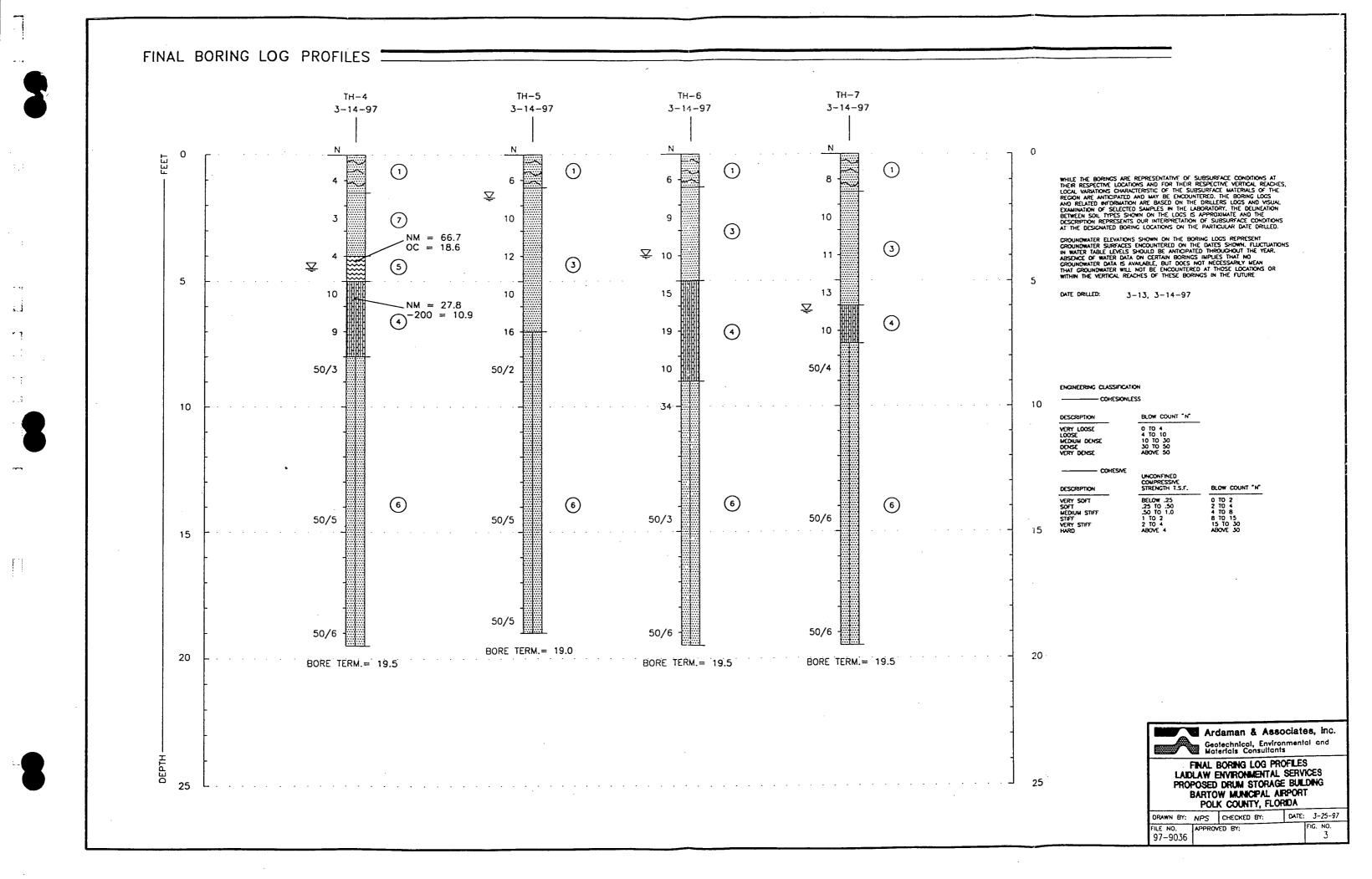
3-13, 3-14-97



Ardaman & Associates, Inc.
Geotechnical, Environmental and
Materials Consultants

SOIL BORING LOCATION PLAN
LAIDLAW ENVIRONMENTAL SERVICES
PROPOSED DRUM STORAGE BUILDING
BARTOW MUNICIPAL AIRPORT
POLK COUNTY, FLORIDA

DRAWN BY: NPS CHECKED BY: DATE: 3-25-97
FILE NO. APPROVED BY: FIG. NO. 1



# APPENDIX I FIELD EXPLORATION PROCEDURES

#### STANDARD PENETRATION TEST

The Standard Penetration Test is a widely accepted method of <u>in-situ</u> testing of foundation soils (ASTM D-1586). A 2-foot long, 2-inch outside diameter, split-barrel ("spoon") sampler, attached to the end of drilling rods, is driven 18 inches into the ground by successive blows of a 140-pound hammer freely dropping 30 inches. The number of blows needed for each six inches of penetration is recorded. The sum of the blows required for penetration of the second and third 6-inch increments of penetration constitutes the test result or N-value. After the test, the sampler is extracted from the ground and opened to allow visual examination and classification of the retained soil sample. The N-value has been empirically correlated with various soil properties allowing a conservative estimate of the behavior of soils under load.

The tests are usually performed at 5-foot intervals. However, more frequent or continuous testing is done by our firm through depths where a more accurate definition of the soils is required. The test holes are advanced to the test elevations by rotary drilling with a cutting bit, using circulating fluid to remove the cuttings and hold the fine grains in suspension. Usually, the circulating fluid, which is a bentonite drilling mud, also serves to keep the hole open below the water table by maintaining an excess hydrostatic pressure inside the hole. In some soil deposits, particularly highly pervious ones, flush-coupled casing must be driven to just above the testing depth to keep the hole open and/or to prevent the loss of circulating fluid.

Representative split-spoon samples from soils at every 5 feet of drilled depth and from every different stratum are brought to our laboratory in air-tight jars for further evaluation and testing, if necessary. Samples not used in testing are stored for at least sixty (60) days prior to being discarded. After completion of a test boring, the hole is kept open until a steady state ground water level is recorded. The hole is then sealed if necessary, and backfilled.

C:appendix.spt

# GEOTECHNICAL EXPLORATION TECHNICAL GLOSSARY

### **TECHNICAL GLOSSARY**

<u>Clean Granular Fill</u> - A natural deposit of granular silica soil or a deposit of silica soil which has been modified to meet with the following criteria:

• Organic Content (ASTM D 2974) -

Less Than 3%

• Plasticity Index (ASTM D 4318) -

Zero

· Maximum Particle Size -

0.75 Inches

Maximum Percent Fines Content (ASTM D 1140) -

12%

U.S.C.S. Classifications -

SP, SW, SP-SM, GP, GW, GP-GM

Free From Debris and Trash

<u>Demolition Debris</u> - The remnant of previous structures, in whole or in fragments, which is the result of removal and or demolition of those structures.

<u>Inert Debris Fill</u> - That mass of material, which is created as the result of intermingling of Inert Demolition Debris with Structural Fill.

Organic Soil - A natural or man-modified soil deposit which contains in excess of 5 percent organic constituents (ASTM D 2974).

Reconditioned Inert Debris Fill - Inert Debris Fill, that has been modified to produce a thoroughly blended composite material, which contains Demolition Debris fragments that are no larger than 4 inches, in any dimension.

<u>Structural Fill</u> - Clean Granular Fill or Select Granular Fill which is designated to be placed below structural elements, and within their zones of stress influence (foundations, slabs-ongrade, pavements), placed and compacted in accordance with site preparation recommendations.

<u>Select Granular Fill</u> - Clean Granular Fill which, when placed and compacted in accordance with site preparation recommendations, will yield a soil mass with coefficient of permeability greater than or equal to that specified in the report.

<u>Trash</u> - Biodegradable manufactured or natural products or objects and/or refuse, which may typically be found in Class I municipal landfill cells.

# IMPORTANT INFORMATION ABOUT YOUR GEOTECHNICAL ENGINEERING REPORT

As the client of a consulting geotechnical engineer, you should know that site subsurface conditions cause more construction problems than any other factor. ASFE/The Association of Engineering Firms Practicing in the Geosciences offers the following suggestions and observations to help you manage your risks.

## A GEOTECHNICAL ENGINEERING REPORT IS BASED ON A UNIQUE SET OF PROJECT-SPECIFIC FACTORS

Your geotechnical engineering report is based on a subsurface exploration plan designed to consider a unique set of project-specific factors. These factors typically include: the general nature of the structure involved, its size, and configuration; the location of the structure on the site; other improvements, such as access roads, parking lots, and underground utilities; and the additional risk created by scope-of-service limitations imposed by the client. To help avoid costly problems, ask your geotechnical engineer to evaluate how factors that change subsequent to the date of the report may affect the report's recommendations.

Unless your geotechnical engineer indicates otherwise, do not use your geotechnical engineering report:

- when the nature of the proposed structure is changed, for example, if an office building will be erected instead of a parking garage, or a refrigerated warehouse will be built instead of an unrefrigerated one:
- when the size, elevation, or configuration of the proposed structure is altered;
- when the location or orientation of the proposed structure is modified;
- · when there is a change of ownership; or
- · for application to an adjacent site.

Geotechnical engineers cannot accept responsibility for problems that may occur if they are not consulted after factors considered in their report's development have changed.

### SUBSURFACE CONDITIONS CAN CHANGE

A geotechnical engineering report is based on conditions that existed at the time of subsurface exploration. Do not base construction decisions on a geotechnical engineering report whose adequacy may have been affected by time. Speak with your geotechnical consultant to learn if additional tests are advisable before construction starts. Note, too, that additional tests may be required when subsurface conditions are affected by construction operations at or adjacent to the site, or by natural events such as floods, earthquakes, or ground water fluctuations. Keep your geotechnical consultant apprised of any such events.

# MOST GEOTECHNICAL FINDINGS ARE PROFESSIONAL JUDGMENTS

Site exploration identifies actual subsurface conditions only at those points where samples are taken. The data were extrapolated by your geotechnical engineer who then applied judgment to render an opinion about overall subsurface conditions. The actual interface between materials may be far more gradual or abrupt than your report indicates. Actual conditions in areas not sampled may differ from those predicted in your report. While nothing can be done to prevent such situations, you and your geotechnical engineer can work together to help minimize their impact. Retaining your geotechnical engineer to observe construction can be particularly beneficial in this respect.

# A REPORT'S RECOMMENDATIONS CAN ONLY BE PRELIMINARY

The construction recommendations included in your geotechnical engineer's report are preliminary, because they must be based on the assumption that conditions revealed through selective exploratory sampling are indicative of actual conditions throughout a site. Because actual subsurface conditions can be discerned only during earthwork, you should retain your geotechnical engineer to observe actual conditions and to finalize recommendations. Only the geotechnical engineer who prepared the report is fully familiar with. the background information needed to determine whether or not the report's recommendations are valid and whether or not the contractor is abiding by applicable recommendations. The geotechnical engineer who developed your report cannot assume responsibility or liability for the adequacy of the report's recommendations if another party is retained to observe construction.

# GEOTECHNICAL SERVICES ARE PERFORMED FOR SPECIFIC PURPOSES AND PERSONS

Consulting geotechnical engineers prepare reports to meet the specific needs of specific individuals. A report prepared for a civil engineer may not be adequate for a construction contractor or even another civil engineer. Unless indicated otherwise, your geotechnical engineer prepared your report expressly for you and expressly for purposes you indicated. No one other than you should apply this report for its intended purpose without first conferring with the geotechnical engineer. No party should apply this report for any purpose other than that originally contemplated without first conferring with the geotechnical engineer.

# GEOENVIRONMENTAL CONCERNS ARE NOT AT ISSUE

Your geotechnical engineering report is not likely to relate any findings, conclusions, or recommendations

about the potential for hazardous materials existing at the site. The equipment, techniques, and personnel used to perform a geoenvironmental exploration differ substantially from those applied in geotechnical engineering. Contamination can create major risks. If you have no information about the potential for your site being contaminated, you are advised to speak with your geotechnical consultant for information relating to geoenvironmental issues.

# A GEOTECHNICAL ENGINEERING REPORT IS SUBJECT TO MISINTERPRETATION

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical engineering report. To help avoid misinterpretations, retain your geotechnical engineer to work with other project design professionals who are affected by the geotechnical report. Have your geotechnical engineer explain report implications to design professionals affected by them, and then review those design professionals' plans and specifications to see how they have incorporated geotechnical factors. Although certain other design professionals may be familiar with geotechnical concerns, none knows as much about them as a competent geotechnical engineer.

# BORING LOGS SHOULD NOT BE SEPARATED FROM THE REPORT

Geotechnical engineers develop final boring logs based upon their interpretation of the field logs (assembled by site personnel) and laboratory evaluation of field samples. Geotechnical engineers customarily include only final boring logs in their reports. Final boring logs should not under any circumstances be redrawn for inclusion in architectural or other design drawings. because drafters may commit errors or omissions in the transfer process. Although photographic reproduction eliminates this problem, it does nothing to minimize the possibility of contractors misinterpreting the logs during bid preparation. When this occurs, delays, disputes, and unanticipated costs are the all-too-frequent result.

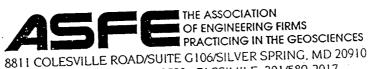
To minimize the likelihood of boring log misinterpretation, give contractors ready access to the complete geotechnical engineering report prepared or authorized for their use. (If access is provided only to the report prepared for you, you should advise contractors of the report's limitations, assuming that a contractor was not one of the specific persons for whom the report was prepared and that developing construction cost estimates was not one of the specific purposes for which it was prepared. In other words, while a contractor may gain important knowledge from a report prepared for another party, the contractor would be well-advised to discuss the report with your geotechnical engineer and to perform the additional or alternative work that the contractor believes may be needed to obtain the data specifically appropriate for construction cost estimating purposes.) Some clients believe that it is unwise or unnecessary to give contractors access to their geotechnical engineering reports because they hold the mistaken impression that simply disclaiming responsibility for the accuracy of subsurface information always insulates them from attendant liability. Providing the best available information to contractors helps prevent costly construction problems. It also helps reduce the adversarial attitudes that can aggravate problems to disproportionate scale.

# READ RESPONSIBILITY CLAUSES CLOSELY

Because geotechnical engineering is based extensively on judgment and opinion, it is far less exact than other design disciplines. This situation has resulted in wholly unwarranted claims being lodged against geotechnical engineers. To help prevent this problem, geotechnical engineers have developed a number of clauses for use in their contracts, reports, and other documents. Responsibility clauses are not exculpatory clauses designed to transfer geotechnical engineers' liabilities to other parties. Instead, they are definitive clauses that identify where geotechnical engineers' responsibilities begin and end. Their use helps all parties involved recognize their individual responsibilities and take appropriate action. Some of these definitive clauses are likely to appear in your geotechnical engineering report. Read them closely. Your geotechnical engineer will be pleased to give full and frank answers to any questions.

# RELY ON THE GEOTECHNICAL ENGINEER FOR ADDITIONAL ASSISTANCE

Most ASFE-member consulting geotechnical engineering firms are familiar with a variety of techniques and approaches that can be used to help reduce risks for all parties to a construction project, from design through construction. Speak with your geotechnical engineer not only about geotechnical issues, but others as well, to learn about approaches that may be of genuine benefit You may also wish to obtain certain ASFE publications. Contact a member of ASFE of ASFE for a complimentary directory of ASFE publications.



TELEPHONE: 301/565-2733 FACSIMILE: 301/589-2017

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April 18, 1997 File Number 97-9036A

Mr. Carl Locke, Jr. SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results, Laidlaw Drum Storage Building, Bartow Air

Base, Bartow, Florida

### REPORT NUMBER 1

#### Gentlemen:

As requested by you, on March 12, 1997 we performed field in-place density tests (ASTM D 2937) on the foundation subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were correlated to the maximum density of the foundation subgrade soils as determined by a Modified Proctor tests (ASTM D1557) on a representative soil sample. Figure No. 1 presents a graphic representation of the moisture-density relationships.

Based on these test results, the foundation subgrade soils meet the specified degree of compaction of 98 percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the foundation subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

alan he

PRM/CAB:krh Enclosures

Project Engineer

Florida Registration No. 41986

PROJECT:

LAIDLAW DRUM STORAGE BUILDING

FILE NO.:

97-9036A DATE:

1

4/18/97

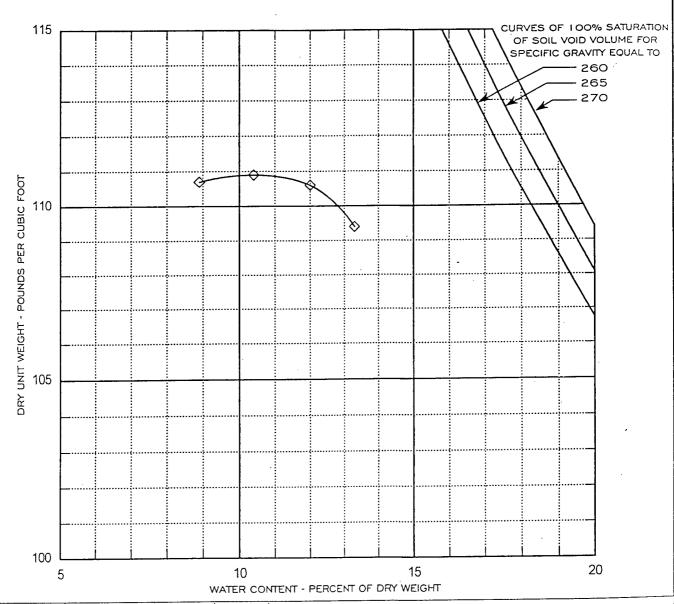
BARTOW AIRBASE, BARTOW, FL C. T: SEMCO CONSTRUCTION

ONSTRUCTION REPORT NO.

PAGE NO.:

1 of 1

Test No.		Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	21' N of SW corner of		3/12	1	106.1	5.6	BOF -1.0	95.7*
2	60' N & 12' W of SW (	Corner of Building	3/12	1	102.4	7.2	BOF -1.0	92.3*
3	18' S of NW Corner o	f Building	3/12	1	104.9	7.8	BOF -1.0	94.6*
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		DES NOT MEET MINIMUM COMPACT 2937  ASTM D 2922						,
MDR		MAXIMUM DENSITY		Орт	IMUM MOISTURE	BOF = BO	TOM OF FOC	TING
1	ASTM D 1557	110.9 PC	F @		10.7	1		



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
-	2/28/97	ASTM DI557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
					·

ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL, ENVIRONMENTAL AND
MATERIALS CONSULTANTS

SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

PRIMARY KH CHECKEN PRM CATE 4/16/97



Revised July 28, 1997 April 25, 1997 File Number 97-9036A

Mr. Carl Locke, Jr. SEMCO Construction P.O. Box 706 Bartow. FL 33831-0706

Subject:

Field In-Place Density Test Results, Laidlaw Drum Storage Building, Bartow Air

Base, Bartow, Florida

### **REPORT NUMBER 2**

#### Gentlemen:

As requested by you, on April 8, 1997 we performed field in-place density tests (ASTM D 2937) on the excavation backfill soils at the subject project. The excavation was to remove the muck soils encountered in our field exploration program, as recommended in our geotechnical report for the project, dated March 15, 1997. We were not present to observe the demucking operation. However, we did observe the excavation bottom prior to backfilling, and it appeared that muck soils had been removed. Page 1 presents the test locations and results. The field density tests were correlated to the maximum density of the excavation backfill soils as determined by a Modified Proctor test (ASTM D1557) on a representative sample. Figure No. 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the excavation backfill soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per the revised project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the excavation backfill soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

P. Rodney Mank, P.E.

Florida Registration No. 41986

Project Engineer /

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

**Technical Services Manager** 

PRM/CAB:krh Enclosures B5:\97-9036a.02

cc: Virogroup, Inc. - John W. Bale, P.E.

PROJECT:

MDR

1

**TEST METHOD** 

**ASTM D 1557** 

MAXIMUM DENSITY

110.9

LAIDLAW DRUM STORAGE BUILDING

BARTOW AIRBASE, BARTOW, FL

FILE NO.:

97-9036A DATE: REVISED:

4/25/97 7/28/97

**SEMCO CONSTRUCTION** 

REPORT NO.

PAGE NO.:

1 of 1

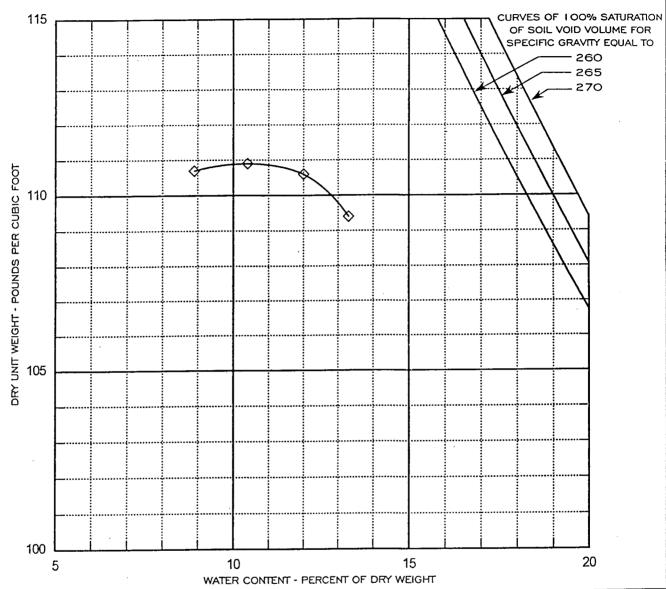
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	63' E & 51' N of SW Corner of Building	4/08	1	109.7	5.5	GR -5.0	98.9
2	SAME LOCATION	4/08	1	107.9	8.0	GR -4.0	97.3
3	SAME LOCATION	4/08	1	109.4	8.2	GR -3.0	98.6
4	SAME LOCATION	4/08	1 _	108.8	9.0	GR -2.0	98.1
5	SAME LOCATION	4/08	1	107.5	5.0	GR -1.0	96.9
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* IN-F	PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION  ST METHOD: ASTM D 2937 ASTM D 2922						

PCF@

OPTIMUM MOISTURE

10.7%

GR = GRADE



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
1	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
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ARDAMAN & ASSOCIATES, IN GEOTECHNICAL, ENVIRONMENTAL AND MATERIALS CONSULTANTS	10
MATERIALS CONSULTANTS	_

SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

DRAVAN BY	кн	CHECKED BY	PRM	DATE	4/16/97
FILE NO.	APPROVE	D67	$\overline{}$		FIGURE NO 1
97-90364	1 /		//		<u>_</u> _



Revised July 28, 1997 April 18, 1997 File Number 97-9036A

Mr. Carl Locke, Jr. SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results, Laidlaw Drum Storage Building, Bartow Air

Base, Bartow, Florida

### REPORT NUMBER 3

#### Gentlemen:

As requested by you, on April 9 and 10, 1997 we performed field in-place density tests (ASTM D 2937) on the foundation subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were correlated to the maximum density of the foundation subgrade soils as determined by a Modified Proctor test (ASTM D1557) on a representative sample. Figure No. 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the foundation subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per the revised project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the foundation subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Þ. Rodnev Mank. Þ.E

Florida Registration No. 41986

Project Engineer

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:krh Enclosures B5:\97-9036a\ipd.03

cc: Virogroup, Inc. - John W. Bale, P.E.

PROJECT:

LAIDLAW DRUM STORAGE BUILDING

BARTOW AIRBASE, BARTOW, FL

FILE NO.:

97-9036A DATE:

DATE: REVISED: 4/18/97 7/28/97

SEMCO CONSTRUCTION

REPORT NO.

3

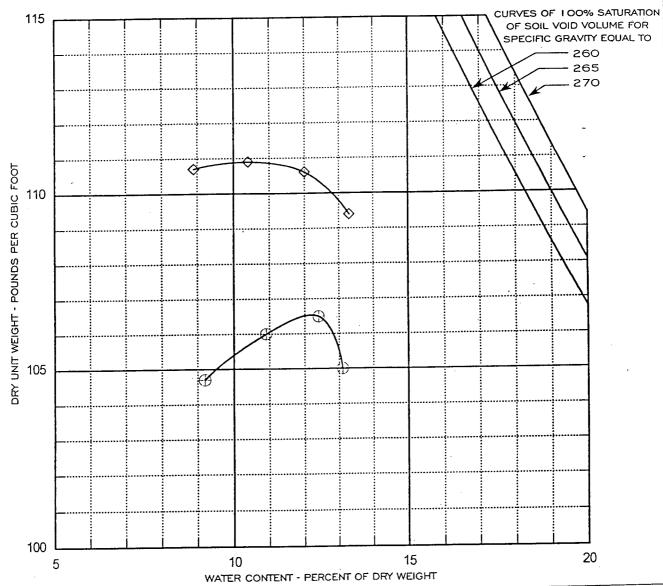
PAGE NO.:

1 of 1

	SEIVICO CONSTRUCTION			REFORT NO		.,	
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
	69' E of NW Corner of Building	4/09	1	101.1	7.0	BOF -4.0	91.2*
2	21' E of NW Corner of Building	4/09	1	103.6	4.0	BOF -4.0	93.4*
3	27' S of NW Corner of Building	4/09	1	103.7	6.0	BOF -4.0	93.5*
4	Retest of Test #1	4/09	1	105.4	6.5	BOF -4.0	95.1
5	Retest of Tets #2	4/09	1	106.8	2.5	BOF -4.0	96.3
6	Retest of Test #3	4/09	1	108.6	5.0	BOF -4.0	97.9
7	20' N of Column Line A3	4/09	1	107.5	8.9	BOF -4.0	96.9
8	10' E of Column Line A4	4/09	1	105.8	9.0	BOF -4.0	95.4
9	Column Line G4	4/10	2	105.5	4.4	BOF -3.0	99.1
10	Column Line G1	4/10	2	103.7	2.8	BOF -3.0	97.3
11	3' E of Column Line B1	4/10	2	109.2	5.8	BOF -3.0	100+
12	10' W of Column Line B3	4/10	2	108.9	6.0	BOF -3.0	100+
13	10' E of Column Line A3	4/10	2	104.8	3.0	BOF -3.0	98.4
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SST METHOD: ASTM D 2937 \_ ✓ ASTM D 2922 \_ \_ ASTM D 2167 \_ ASTM D 1556 FIE' BOF = BOTTOM OF FOOTING OPTIMUM MOISTURE MD, TEST METHOD MAXIMUM DENSITY PCF@ 10.7% 1 **ASTM D 1557** 110.9 12.2% PCF@ **ASTM D 1557** 106.5 2

\* In-Place Density Test does not meet minimum compaction requirement of 95 Percent



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
ı	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
2	4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
					-

CURVE IDENTIFICATION

MDR I DATA CURVE

 $\oplus$ MDR 2 DATA CURVE



ARDAMAN & ASSOCIATES, INC. GEOTECHNICAL, ENVIRONMENTAL AND MATERIALS CONSULTANTS

SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

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Mr. Carl Locke, Jr. SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results, Laidlaw Drum Storage Building, Bartow Air

Base, Bartow, Florida

### **REPORT NUMBER 4**

#### Gentlemen:

As requested by you, from April 11 through April 21, 1997 we performed field in-place density tests (ASTM D 2937) on the foundation subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were correlated to the maximum density of the foundation subgrade soils as determined by a Modified Proctor test (ASTM D1557) on a representative sample. Figure No. 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the foundation subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the foundation subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

alan L

PRM/CAB:krh Enclosures B5:\97-9036a\ipd.4 P. Rodney Mank, P.E.

Project Engineer

Florida Registration No. 41986

PROJECT:

LAIDLAW DRUM STORAGE BUILDING

FILE NO.:

97-9036A DATE:

4/25/97

BARTOW AIRBASE, BARTOW, FL

REPORT NO.

PAGE NO.:

1 of 1

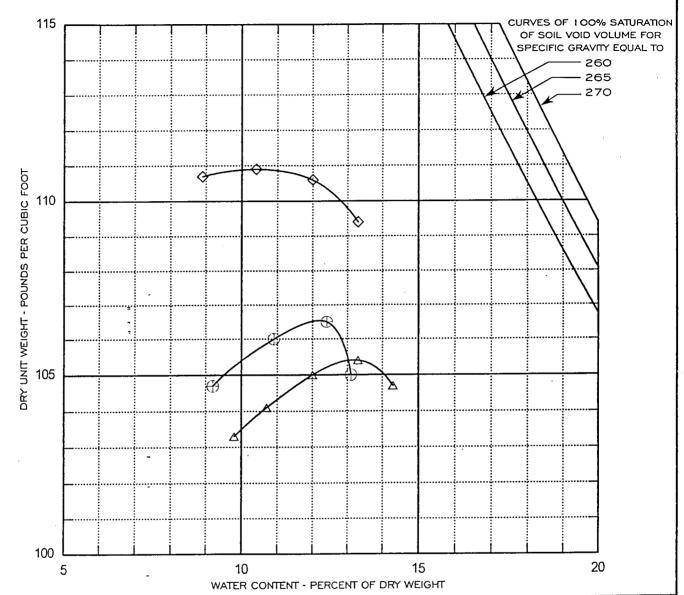
SEMCO CONSTRUCTION	SEM	1CO	CONS	TRUC	TION
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Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	54' E of NW Corner of Building	4/11	2	104.3	3.3	BOF -2.0	97.9
2	4' E of NW Corner of Building	4/11	2	103.0	3.7	BOF -2.0	96.5
3	12' E & 33' S of NW Corner Building	4/11	2	104.4	6.8	BOF -2.0	98.0
4	39' N of SW Corner of Building	4/11	2	102.0	6.6	BOF -2.0	95.8
5	15' N of SW corner of Building	4/11	2,	101.4	3.1	BOF -3.0	95.2
6	Same Location	4/11	2	101.2	3.3	BOF -2.0	95.1
7	50' W of NE Corner of Building	4/16	3	103.8	11.4	BOF -3.5	98.5
8	3' S of NE Corner of Building	4/16	3	100.9	7.5	BOF -3.5	95.7
9	33' S & 10' W of NE Corner of Building	4/16	3	104.2	13.4	BOF -3.5	98.9
10	26' S of NW Corner of Building	4/16	2	104.1	5.3	BOF -1.0	97.7
11	24' E of NW Corner of Building	4/16	2	101.8	5.5	BOF -1.0	95.6
12	74' E of NW Corner of Building	4/16	2	104.2	4.8	BOF -1.0°	97.8
13_	10' E & 33' S of NW Corner of Building	4/16	2	105.3	6.4	BOF -1.0	98.9
14	20' N of SW Corner of Building	4/16	2	105.6	3.5	BOF - 1.0	99.1
15	`1' W of SE Corner of Building	4/17	1	107.8	13.3	BOF -3.5	- 97.2
16	130' N of SE Corner of Building		3	113.3	14.4	BOF -3.5	100+
17	32' S & 21' W of NE Corner of Building	4/17	2	102.3	6.4	BOF -2.0	96.1
18	10' S of NE Corner of Building	4/17	2	102.1	5.0	BOF -2.0	95.7
19	39' W of NE Corner of Building	4/17	2	108.2	7.9	BOF -2.0	100+
20	45' W of NECorner of Building	4/18	2	103.6	7.5	BOF -2.0	97.2
21	10' S of NE Corner of Building	4/18	2	104.2	9.6	BOF -2.0	97.9
22	36' S & 27' W of NE Corner of Building	4/18	2	102.6	5.5	BOF -2.0	96.3
23	24' N of SE Corner of Building	4/18	2	105.9	5.7	BOF -2.0	99.5
24	27' W of SE Corner of Building	4/18	2	101.4	8.7	BOF -2.0	95.2
25	51' E of SW Corner of Building	4/18	2	103.6	5.7	BOF -2.0	97.3
	62' W of NE Corner of Building	4/21	2	102.5	5.5	BOF -1.0	- 96.2
27	12' W of NECorner of Building	4/21	2	109.2	4.8	BOF -1.0	100+
28	33' S of NE Corner of Building	4/21	2	105.9	8.0	BOF -1.0	99.5
	50' N of SE Corner of Building	4/21	2	101.3	4.4	BOF -1.0	95.1
30	SE Corner of Building	4/21	2	102.8	6.6	BOF -1.0	96.5
31	50' W of SE Corner of Building	4/21	2	102.5	5.0	BOF -1.0	96.2

<sup>\*</sup> In-Place Density Test does not meet minimum compaction requirement of 95 percent

FIL :ST METHOD: ASTM D 2937 \_ ASTM D 2922 \_\_\_ ASTM D 2167 \_\_\_ ASTM D 1556 \_\_\_\_

MDR	TEST METHOD	MAXIMUM DENSITY		OPTIMUM MOISTURE	BOF = BOTTOM OF FOOTING
1	ASTM D 1557	110.9	PCF @	10.7%	
2	ASTM D 1557	106.5	PCF@	12.2%	
3	ASTM D 1557	105.4	PCF @	13.3%	



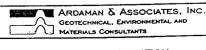
MDR NO.	DATE TESTED	TEST METHOD :	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
2	4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
3		ASTM D1557	105.4	13.3	WHITE TO LIGHT GRAY SAND WITH SILT & SMALL ROOTS
	4/10/97	A3114 01337	100.4	10.0	White to beam end, end, end, end, end, end, end, end,

#### CURVE IDENTIFICATION

MDR I DATA CURVE

MDR 2 DATA CURVE

MDR 3 DATA CURVE



SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

FILE NO. APPROJECT BY CO. 07-0036A

4/23/97 FIGURE NO. 1

ORF4WIN/B:/97-9036A/02.GRF



Revised: August 21, 1997 May 23, 1997

File Number 97-51-9036A

Mr. Carl Locke, Jr. SEMCO Construction P.O. Box 706 Bartow, FL 33830

Subject:

Field In-Place Density Test Results, Laidlaw Drum Storage Building, Bartow Air Base,

Bartow, Polk County, Florida

### REPORT NUMBER 5

#### Gentlemen:

As requested by you, on April 24 through May 1, 1997, we performed field in-place density tests (ASTM D 2937) on the natural ground and foundation subgrade soils at the subject project. Pages 1 and 2 present the test locations and results. The field density tests were compared to the maximum density of the natural ground and foundation subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on representative soil samples. Figure No. 1 presents a graphic representation of the moisture-density relationships.

Based on these test results, the natural ground and foundation subgrade soils meet the specified degree of compaction (95 percent Modified Proctor) at the tested location as per project specifications, except where noted.

The test locations were established by tape measurement from building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the natural ground and foundation subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

. Rodney Wank, P.E.

Project Engineer

Florida Registration No. 41986

PRM/CAB:tc Enclosures B5/QC REPORTS/97-9036a.5

CC: Virogroup, Inc. - Mr. John W. Bale, P.E.



LAIDLAW DRUM STORAGE BUILDING

FILE NO.:

97-9036A **DATE**:

5/23/97 8/21/97

BARTOW AIRBASE, BARTOW, FL

REVISED: PAGE NO.:

1 of 2

CLIEN	T: SEMCO CONSTRUCTION		REPO	ORT NO.	5	PAGE NO.:	1 of 2
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	10' N & 15' E OF SW CORNER OF BUILDING	4/24	1	111.4	6.8	NG -1.0	100+
2	SAME LOCATION	4/24	1	100.2	6.4	NG -2.0	90.4*
3	15' N & 10' N OF SE CORNER OF BUILDING	4/24	1	105.9	4.8	NG -1.0	95.5
4	RETEST OF #2	4/24	1	104.9	6.4	NG -2.0	94.5*
5	RETEST OF #4	4/24	1	105.6	6.4	NG -2.0	95.7
6	SAME LOCATION	4/24	1	106.5	7.5	NG -2.0	96.1
7	10' S & 25' E OF NW CORNER OF BUILDING	4/24	1	107.4	8.2	NG -1.0	96.9
8	SAME LOCATION	4/24	1	106.6	5.3	NG -2.0	96.1
9	15' S & 20' W OF NE CORNER OF BUILDING	4/24	1	105.3	9.6	NG -1.0	95.0
10	SAME LOCATION	4/24	1	114.4	3.3	NG -2.0	100+
11	45' N & 24' W OF SE CORNER OF BUILDING	4/25	1	105.6	5.9	NG -1.0	95.2
12	SAME LOCATION	4/25	1	105.7	3.6	NG -2.0	95.4
13	46' N & 20' E OF SW CORNER OF BUILDING	4/25	1	109.3	6.7	NG -1.0	98.6
-	SAME LOCATION	4/25	1	105.3	6.4	NG -2.0	95.0
15	EAST TRUCK LOADING PAD, SOUTH COLUMN PAD	4/25	2	108.9	12.9	BOF -3.5	100+
16	SAME LOCATION	4/25	2	106.2	11.4	BOF -3.5	99.8
17	EAST EAST TRUCK LOADING PAD, NORTH COLUMN PAD	4/25	2	104.9	15.7	BOF -3.5	98.5
18	40' E & 12' N OF SE CORNER OF BUILDING, CANOPY COLUMN PAD	4/29	2	109.7	12.4	BOF -1.0	100+
19	SAME LOCATION	4/29	2	107.7	12.1	BOF -2.0	100+
20	40' E & 12' N OF SE CORNER OF BUILDING, CANOPY COLUMN PAD	4/29	2	108.2	14.9	BOF -3.0	100+
21	SAME LOCATION	4/29	2	106.3	6.2	BOF -1.0	99.8
22	40' E & 51' N OF SE CORNER OF BUILDING, CANOPY COLUMN PAD	4/29	2	103.8	6.8	BOF -2.0	97.5
23	SAME LOCATION	4/29	2	104.1	17.5	BOF -3.0	97.7
24	40' E & 31' N OF SE CORNER OF BUILDING, CANOPY COLUMN PAD	4/29	2	109.1	8.8	BOF -1.5	100+
25	SAME LOCATION	4/29	2	110.3	9.5	BOF -2.5	100+
26	SAME LOCATION	4/29	2	102.6	14.5	BOF -3.5	96.4
27	12' N & 2' E OF SE CORNER OF BLDG @ FORK LIFT RAMP FOOTINGS	4/30	2	106.7	13.9	BOF -3.0	100+
28	16' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	4/30	1	106.3	21.7	BOF -3.0	95.8
29	42' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	4/30	3	109.5	18.2	BOF -3.0	100+

IN-PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION REQUIREMENT OF 95 PERCENT ASTM D 1556 ASTM D 2167

FIF' TEST METHOD: ASTM D 2937 \_ ASTM D 2922 OPTIMUM MOISTURE MAXIMUM DENSITY **TEST METHOD** 10.7% PCF@ **ASTM D1557** 110.9 1 12.2% PCF@ 106.5 2 **ASTM D1557** 13.3% PCF@ **ASTM D1557** 105.4 3

NG = NATURAL GROUND BOF - BOTTOM OF FOOTING

### CIATES, INC. FIELD IN-PLACE DENSITY TEST REPORT

LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

FILE NO.:

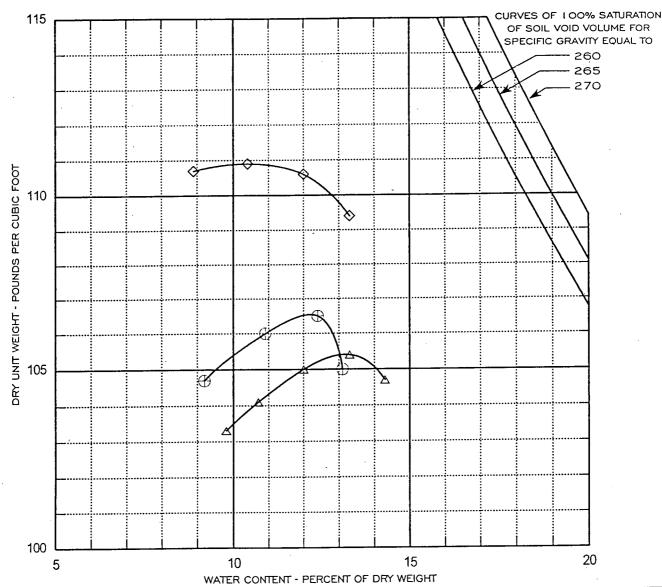
97-9036A DATE: **REVISED:**  5/23/97 7/23/97

SEMCO CONSTRUCTION

REPORT NO.

5 PAGE NO.: 2 of 2

CLIEN	IT: SEMCO CONSTRUCTION		REPUR	1 110.		FAGE NO	2 012
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%
30	12' N & 2' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	4/30	2	105.2	5.5	BOF -2.0	98.8
	16' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	4/30	2	108.2	8.1	BOF -2.0	100+
	42' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS		2	103.7	7.7	BOF -2.0	97.4
	12' N & 2' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	5/01	2	103.9	6.9	BOF -1.0	97.6
- 1	16' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	5/01	2	105.4	5.8	BOF -1.0	99.0
1	42' N & 12' E OF SE CORNER OF BLDG @ FORKLIFT RAMP FOOTINGS	<del></del>	2	107.2	6.8	BOF -1.0	100+
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MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
2	4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
3	4/16/97	ASTM D1557	105.4	13.3	WHITE TO LIGHT GRAY SAND WITH SILT & SMALL ROOTS

### **CURVE IDENTIFICATION**

MDR I DATA CURVE

MDR 2 DATA CURVE

MDR 3 DATA CURVE



SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

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ORF 4WIN/B:/97-9036A/02.GRF



Revised July 28, 1997 July 15, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 6**

#### Gentlemen:

As requested by you, from June 19 through June 24, 1997 we performed field in-place density tests (ASTM D 2937) on the floor slab subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the floor slab subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Figure No. 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the floor slab subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the floor slab subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Project Engineer

Florida Registration No. 41986

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:krh Enclosures B10\97-9036A.06

cc: Viro Group, Inc., Mr. John Bale, P.E.

PROJECT: LAIDLAW DRUM STORAGE BUILDING

TEST METHOD

**ASTM D 1557** 

**ASTM D1557** 

MDR

2

MAXIMUM DENSITY

106.5

105.4

@ PCF

@ PCF

BARTOW AIR BASE, BARTOW, FLORIDA

FILE:

97-9036A

DATE:

7/28/97

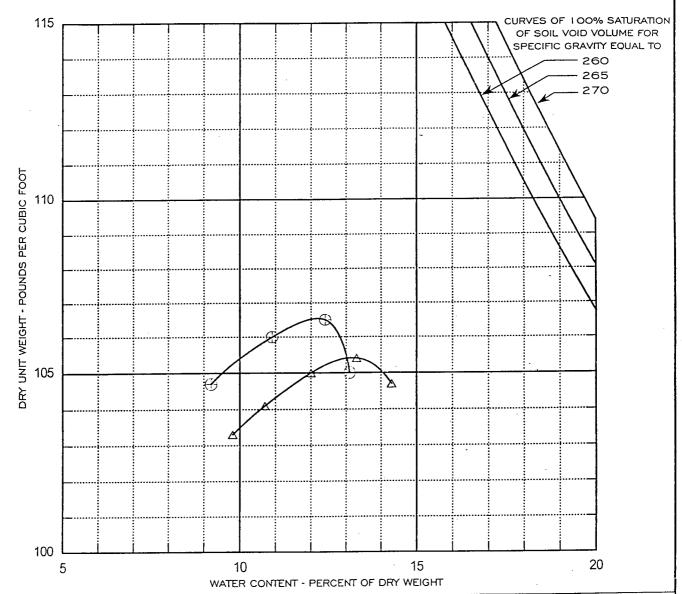
CLIE	NT: SEMCO CONSTRUCTION			REPORT:	6	PAGE NO.:	1 of 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	28' W & 15' N of SE corner of building	6/19	3	107.2	8.3	FS -3.5	100+
2	28' W & 60' N of SE Corner of Building	6/19	3	104.1	7.3	FS -3.5	98.8
3	12' S & 12' W OF NE CORNER OF BUILDING	6/19	3	105.4	6.6	FS -3.5	100
4	18' W & 18' N of SE corner of Building	6/19	3	102.6	9.3	FS -2.5	97.3
5	18' W & 51' N OF SE CORNER OF BUILDING	6/19	3	103.8	6.7	FS -2.5	98.5
6	26' W & 21' S OF NE CORNER OF BUILDING	6/19	3	105.9	9.6	FS -2.5	100+
7	1' N & 25' W OF SE CORNER OF BUILDING	6/23	2	99.7	4.2	FS -0.5	93.6*
8	32' S & 35' W o F NE CORNER OF BUILDING	6/23	2	102.9	8.8	FS -0.5	96.6
9	25' S & 42' W OF NE CORNER OF BUILDING	6/23	2	104.3	7.4	FS -0.5	98.0
10·	1' N & 25' W of SE corner of Building	6/23	2	98.9	5.5	FS -1.5	92.9*
11	32' S & 35' W o F NE Corner of Building	6/23	2	102.4	6.3	FS -1.5	96.2
12	25' S & 42' W OF NE CORNER OF BUILDING	6/23	2	108.8	4.4	FS -1.5	100+
13	RETEST OF TEST #7	6/24	2	103.8	7.1	FS - 0.5	97.5
- 1	RETEST OF TEST #10	6/24	2	101.6	7.5	FS - 1.5	95.4
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N-	PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION REQUIRE			PERCENT	TAA D 4550	· · · · · · · · · · · · · · · · · · ·	
T <sup>D</sup>	TEST METHOD: ASTM D 2937   ASTM D 2922	MO HIND	4107	AS	TM D 1556		

FS = FLOOR SLAB SUBGRADE

OPTIMUM MOISTURE

12.2%

13.3%



MDR NO,	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
2	4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
_3	4/16/97	ASTM D1557	105.4	13.3	WHITE TO LIGHT GRAY SAND WITH SILT & SMALL ROOTS

#### **CURVE IDENTIFICATION**

MDR 2 DATA CURVE

MDR 3 DATA CURVE



SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

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GBF AWIN/R-/97-903



July 17, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### REPORT NUMBER 7

#### Gentlemen:

As requested by you, from June 26 through July 9, 1997 Ardaman and Associates, Inc. performed field in-place density tests (ASTM D 2937) on the subgrade fill and floor slab subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the subgrade fill and floor slab subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Figure No. 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the subgrade fill and floor slab subgrade soils meet the specified degree of compaction of 95 percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the subgrade fill and floor slab subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

P. Rodney Mank

Project Engineer

Florida Registration No. 41986

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

alan K

PRM/CAB:krh Enclosures B10\97-9036A.7

cc: Viro Group, Inc., Mr. John Bale, P.E.

1525 Centarcial Drive (33830). Post Office Box 812. Bartow, Florida 33831 - Phone (941) 533-0858 - FAX (941) 533-7325 - Offices of Entrance For Laudendale For Payers, Miami, Orlando, Port Charlotte, Port St. Lucie, Sarasota, Tallahaosee, Tampa, W. Palm Beach

DJECT: LAIDLAW DRUM STORAGE BUILDING

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97-9036A

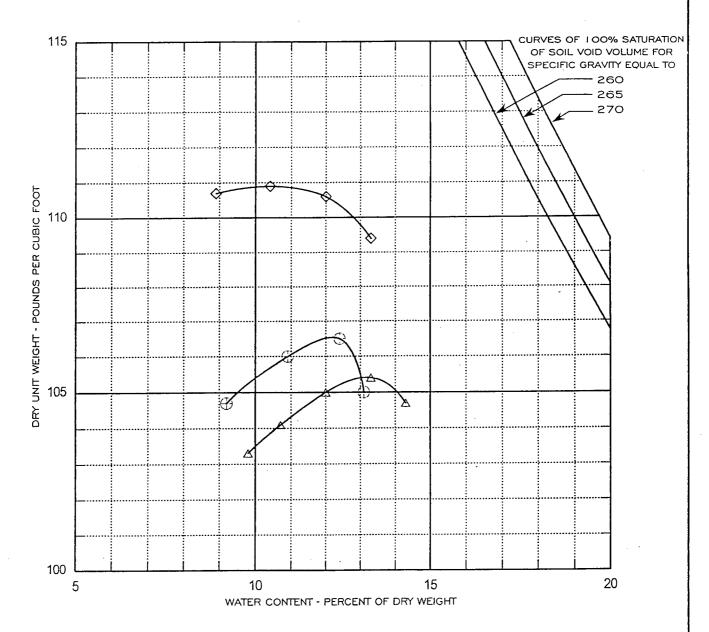
DATE: 7/17/97

BARTOW AIR BASE, BARTOW, FLORIDA	

CLIE	NT: SEMCO CONSTRUCTION			REPORT:	7	PAGE NO.:	1 of 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	25' N & 65' E OF SW CORNER OF BUILDING	6/26	2	106.4	11.9	FS -3.5	99.9
2	50' N & 25' E OF SW CORNER OF BUILDING	6/26	2	107.1	7.8	FS -3.5	100+
3	10' S & 45' E OF NW CORNER OF BUILDING	6/26	2	105.9	5.9	FS -3.5	100+
4	10' S & 1' E OF NW CORNER OF BUILDING	6/30	2	107.8	5.7	FS -3.5	100+
5	30' S & 60' E OF NW CORNER OF BUILDING	6/30	2	105.3	6.2	FS -2.5	98.9
6	15' N & 55' E OF SW CORNER OF BUILDING	6/30	2	103.3	6.2	FS -2.5	96.9
7	FOUNDATION PAD, COLUMN LINE #1, PIER B	7/01	1	110.3	7.3	BOF -3.5	99.5
8	SAME LOCATION	7/01	2	105.8	6.4	BOF -2.5	99.3
9	FOUNDATION PAD, COLUMN LINE #1, PIER C	7/01	2	103.3	6.8	BOF -2.5	96.9
10	SAME LOCATION	7/01	1	111.4	10.4	BOF -3.5	100+
11	FOUNDATION PAD, COLUMN LINE #1, PIER D	7/01	1	112.6	9.7	BOF -2.5	100+
12	SAME LOCATION	7/01	1	110.9	11.4	BOF -3.5	100+
13	FOUNDATION PAD, COLUMN LINE #1, PIER B	7/01	2	104.1	3.9	BOF -0.5	97.7
	FOUNDATION PAD, COLUMN LINE #1, PIER C	7/01	1	113.8	6.9	BOF -0.5	100+
٠. ا	FOUNDATION PAD, COLUMN LINE #1, PIER B	7/01	2	104.9	4.4	BOF -1.5	98.5
16	FOUNDATION PAD, COLUMN LINE #1, PIER C	7/01	1	107.5	7.1	BOF -1.5	96.9
17	FOUNDATION PAD, COLUMN LINE #1, PIER D	7/01	2	104.8 .	3.9	BOF -0.5	98.4
18	SAME LOCATION	7/01	2	102.4	7.2	BOF -1.5	96.2
19	1' N & 25' E OF SW CORNER OF BUILDING (WEST WING)	7/02	2	106.5	7.3	FS -1.5	100
20	1' S & 65' E OF NW CORNER OF BUILDING	7/02	2	104.7	4.2	FS -1.5	98.3
21	30' N & 30' E OF SW CORNER OF BUILDING	7/02	2	106.4	6.8	FS -2.5	99.9
22	15' E & 18' S OF NW CORNER OF BUILDING	7/09	3	104.7	6.0	FS -0.5	99.4
23	SAME LOCATION	7/09	3	104.5	7.2	FS -1.5	99.2
24	75' E & 15' N OF SW CORNER OF BUILDING	7/09	3	103.7	5.8	FS -0.5	98.4
25	75' E & 40' N OF SW CORNER OF BUILDING	7/09	3	104.1	7.5	FS -0.5	98.8
26	75' E & 75' N OF SW CORNER OF BUILDING	7/09	3	104.2	6.0	FS -0.5	98.9
27	9' W & 9' N OF SE CORNER OF BUILDING	7/09	3	104.0	4.5	FS -0.5	98.7
28							
29							_,
30							

ASTM D 1556 ASTM D 2167 D TEST METHOD: ASTM D 2937 ✓ ASTM D 2922 TEST METHOD MAXIMUM DENSITY OPTIMUM MOISTURE FS = FLOOR SLAB SUBGRADE **BOF = BOTTOM OF FOUNDATION ASTM D 1557** 110.9 @ PCF 10.7% 1 @ PCF 12.2% 2 **ASTM D 1557** 106.5 @ PCF 13.3% **ASTM D1557** 105.4

\* In-Place Density Test does not meet minimum compaction requirement of 95 Percent



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
ı	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
2	4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
3	4/16/97	ASTM D1557	105.4	13.3	WHITE TO LIGHT GRAY SAND WITH SILT & SMALL ROOTS

### CURVE IDENTIFICATION

MDR I DATA CURVE  $\Diamond$ 

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MDR	3	DATA CURVE
MDR	z	DATA CURVE



LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

4/23/97



Revised August 1, 1997 July 31, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 9**

#### Gentlemen:

As requested by you, from July 10 and July 17, 1997 we performed field in-place density tests (ASTM D 2937) on the floor slab subgrade soils at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the floor slab subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Figure 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the floor slab subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per project specifications, except where noted

The test locations were established by tape measurement from the building corner locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the floor slab subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:krh Enclosures B12\97-9036A.09

cc: Viro Group, Inc., Mr. John Bale, P.E.

Rodney Manl

Florida Registration No. 41986

Project Engineer

**PJECT: LAIDLAW DRUM STORAGE BUILDING** 

BARTOW AIR BASE, BARTOW, FLORIDA

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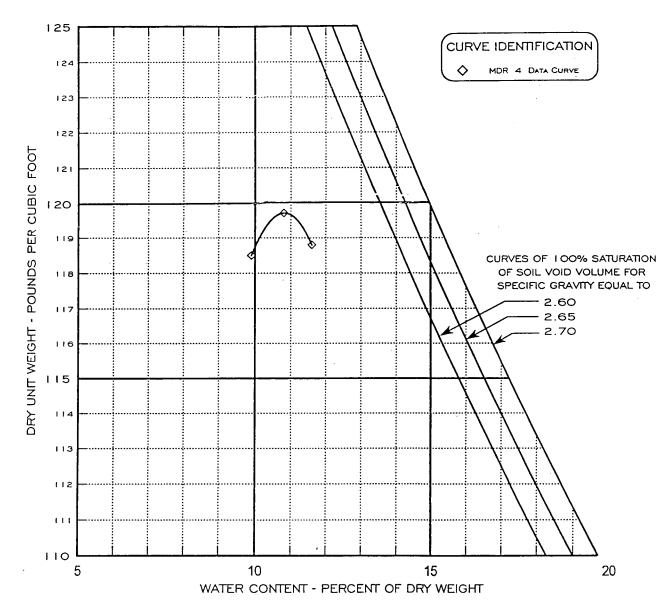
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DATE:

7/31/97 **REVISED:** 8/01/97

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Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	6'S OF NORTH END OF EAST RAMP, ON CENTERLINE	7/10	4	110.0	7.3	FS -1.0	92.0 <del>*</del>
2	SAME LOCATION	7/10	4	108.9	8.1	FS -3.0	91.0*
3 -	21'S OF NORTH END OF EAST RAMP, ON CENTERLINE	7/10	4	110.6	9.6	FS -0.5	92.4*
4	RETEST OF TEST #1	7/17	4	113.4	7.3	FS -1.0	94.7₩
5	RETEST OF TEST #2	7/17	4	108.9	8.1	FS -3.0	91.0 <del>*</del>
6	RETEST OF TEST #3	7/17	4	114.1	7.2	FS -0.5	95.3
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**ASTM D 1556** ✓ ASTM D 2922 ASTM D 2167 D TEST METHOD: ASTM D 2937 MAXIMUM DENSITY OPTIMUM MOISTURE FS = FLOOR SLAB SUBGRADE TEST METHOD MDR @ PCF 11.0% 119.7 **ASTM D 1557** 



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
4	7/10/97	ASTM D 1557	119.7	11.0	YELLOWISH SILTY SLIGHTLY CLAYEY SAND

Ardaman & Associates, Inc.

GEOTECHNICAL, EMMONMENTAL AND
MATERIALS CONSULTANTS

SEMCO CONSTRUCTION
LAIDLAW DRUM STORAGE BUILDING
BARTOW AIRBASE, BARTOW, FLORIDA

PRIMO DATE 7/30/97
FILE NO. APPENDIA PRIMO DATE 7/30/97
FILE NO. APPENDIA PROJECT NO. APPENDI

IN/B5:97 8036A.O.



September 8, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 10**

#### Gentlemen:

As requested by you, on August 6, 1997 we performed field in-place density tests (ASTM D 2937) on the subgrade soils for the fork lift ramp at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the ramp slab subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Figure 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the ramp slab subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the ramp slab corner as located locations by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the floor slab subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

/P. Rodney Mank, P.ビ

Florida Registration No. 41986

Project Engineer

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:krh Enclosures B14\97-9036A.10

cc: Viro Group, Inc., Mr. John Bale, P.E.

1505 Centerrold Drive (33830), Post Ottice Box 812 Barros. Florida 33831 - Phone (941) 533-0858 - FAX (941) 533-7325 Cifices in Pariov. Cocon. Fort Lauderdale, Fort Myers, Miann, Orlando, Peri Charlotte, Peri St. Lucie, Sarasota, Tallahassee, Tampa, W. Palm Beach

### ARDAMAN & ASSOCIATES, INC. FIELD IN-PLACE DENSITY TEST REPORT

**PJECT: LAIDLAW DRUM STORAGE BUILDING** 

BARTOW AIR BASE, BARTOW, FLORIDA

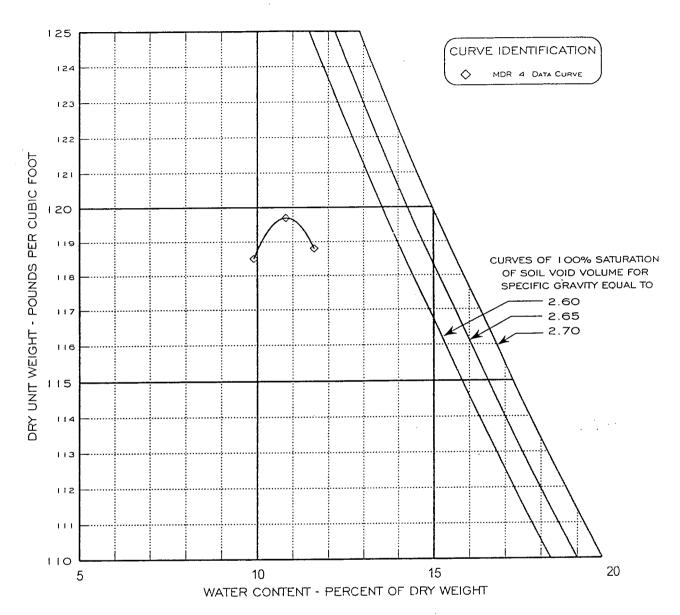
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97-9036A

**DATE:** 9/05/97

CLIE	NT: SEMCO CONSTRUCTION			REPORT:	10	PAGE NO.:	1 of 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	RETEST OF TEST #4, REPORT #9 6' S OF NORTH END OF EAST RAMP, ON CENTERLINE	8/06	4	119.7	9.4	FS - 1.0	100
2	3' N & 4.5' W OF SE CORNER OF RAMP, EAST END	8/06	4	115.7	11.8	FS - 0.6	96.7
3	RETEST OF TEST #5, REPORT #9 6' S OF NORTH END OF EAST RAMP, ON CENTERLINE	8/06	4	121.3	8.9	FS - 3.0	100+
						-	
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_							
7-	PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION	ON REQUIREMENT OF	95	PERCENT			
	D TEST METHOD: ASTM D 2937 ASTM D 292						
MDR	TEST METHOD MAXIMUM DENSITY OPTIMUM MC		OOR SLA	AB SUBGRA	DE		
4	ASTM D 1557 119.7 @ PCF 11.09	/6		· · · · · · · · · · · · · · · · · · ·			

### MOISTURE - DENSITY RELATIONSHIP



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
4	7/10/97	ASTM D   557	119.7	11.0	YELLOWISH SILTY SLIGHTLY CLAYEY SAND

Ardaman & Associates, Inc.

Geotechnical, Environmental and
Materials Consultants

SEMCO CONSTRUCTION
LAIDLAW DRUM STORAGE BUILDING
BARTOW AIRBASE, BARTOW, FLORIDA

FILE NO APPROVED BY PRM DATE
97-9036A

PATE 7/30/97

GRF 4WIN/B5:97-9036A,03



September 12, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### REPORT NUMBER 11

#### Gentlemen:

As requested by you, on August 19, 1997 we performed field in-place density tests (ASTM D 2937) on the subgrade soils for the west fork lift ramp at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the ramp slab subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Figure 1 presents a graphic representation of the moisture-density relationship.

Based on these test results, the ramp slab subgrade soils meet the specified degree of compaction of **95** percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the ramp slab corner as located locations by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the floor slab subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

P. Rodney Mank,

Project Engineer

Florida Registration No. 41986

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB krh Enclosures B14\97-9036A.11

cc: Viro Group, Inc., Mr. John Bale, P.E.

1525 Centennial Drive (33830), Post Office Box 812, Bartow, Florida 33831 Phone (941) 533-0858 FAX (941) 523-7325

### ARDAMAN & ASSOCIATES, INC. FIELD IN-PLACE DENSITY TEST REPORT

JECT: LAIDLAW DRUM STORAGE BUILDING

FIELD TEST METHOD: ASTM D 2937

TEST METHOD

**ASTM D 1557** 

**ASTM D 1557** 

MDR

MAXIMUM DENSITY

110.9

106.5

✓ ASTM D 2922

PCF@

PCF@

OPTIMUM MOISTURE

10.7%

12.2%

BARTOW AIR BASE, BARTOW, FLORIDA

FILE:

97-9036A

ASTM D 1556

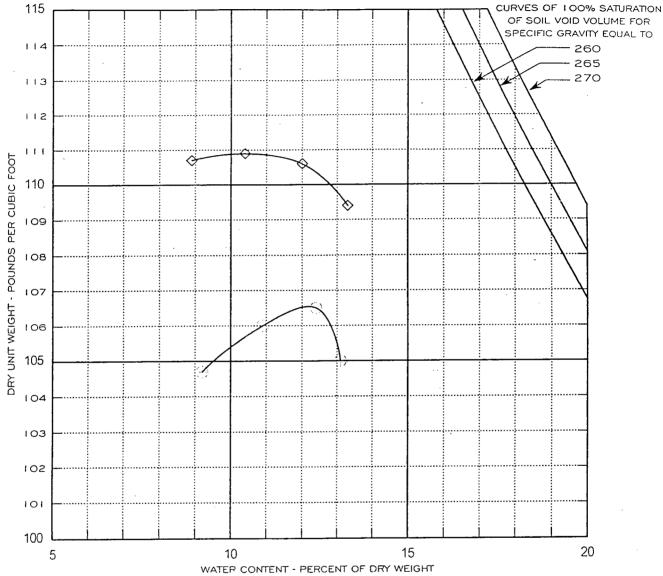
DATE: 9/05/97

CLIE	NT: SEMCO CONSTRUCTION	<del></del>		REPORT:	11	PAGE NO.:	1 of 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compactio (%)
1	WEST RAMP, 10' N & 4' E OF SW CORNER	8/18	2	107.9	10.6	FS -3.0	100+
2	WEST RAMP, 40' N & 4' E OF SW CORNER	8/18	• 2	106.0	7.4	FS -3.0	100
3	WEST RAMP FOOTER, 10' N OF SW CORNER	8/19	1	116.9	9.0	BOF -3.0	100+
4	WEST RAMP FOOTER, 4' E OF SW CORNER	8/19	2	105.8	16.3	BOF -2.0	99.3
5	WEST RAMP, 15' N & 4' E OF SW CORNER	8/19	2	112.4	5.0	FS -1.5	100+
6	WEST RAMP FOOTER, 12' NOF SW CORNER	8/19	1	114.9	4.0	BOF -0.5	100+
7	WEST RAMP, 12' N & 4' E OF SW CORNER	8/19	2	112.4	8.0	FS -0.5	100+
8	WEST RAMP FOOTER, 6' N OF SW CORNER	8/19	1	115.4	8.2	BOF -1.0	100+
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ASTM D 2167

FS = RAMP SLAB SUBGRADE BOF = BOTTOM OF FOOTER

### MOISTURE - DENSITY RELATIONSHIP



DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
4/07/97	ASTM D1557	106.5	12.2	WHITE SAND WITH SILT
	TESTED 2/28/97	TESTED METHOD	DATE TEST DRY DENSITY (PCF)  2/28/97 ASTM D1557 110.9	DATE TEST         DRY DENSITY (PCF)         WATER CONTENT (%)           2/28/97         ASTM D1557         110.9         10.7

### CURVE IDENTIFICATION

MDR I DATA CURVE

ARDAMAN & ASSOCIATES, INC.
GEOTECHNICAL ENVIRONMENTAL AND
MATERIALS CONSULTANTS

SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

REVISION KH CHECKED BY CATE 9/10/97

. 80000



October 2, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 12**

#### Gentlemen:

As requested by you, on September 22 and 23, 1997 we performed field in-place density tests (ASTM D 2937) on the ramp slab subgrade fill soils for the west fork lift ramp at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the ramp slab subgrade fill soils as determined by Modified Proctor tests (ASTM D 1557) on representative samples. Figure 1 presents a graphic representation of the moisture-density relationships.

Based on these test results, the ramp slab subgrade fill soils meet the specified degree of compaction of 95 percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the ramp slab corner as located locations by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the ramp slab subgrade fill soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

P. Rodney Mehk, Project Engineer

Florida Registration No. 41986

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:kms Enclosures B17\97-9036A 12

cc: Viro Group, Inc., Mr. John Bale, P.E.

### ARDAMAN & ASSOCIATES, INC. FIELD IN-PLACE DENSITY TEST REPORT

ROJECT: LAIDLAW DRUM STORAGE BUILDING

BARTOW AIR BASE, BARTOW, FLORIDA

FILE:

97-9036A

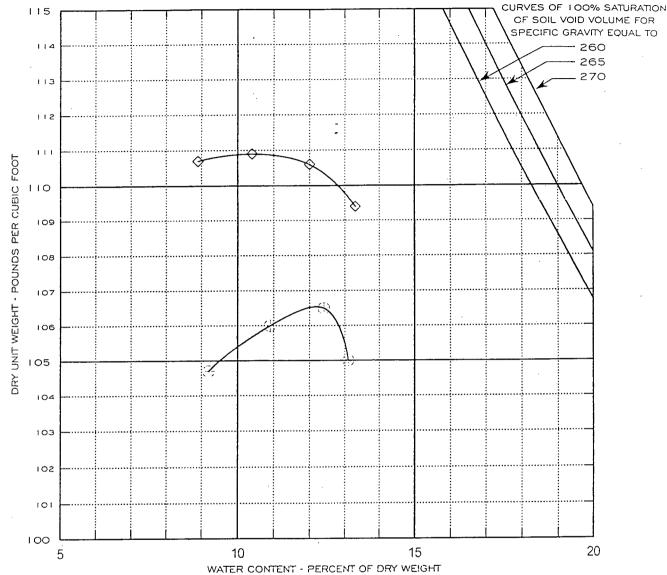
**DATE:** 10/2/97

CLIE	NT: SEMCO CONSTRUCTION			REPORT:	12	PAGE NO.:	1 of 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	10' N & 6' E OF SW CORNER OF WEST FORKLIFT RAMP	9/22	2	109.4	12.3	GR -1.5	100+
2	6' S & 6' E OF NW CORNER OF WEST FORKLIFT RAMP	9/22	2	105.0	4.4	GR -2.0	98.6
3	SAME LOCATION	9/22	2	111.1	11.2	GR -3.0	100+
4	RAMP WEST SIDE	9/23	1	108.6	5.0	FS -1.0	97.9
5	SAME LOCATION	9/23	1	109.2	7.4	FS -0.5	98.5
6	EAST SIDE DRIVE	9/23	1	104.9	12.4	FS -1.0	99.1
7	SAME LOCTION	9/23	1	111.3	6.0	FS -0.5	100+
8	FOAM ROOM -	9/23	1	110.0	6.0	FS -1.0	99.2
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ASTM D 1556 ASTM D 2167 LD TEST METHOD: ASTM D 2937 ASTM D 2922 OPTIMUM MOISTURE FS = RAMP SLAB SUBGRADE MDR TEST METHOD MAXIMUM DENSITY GR = GRADE PCF@ 10.7% 110.9 1 **ASTM D 1557** PCF@ 12.2% 2 106.5 **ASTM D 1557** 

IN-PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION REQUIREMENT OF 95 PERCENT

# MOISTURE - DENSITY RELATIONSHIP



1					
MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
1	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
2	4/07/97	ASTM D   557	106.5	12.2	WHITE SAND WITH SILT
					·

CURVE IDENTIFICATION

MDR I DATA CURVE

MDR 2 DATA CURVE



ARDAMAN & ASSOCIATES, INC GEOTECHNICAL, ENVIRONMENTAL AND
MATERIALS CONSULTANTS

SEMCO CONSTRUCTION LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FL

BRANNEY KMS CHECKEDEY

10/01/97

ORF 4WIN/B:/97-9036A/02.GRF

November 12, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Field In-Place Density Test Results

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 14**

#### Gentlemen:

As requested by you, on October 30, 1997 we performed field in-place density tests (ASTM D 2937) on the concrete slab subgrade soils for the southwest loading dock at the subject project. Page 1 presents the test locations and results. The field density tests were compared to the maximum density of the concrete roadway subgrade soils as determined by a Modified Proctor test (ASTM D 1557) on a representative sample. Graphic representation of the moisture-density relationship is presented in Figure 1.

Based on these test results, the concrete slab subgrade soils meet the specified degree of compaction of 95 percent Modified Proctor at the tested locations as per project specifications, except where noted.

The test locations were established by tape measurement from the locations as provided by others. The degree of accuracy of test locations is that implied by the method of layout. The in-place density test results are representative of the concrete roadway subgrade soils at each respective test location and vertical reach at the time the test was performed.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

P. Rodney Mark, P.E

Florida Registration No. 41986

Project Engineer

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

PRM/CAB:kms Enclosures B20\97-9036A.14

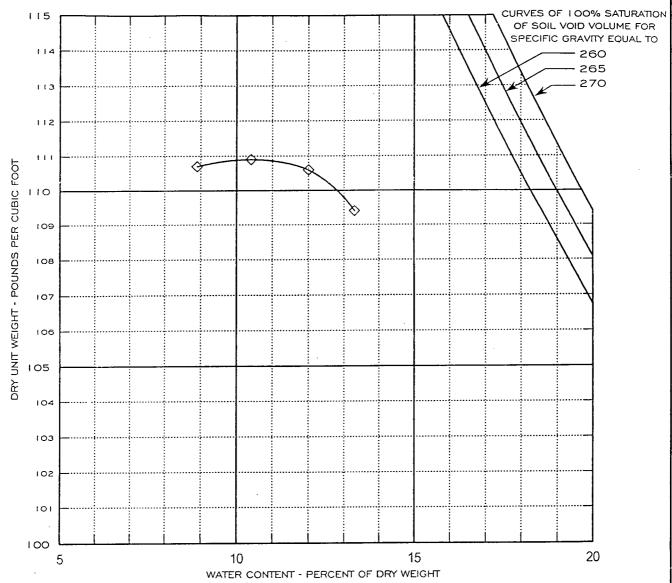
cc: Viro Group, Inc., Mr. John Bale, P.E.

itber i vitemad Dimerbitötin, Fost Otice Box 512, Barton, Florida 33831 - Phone (941) 533-0858 - FAX (941) 553-7325 Otice, i información cal Fost Laurordiale-Fost Myers, Miami, Orlando-Port Charlotte, Port St. Lucie, Sarasota, Taliahaesee, Tampa, W. Palin Beach

# ARDAMAN & ASSOCIATES, INC. FIELD IN-PLACE DENSITY TEST RESULTS

	OJECT: LAIDLAW DRUM STORAGE BUILDING BARTOW AIRBASE, BARTOW, FLORIDA		FILE I	NO. 97-90	36A	DATE	11/12/97
	CLIENT: SEMCO CONSTRUCTION	RE	PORT	NO. 14	PA	GE NO.	1 OF 1
Test No.	Location	Test Date	MDR NO.	Dry Density (pcf)	Moisture (%)	Depth Elevation (feet)	Percent Compaction (%)
1	10' E of SW Corner of SW Loading Dock	10/30	1	108.8	6.2	GR -0.6	98.1
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31 *	PLACE DENSITY TEST DOES NOT MEET MINIMUM COMPACTION R	REQUIREM	MENT OF	<b>95</b> PER	CENT	<del></del>	
		ASTM D			M D1556		
MDR	TEST METHOD MAXIMUM DENSITY OPTIMUM MOISTURE	GR = C	ONCRE	TE ROADW	AY SUBG	RADE	;
1	ASTM D1557 110.9 PCF @ 10.7%						

### MOISTURE - DENSITY RELATIONSHIP



MDR NO.	DATE TESTED	TEST METHOD	MAXIMUM DRY DENSITY (PCF)	OPTIMUM WATER CONTENT (%)	SOIL DESCRIPTION
1	2/28/97	ASTM D1557	110.9	10.7	DARK GRAYISH-BROWN SAND WITH SILT
					·

CURVE IDENTIFICATION

MDR I DATA CURVE



ORWANDY KMS CHECKEDS PRM CA

11/11/97

3RF4WIN/B:/97-9036A/OL

July 17, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Concrete Reinforcement Steel Inspection

Laidlaw Drum Storage Building, Bartow Air Base

Bartow, Florida

### **REPORT NUMBER 8**

### Gentlemen:

As requested by you, on May 8, 30 and June 20, 1997 Ardaman and Associates, Inc. visited the subject site to conduct a visual inspection of the concrete reinforcement steel for size, placement, and concrete cover. Please find enclosed copies of our Field Inspection Reports and associated findings.

Based our observations as recorded on the field inspection reports, it is the opinion of Ardaman and Associates, Inc. that the concrete reinforcing steel within the inspected elements has been installed in accordance with the project plans and specifications.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours.

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

**Technical Services Manager** 

P. Rodney Mant, P.E.

Project Engineer

Florida Registration No. 41986

PRM/CAB:krh Enclosures B10\97-9036A.8

cc: Viro Group, Inc., Mr. John Bale, P.E.

	Total Time: 2.5 hrs.
Project: Laidlaw Drum Storage Date: 5/8/97 File No. 97-9036A	Travel Time: hrs. Time on Job: hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:  Structural Shop drawings	
	·
Elements Inspected and Location:	FIGURE
1. Foundations, AS ON Sketch	
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DEVIATIONS, NOTES AND CONVERSATIONS:	1 : 20 dall at ille who is
The Foundation system reinforcing Stee.	2 INSPECTED AT THO ADODE
depicted area was found to be in AC	1 / //
Except: ALL # 4 deformed bar used	MANUFACTURES MILL CONFICERTION & SHARMENT AHACKED
Bar Splice on North WALL A	months to will the N.E. Attacked
Corner does not provide for	
Added providing Correct LAP.	
Contractor Notified of Bar to Form	Clearance, Resupporting or movement
of rebar done during concrete pour providing Proper Concrete Coverage	gInspected By (, Clan Bert



# QUALITY PRECAST & CO.

"STRONG" ON SERVICE P.O. Box 11 - Brandon, Florida 33509-0011 (813) 685-5815 Fax: (813) 653-3240

Orlando (407) 877-1000 Lake Helen (904) 228-2112 May 8, 1997

Pinellas (813) 821-6227

Lakeland (941) 425-3070 Eastern Polk County (941) 421-2019

SEMCO CONSTRUCTION P.O. Box 706
Bartow,FL 33830

To Whomit May Concern:

Re: Bartow Airport Job

Please be advised that all rebar delivered to this job was Grade 60, per ASTM-A615M.

Strogrely,

Robert M. Pholps

Vice Pres.

CHEMICAL AND PHYSICAL TEST REPORT

JACKSONVILLE STEEL MEM MAYISTOM

METALLURGICAL DEPARTMENT

P.O. BOX 518 BALDNIN. FLORIDA 32234

PRODUCING MILL IS KNOWN BY HEAT ID MUMBER PREFIX:

C = CHARLOTTE. J = JACKSONVILLE. K = KNOXVILLE. I = TAMPA. V = WEST TENNESSEE

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THIS MATERIAL. INCLUDING THE BILLETS.

AS PRODUCED AND MANUFACTURED IN THE TIED STATES OF AMERICA.

A. J. TURNER

BUALITY ASSURANCE HGR.

HILL GROUP

WE MERENY CENTRY TIME THE ANCIE PICHMEN AND CONTROL AT COMPANIO IN THE INCOMPS OF THE COMPANY

### CHEMICAL AND PHYSICAL TEST REPORT

JACKSDAVILLE STEEL WERNEYISTON

HETALLURGICAL DEPARTMENT

P.O. ROX 518 HALDNIN, FLORIDA 32234

ERESTEEL PRODUCING HILL IS KNUWN BY HEAT ID NUMBER PREFIX:

C = CHARLUTTE, J = JACKSUNVILLE, K = KNOXVILLE, F = TAMPA, V = WEST TENNESSEE

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7-9	L_CH_		سدسانا	-5/1	<u> 194</u>	<del></del>	_ <del></del>	•	1		·		<u></u>		O:	azsa.	<u> </u>	1	ــــــــــــــــــــــــــــــــــــــ			3
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य राज्य	<del></del>	TERL	:		JUXNG	- V 146	N.Y.	42.70		<del></del>		<u> </u>			<u> </u>				<del></del>			<del></del>

THIS MATERIAL. INCLUDING THE BILLETS. NAS PRODUCED AND MANUFACTURED IN THE NITED STATES OF AMERICA.

A. J. TURNER

QUALITY ASSURANCE NGR.

MILL GROUP



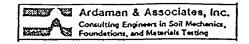
# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (941) 533-0858 / 533-3893

Job	Sheet	of
	Date	
	jop	

	D 460,550000	Pe x 1 psi 6894.76 Pa	[ 66,797 psi } Day 66 500 psi
TENSILE 742.30 MPa	742,300,000	0 Pa x <u>1psi</u> 6394.76 Pa	= 107,661 psi
45/,63 MPa		Pax 1psc 6994.76	= 65503 psi Pa Day 65,500 psi
TENSILE / 7/2,0/ MPa	7/2,0/0,000	3 Pax 1psi 6894.76	= [103,268 psi] Pa say 103, ou psi

	Total Time: /.25 hrs.
Project: AAAAW Drum Storage Date: 5/30/97 File No. 97-9036 A	Travel Time: .50 hrs. Time on Job: .75 hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:  Structural  Shop drawings	
Elements Inspected and Location:  1. Stem WALL & Columns, See Sketch  2.	FIGURE
3	
5	F 70' ->)
7	
9	· ·
11	<del></del>
Reinforcing Steel found to be of however water stop is not p	Correct size and phreement.
time of Inspection. Reinspection Concrete pour showed water-stop	Monday 9/2/97 prior to
	A Al D
	Inspected By ( Wan Dest



	Total Time: /.75 hrs.
Project: 1/20/400, Drem 5 do HOO  Date: 6/20/47  File No. 97-9036A	Travel Time: .75 hrs. Time on Job: /.0 hrs. Time in Office: hrs.
Drawing Used:  [9 structural	Delay Time:hrs.
Elements Inspected and Location:  Stem WALL, N. W. \$5, 2 W. LLS  Columns Samo See Skotal	FIGURE
DEVIATIONS, NOTES AND CONVERSATIONS:	· <del></del>
Top #3 Board of 40 Ed (1). Cohumis, Epid or Stirup placed is	Column. Area of Inspertion
Anoronel. For Concrete pour.	, , , , , , , , , , , , , , , , , , ,
	Inspected By Allan Box



	Total Time: // nrs.
Project: Bidlaw Drum Storage Date: 7/18/97 File No. 97-9036A	Travel Time: .5 Ho hrs.  Time on Job: hrs.  Time in Office: hrs.  Delay Time: hrs.
Drawing Used:	Dorag 11mo.
🦢 . 🛛 structural	
· hop drawings	
,	•
·	
Elements Inspected and Location:	FIGURE 1
	, i
1. FLOOR SLAD, COLLS F & G. D.F. Comer	.
2. of Building See Sketch	
3.	Cell Cell
J.	$F \downarrow G$
4	
5	
J.	
· 6	
_ •	(
8	
9:	
10.	·
11	
12.	
	w.*
DEVIATIONS, NOTES AND CONVERSATIONS:	
#1 Inspection of Floor State in Pells F	& G Showed #3 bars to
	#3 4 3/1 40/2
Analyse A /2 × 12 Spacing exst Was	1. #3 pars show No Grade of
60 CAST MARKINYS! See Mill Cold.	Ficato & Ociodi Fication Latter Report
#2 6x6x8 gaze welded line Fronce is / kg	e will need to he lifted
during pour to provide proper clause	TION IN SLAD.
#3. 3/2 " Smooth Dowels of Construction Ju	int to be installed
After Concrete Obscarant.	·
Inoposted Area approved for Conside	Oton quant Down deal Ahmon Items
#2 #3 AD CONSTRUCT A STATE A	inspected By C. Clar Best
#2\$3 Are Completed dufing and after pour. A	mopos dou by the first the



### ARDAMAN & ASSOCIATES, INC.

1525 CENTENNIAL DRIVE BARTOW, FL 33830 (941)453-4528 FAX: (941)533-7325

Te:	Virogroup Inc Date: 7/18/97
ATTN:	TIGNIN BOLOPE
Fax#:	803_957-3845 Pages: 2, including cover sheet.  C. Alan Best, Androwant Sheet Insportion
From:	C. Alan Best, Androw Barton
Subject	Concrete Reinforcement Steel Insportion
COMMENTS:	Area Appears Ready For Concrete
Place	a-crant 1
- Jankara	
<del></del>	
If this mos	ssage is incomplete, or requires further explanation, please call (941)533-0858.

October 27, 1997 File Number 97-9036A

Mr. Ed Locke SEMCO Construction P.O. Box 706 Bartow, FL 33831-0706

Subject:

Concrete Reinforcement Steel Inspection.

Laidlaw Drum Storage Building, Bartow Air Base, Bartow, Florida

### **REPORT NUMBER 13**

### Gentlemen:

As requested by you, from July 18 through October 24, 1997 Ardaman and Associates, Inc. visited the subject site to conduct a visual inspection of the concrete reinforcement steel for size, placement, and concrete cover. Please find enclosed copies of our Field Inspection Reports and associated findings.

Based our observations as recorded on the field inspection reports, it is the opinion of Ardaman and Associates, Inc. that the concrete reinforcing steel within the inspected elements has been installed in accordance with the project plans and specifications.

It has been a pleasure assisting you with this important phase of your project. If there are any questions or when we may be of further service, please contact us.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

P. Rodney Mank, P.E.

Project Engineer

Florida Registration No. 41986

PRM/CAB:kms Enclosures B19\97-9036A.13

cc: Viro Group, Inc., Mr. John Bale, P.E.

	10 tal lime. // Ills.
Project: Aistaw, Drum Storage Date: 7/18/97	Travel Time: .5 Hr hrs. Time on Job: 1.0 Hr hrs. Time in Office:a5 hrs.
File No. 47-9036A	Time in Office:hrs. Delay Time: hrs.
Drawing Used:	Delay Time.
. 🛛 structural	
shop drawings	
The state of the s	FIGURE
Elements Inspected and Location:	
1. FLoor Shop, Calls FJG@ N.E. Comer	<u>-</u>   . N
2. of Building See Skelel	
2. of Building See Steel	- Joseph 1
3.	-   Josh   Josh   Josh   G
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11.	<b>-</b>
11.	
12	• •
DEVIATIONS, NOTES AND CONVERSATIONS:	
	"+" C' Showed #3 bars to
#1 INSpection of FLOOR SLAD IN ('ell's F	4 G Chowar TO NATE FO
Austria A /2" × 12" Spacing EAS W	My. #3 pars slow No (TIESR of
60 CAST Medicys! See Mill Oky	Lificato & Oriol Fichtion Latter Report
#2 6x6x 8 2000 welded wire foods in MA	se, will need in he lifted
Lucing pour to provide proper Love	
# 5/2" Smooth Dowels of Construction=	Toin to be installed
After Concrete Obcoment.	/
Insuled fred manuel for Consult	e Otenant, provided Above Hans
	Inspected By C. Clan Blox

1	Total Time:nrs.
Project: And Aw Drum Stored Date: 8/6/97 File No. 97-9036  Drawing Used:    structural   shop drawings	Travel Time: hrs. Time on Job: hrs. Time in Office: hrs. Delay Time: hrs.
Elements Inspected and Location:  1. Stem Well Footing with Column Pads of  2. Verfical Steek. Inside world wes  3. Ramp From the S. W. Conver of Priv.  4. North Approximately 40  5.  7.  8.	FIGURE
9	
DEVIATIONS, NOTES AND CONVERSATIONS:  Vertical Seel For Columns for  4" Enst out of Walk, Vertical  Approved for pour.	Listed moved & retted.
	Inspected By . Max Dest

FIELD INSPECTION REPORT	
PROJECT NAME: Jaidlaw	DATE: 8/12/97
FILE NUMBER:	INSPECTOR:
TYPE OF INSPECTION (CHECK ONE OR MORE)	DID YOU OBTAIN:
CLEARING & GRUBBING	TEST ELEVATION YES NO DESCRIPTIVE LOCATION YES NO DESCRIPT
FOUNDATION SUBGRADE COMPACTION	
FOUNDATION BACKFILL COMPACTION	
FLOOR SLAB SUBGRADE (FILL)	ADEQUATE COVERAGE YES NO
TRENCH BACKFILL COMPACTION	SOILS DESCRIPTION YES NO
OTHER	DID YOU READ, OR ARE YOU FULLY AWARE OF THE PROJECT'S SPECIFICATIONS?
SAMPLE SOILS, PROCTOR, FBV, LBR, CBR, A/C, ETC.)	YES NO (IF NO, EXPLAIN IN REMARKS SECTION)
JOB SITE TIME	ROAD TIME
	TRIP MILEAGE: TRIP TIME:
ARRIVAL TIME: DEPARTURE TIME:	TRIP MILEAGE: TRIP TIME
REMARKS	
Along NW Stew wall. All A and all steel looked corresponding tom.	orell pour. Theched Stee opscings were correct oct According to
	,

FIELD INSPECTOR SIGNATURE

A5134 8/95

SIGN EACH DATA SHEET & ATTACH

Ardaman & Associates, Inc.

Geotechnical, Environmental and Materials Consultants

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (941) 533-0858 • Fax (941) 533-7325

	Total Time: /.5 hrs.
Project: <u>Aidlaw Dram Storage</u> Date: <u>8/25/97</u> File No. <u>97-9036</u>	Travel Time: .50 hrs. Time on Job: .75 hrs. Time in Office: .25 hrs. Delay Time: hrs.
Drawing Used:  [] structural  [] shop drawings	
Elements Inspected and Location:	FIGURE
1. Floor SLAB At N. E \$5. W. QUARTERS of Cells	
J. A Hru E.	
2. Exterior Columns (3) West sided West	
Londing Dock.	
Foundation, West & South of West RA	mp)
	<u>/</u>
7	
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1.	· ·
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DEVIATIONS, NOTES AND CONVERSATIONS:	
Exterior Columns of Foundation AS I FLOOR SLAD - 6x6x8ga WWF Elimina NOW Supported ON H" Chairs. Concin NO Drawings on site reflecting	Der DANS, MARTINED FOR POUR.
FLOORSLAD - 6X6X8GA WWF Elimient	CLA) #3 BARS EACH WAY 12 ON-CENTER
NOW Supported ON 4 Chairs. Concre	HE NOW to include Fiber-nesh,
10 drawings on site reflecting	1 lenges.
	Inspected By C. Man Best
	Thopecoul by C. Do toto too



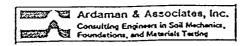
	rotal rime: /a// nrs.
- lida D Hara	AC Travel Time: .50 hrs.
Project: LAid Au Drum StorA	Time on Job: .50 hrs.
Date: 8/99/47	Time on office: hrs.
File No. 77-9036A	Delay Time: hrs.
Drawing Used:	D0101 1110 - 110 -
structural	
shop drawings	
D prob arautuge	
	FIGURE
Elements Inspected and Location	<u>ı:</u>
1. FLOOR SLAD, N. F&S. W.	$A \cdot A \cdot A$
1. FLOOR SLAD, N. E & S. W.	CleAdvar93
a displie my P&O.	
# g 1,8223 111,10, 1 ) Q	
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J	
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2.	·
DEVIATIONS, NOTES AND CONVERSATIONS:	. 1
A A A A A A	be is secondance with Propert
In perses Edement's found to	Le is pecondance with light
DEANS & PRENTICATIONS	
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Inspected By\_

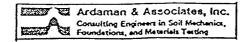
4	Total Time: /, hrs.
Project: Adlaw Drem Storge	Travel Time:50 hrs.
Date: 9/3/9/	Travel Time: 50 hrs. Time on Job: ,50 hrs. Time in Office: hrs.
File No. 47-9036	Delay Time:hrs.
Drawing Used:  [ structural	
Shop drawings	
	FIGURE
Elements Inspected and Location:	1100KC
1. FLOOTSLAD, W. W. F.S. E. Quadrants of	_
2. Cells A Hru E.	
·	
3	_
4	-
5	_
7.	
8	_
9	_
10	_
11.	· · · · · · · · · · · · · · · · · · ·
12.	•
	-
DEVIATIONS, NOTES AND CONVERSATIONS:	1 h de la
Noted A Few of the 1" Smooth down	JEL BATS, KOWELLA INTO
Drevious Cold Quadiant pours t	sit to have clearance
From top & Slab. These DA	ers bent down SLightly
providing proper Cherryco. o De	they preps where # 4
have see the walk as the day see	Corner Hod.
DAYS WEEKE, TOUCHING WATER STON	
INSpected that approved to	Dour.
· · · · · · · · · · · · · · · · · · ·	
	· AMKT
	Inspected By (2) Wan War



	Total Time: /, 25 hrs.
Project: Alfal Drem Sforts  Date: 974/97  File No. 97-9036	Travel Time: .50 hrs. Time on Job: .75 hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:  Ustructural  Shop drawings	
Elements Inspected and Location:  1. Floor Slab, N.W. \$5.E, Qualitant's  4 Cells M, N, P, Q \$2  3.	FIGURE
5	-
7	
9. 10.	• •
12	<u>.</u>
Some l'Dowels readed More (  fouching the water stop. The  INSPERSENT ANDROWS FO	Se Areas, Corrected for Concrete placement.
	1 Markon I
	Inspected By Ci Mulling



	10 tal lime. 700 miles
Project: (AIDLAW) Drum SOIALO Date: 9/8/97 File No. 97-9036A	Travel Time: 50 hrs. Time on Job: 50 hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:	
g structural	
shop drawings	
	•
•	
The state of Toolstion:	FIGURE
Elements Inspected and Location:	
1. FLOOSLAD N. E. I.S. W. Queliants of	
& Cells J.K. #L.	
2. Cells S. N. 4.	<del>-</del>
. A. Floor Slob EW. ForkLift Kunnyay	
	2
From E. End of Building West 60	
* I to South to the slope of the	2
EAST KAMP	<b>-</b>
7.	
1	-
8.	
9	<del>-</del>
10.	_
11.	<del>_</del>
12.	
1. C. •	<del></del>
DEVIATIONS, NOTES AND CONVERSATIONS:	
Pairton add don't found to be traign	AL #3 bars oN/2 Carders
New Comments Top & Top of The Comments Top of	1 11 (11)
EACH WAY Supported by of Chapt's. Will	090x 540D 1.054PHDED DEFUEDI)
aining audia de / "Smooth Social	I ungreased Dowels on 12"
A STATE OF THE STA	1 1 1
Centers Are inserted into previously	everas Quadratts appoint to
- Dour greas. Per cay S. E. & N.W.	Aundrated CPM 1" Are
Dour greas. In CRY J. I 4 10, W.	51 1 C VIVEP
doweled. Againing Areas of Cell	LADOT TO TOTA-LIFT KENNEY
floor has #3 BATS ON 18" Cente	ers doueled between 3/465
Insperked Areas Approved for	- Pour A A
THE SHAREST THEY S THINGS OVER TOO	/ DON
, v 4	Inspected By / Who was



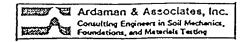
		Total Time: // hrs.
	Project: LAIDLAW Drum Home Bldg Date: 9/10/97 File No.	Travel Time: .50 hrs. Time on Job: .50 hrs. Time in Office: hrs. Delay Time: hrs.
	Drawing Used:    structural	
(i) 3: 4. (b) ( )	Elements Inspected and Location:  Floor Slab Fork-Lift Runway From  61 - 123 From E. Enlight  Floor Slab in S. E. & M. W. Qualitats  Liells K. & J.  Floor Slab Fork List From My From  1-1). Run, East Runway to South  WALL.	FIGURE
8. 9. 0.		
1 2 .		
<i>i</i>	DEVIATIONS, NOTES AND CONVERSATIONS:  TOURS AND FOUND TO DR I  Project PLANS F Spenification  Inspected areas Approved	Accordance with
-		1 M B
		Inspected By (, Man DU)

	Total Time: /. O. hrs.
Project: Laidlaw Drum Storage Date: 4/15/87 File No. 47-9036 B  Drawing Used:  Structural Shop drawings	Travel Time: 50 hrs. Time on Job: 50 hrs. Time in Office: hrs. Delay Time: hrs.
Elements Inspected and Location:  1. Floor SLAD, N.W. & S. E. Quadrants of  P. Cells H, I & O'  B. Floor SLAD, Forklift Runway From W.  P. Tid d. Emilling 70 E. & South Lege  8. fo S. W. Ramp  7.  8.  9.	FIGURE
10	•
Leinforcement Steel and Approved for	drass Correctly.
	Inspected By



	Total Time: .50 hrs.
Project: LA: JAW Drun 5401000 Date: 9/19/97 File No. 97-9036	Travel Time: .25 hrs. Time on Job: .25 hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:  Structural  shop drawings	
Elements Inspected and Location:  Floor Slab, N. E. & S. W. Quadrates  Letter 1. " H" L" " L" " L" " L" " L" " L" L" L" L" L	FIGURE
West End WALL & WEST RAMP	
•	
DEVIATIONS, NOTES AND CONVERSATIONS:	<u>-</u>
in place. Areas approved for	pour
	Inspected By (A. )

	Total Time:
Project: Addsu Drem Storage Date: 9/23/97 File No. 97-9036 A	Travel Time: .50 hrs. Time on Job: .25 hrs. Time in Office: hrs. Delay Time: hrs.
Drawing Used:  2 structural  3 shop drawings	
Elements Inspected and Location:  1. FLOOR SLAD, EW., FORKLIFT  2. Reenway From 65 +0 90 E. f. th  3. W. End & Building & South Reenway  4. to S. End & Building  5.	FIGURE
9	
10	
No Deviations:  No Deviations s Notes from  This rected Area Approved a	plans & Soges for Concrete planament
	Inspected By ( Mankey)



,	Total Time: -/5 hrs.
Project: Stal sur Drum Storage	Travel Time: 50 hrs.
Date: 10/24/97	Time on Job: 25 hrs.
File No. 9769036 A	Time in Office: hrs. Delay Time: hrs.
Drawing Used:	
structural shop drawings	
C onet are and are	
Elements Inspected and Location:	FIGURE
D C // // // £ D	
1. Roof Slab, HAZ-Mit Room, Coll 1	<b>-</b> ·   ·
2	_
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DEVIATIONS, NOTES AND CONVERSATIONS;	
Ma daviding For Mind -	cent Noted
100 NEVIATIONS FILM 1405 4 30	0/-
Hyproved for Conside photom	1,7.
/ <i>V</i>	
	·
	<u> </u>
	Inspected By C. MON LOW





### Ardaman & Associates, Inc.

1525 Centennial Drive Bartow, Florida 33830



### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:	
Project Name: LAIDLAW - DRUM STORAGE BUILDING VIROGROUP, INC. Project Location: BARTOW AIR BASE ATTN: JOHN BALE, P.E. Project Contractor: SEMCO CONSTRUCTION Concrete Supplier: FLORIDA ROCK INDUSTRIES											
	Specified Strength: Slump (inches): Air Content (percent							nt (percent):			
DESIGN	11.1								N/A		
DATA	Mix Type	4000 p.s.i.@		28	uays	3 - 42			14/21		
52-5217		Tomar VI. C. Eigin	woight [		··_ — ·					/	
52-5217	1 201	Transit Mixed:		Pump Mix			(	Other			
FIELD	Date:	· · · · · · · · · · · · · · · · · · ·	Time Co	ncrete Bato	hed: T	rime Co	oncrete Sam	pled:	Sampled	By:	
and LAB		4-11-97		8:11			9:10			EN WATSON	
DATA	Concrete	Truck No.:	Ticket N	0.:	5	Size of L	_oad (C.Y.):		Weather (	Conditions:	
<i>-</i>		4489	17	3278			10		CLOUDY & COOL		
	Water Ad	ded At Job Site:							Extra Wat	ter Authorized By:	
			Yes	Ga	al. To			C.Y.			
	Slump: (ii			erature (°F)	): C	Concret	e Temperatu	ıre (°F):	Wet Weig	ht (P.C.F.):	
		3½"	1 .	10°	1		76°		N/A		
	Air Conte	ent (% by Vol.):	Molded	and Cured *	to ASTM	O ASTM C-31 Tested to ASTM			ASTM C-39		
		3.0%						∕es □ No			
	Location of Concrete Placement:				=						
	DRIVE WAY SLAB AT COOLING TOWER.										
	DICTUD WITH CHILD HIT COODERS TOWNS										
	DATE	UNIL	AGE	TEST SPEC	IMEN SIZE		TOTAL	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT	
SET NO.	RECEIVI		(DAYS)	DIAMETER (IN.)	AREA (SO III	N)	LOAD (LBS)	(PSI)	FRAC	(AIR DRY-LBS)	
	<u> </u>									2	
LDSB-1	4-14		_					41.00		NAIS2	
1		4-18	7	6.00	28.27		16,500	4120	2	145	
2		4-18	7	6.00	28.27		18,000	4170	2	135	
3		5-09	28	5.98	28.09		50,500	5360	2	5/3	
4		5-09	28	5.98	28.09	)   14	47,500	5250	2		
5		5-09	SP			-					
6		5-09	SP								
REMARKS	: *Concre	ete Test Specimer	Cured i	n Accorda	nce wit	th AST	M C-31 Af	ter Being	Receive	d in Laboratory	
						1	2	3	•	4 5	
						Cone	Cone-Shear	Shea	r S	plit Cone & Split	
A5111 (9/91)							450		SOCIATE	6 W0 A	

Florida Registration No. .



Florida Registration No.

## Ardaman & Associates, Inc.

1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

		TO:		<del>" - '</del> '.	(		DATE:				
	Project Project Lo- Project Cont Concrete Su	cation: BA ractor: SE	IDLAW DRUM RTOW AIR BA MCO CONSTRU ORIDA ROCK	SE CTION		NG	ATTN: BOY DEN VIROGROUE	TD ROBERTS NIS WALTO , INC.			
ł	DECICN	Specified Str	enath:			S	lump (inches)		Air Content	(percent):	
١	DESIGN DATA	1 -	00 p.s.i. @		28 d	- 1	4 1/2"		3 -	6%	
1		Mix Type:									
1		_XNorn	nal wt. Light	weight [	] Mortar Mix	Gu	nite Grou	t Other			
	525217	<b>X</b> Tran:	sit Mixed:		Pump Mix			Other	3" PUMP		
Ì	FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Concrete	Sampled:	Sampled B	y:	
ı	and LAB	5-	08-97		:05		2:40			WATSON	
.	DATA	Concrete True	ck No.:	Ticket N	0.:	S	ize of Load (C	.Y.):	Weather Co	onditions:	
١		42	·	1	0452		10		P/C &	HOT	
		Water Added			0			0.1/	1	r Authorized By:	
$\langle$		X Yes					10 Concrete Temp	C.Y.			
7		Slump: (inche	es):	Air Temperature (°F): 85°			oncrete temp	erature ( F).	Wet Weight (P.C.F.):		
١		Air Content (		and Cured * t	O ASTM			N/A Tested to A	STM C-39		
		4.				∏No	□Unk	nown	√ Ye		
1			Concrete Placem	ent:	OUNDATIO			•			
					30' NORTH OF SOUTHWEST						
				С	ORNER OF						
	SET NO.	DATE RECEIVED	DATE TESTED	AGE (DAYS)	TEST SPECIA	1	LOAD STRENG			SPECIMEN WEIGHT	
1		INLAB	163160	(0/10)	DIAMETER (IN )	AREA (SO:IN	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)	
١	LDSB-1	5-09								75	
ļ	1		5-15	7	6.00	28.2	102,500	3630	3 🕻	ONW	
١	2		5-15	7	6.00	28.2	7 101,000	3570	4 (	Mar 2	
۱ ۾	3		5-22	14	6.00	28.2				114 P	
TM-C39	4		6-05	28	6.00	28.2	1	i	i i	(2)	
O AS	5		6-05	28	6.00	28.2	7 143,000	5060	2	CAD	
ORMS T	6		6-05	SP							
HIS FORM CONFORMS TO AST	REMARKS	: *Concrete	lest Specimen	Cured i	n Accorda	nce wit	h ASTM C-3	1 After Being	g Received	in Laboratory	
e E							1 2	3	4	5	
ť					·						
2	S111 (9/91)	<del></del>	·		<del></del>		cone Cone-	Shear Shear	<del></del>		

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



FILE NO.: 97-9036/B





DATE:

#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

5-08-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET	NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	TRUCK WAS	TESTED	- C	LINDERS I	OLDED,	SET #1.			
2	TRUCK WAS	TESTED	- C	LINDERS I	MOLDED,	SET #2.			
3	8999	10455		3:10	4:35	15	10	4 1/4	N/A
4	6011	10456		3:25	5:15	10	10	4	N/A
5	3505	10457		4:55	5:57	5	10	4	N/A
6	TRUCK WAS	TESTED	- C	LINDERS I	OLDED,	SET #3.			
7	6011	10459		6:15	7:00	10	10 .	4 1/4	N/A
8	TRUCK WAS	TESTED	- C7	LINDERS 1	OLDED,	SET #4.			
					1 .				
					,			<u></u>	
-									
									1
FLORIDA	REGISTRATION I	NO	419	184		вү	Plakes W,	land 51	15 97

FLORIDA REGISTRATION NO	41984	ву	I Carriery V	your s	<del>(13/4/</del>
FLORIDA REGISTRATION NO AS A MUTUAL PROTECTION TO CLIENTS. PUBLICATION OF STATEMENTS, CONCLUS	THE PUBLIC AND OURSELVES ALL REPO IONS OR EXTRACTS FROM OR REGARDIN	RTS ARE SUBMITTED AS THE IG OUR REPORTS IS RESERVED	CONFIDENTIAL PRO PENDING OUR WRIT	PERTY OF CLIENTS TYEN APPROVAL.	AND AUTHORIZED FO



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			(		DATE:					
Project N Project Loc Project Contr Concrete Su	cation: B.	AIDLAW DRUM ARTOW AIR B EMCO CONSTR LORIDA ROCK	ASE UCTION		OING ·	VIRONME ROBERT IS WALT INC. BALE,	ON				
5501011	Specified Stre	enath:			SI	ump (inches):		Air Content	(percent):		
DESIGN DATA	1 '	000 p.s.i. @	28 days			4 1/2"		3 - 6	11		
DAIA	Mix Type:	000 p.s.i. @				· · · · · · · · · · · · · · · · · · ·		<u> </u>			
	⊠ Norm										
52517	Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other										
32317		sit Mixed:		Pump Mix				" PUMP			
FIELD	Date:		Time Co	ncrete Batch	ned: Ti	me Concrete Sam	pled:	Sampled B	y:		
and LAB	ł	-08-97	2	:35		3:20		ALLEN	WATSON		
DATA	Concrete Truc		Ticket No		Si	ze of Load (C.Y.):		Weather Co	onditions:		
DAIA	1	505	1	0453		10		P/C &	HOT		
	Water Added			<u> </u>				Extra Wate	r Authorized By:		
	∑ Yes		Yes 20 Gal. To			10	C.Y.	PUMPM	AN		
	Slump: (inche					oncrete Temperati	ıre (°F):	Wet Weight	(P.C.F.):		
	1 ' '	3/4" *		5°		80°		N/A			
	Air Content (%		Molded a	and Cured *	to ASTM	C-31		Tested to ASTM C-39			
	1	.0%	1	Yes	□No	☐ Unknow	n	∑ Ye:	s No		
		Concrete Placem									
			F	OUNDATIO	)NN						
			1	5' EAST	OF NO	RTHWEST					
			C	ORNER OF	BUILI	OING.			·		
- "	DATE	DATE	AGE	TEST SPECI		TOTAL	TEST	TYPE	SPECIMEN WEIGHT		
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN)	LOAD (LBS)	STRENGTI (PSI)	H OF FRAC	(AIR DRY - LBS)		
						,					
LDSB-2	5-09				00 07	107 500	2000	1 ,	Ath		
1		5-15	7	6.00	28.27	107,500	3800	3	NE R		
2		6-05	28	6.00	28.27	157,500	5570	2	They		
3		6-05	28	6.00	28.27	159,000	5620	3	CAD		
4		6-05	SP								
4 .		0 03									
			}								
REMARKS:	*Concrete	est Specimen	Cured i	n Accorda	nce witl	n ASTM C-31 Af	ter Being	Received	in Laboratory		
						1 2	3	4	5		
* THI	S IS AN E	XTRA SET OF	CYLIN	IDERS	1/2		$\cdots$				
MAD	E, DUE TO	HIGH SLUME	AS C	RDERED			///				
BY	B. ROBERT	SON; LAIDLA	W REPS	ENTATIV	≘.   <i>∷</i> /		//.				
					Ę,	의 (Cara Shari	تنا∕ا دمو	لتاليا ك	t Cone & Split		
					C	one Cone-Shea	Shea Shea	r Spli	Colle a Opin		
A5111 (9/91)						ΔRDΔ	MAN & AS	SOCIATES	INC.		

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.

41986

Florida Registration No. .



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:		CC.						DATE:
Project I Project Loo Project Cont Concrete Su	cation: Bi	AIDLAW DRUM ARTOW AIR BA EMCO CONSTRU LORIDA ROCK	SE ICTION		NG	LAIDLAW ENVIRONMENTAL SERVICES, IN ATTN: BOYD ROBERTSON - SITE DENNIS WALTON VIROGROUP, INC. ATTN: JOHN BALE, P.E.			
DESIGN	Specified St	renath:			S	Slump (inches):		Air Content (percent):	
DATA	1 '	000 p.s.i. @		28 c	lays	4 1/2"		3 - 6	8
DAIR	Mix Type:								}
525217	⊠ Nor	mal wt. Light	weight [	] Mortar Mix	( □Gu	ınite 🗌 Grout	Other		
		nsit Mixed:	Pump Mix				Other	·	
FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Concrete Sar	npled:	Sampled B	1
and LAB	5-	-08-97		:35		6:20			WATSON
DATA	Concrete Tru	ick No.:	Ticket No		S	Size of Load (C.Y.):		Weather Co	1
		999	10458			10		P/C &	
	1	d At Job Site: ☐ No If					<b>0</b> V	1	r Authorized By:
	X Yes	Yes 5 Gal. To			10	C.Y.	Wet Weight	ACTOR	
	Slump: (inch		Air Temperature (°F): 85°			Concrete Temperat 83°	ure (F):	N/A	(F.C.F.).
	5		1	and Cured *	to ASTM			Tested to A	STM C-39
	Air Content (% by Vol.): 3.2%				□ No	Unknov	vn	X Ye	
	l	. 2% Concrete Placem		Yes		UNINIOV		<u> </u>	
	Location of	Concrete Flacen		OUNDATIO	ONS				ĺ
	ļ			OONDITTE	<u> </u>				
			. 1	0' SOUTH	OF N	ORTHEAST			
			C	ORNER OF	BUIL	DING.			
	DATE	DATE	AGE	TEST SPECI	MEN SIZE	TOTAL LOAD	TEST STRENGT	TYPE OF	SPECIMEN WEIGHT
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN		(PSI)	FRAC	(AIR DRY - LBS)
LDSB-3	5-09		_				20.40		200
1	1	5-15	7	1	28.27		3940 3890	2 2	1000
2		5-15	7	6.00	28.27 28.27		4670	4	7/4/2
3		5-22	14 28	6.00 6.00	28.27		5360	2	CASS
4		6-05	28	6.00	28.27		5410	2	CAB
5		6-05 6-05	SP	0.00	20.2.	133,000			
6		0-03	J.						
REMARKS	: *Concrete	Test Specimen	Cured i	n Accorda	nce wit	h ASTM C-31 A	fter Being	Received	in Laboratory
		•				1 2	3	4	5
						Cone Cone-Shea	ar Shea	r Spli	t Cone & Split
A5111 (9/91)								SOCIATES	

Florida Registration No.

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

- · · · · · · · · · · · · · · · · · · ·	TO:				CC.				DATE:		
Project Project Lo Project Cont Concrete Su	cation: BAF ractor: SEN	DLAW DRUM RTOW AIR BA MCO CONSTRU DRIDA ROCK	SE OCTION		NTAL SER SON - SI ON P.E.	VICES, INC. TE					
DECION	Specified Stre	noth:			Is	lump (inches):	Air Content (percent):				
DESIGN DATA	1 '	)0 p.s.i. @		28	days	4 1/2"		3 - 6	ુ જ		
	Mix Type:	70 p.s e									
		al wt. Light	weight [	Mortar Mix	< □Gu	inite Grout	Other				
525217	▼ Transi	t Mixed:		Pump Mix			Other 3	" PUMP			
FIELD	Date:		Time Co	ncrete Batcl	ned: T	ime Concrete Sam	pled:	Sampled B	y:		
and LAB	1	08-97	7:	00		8:35			WATSON		
DATA	Concrete Truck		Ticket No	0.:	S	ize of Load (C.Y.):		Weather Co	onditions:		
]	350		10460			10		P/C &			
	Water Added A		V - Col To 10			C.Y.		Authorized By:			
Ì			Yes 0 Gal. To 10  Air Temperature (°F): Concrete Temperature (°F						(PC E):		
	Slump: (inches	•	Air iemp		.	83°	ne ( r ).	Wet Weight (P.C.F.): N/A			
	Air Content (%	/ 3" *		and Cured *	to ASTM			Tested to ASTM C-39			
	N/A		l .	Yes	□No	Unknow	n	∑ Yes			
		oncrete Placem	1	ent:							
			F	OUNDATIO	ON			<del></del>			
			S	OUTHWEST	CORN	ER OF BUILDI	NG.				
SET NO.	DATE RECEIVED	DATE TESTED	AGE (DAYS)	TEST SPECI	Т	TOTAL LOAD	TEST STRENGTH		SPECIMEN WEIGHT		
	IN LAB	123123	(6/1/6/	DIAMETER (IN.)	AREA (SO:1N	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)		
LDSB-4	5-09							·	atv		
		5-15	7	6.00	28.27	119,000	4210	3	Q40 ,		
1		3-13	'	0.00	20.27				SAR		
2 ·		6-05	28	6.00	28.27	168,750	5970	2			
·							4				
1											
		•									
	<u></u>				<u> </u>		6	<u> </u>	:- 1 -b		
REMARKS	: *Concrete Te	est Specimen	Cured i	n Accorda	nce wit	h ASTM C-31 Af	ter Being 3	Received 4	in Laboratory		
1/2 EXTI	UCK SENT BACK TO PLANT TO ADD  2 YARD OF CONCRETE TO DRY UP LOAD.  TRA SET ORDERED BY ROBERTSON;  IDLAW REPRESENTATIVE.										
A5111 (9/91)			· · · · · · · · · · · · · · · · · · ·					SOCIATES,			

41986 Florida Registration No.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:	
Project Project Lo Project Con Concrete Su	cation: BART tractor: SEMC	LAW DRUM S OW AIR BAS O CONSTRUC IDA ROCK 1	SE CTION		1G	ATTI VIR	N: BOYD	ROBERTS S WALTO INC.	ON - SI N	VICES, INC. TE	
DECION	Specified Stren	ath:			5	Slump (	inches):		Air Conter	nt (percent):	
DESIGN DATA	4000	_		28 (	days		MAX.		N/I	**	
DAIA	Mix Type:	<u> </u>									
		ıl wt. ∐Light	weight [	Mortar Mi	κ 🗀 Gι	unite	☐ Grout (	Other			
525217											
		Mixed:		Pump Mix			···· - — ···· ·	Other 3	" PUMP		
FIELD	Date:		Time Co	ncrete Batcl	hed: T	rime Co	oncrete Sam	pled:	Sampled I	Ву:	
and LAB	6-02	-97		03		9:	:50		ALLEN	WATSON	
DATA	Concrete Truck	No.:	Ticket N	0.:	S	Size of I	Load (C.Y.):		Weather C	Conditions:	
	3505		10827				10		=		
-	Water Added A		Yes 8 Gal. To					O V		er Authorized By:	
			Yes			S	10	C.Y.		DA ROCK REP.	
	Slump: (inches	•	Air Temperature (°F):			Concrete Temperature (°F):			Wet Weight (P.C.F.):		
	6"			and Cured *	to ACTN	1 ( 21	86°		N/A Tested to ASTM C-39		
	Air Content (%	by voi.):	1		IOASTIV □No	10-31	Unknow	_	Yested to A		
	1.4% Location of Co	narata Placam								35	
	Location of Co	ncrete Placen		TEM WALI							
	-			TEM WELL	J						
			1	.5' WEST	OF SOL	JTHEA	ST CORNE	R			
			C	F BUILD	ING.						
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECI	MEN SIZE		TOTAL LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT	
	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ/IN	4)	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)	
_										1.0	
LDSB-5	6-03	6-09	7	6.00	28.2	7	96,500	3410	3	(AL)	
1		6-09	7	6.00	28.2	,	95,000	3360	l l	CABO	
2	-	6-16	14	6.00	28.2		25,750	4450	1	CAO	
3		6-30	28	5.99	28.1		17,000	5220		MB	
4		6-30	28	5.99	28.1	1	17,500	5230	l l	MAR	
5		6-30	SP	3.33	20.1		17,500	3230			
6		0 00									
REMARKS	: *Concrete Te	st Specimen	Cured i	⊥ n Accorda	nce wit	h AST	M C-31 Af	ter Being	Received	in Laboratory	
		•				1	2	3	. 4	5	
* SI	AMPLE TAKEN	FROM CHUT	E OF T	RUCK.							
		·				Cone	Cone-Shear	Shear	r Sp	lit Cone & Split	
(5111 (9/91)									-		

41986 Florida Registration No.



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.:

**97-9**036/B



# **CONCRETE DATA RECORD**

DATE:

6-02-97

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO

CONCRETE SUPPLIER:

FLORIDA ROCK

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED			SLUMP (inches)	CONCRETE TEMP.
1	8999	10826	8:20	9:27	5	10	5	75°
2	LOAD WAS	TESTED - C	YLINDERS !	OLDED,	ET #5.			
3	8999	10831	10:10	11:04	0	10	6 1/2	85°
4	3505	10833	11:10	12:08	10	10	6 1/2	85°
5	8999	10836	11:45	1:00	0	10	5 3/4	86° ()
6	LOAD WAS	TESTED - C	LINDERS 1	OLDED,	SET #6.			
7	6011	10845	2:35	3:30	13	10	5 3/4	85°
					·			
								·
<u></u>			<u> </u>					

•		
LORIDA REGISTRATION NO.	BY _	



Florida Registration No. \_

# Ardaman & Associates, Inc.

1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			-	CC.					0	DATE:
Project I Project Lor Project Cont Concrete Su	cation: BA ractor: SE	AIDLAW DRUM ARTOW AIR BA EMCO CONSTRU LORIDA ROCK	SE CTION		ING	ATI VIF	N: BOYD	ROBERT S WALT	SON - ON		CES, INC.
DESIGN	Specified Str	enath:			5	Slump (i	nches):		Air Cor	tent (pe	ercent):
DESIGN	1 '	000 p.s.i. @		28	days	6 ½	" MAX.		N,	/A	
	Mix Type:										
	Norr     Nor	nal wt. Light	weight [	] Mortar Mi	x 🔲 Gı	unite [	Grout (	Other			
525217		sit Mixed:		Pump Mix					" PUI		
FIELD	Date:		Time Co	ncrete Batc	hed: 1		ncrete Sam	pled:	Sample	•	
and LAB		-02-97		2:30			.:05			LEN WA	
DATA	Concrete Tru		Ticket N		٤		oad (C.Y.):		1	r Condi	
		197	10838				10				LT. RAIN
	Water Added		Yes Gal. To				C.Y.	Extra Water Authorized By:			
	Slump: (inch					Concret	e Temperati			eight (P.0	C.E.):
	6		90°			Concrete Temperature (°F): 86°			Wet Weight (P.C.F.): N/A		
	Air Content (			and Cured *	to ASTM	л C-31		·	Tested to ASTM C-39		
	4	.0%	1	Yes	□No		Unknow	n	X	] Yes	☐ No
		Concrete Placem	ent:						-		
				STEM WA	LL						
				45' WES	T OF N	ORTHE	EAST		****		
				CORNER	OF BUI	LING.	•				
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPEC	IMEN SIZE		TOTAL LOAD	TEST STRENGTH	TY		SPECIMEN WEIGHT
SET NO.	INLAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ/ff	N)	(LBS)	(PSI)	FR/		(AIR DRY - LBS)
							,			İ	
LDSB-6	6-03	6-09	. 7	6.00	28.27	,   (	98,000	3470	2	0	142 I
1		6-09	7	6.00	28.27	1	7,000	3430	3		9D)
2		6-16	14	6.00	28.27		28,500	4540	2		400
3	-	6-30	28	5.99	28.18		53,500	5450	2	0	<i>413</i>
4 5		6-30	28	5.99	28.18		52,500	5410	3	C	4B
6		6-30	SP								}
Ŭ											
REMARKS	: *Concrete	Test Specimen	Cured i	n Accorda	nce wit	th AST	M C-31 Aft	ter Being	Recei	ved in L	aboratory 5
* SAMI	PLE TAKEN	FROM CHUTE	OF TRU	JCK.		Cone	Cone-Shear	Shear		Split	Cone & Split
A5111 (Q/Q1)									2000143		

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

····	TO:				CC.					DATE:			
Project Project Lo Project Cor Concrete S	ocation: BAI	IDLAW DRUM RTOW AIR B. MCO CONSTR DRIDA ROCK	ASE UCTION		ING		ROGROUP, TN: JOHN		P.E.				
DECICN	Specified Stre	enath.			1:	Slump	(inches):		Air Content (percent):				
DESIGN DATA	1 '	00 p.s.i. @		28	days		1/2" MA	Х.	N/				
DAIA	Mix Type:	JU PISIT C											
	Norm	nal wt. Ligh	tweight	☐ Mortar Mi	x □G	unite	Grout	Other	1.00				
525217		. ta. 6 41		Dumo Miy				Othor		DINED MEN			
		sit Mixed:		Pump Mix		T				PUMP MIX			
FIELD	Date:		1	oncrete Batc	nea:		oncrete Sam	ipiea:	Sampled I	•			
and LAB	Concrete Truc	20-97	Ticket N	55			0 : 46 Load (C.Y.):	· .		Y PURVIS Conditions:			
DATA				-	[`	J126 01	10		HAZY				
	Water Added			1249			10	·		er Authorized By:			
	X Yes		Yes	16 Ga	al. To		8	C.Y.	1	•			
	Slump: (inche			perature (°F)		Concre	te Temperati	-	Wet Weigh				
	, ,	L/2"	92			86°			N/				
	Air Content (%	Molded	and Cured *	to ASTN	И C-31			Tested to ASTM C-39					
	N/A	-	. 🛭	Yes	□No		Unknow	n	X Y	es 🗌 No			
	Location of C	oncrete Placer	ment:					•					
			-	STEM W	ALL								
		75' EAST OF NORTHWEST CORNER OF BUILDING.											
<del></del>	DATE	DATE	AGE	TEST SPEC	MEN SIZE	1	TOTAL	TEST	TYPE	SPECIMEN			
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO I	IN <sub>j</sub>	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)			
LDSB-7	6-23				į					118			
1	0-23	6-27	7	6.00	28.27	7 1	10,500	3910	2	(40)			
2		6-27	7	6.00	28.27	7   1	12,000	3960	2	CAD			
3		7-07	17										
4		7-18	28										
5		7-18	28										
6		7-18	SP										
REMARKS	S: *Concrete T	est Specimer	n Cured i	n Accorda	ince wi	th ASI 1	「M C-31 Af 2	ter Being 3	Received 4	d in Laboratory 5			
5111 (9/91)			· · · · · · · · · · · · · · · · · · ·		(	Cone	Cone-Shear		· · · · · · · · · · · · · · · · · · ·				
J (0/01)		NO.					ARDA	MAN & AS	SOCIATES	s, INC.			
Iorida Begist	tration No	V <sub>i</sub> o			С	٦v٠							

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:
Project Lo Project Cont Project Cont Concrete Su	cation: BAR ractor: SEM	TOW AIR BA							P.E.	
	Specified Stree	nath:				Slump (in	iches):		Air Conte	nt (percent):
DESIGN	1 '	o p.s.i. @		28	days		1/2" MA	х.	N/	'A
DATA	Mix Type:	<u>υ ρ.s.i. ω</u>			<u>aujo</u>				<del></del>	
		al wt. 🔲 Light	weight [	□ Mortar Mi	x □G	unite [	Grout (	Other		
525217									<del></del>	
32321,	∏transi	t Mixed:		Pump Mix				Other PE	A ROCK,	PUMP MIX
FIEL D	Date:		Time Co	ncrete Batc	hed:	Time Cor	ncrete Sam	pled:	Sampled	By:
FIELD and LAB	ł	0-97	9.	55	1	10:	: 46		JOHNN	Y PURVIS
DATA	Concrete Truck		Ticket N		:	Size of Lo	oad (C.Y.):		Weather (	Conditions:
DAIA	601		ł				10		HAZY	& HOT
=	Water Added A		11249						Extra Wat	er Authorized By:
	X Yes		Yes 16 Gal. To				8	C.Y.	M.D.	MONIT
	Slump: (inches		20			Concrete	Temperatu	ıre (°F):	Wet Weig	ht (P.C.F.):
=	6 1	92				86°		N/	'A	
	Air Content (%		and Cured *	to ASTN				Tested to ASTM C-39		
	N/A		1	Yes	□No				XY	′es ☐ No
•		oncrete Placer			<u> </u>		<del>'</del> -			
-	Location of o	31101010 1 14001		STEM W	ALL					
			<del></del>	75' EAS	ST OF	NORTH	WEST CO	RNER OF	BUILD	ING.
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	TEST SPEC			TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY · LBS)
LDSB-7 1 2 3 4 5	6-23	6-27 6-27 7-07 7-18 7-18 7-18	7 7 17 28 28 SP	6.00 6.00 6.00	28.27 28.27 28.27	7   11.	0,500 2,000 0,500	3910 3960 4260	2 2 2	
REMARKS	: *Concrete Te	est Specimer	n Cured i	n Accorda	ance wi	1	2	3		d in Laboratory 4 5  plit Cone & Split
V5111 (9/91)						Cone	Cone-Shear		SOCIATE	
, ,		Mō ·					ANDA	III A A	COUNTE	<u>.,</u>

FORM TOOL D-FT THIS FORM C



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.	CC.				DATE:
Project N Project Loc Project Contr Concrete Sup	ation: BAR actor: SEM	DLAW DRUM TOW AIR BA CO CONSTRU RIDA ROCK	SE ICTION		ING		OGROUP, N: JOHN		P.E.	
DESIGN	Specified Stre	•		2.0		Slump (in		v	Air Conten N/2	t (percent):
DATA	400 Mix Type:	0 p.s.i. @		28	days	0.	1/2" MA	Λ.	14/2	3
•		al wt. Light	weiaht Γ	□ Mortar Mi	ix ∏Gu	unite 📋	Grout (	Other		
525217	<u></u>									
	∏Transi	t Mixed:		Pump Mix						PUMP MIX
FIELD	Date:		Time Co	ncrete Batc	hed: T	Time Cor	ncrete Sam	pled:	Sampled E	-
and LAB		0-97		55		10:	: 46		JOHNN.	Y PURVIS
DATA	Concrete Truck	(No.:	Ticket N		15	Size of Lo	oad (C.Y.):		Weather C	
	601		11	249			10		HAZY	& нот er Authorized By:
	Water Added A		Yes	16 Ga	al. To		8	C.Y.		
1-	Yes Slump: (inches			erature (°F)		Concrete	Temperatu		Wet Weigh	
	6 1	*	92		. [	501101010	86°		N/	
}	Air Content (%			Molded and Cured * to ASTM C-31						ASTM C-39
	N/A	•	8					n	∑ Ye	es 🗌 No
		oncrete Placem	ient:							
:				STEM W	ALL					
									DUTER	170
-				75' EAS	ST OF	NORTH	WEST CO.	RNER OF	BUILDI	NG.
										·
			AGE	TEST SPEC	IMEN SIZE	1	OTAL	TEST	TYPE	20000000
ı i	DATE	DATE	) AGE				1			SPECIMEN
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO:IN	ι	LOAD (LBS)	STRENGTH (PSI)		SPECIMEN WEIGHT (AIR DRY · LBS)
	RECEIVED IN LAB			DIAMETER (IN.)	AREA (SO:IN	ι			I OF	WEIGHT
LDSB-7	RECEIVED	TESTED	(DAYS)			N) (	LBS)	(PSI)	OF FRAC	WEIGHT
LDSB-7	RECEIVED IN LAB	6-27		6.00 6.00	28.27	110	D,500		I OF	WEIGHT
LDSB-7 1 2	RECEIVED IN LAB	TESTED	(DAYS)	6.00		110	0,500 2,000	3910 3960	OF FRAC	WEIGHT
LDSB-7 1 2 3	RECEIVED IN LAB	6-27 6-27 7-07	7 7	6.00	28.27 28.27	110	D,500	(PSI) 3910	2 2 2 3	WEIGHT
LDSB-7 1 2	RECEIVED IN LAB	6-27 6-27	7 7 17	6.00 6.00 6.00	28.27 28.27 28.27	110 1110 1110 1110 1110 1110 1110	0,500 2,000 0,500	3910 3960 4260	OF FRAC	WEIGHT
LDSB-7 1 2 3 4 5	RECEIVED IN LAB	6-27 6-27 7-07 7-18	7 7 17 28	6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27	110 1110 1110 1110 1110 1110 1110	0,500 2,000 0,500 2,000	3910 3960 4260 5380	2 2 2 3	WEIGHT
LDSB-7 1 2 3	RECEIVED IN LAB	6-27 6-27 7-07 7-18 7-18	7 7 17 28 28	6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27	110 1110 1110 1110 1110 1110 1110	0,500 2,000 0,500 2,000	3910 3960 4260 5380	2 2 2 3	WEIGHT
LDSB-7 1 2 3 4 5	RECEIVED IN LAB	6-27 6-27 7-07 7-18 7-18 7-18	7 7 17 28 28 SP	6.00 6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27 28.27	110 2 112 7 120 15:	0,500 2,000 0,500 2,000 7,000	3910 3960 4260 5380 5340	2 2 2 2 3 3	WEIGHT (AIR DRY LBS)
LDSB-7 1 2 3 4 5	RECEIVED IN LAB	6-27 6-27 7-07 7-18 7-18 7-18	7 7 17 28 28 SP	6.00 6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27 28.27	110 2 112 7 120 15:	0,500 2,000 0,500 2,000 7,000	3910 3960 4260 5380 5340	2 2 2 2 3 3	WEIGHT
LDSB-7 1 2 3 4 5	RECEIVED IN LAB	6-27 6-27 7-07 7-18 7-18 7-18	7 7 17 28 28 SP	6.00 6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27 28.27	110 2 112 7 120 15:	0,500 2,000 0,500 2,000 7,000	3910 3960 4260 5380 5340	2 2 2 3 3 3 3 Received	weight (AIR DRY LBS)

Florida Registration No.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			(	CC.				DATE:
Project Project Lo Project Cont Concrete Su	cation: BAF tractor: SEM	DLAW DRUM RTOW AIR BA ICO CONSTRU DRIDA ROCK	ASE JCTION		NG		GROUP, IN	IC. ALE, P.E.	
							·	T	
DESIGN	Specified Stre	-			i	Slump (inches):		Air Content	
DATA		00 p.s.i. @		28 c	lays	6 1/2" N	IAX.	N/	A
	Mix Type:						045		
505015	XNorm	al wt. Light	weignt (	Mortar Mix	( [] ()	unite Grout	Other		
525217	Trans	it Miyed:		Pump Mix			Other pr	TA POCK	PUMP MIX
	1	it iviixed.		ncrete Batch	and: IT	ime Concrete Sa		Sampled B	
FIELD	Date:	:0-97	1	L:10	ieu.	1:50	ampieo.		PURVIS
and LAB DATA	Concrete Truc		Ticket N			Size of Load (C.Y.	):	Weather Co	onditions:
DAIA	601			.1256		10	.,,	HAZY 8	
	Water Added A			.1250					r Authorized By:
	1		Yes	3 Ga	I. To	10	C.Y.	1	A ROCK
	Slump: (inche			perature (°F):		Concrete Temper		Wet Weight	
		/2"		4°		89°	, ,	N/A	
	Air Content (%			and Cured *1	lo ASTM			Tested to A	STM C-39
	N/A	- '	1		□No	□Unkno	own	∑ Ye	s □No
		oncrete Placen							
				STEM WAL	L				
				<u> </u>					
				WEST WAL	L, NO	RTHWEST COF	RNER.		
							<del></del>		
SET NO.	DATE RECEIVED	DATE TESTED	AGE (DAYS)	TEST SPECIF	1	TOTAL LOAD	TEST STRENGT		SPECIMEN WEIGHT
	IN LAB	105100	104101	DIAMETER (IN.)	AREA ISO IN	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)
									6
LDSB-8	6-23	6-27	7	6.00	28.2	7 129,500	4580	2	Chli
1		6-27	7	6.00	28.2		4420	3	CAB.
2		7-07	17	0.00	20.2	123,000	4420		C ,,
3		7-07	28		1				
4		7-18	28		1				
5		7-18	SP						
6		/-18	JF						
				<u> </u>	1		1 5 1	5	
REMARKS	: *Concrete Te	est Specimen	Cured	n Accorda	nce wit				in Laboratory
					<u> </u>	1 2	3	4 50	G 6767
						# 1 1:3\			
				•					
					Ū	Cone Cone-Sh	ear Shea	النباليا الـ r Spli	t Cone & Split
A5111 (9/91)						455	ABAANOAS	COCIATEO	1110
(5/5/)						ARD	AMAN & AS	SOCIATES,	INC.
Elorido Danier	ration No	Nº .	,		0	v.			
Florida Registr	auon no	11		<del></del>	0	y:			

Florida Registration N	10	<del></del>	ву:	
AS A MUTUAL PROTECTION	TO CLIENTS, THE PUBLIC AND OU	RSELVES, ALL REPORTS ARE SUE	BMITTED AS THE CONFIDENTIA	AL PROPERTY OF CLIENTS AND AUTHORIZATION FOF
PUBLICATION OF STATEMEN	TS, CONCLUSIONS OR EXTRACTS !	FROM OR REGARDING OUR REPO	DRTS IS RESERVED PENDING O	DUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			. (	CC.					DATE:	
Project Project Lo Project Cont Concrete Su	cation: BART ractor: SEMC	DLAW DRUM COW AIR B. CO CONSTRI RIDA ROCK	ASE UCTION		NG	VIROGROUP, INC. ATTN: JOHN BALE,				L	
DESIGN	Specified Stren	ath:			15	Slump (i	nches):		Air Conten	(percent):	
DESIGN DATA	1 '	9 ) p.s.i. @		28 d	lays		1/2" MA	х.	N/		
אוא	Mix Type:			,,,,,,							
	Norma	wt. 🔲 Ligh	tweight [	] Mortar Mix	G	unite [	Grout (	Other			
525217											
	∏Transit	Mixed:		Pump Mix						PUMP MIX	
FIELD	Date:		Time Co	ncrete Batch	ned:	Time Co	ncrete Sam	pled:	Sampled B	•	
and LAB	6-20	97	] 1	:10			:50			PURVIS	
DATA	Concrete Truck	No.:	Ticket N	0.:	. 5	Size of L	.oad (C.Y.):		Weather C	onditions:	
	6011		1	1256		1	.0		HAZY 8		
	Water Added At	Job Site:							1	r Authorized By:	
		□ No II	Yes	3 Ga			.0	C.Y.		DA ROCK	
	Slump: (inches)	:		erature (°F):		Concrete	e Temperatu	ıre (°F):	Wet Weigh		
	6 1/	′2"	94° 89°					N/2	1		
	Air Content (% t	oy Vol.):		and Cured * 1	to ASTM				Tested to A		
	N/A			Yes	□No		Unknow	n	☑ Ye	s 🔲 No	
	Location of Co	ncrete Placer		STEM WAL	.L						
				WEST WAL	L, NO	RTHWE	ST CORN	ER.	·····-		
	DATE	DATE	AGE	TEST SPECI	MEN SIZE		TOTAL LOAD	TEST STRENGTH	TYPE:	SPECIMEN WEIGHT	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ II	Nj	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)	
LDSB-8	6-23									all.	
1		6-27	7	6.00			9,500	4580	3	OPP	
2		6-27	7	6.00	28.2		5,000	4420	3		
3		7-07	17	6.00	28.2	7 14	2,500	5040	2	(peus)	
4		7-18	28								
5		7-18	28							1	
6		7-18	SP								
REMARKS	: *Concrete Tes	st Specime	n Cured i	n Accorda	nce wit	th AST 1	M C-31 Af 2	ter Being 3	Received 4	in Laboratory 5	
,						Cone	Cone-Shear	Shea	r Spl	t Cone & Split	
5111 (0/01)				<u> </u>		-			i	<u></u>	
5111 (9/91)		•					ARDA	MAN & AS	SSOCIATES	, INC.	
orida Registi	ration No	<u>10</u> .		•	Ε	Зу:					

Florida Registration No.	·	Ву:	
AS A MUTUAL PROTECTION TO CLIENTS, THE PU	IBLIC AND OURSELVES, ALL REPORTS	ARE SUBMITTED AS THE CONFIDENTIAL	PROPERTY OF CLIENTS AND AUTHORIZATION FOR R WRITTEN APPROVAL.
PUBLICATION OF STATEMENTS, CONCLUSIONS O	OR EXTRACTS FROM OR REGARDING O	UR REPORTS IS RESERVED PENDING OU	



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			(	CC.					DATE:	
Project I Project Loc Project Cont Concrete Su	cation: BA: ractor: SEI	IDLAW DRUM RTOW AIR BA MCO CONSTRU ORIDA ROCK	SE CTION		NG		VIROGRO		C. LE, P.E.		
DESIGN DATA 525217	Specified Strength:  4000 p.s.i. @ 28 days 6 1/2" MAX. N/A  Mix Type:  Normal wt. Lightweight Mortar Mix Gunite Grout Other										
FIELD and LAB DATA	☑ Transit Mixed:       ☐ Pump Mix       Other PEA ROCK, PUMP M         Date:       Time Concrete Batched:       Time Concrete Sampled:       Sampled By:         6-20-97       1:10       1:50       JOHNNY PURVI         Concrete Truck No.:       Ticket No.:       Size of Load (C.Y.):       Weather Conditions:         6011       11256       10       HAZY & HOT         Water Added At Job Site:       Extra Water Authoriz										
	Air Content (9	No If Ps): 1/2" % by Vol.):	Molded a	erature (°F): 4° and Cured * t Yes	3 Gal. To 10 C.Y. FLC rature (°F): Concrete Temperature (°F): Wet W 89°  Ind Cured * to ASTM C-31 Tested			FLORII Wet Weigh	DA ROCK t (P.C.F.): A ASTM C-39		
	DATE	DATE	AGE	WEST WAL		RTHWE	EST CORN	TEST	TYPE	SPECIMEN	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN	0	LOAD (LBS)	STRENGTH (PSI)	f OF FRAC	WEIGHT (AIR DRY-LBS)	
LDSB-8 1 2 3 4 5	6-23	6-27 6-27 7-07 7-18 7-18 7-18	7 7 17 28 28 SP	6.00 6.00 6.00 6.00	28.2 28.2 28.2 28.2 28.2	7 12 7 14 7 15	29,500 25,000 2,500 7,000 9,000	4580 4420 5040 5550 5620	3 3 2 3 3	CAG CAG CAG	
REMARKS	: *Concrete 1	Test Specimen	Cured i	n Accorda		th AST	M C-31 Af 2 Cone-Shear	3		in Laboratory 5 Cone & Split	

FORK SOI DESTRIS FORM

Florida Registration No.

P. 41986

ARDAMAN & ASSOCIATES, INC.

Jan 7/18/9)



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.:

97-9036/B



# CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

**DATE**: 6-20-97

PROJECT LOCATION:

BARTOW

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

	LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)	
Ŀ	1	LOAD WAS	TESTED - CY	LINDERS M	DLDED, S	ET #7.				
	2	3505	11250	10:55	12:00	10	10	4 & 6 1/2	N/A N/A	
-	3	6011	11251	11:40	12:45	0	10	6	N/A	4
	4	3505	11254	12:55	- 1:32	0	10	6 1/2	N/A	1
	5	LOAD WAS	TESTED - CY	LINDERS M	OLDED, S	ET #8.				
	6	8999	11260	2:22	3:15	6	10	4 3/4&6½	N/A	1
					<u>-</u>					
					-					
}										
ŀ										
1										
1										
Ä.								1		

FLORIDA REGISTRATION NO.	ВҮ	



1525 Centennial Drive Bartow, Florida 33830

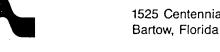


#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:		
Project Project Lo Project Conf Concrete Su	cation: I	LAIDLAW DRUM BARTOW SEMCO CONSTR FLORIDA ROCK	UCTION				VIROGROUP, INC. ATTN: MR. JOHN W. BALE, P.E. LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON					
DESIGN	Specified S	trength:			S	Slump (	inches):		Air Conten	t (percent):		
DATA	, .	1000 p.s.i. @		28 (	days		3 1/2"		N/A			
	Mix Type:											
	☑ Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other											
25602	Tro	nsit Mixed:		Pump Mix			(	Other 6	5" BOOM	DIIMD		
	Date:	ITSILIVIIXEG.		ncrete Batc	hed: IT	ime Co	oncrete Sam		Sampled B			
FIELD	1	7-21-97		:05	ileu.		9:35	pica.		Y PURVIS		
and LAB DATA	Concrete Tr		Ticket N		s		Load (C.Y.):		Weather C	onditions:		
DAIA	1	3875		754			10		P/C &	MILD		
	Water Adde	ed At Job Site:			<u>+</u>				Extra Wate	r Authorized By:		
	☐ Ye		Yes		al. To			C.Y.				
	Slump: (inc	hes):	Air Temp	erature (°F)	:  C	Concret	te Temperatu	ire (°F):	Wet Weigh	t (P.C.F.):		
	4 1/2"	/ 3 3/4"		88°			82°		N/A			
	Air Content	(% by Vol.):	Molded and Cured * to ASTM C-3			1 C-31			-	STM C-39		
		N/A	☐XYes ☐ No ☐ Unknow				n	∑ Ye	s No			
	Location of	Concrete Placem						•				
				25' WEST	r & 15	' SO	UTH OF					
				NO DOLLED O	מרט שב	משואו	OF BUILD	TNC				
				NORTHEAS	ST COR	MER '	OL BOILD	TING.				
				[FLOOR S	SLAB]							
	DATE	DATE	AGE	TEST SPEC	MEN SIZE		TOTAL	TEST	TYPE	SPECIMEN WEIGHT		
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ/IN	۷)	LOAD (LBS)	STRENGTH (PSI)	H OF FRAC	(AIR DRY · LBS)		
11000	7 22									.1		
LLSB-9	7-22	7-28	7	6.00	28.27	, 1	33,000	4700	2	CAPO		
1		7-28	7	6.00	28.27	1	36,000	4810	3	340		
2		8-11	28	0.00	20.2.	1 ~	30,000					
3		8-11	28									
4		8-11	SP									
6		8-11	SP									
°												
DEMARKS	. *Concret	Test Specimen	Curca:	n Accorda	nco wit	h AST	FM C-31 A4	ter Reins	Received	in Laboratory		
UCMNWV9	. Concrete	s rear aheomien	Juieu I	ii Accorda	mice Wil	A.J.I	1 IVI C-31 AI	3	, neceiveu 4	5		
* SAM.	PLED FRO	M HOSE.										
1					Ü	Cone	Cone-Shear	U /∟ Shea	لناليا از r Spl	it Cone & Split		
A5111 (9/91)		·		<u> </u>					<del></del>			
(0.01)							AHDA	MAN & AS	SOCIATES	, INC.		

lorida Registration NoB	3y:
-------------------------	-----

1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:	······································		·····	CC.				<del> </del>	DATE:			
Project Project Lo Project Con Concrete Si	ocation: BA tractor: SE	IDLAW DRUM RTOW MCO CONSTR ORIDA ROCK	UCTION	-	DING	VIROGROUP, INC. ATTN: MR. JOHN W. BALE, P.E. LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON							
DESIGN	Specified Stre	ngth:		(inches):		Air Conte	nt (percent):						
DATA	40	00 p.s.i. @		28	days		3 1/2"		N/I	., .			
	Mix Type:												
	Norm     Norm     Norm     Norm     Norm     Norm	al wt. 🔲 Light	weight	☐ Mortar M	ix □G	unite	Grout	Other					
25602	☑ Transit Mixed: □ Pump Mix Other 6" BOOM PUMP												
	Date:	it wince.		oncrete Bate	abod: I	Time C	oncrete San						
FIELD and LAB	!	21-97		):05	nea.		9:35	npiea:	Sampled	By: NY PURVIS			
DATA	Concrete Truck		Ticket N				Load (C.Y.):		<del></del>	Conditions:			
DAIA	88			.754		0126 01	10			& MILD			
	Water Added A		L	. 7 3 4			10			er Authorized By:			
	☐ Yes		Yes	G	al. To			C.Y.	1	ci ridinonzed by.			
	Slump: (inches			perature (°F		Concre	te Temperat		Wet Weigl	nt (P.C.F.):			
	4 1/2" /	*		88° `	´		82°	( - ,-	N/Z	· · · · · · · · · · · · · · · · · · ·			
	Air Content (%	by Vol.):	Molded and Cured * to ASTI						Tested to ASTM C-39				
	N/2	A	[]≵Yes ☐ No				Unknow	'n	[X Y				
	Location of Co	oncrete Placem	ent:						·				
				25 WES	T & 15	5' SO	UTH OF						
					-								
			· · · · · -	NORTHEA	ST COF	RNER	OF BUILD	ING.					
				[FLOOR :	SLAB]								
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPEC			TOTAL	TEST	TYPE	SPECIMEN			
SET NO.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO II	N <sub>I</sub>	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)			
LLSB-9	7-22							<del></del>		1			
	1-22	7-28	7	6 00	28.27	, ,	22.000	4700		BBB			
1		7-28	7	6.00	28.27		33,000 36,000	4700 4810	2 3	1346			
2		7-28 8-11	28	6.00	28.27		55,000	5480	3	347			
3		8-11	28	6.00	28.27	1	60,000	5660	3	745			
. 4		8-11	SP	0.00	20.27		00,000	3000					
6		8-11	SP										
6		0 11	51										
REMARKS:	*Concrete Te	st Specimen	Cured in	l n Accorda	nce wit	h AST	M C-31 Af	ter Being	Received	in Laboratory			
						1	2	3	4	5			
SAME	TED : ROM :	ED FROM HOSE.  Cone Cone-Shear Shear Split Cone & Split											
5111 (9/91)	~ <u>-</u> ~								SOCIAŢES				
Tlavida Desiri	-A: A1-	U199C					PI		1/1	1 8 / /6-			

1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

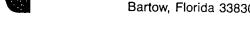
	TO:			•	CC.					DATE:
Project I Project Loo Project Conti Concrete Su	cation: BA ractor: SE	IDLAW DRUM RTOW MCO CONSTR ORIDA ROCK	UCTION		DING VIROGROUP, INC. ATTN: MR. JOHN W. BALE, P.E. LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON					
5501011	Specified Stre	angth:			Slump (inches):				Air Conten	t (percent):
DESIGN DATA	1 '	00 p.s.i. @		28 0	7	J.Gp (	3 1/2"		N/	
DATA	Mix Type:	00 p.s.i. @			24/5		<u> </u>			
		al wt. Light	veight [	☐ Mortar Mix	k ∏G	unite	☐ Grout	Other		
25602	41,110			<u> </u>			<del></del>		•	
23002	X Trans	sit Mixed:		Pump Mix			•	Other 6	" BOOM	PUMP
FIELD	Date:		Time Co	ncrete Batcl	ned:	Time C	oncrete Sam	pled:	Sampled B	y:
and LAB	7-	21-97	9	:42		1	0:15		JOHNN	Y PURVIS
DATA	Concrete Truc		Ticket N	0.:		Size of	Load (C.Y.):		Weather C	onditions:
	66	11	11	755			10		P/C &	HOT
1	Water Added	At Job Site:							Extra Wate	r Authorized By:
	☐ Yes	No If	Yes		ıl. To			C.Y.		
	Slump: (inche	s):		erature (°F):	: (	Concre	te Temperati	ure (°F):	Wet Weigh	t (P.C.F.):
	6_	1/2" *		90°			85°		N/	
	Air Content (%	6 by Vol.):	Molded and Cured * to AST						Tested to A	
	N/			Yes	□No	Unknown				s 🗌 No
	Location of C	oncrete Placem	ent:							
			4	5' WEST	& 15'	SOU'	TH OF			
			N <sub>1</sub>	ORTHEAST	CORN	ER O	F BUILDI	NG.		
			ί.	FLOOR SI	ARÌ					
	DATE	DATE	AGE	TEST SPECI		1	TOTAL	TEST	TYPE	SPECIMEN
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ:1	Ni	LOAD (LBS)	STRENGTH (PSI)	I OF FRAC	WEIGHT (AIR DRY - LBS)
**	INCAB				1	+	-(200)	(, 0,1	11,,,,0	(///// 2007
LDSB-10	7-22									all
1		7-28	7	1	28.27	1	39,500	4930	2	CAD
2		7-28	7	6.00	28.27	1	39,000	4920	3	(11)
3		8-11	28							
4		8-11	28							
5	1	8-11	SP							
6		8-11	SP	:		-				•
			1							
REMARKS:	*Concrete T	est Specimen	Cured i	n Accorda	nce wi	th AST	rM C-31 Af	ter Being	Received	in Laboratory
+ ==		n				1	2	3	4	5
· `TR	RUCK SENT	BACK.								
	•				ن ،	ك لنيار Cone	Cone-Shear	Shear	Spli	t Cone & Split
A5111 (9/91)	1317						ADDA	MAN & AC	SOCIATES	INC
							ARDA	AII & A3	COUNTES	, 1110.

0.9-74 THIS FORM CONFORMS TO ASTM-C39

Florida Registration No.	Ву:
AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUPUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REP	IBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830





## COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	Í	TO:				CC						
						CC.				DATE:		
	Project Project Lo Project Con Concrete S	ocation: Entractor: S	BARTOW SEMCO CONS	TRUCTIC	STORAGE BUILDING VIROGROUP, INC ATTN: MR. JOHN JCTION LAIDLAW ENVIRO INDUSTRIES ATTN: DENNIS W. BOYD ROB					N W. BALE, P.E. DNMENTAL SERVIGES VALTON		
	DESIGN	Specified St	renath:				Slump (inches):	<del></del>	T.: .			
	DATA	1	000 p.s.i. @		28	days	3 1/2"		1	ent (percent):		
		Mix Type:	F. S. G.			days	3 1/2		N	I/A		
		⊠ Nor	mal wt. 🔲 Lig	htweight	☐ Mortar N	dix ∏G	unite Grout	Other				
	25602											
			nsit Mixed:		] Pump Mix				б" воом	PUMP		
ı	FIELD	Date:		i	oncrete Ba	tched:	Time Concrete Sa	mpled:	Sampled	By:		
- 1	and LAB DATA		-21-97		9:42		10:15		JOHN	NY PURVIS		
-	DATA	Concrete Tru		Ticket I		;	Size of Load (C.Y.)	:	Weather	Conditions:		
1			611 At Job Site:	1. 1.	1755		10			& HOT		
N		☐ Yes		If Yes	C	al. To				ter Authorized By:		
		Slump: (inch			perature (°F		Concrete Tempera	C.Y.	<u></u>			
'		1	1/2" *		90°	<i>'</i> .	85°	ture (°F):	Wet Weight (P.C.F.):			
١		Air Content (		Molded	and Cured	* to ASTN	1 C-31		N/A Tested to ASTM C-39			
ł		N/			Yes	□No	Unknov	vn	∑ Yes			
1		Location of (	Concrete Place	ment:					(2)	00 1140		
١					5' WEST	& 15'	SOUTH OF	•				
ı												
ł					ORTHEAS	T CORN	NER OF BUILDING.					
ı				ſ	FLOOR S	ומוד						
Γ	SET NO.	DATE	DATE	AGE	TEST SPEC		TOTAL	TEST	TYPE SPECIMEN			
-	SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)		- LOAD	STRENGTH (PSI)	OF FRAC	SPECIMEN WEIGHT (AIR DRY+LBS)		
1	LDSB-10	7-22							Trine	(AIR DAY - LBS)		
İ	1	1 22	7-28	7	6.00	28.27	130 500	4020		nh		
1	2		7-28	7	6.00	28.27	139,500	4930	2	Ork 1		
,	3		8-11	28	6.00	28.27	168,000	4920 5940	3	Brok.		
	4		8-11	28	6.00	28.27	172,000	6080	2 3	94		
	5		8-11	SP			172,000	0000	3	0.0		
	6		8-11	SP								
L												
Г	REMARKS:	Concrete Te	est Specimen	Curedin	Accorda	nco with	ACTM C 24 A4	- D : .		in Laboratory		
ı				· ourcu ii	Accorda	TICE WILL	1 2		Received	in Laboratory		
	* TRU	JCK SENT	BACK.			U.Z	7/3 N	3				
A51	11 (9/91)	·	<del></del>		-		ne Cone-Shear	Shear	Spli			
	·						ARDAN	1417& ASS	ocia#es,	INC. / /		
Flo	orida Registrat	ion No	41980	1		Bv:	· ///(0X	Sus 1	M.	( 9/1/97		

D-9-74 THIS FORM CONFORMS TO ASTM



FILE NO.: 97-9036/B





#### **CONCRETE DATA RECORD**

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDINGS

DATE:

7-21-97

PROJECT LOCATION:

SEMCO CONSTRUCTION

BARTOW

PROJECT CONTRACTOR:

FLORIDA ROCK INDUSTRIES

CONCRETE SUPPLIER:

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	8999	11753	8:23	9:18	10	10	2 3/4*# 4	N/A
2	LOAD WAS	TESTED - C	LINDERS 1	OLDED,	SET #9.		· · · · · · · · · · · · · · · · · · ·	
3	LOAD WAS	TESTED - C	LINDERS 1	OLDED,	SET #10.			
4	8875 .	11757	10:33	11:18	. 0	10	4 3/4 *	N/A
<u> </u>								
**	ADDED 10 G	ALLONS AFTE	R 1ST SLU	MP.				
*	OUT OF PUM	P HOSE.						

•	•
LORIDA REGISTRATION NO.	8Y
	ALTHORIS

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZED FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

<u> </u>									
	TO:			. (	CC.				DATE:
Project I Project Loc Project Cont	cation: BART	LAW DRUM SOW AIR BASON CONSTRUC	SE	E BUILDI	NG	LAIDLAW I		ON	RVICES
Concrete Su		IDA ROCK I		RIES		VIROGROU			
	r L LOI	TDII ROCK 3		. (ILDO		ATTN: JOI		P.E.	
	,								
DESIGN	Specified Strer	-				lump (inches):		Air Conten	t (percent):
DATA	4000	p.s.i. @		28 c	ays	5"		N/A	
	Mix Type:  Norma	HOSE,	50' LONG						
525217		Mixed:		Pump Mix			Other P.	R.P.M.	
FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Concrete S	ampled:	Sampled B	
and LAB	8-12			9:42		10:29		I	NY PURVIS
DATA	Concrete Truck		Ticket N		S	ize of Load (C.)	c.):	Weather Co	
	8999			12072		10		P/C 8	Σ НОТ r Authorized By:
	Water Added A		Yes	9 Ga	L To	10	C.Y.		i Adiilolized by.
	Slump: (inches			erature (°F):		oncrete Temper		Wet Weight (P.C.F.):	
	4 1/	•	92°			88°		N/A	. (
	Air Content (%	by Vol.):		and Cured * 1	o ASTM		••	Tested to A	STM C-39
	N/A		χ	Yes	□No	Unkn	own	∑ Ye	s 🔲 No
	Location of Co	ncrete Placem	ent:						
				30' NORT	H OF S	SOUTHWEST			
			,	CORNER O	ודוום ה	DING.			
				COMMUNIC O	1 1011	BEING			·
			:	STEM WAL	L.				
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECIA	MEN SIZE	TOTAL	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT
321110.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ:1N)	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)
LDSB-11	8-13								21R
1		8-19	7	6.00	28.27	131,500	4650	3	G50
2		8-19	7	6.00	28.27	132,000	4670	3	(NO)
3		9-09	28						
4		9-09	28						
5		9-09	SP						
6		9-09	SP						
	L					<u> </u>			
REMARKS:	*Concrete Te	st Specimen	Cured ii	n Accordai	nce with		_	Received	in Laboratory
					0.4	1 2	3	4 1 EC	u (c)(c)
						Y: \ \\		(1   ))	
							$\mathbb{V}$		
					c	one Cone-Sh	ear Shear	. Spli	t Cone & Split
<b>45111</b> (9/91)						ARE	DAMAN & AS	SOCIATES,	INC.

FORM 1001 D-9-74 THIS FORM CONFORMS TO ASTM-C39

lorida Registration No.	B	y:	 	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

Project Name: LAIDLAW DRUM STORAGE BUILDING Project Location: BARTOW AIR BASE ATTN: DENNIS WALTON BOYD ROBERTSON  Project Contractor: SEMCO CONSTRUCTION BOYD ROBERTSON  Concrete Supplier: FLORIDA ROCK INDUSTRIES VIROGROUP, INC. ATTN: JOHN BALE, P.E.  DESIGN DATA    Specified Strength:   Slump (inches):   Air Content (percent): N/A
DATA         4000 p.s.i. @ 28 days 5" N/A           Mix Type:
DATA         4000 p.s.i. @ 28 days 5" N/A           Mix Type:
Mix Type:
Normal wt.   Lightweight   Mortar Mix   Gunite   Grout Other 2" HOSE, 50' LONG
Transit Mixed:
And LAB DATA         8-12-97         9:42         10:29         JOHNNY PURVIS           Concrete Truck No.:         Ticket No.:         Size of Load (C.Y.):         Weather Conditions:         P/C & HOT           Water Added At Job Site:         Extra Water Authorized By:           ☑ Yes         No         If Yes         9 Gal. To         10         C.Y.           Slump: (inches):         Air Temperature (°F):         Concrete Temperature (°F):         Wet Weight (P.C.F.):           A 1/2"         92°         88°         N/A           Air Content (% by Vol.):         Molded and Cured * to ASTM C-31         Tested to ASTM C-39           N/A         X Yes         No         Unknown         X Yes         No
and LAB DATA       8-12-97       9:42       10:29       JOHNNY PURVIS         Concrete Truck No.:       Ticket No.:       Size of Load (C.Y.):       Weather Conditions:         8999       12072       10       P/C & HOT         Water Added At Job Site:       Extra Water Authorized By:         Slump: (inches):       Air Temperature (°F):       Concrete Temperature (°F):       Wet Weight (P.C.F.):         4 1/2"       92°       88°       N/A         Air Content (% by Vol.):       Molded and Cured * to ASTM C-31       Tested to ASTM C-39         N/A       Yes       No       Unknown       Yes       No
DATA         Concrete Truck No.:         Ticket No.:         Size of Load (C.Y.):         Weather Conditions:         P/C & HOT           8999         12072         10         Extra Water Authorized By:           Water Authorized By:           Slump: (inches):         Air Temperature (°F):         Concrete Temperature (°F):         Wet Weight (P.C.F.):           4 1/2"         92°         88°         N/A           Air Content (% by Vol.):         Molded and Cured * to ASTM C-31         Tested to ASTM C-39           N/A         X Yes         Unknown         X Yes         D No
Water Added At Job Site:
☑ Yes         ☐ No         If Yes         9 Gal. To         10         C.Y.           Slump: (inches):         Air Temperature (°F):         Concrete Temperature (°F):         Wet Weight (P.C.F.):           4 1/2"         92°         88°         N/A           Air Content (% by Vol.):         Molded and Cured * to ASTM C-31         Tested to ASTM C-39           N/A         Yes         No         Unknown         Yes         No
Slump: (inches):  4 1/2"  92°  88°  N/A  Air Temperature (°F):  92°  Molded and Cured * to ASTM C-31  N/A  Yes  No  Wet Weight (P.C.F.):  N/A  Tested to ASTM C-39
4 1/2"         92°         88°         N/A           Air Content (% by Vol.):         Molded and Cured * to ASTM C-31         Tested to ASTM C-39           N/A         X☐ Yes         No         ☐ Unknown         ☒ Yes         ☐ No
Air Content (% by Vol.): Molded and Cured * to ASTM C-31 Tested to ASTM C-39  N/A X Yes No Unknown X Yes No
N/A x☐Yes ☐No ☐Unknown ☒ Yes ☐ No
Location of Concrete Placement:
30' NORTH OF SOUTHWEST
CORNER OF BUILDING;
STEM WALL.
DATE DATE AGE TEST SPECIMEN SIZE TOTAL TEST TYPE SPECIMEN SET NO. RECEIVED TESTED (DAYS)  LOAD STRENGTH OF WEIGHT
SET NO. HECEIVED TESTED (DAYS) DIAMETER (IN.) AREA (SO:IN) (LBS) (PSI) FRAC (AIR DRY-LBS)
LDSB-11 8-13   ///
1 8-19 7 6.00 28.27 131,500 4650 3
8-19 7 6.00 28.27 132,000 4670 3
3   9-09   28   6.00   28.27   161,000   5690   2
9-09 28 6.00 28.27 164,500 5820 3 CAD
5 9-09 SP
6 9-09 SP
REMARKS: *Concrete Test Specimen Cured in Accordance with ASTM C-31 After Being Received in Laboratory  1 2 3 4 5
グムマーデータ はんぱ マンコー Cone Cone-Shear Shear Split Cone & Split

RM 1001 D-9-74 THIS FORM CONFORM

A5111 (9/91)

Florida Registration No. 41986

ARDAMAN & ASSOCIATES, INC.

By: //osney Man 4/10/9

1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO: CC. DATE:											
Project l Project Loc Project Cont Concrete Su	cation: BA ractor: SE	AIDLAW DRUM ARTOW AIR BA EMCO CONSTRU JORIDA ROCK	ASE JCTION		ING	LAIDLAW E ATTN: BOY DEN VIROGROUP ATTN: JOH	D ROBERTS NIS WALTO , INC.	ON ON	VICES			
DESIGN DATA	Mix Type:	000 p.s.i. @	veight [	Slump (inches):  28 days N/A  ht Mortar Mix Gunite Grout Other W			Other W/	Air Content (percent): N/A  /SUPERPLASTICIZER				
25606	6606 ☑ Transit Mixed: ☑ Pump Mix Other 6" BOOM PUMP								UMP			
FIELD and LAB DATA	Concrete True	-28-97 ck No.:	7 Ticket N	ncrete Batch : 48 o.: 92295		Time Concrete S 8:30 Size of Load (C.\) 9.0		Weather C	SKIPPER conditions: WARM			
	Water Added  [X] Yes Slump: (inche 6" Air Content (some of the content of the con	□ No If 'es):  * % by Vol.):	C.Y. rature (°F):	Extra Water Authorized By:  M.D.  Wet Weight (P.C.F.):  N/A  Tested to ASTM C-39  X Yes								
,					T COR	' WEST OF	LDING.					
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	TEST SPECIA DIAMETER (IN.)	AREA (SO IF	TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY - LBS)			
LL-12 1 2 3 4 5		9-04 9-14 9-25 9-25 9-25 9-25	7 7 28 28 SP SP	6.00 6.00	28.2	7 123,500	4370 4420	) 2	OSB CAB			
REMARKS:	*Concrete T	est Specimen	Cured in	n Accordar	nce wit	th ASTM C-31	After Being 3	Received	in Laboratory			
* SAM	PLED FROM	CHUTE OF T	RUCK.			Cone Cone-Sh		Spl	it Cone & Split			
·5111 (9/91)												

FORM 10.

ARDAMAN & ASSOCIATES, INC.

	•
Florida Registration No.	Rv:
Tionda registration 140.	Oy



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:	
Project I Project Loo Project Cont Concrete Su	cation: BAI ractor: SEN	DLAW DRUM RTOW AIR BA ICO CONSTRI DRIDA ROCK	ASE JCTION	·	ING	ATTN VIRO	DLAW ENV N: BOYD DENNI DGROUP, N: JOHN	ROBERTS S WALTO INC.	ON ON	/ICES	
DESIGN	Specified Stree	ngth:		······	5	Slump (	inches):	Air Content (percent):			
DATA		00 p.s.i. @		28 c	lays		N/A		N/A		
	Mix Type:	alwt. 🔲 Lightv	voight [	∃ Mortar Mix	, Пе	ınita	□ Grout 1	Other W/	CHERRET	ASTICIZER	
25606	K NOTH	arwicignit	veigrit [	_ IVIOI LAI IVII)	<u> </u>	unite	Glout	Other W/	SUPERPLA	ASTICIZER	
		t Mixed:	X	Pump Mix			(	Other 6"	BOOM P	JMP	
FIELD	Date:			ncrete Batch	ned: T	Time Co	oncrete Sam	pled:	Sampled B	•	
and LAB		28-97		: 48		2:	8:30			SKIPPER	
DATA	Concrete Truck 887		Ticket No	o.: 92295		Size of I	Load (C.Y.): 9.0		Weather C	•	
	Water Added A		1 1:	72293			9.0	-	<u> </u>	r Authorized By:	
			Yes	18 Ga	I. To	9.0 C.Y			l	· i	
	Slump: (inches	s):	Air Temp	erature (°F):	: [0	Concrete Temperature (°F):			Wet Weight (P.C.F.):		
	6"	*	85°			88°			N/A		
-	Air Content (%	•	1	and Cured *		1 C-31			Tested to A	i	
	N/A	oncrete Placem		Yes	□No		Unknow	n :	X Ye	s No	
	Location of Co			4' SOUTH	& 78	' WES	ST OF	•			
			1	NORTHEAS	T COR	NER C	OF BUILD	ING.			
				[FLOOR S	LABI						
	DATE	DATE	AGE	TEST SPECIA			TOTAL	TEST	TYPE	SPECIMEN	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO:IN	V)	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)	
LL-12			:							0	
1		9-04	7	6.00	28.2	7 12	23,500	4370	2	BB 1	
2		9-14	7	6.00	28.2	L	25,000	4420		CALL	
3		9-25	28	6.00	28.2		15,250	5140	2	CA32	
4		9-25	28	6.00	28.2	7 19	51,000	5340	2	CAD	
5		9-25	SP								
6		9-25	SP								
DEMARKO	*0		0 11		<u> </u>						
HEMARKS:	"Concrete le	st Specimen	Curea	1 Accorda	nce wit	1 AS I	M C-31 An	er Being 3	Heceivea	in Laboratory 5	
* SAM	PLED FROM	CHUTE OF T	RUCK.		<i>U</i> .	S7/1	N	<u>[</u> /	4 F)(-)	ന ത്ത 📗	
			,								
A5111 (9/91)	***************************************					Cone	Cone-Shear		` ,		
₩ (3131)							AROAL	MAN& AS	SOCIATE\$	INC. / / /	

FORM 1001 D-9-74 THIS FORM CONFORMS TO ASTM-C39

Florida Registration No.

August 28, 1997 File Number: 97-51-9036A

Geotechnical, Environmental and Materials Consultants

FAX: (803) 957-6270

Mr. Mike Clough Virogroup, Inc. 1445 Pisgah Church Road Lexington, SC 29072

Subject: Concrete Testing @ Laidlaw's Drum Storage Building, Bartow, Florida

Dear Mr. Clough;

Ardaman & Associates, Inc. performed concrete testing at the subject project during today's pour. Specifically, slump tests were performed on each load at the plant, prior to the addition of Daracem 100 (superplasticizer), and at the job site, after this addition and water, if any, was added. One set of cylinders was cast after the first load. The concrete temperature was also taken on the first load. The slump and temperature measurements are tabulated below:

LOAD NO.	TRUCK NO.	CONTROL NO.	TIME BATCHED	TIME POURED	WATER ADDED AT SITE (gal)	CUBIC YARDS CONCRETE	SLUMP (ins) PLANT / SITE	TEMP (°F)
*1	8875	192295	7:48	8:55	18	9	1/2" / 6"	88°
2	8999	192298	8:35	9:34	5	9	1/2" / 7-1/4"	
3	3505	192300	9:25	10:16	5	9	1-3/4" / 7"	_
4	8875	192302	9:58	10:47	0	9	2" / 7-3/4"	

<sup>\*</sup> Test Load

It has been a pleasure assisting you with this phase of your project. If there are any questions or when we may be of further assistance, please contact the undersigned at (941) 533-0858.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

P. Rodney Mank, P.E.

Project Engineer

Florida Registration No. 41986

PPM/CAB:tc B1TREPORTS\97-9036A.ctr



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830

(813) 533-0858

FILE NO.: 97-9036/B





#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

DATE:

8-28-97

PROJECT LOCATION:

BARTOW

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	LOAD WAS	TESTED - CY	LINDERS N	OLDED, S	ET #12.			
2	8999	192298	8:35	9:34	5	9 / 18	7 1/4	N/A
3	3505	192300	9:25	10:16	. 5	9 / 27	7	N/A
4	8875	192302	9:58	10:47	0	9 / 36	7 3/4	N/A
								_
						·		
						·		

FLORIDA REGISTRATION NO.	BY	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.	DATE:			
Project Project Lo Project Con Concrete S	tractor:	LAIDLAW DRUM BARTOW AIR B SEMCO CONSTR FLORIDA ROCK	ASE UCTION		DING	LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON VIROGROUP, INC. ATTN: JOHN BALE, P.E.			
DESIGN	Specified	Strength:			İs	lump (inches):		Air Conten	t (percent):
DATA	'	4000 p.s.i. @		28 0	days	7½" MAX		N/	
	Mix Type:				d1			<u></u>	
	⊠ N	ormal wt. Light	weight [	Mortar Mix	k ∏Gu	nite Grout	Other		
				Duna Min			045		
	<del>-</del>	ransit Mixed:		Pump Mix	. 1==		Other	T2	
FIELD	Date:	0 00 07		ncrete Batch	ned: T	ime Concrete San	npled:	Sampled E	
and LAB	0	8-29-97	+	: 55		8:40	<del></del>	C.A.	
DATA	Concrete	Truck No.:	Ticket N		3	ize of Load (C.Y.):		Weather C	
	Mater Ade	5 led At Job Site:	1 1	2306		9			& WARM er Authorized By:
	VValer ∧uc		Yes	Ga	I. To		C.Y.	1	a Additionized by.
	Slump: (in			perature (°F):		oncrete Temperati		Wet Weigh	t (PC F):
		7"		3°		85°	( . ).	True true	. ( , .
	Air Conter	nt (% by Vol.):	1	and Cured *	to ASTM			Tested to A	STM C-39
	•	N/A	[X]	Yes	□No	Unknow	n	X Ye	s □No
	Location of	of Concrete Placem	nent:			•			
				FLOOR SL	AB				,
			1	NORTHEAS	T & SC	UTHWEST			
			(	QUADRANT	S OF C	ELL O.			
057.110	DATE	DATE	AGE	TEST SPECI		TOTAL	TEST	TYPE	SPECIMEN
SET NO.	RECEIVEI IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO.IN)	LOAD (LBS)	STRENGTI (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)
LDS-13									DAR
1		9-05	7	6.00	28.27	1 1	4700		CAT
2		9-05	7	6.00	28.27	137,750	4870	) 5	CAD
3		9-12	14	j					
4		9-26	28						
5		9-26	28						
6		9-26	SP						
			l						·
REMARKS	: *Concret	e Test Specimen	Cured in	n Accordai	nce with	n ASTM C-31 Af 1          2	ter Being 3	Received ر 4	in Laboratory 5
						One Cone-Shear	Shear	Spli	t Cone & Split
5111 (9/91)						<u> </u>		<u>`</u>	
•						AHDAI	MAN & AS	SOCIATES,	INC.
Florida Registr	ration No				Ву	,.			

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.				-	DATE:	
Project Project Con Project Con Concrete S	tractor:	LAIDLAW DRUM BARTOW AIR E SEMCO CONSTE FLORIDA ROCK	BASE RUCTION		ING	TTA VIF	ON: DENN BOYD ROGROUP,	TIS WALT ROBERT	rson	RVICES	
						ΓΤΑ	N: JOHN	BALE,	P.E.		
DESIGN	Specified	-			S		nches):		Air Conter	nt (percent):	
DATA	Mix Type:	4000 p.s.i. @		28 c	days		7½" MAX	•	N/	A	
		lormal wt. Light	Other								
					k ∏Gu		_] Grout				
		ransit Mixed:		Pump Mix		0 -		Other	lo		
FIELD	Date:	8-29-97	1	ncrete Batcl : 55	nea:   I		ncrete San 3 : 40	ipled:	Sampled I	· =	
and LAB DATA	Concrete	8-29-97 Truck No.:	Ticket N				oad (C.Y.):		C.A. Weather C		
DAIA	Concrete	5	1	2306	١٥	120 01 0	9			& WARM	
•	Water Add	ded At Job Site:	1 1	2300						er Authorized By	
	□ Y		Yes	Ga	l. To			C.Y.	1	or realismed by	
	Slump: (in			perature (°F):		oncret	e Temperati		Wet Weigh	nt (P.C.E):	
		7"	1	3°			85°			(,.	
	Air Conter	nt (% by Vol.):	_ 1	and Cured *	to ASTM	C-31			Tested to ASTM C-39		
	i	N/A		Yes	□No		Unknow	n	I ∑ Ye	es 🗆 No	
		of Concrete Placer									
				FLOOR SL	AB						
				NORTHEAS	T & SC	OUTHW	EST				
				QUADRANT	S OF C	CELL					
SET NO.	DATE RECEIVE IN LAB	D DATE TESTED	AGE (DAYS)	DIAMETER (IN.)	MEN SIZE	-	TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY · LBS)	
										0	
LDS-13		0.05	,	6.00		, ,	22 750	4700		PAB	
1		9-05 9-05	7 7	6.00	28.27		32,750	4700	E	ask	
2		9-03	14	6.00	28.27 28.27	1	37,750 45,750	4870 5150	1	1240	
3		9-12	28	0.00	20.27	1	43,730	2130	2		
4		9-26	28								
5		9-26	SP								
6		9-20	J.F								
REMARKS	: *Concre	te Test Specimer	Cured i	n Accorda	nce with	h AST	M C-31 Af	ter Being	Received	in Laboratory	
					-	1	2	3	4	5	
						<b>V</b>		1 1/1	( [ )		
						) <u> </u>					
					1./	$\Lambda$		//·	1 111		
					C.	one	لا لاستاء كا Cone-Shear	U/L Shear	تا لالنا Spl	it Cone & Spli	
111 (9/91)							ARDAI	MAN & AS	SOCIATES	· · · · · · · · · · · · · · · · · · ·	
							AIIDAI	Ait a A3	COUNTES	, 1110.	
orida Registi	ration No				Ву	<b>/</b> :				•	

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS. CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

•	TO:				CC.					DATE:	
Project Project Lor Project Cont Concrete Su	cation: BA ractor: SE	IDLAW DRUM RTOW AIR B MCO CONSTRI ORIDA ROCK	ASE UCTION		ING	ATTN VIRO	: DENN BOYD GROUP,	IS WALT	rson	RVICES	
DESIGN	Specified Stre	_			1	Slump (inc			Air Conten		
DATA	4000 p.s.i. @ 28 days 7½" MAX. N/A Mix Type:										
		al wt. ☐ Lightv	veight [	☐ Mortar Mix	⟨ □ Gu	unite 🔲	Grout	Other			
		it Mixed:		Pump Mix				Other			
FIELD	Date:		ŧ	ncrete Batch	ned: T	Time Cond		npled:	Sampled B	y:	
and LAB		29-97		: 55		8:-			C.A.		
DATA	Concrete Truc 5	K NO.:	Ticket N	o.: 2306	٥	Size of Loa	30 (C. Y.): 9		Weather C		
	Water Added A	At Job Site:	1	2300			_9			& WARM r Authorized By:	
	☐ Yes		Yes	Ga	I. To			C.Y.		. ,	
	Slump: (inche	s):	Air Temp	erature (°F):	C	Concrete T	emperati	ıre (°F):	Wet Weigh	(P.C.F.):	
	7"		8.				85°				
	Air Content (%			and Cured *					Tested to A		
	N/A	oncrete Placem		Yes	□ No	L	] Unknow	n	X Ye	s 🗍 No	
	Location of C	oncrete Flacem	•	FLOOR SL	N D						
				LOOK SL	MD						
			1	ORTHEAS	T & S(	OUTHWE	ST			i	
			(	QUADRANT	S OF (	CELL Q	•				
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECIA		то	TAL DAD	TEST STRENGTH	TYPE OF	SPECIMEN	
<b>32</b> 1113.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO:IN		BS)	(PSI)	FRAC	WEIGHT (AIR DRY - LBS)	
LDS-13										1.0	
1		9-05	7	6.00	28.27	7 132	2,750	4700	2	CAR	
2		9-05	7	6.00	28.27	<b>I</b>	7,750	4870	i	CAGO	
3		9-12	14	6.00	28.27	1	5,750	5150	2	and I	
4		9-26	28	6.00	28.27	1	2,500	5750	2	CAR !	
5		9-26	28	6.00	28.27	7 161	,000	5690	3	CAN	
· 6		9-26	SP								
DEMARKS	*Conoroto To	ot Cnopimon	Cad i			- AOT14	0.04.46	. 5 .	5		
NEWARKS.	Concrete le	st Specimen	Curea II	1 Accordar	ice witi	n ASIM 1	C-31 Aft	er Being 3	Heceived 4	in Laboratory	
						Cone C	one-Shear	Shear	Split	Cone & Split	
V5111 (9/91)							ARDA	AAN & AS	SOCIATES,	INC. /	

Florida Registration No.



Geotechnical, Environmental and Materials Consultants

FAX: (803) 957-6270

Mr. Mike Clough Virogroup, Inc. 1445 Pisgah Church Road Lexington, SC 29072

Subject: C

Concrete Testing @ Laidlaw's Drum Storage Building, Bartow, Florida

Dear Mr. Clough,

Ardaman & Associates, Inc. performed concrete testing at the subject project during today's pour. Specifically, a slump test was performed on the first load at the plant, prior to the addition of Daracem 100 (superplasticizer). Slump tests were performed on each truck at the job site after water, if any, was added. The concrete temperature was also taken on each load. The slump and temperature measurements are tabulated below:

LOAD No.	TRUCK No.	TICKET No.	TIME BATCHED	TIME POURED	WATER ADDED AT SITE (GAL)	CUBIC YARDS CONCRETE	SLUMF PLANT	(INS) SITE	TEMP (°F)
1	4489	12303	7:30	8:40	10	9	0	5"	88
2*	NR	12306	7:55	8:40	0	9	NM	7"	85
3	5110	12307	8:35	9:15	4	9	NM	6-1/2"	86
4	4489	12309	8:55	9:45	5	9	NM	7-1/2"	86
5	5110	12313	9:48	10:20	0	6.5	NM	7-1/4"	90

\*One Set of test cylinders was cast on this load

NR = Not Recorded

NM = Not Measured

A unit weight test was performed on a sample of the concrete obtained from the second load. The result was 142 pounds per cubic foot (pcf).

It has been a pleasure assisting you with this phase of your project. If there are any questions or when we may be of further assistance, please contact the undersigned at (941) 533-0858.

Very truly yours,

ARDAMAN & ASSOCIATES, INC.

C. Alan Best

Technical Services Manager

P. Rodney Mank, P.E

Project Engineer /

Florida Registration No. 41986

PPM/CAB:krh B1T\REPORTS\97-9036A.ltr

cc: Ed Locke, Jr., Semco Construction, P.O. Box 706, Bartow, FL 33831 (Fax #941/533-3376)



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.: 97-9036/B





DATE:

#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

8-28-97

PROJECT LOCATION:

BARTOW

PROJECT CONTRACTOR:

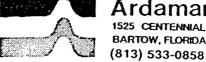
SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	LOAD WAS	TESTED - C	LINDERS N	OLDED, S	ET #12.		(e	
2	8999	192298	8:35	9:34	5	9 / 18	7 1/4	N/A
3	3505	192300	9:25	10:16	5	9 / 27	7	N/A
4	8875	192302	9:58	10:47	0	9 / 36	7 3/4	N/A
	Notis:	Slumps at	Concret	e Plan	t as 5	v//ows:		
1		7		,			1/2"	
2							1/2" 1/2"	
3							13/4"	
4							2".	
						·		
-								
					İ			

FLORIDA REGISTRATION NO.	RV	



FILE NO.: 97-9036/B





DATE:

#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

8-29-97

PROJECT LOCATION:

BARTOW

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	CONCRETE TEMP.
1	4489	12303	7:30	8:40	10	9	0 / 5	88°
2	LOAD WAS	TESTED - CY	LINDERS N	OLDED, S			<u> </u>	
3	5110	12307	8:35	9:15	4	9	6 1/2	86° /
4	4489	12309	8:55	9:45	5	9	7 1/2	86° Z
5	5110	12313	9:48	10:20	0	6.5	7 1/4	90°
		· · · · · · · · · · · · · · · · · · ·						
	INDICAL	ED SLUMP OF	1ST LOAD	IS BEFO	RE & AFTE	R ADDITION OF	SUPERPLASTI	CIZER & WAT

FLORIDA REGISTRATION NO.		•
LONIDA REGISTRATION NO.	вү	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:			
	10.				00.					DAIL.			
		DLAW DRUM		E BUILDI	NG	LA	AIDLAW EN	VIRONME	ENTAL SE	RVICES			
Project Lo	· ·	TOW AIR BA				ΑT	TN: DENN	IS WALT	ron				
Project Cont		CO CONSTRU						ROBERT	rson				
Concrete Su	ibblier: F.FOI	RIDA ROCK	INDUST	RIES			ROGROUP,						
						A'I	TN: JOHN	BALE,	P.E.				
DESIGN	Specified Strength: Slump (inches): Air Content (percent):												
DATA	4000	) p.s.i. @		28 (	days		6"						
	Mix Type:			<b></b>				0.1					
25606	<u>[X]</u> (Norma	al wt. Light	weight [	Mortar Mix	(G	unite	Grout (	Other W/	SUPERPL	ASTICIZER			
23000	X Transi	t Mixed:		Pump Mix				Other					
FIELD	Date:		Time Co	oncrete Batcl	hed:	Time C	Concrete Sam	pled:	Sampled 6	Ву:			
and LAB	9-03			8:20			9:05	<del></del>	1	SKIPPER			
DATA	Concrete Truck		Ticket N			Size of	Load (C.Y.):		Weather C	1			
	3505 Water Added A		T	92364			9 .			& WARM er Authorized By:			
	1		Yes	5 Ga	l To		9 .	C.Y.		MERIT			
	Slump: (inches			perature (°F):		Concre	ete Temperatu		Wet Weigh				
	6 3/	′4"		85°	1		85°	` '		· · ·			
	Air Content (%	by Vol.):	Molded	and Cured *	to ASTA	/I C-31			Tested to A	ASTM C-39			
	N/A			Yes	□No		Unknow	n	∑ Y∈	s 🗌 No			
	Location of Co	oncrete Placem	-	1 00117711	- 001			•		İ			
			5	' SOUTH	£ 98.	EAS	T OF		· · · · · · · · · · · · · · · · · · ·				
			N	ORTHWEST	CORN	ER O	F BUILDI	NG.					
			[:	FLOOR SL	AB]								
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECIA	MEN SIZE		TOTAL	TEST	TYPE	SPECIMEN			
	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO II	Nj	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)			
LDSB-14	9-04								·	110			
1	3-04	9-10	7	6.00	28.2	7 1	26,000	4460	2	CAB			
2		9-10	7	6.00	28.2	1	27,500	4510	2	MAS			
3		10-01	28										
4		10-01	28										
5		10-01	SP										
6		10-01	SP										
DEMARKS.	*O	-10			<u> </u>								
HEIVIAHNS;	Concrete le	st Specimen	Curea II	n Accordar	nce wit	n AS	IM C-31 Aft 2	er Being 3	Received	in Laboratory			
		•			Ð	Wa	المراجعة	ر ت	1 F\⊡				
					[4.5] [4.5]	Y.							
						八十				自			
								V/					
NS111 (9/91)						Cone	Cone-Shear	Shear	- Spli				
2 ( <i>3131)</i>							ARDAN	MAN & AS	SOCIATES	INC.			

onda negistration No.	ву:



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.				DATE:				
Project Lo Project Cont	Project Name: LAIDLAW DRUM STORAGE BUILDING Project Location: BARTOW AIR BASE Spect Contractor: SEMCO CONSTRUCTION CONCRETE Supplier: FLORIDA ROCK INDUSTRIES  ATTN: DENNIS WALTON BOYD ROBERTSON VIROGROUP, INC. ATTN: JOHN BALE, P.E.												
DESIGN DATA	Specified Strength:  4000 p.s.i. @ 28 days 6"  Mix Type:  Mix Type:  Slump (inches): Air Content (percent):  6"  Air Content (percent):  6"  Mix Type:												
25606													
FIELD and LAB DATA	Date: 9-03 Concrete Truck	3-97 :No.:	Time Co	oncrete Batch 8:20 lo.:		Fime Concrete Sa 9:05 Size of Load (C.Y		Weather C	SKIPPER onditions:				
	3505 Water Added A  X Yes	t Job Site:	Yes	92364 5 Ga		9 Operate Temper	C.Y.	Extra Wate	& WARM er Authorized By: MERIT				
	6 3/ Air Content (%	Slump: (inches): Air Temperature (°F): Concrete Temperature (°F):  6 3/4" 85° 85° Air Content (% by Vol.): Molded and Cured * to ASTM C-31							Tested to ASTM C-39				
	N/A Location of Co	oncrete Placen	nent:	Yes ' SOUTH	□No & 98'	☐ Unkno	own	∑ Ye	es No				
			N	ORTHWEST	CORN	ER OF BUILI	DING.						
			[	FLOOR SL									
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	DIAMETER (IN.)	MEN SIZE AREA(SO/IN	TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY - LBS)				
LDSB-14 1 2 3 4 5 6	9-04	9-10 9-10 10-01 10-01 10-01 10-01	7 7 28 28 28 SP SP	6.00 6.00 6.00 6.00	28.2 28.2 28.2 28.2	7 127,500 7 152,500	4460 4510 5390 5450	2 2 2 2 2	CAB CAB				
REMARKS:	*Concrete Te	st Specimen	Cured i	n Accorda	nce wit	th ASTM C-31 /	After Being	Received	in Laboratory 5				
REMARKS:						Cone Cone-Sh	ear Shea	r Spi	it Cone & Split				
A5111 (9/91)			• • •				ARANI O AC	<del></del>					

Florida Registration No. .

By:

41980



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO .:

DATE:

97-9036/B



#### CONCRETE DATA RECORD

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PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

9-03-97

PROJECT LOCATION:

BARTOW, FLORIDA

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	4489	192362	7:13	8:10	. 0	9	6 3/4	N/A
2	LOAD WA	S TESTED -	CYLINDERS	MOLDED,	SET #14.			
3	6011	192365	8:42	10:00	0	9 / 27	7 1/2	N/A
4	4489	192369	9:40	10:20	0	9 / 36	7 1/2	N/A
				·				
				· · · · · · · · · · · · · · · · · · ·				
							· · · · · · · · · · · · · · · · · · ·	
						15-15-11-11-11-11-11-11-11-11-11-11-11-1		
	•							

FLORIDA REGISTRATION NO.	BY	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

TO:			CC.					DATE:			
Project Name: LAIDLAW DRUM Project Location: BARTOW AIR BA Project Contractor: SEMCO CONSTRU Concrete Supplier: FLORIDA ROCK			ASE ATTN: DENNIS WA UCTION BOYD ROB			IIS WALT ROBERT	ERTSON				
DESIGN	Specified Strength:				Slump (inches):			Air Content (percent):			
DATA	4000 p.s.i. @			28 (		7"		N/A			
	Mix Type:										
	Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other 6" BOOM PUMP										
25606	☐ Transit Mixed: ☐ Pump Mix Other SUPER PLASTICIZER										
FIBER	<u> </u>	sit wiixeu.	Pump Mix			ima Canarata Sar		JPER PLASTICIZER			
FIELD			Time Concrete Batched:		nea:   1	Time Concrete Sampled: 8:30		Sampled By: JOHNNY PURVIS			
and LAB DATA	Concrete Truc		7:45 Ticket No.:		s	Size of Load (C.Y.):		Weather Conditions:			
BAIA	35		12390			9		1	CLEAR & WARM		
	Water Added							Extra Water Authorized By:			
	☐ Yes	x No If	Yes		ıl. To		C.Y.	1	·		
	Slump: (inche	es):	Air Temperature (°F):		: C	Concrete Temperature (°F):		Wet Weight (P.C.F.):			
	7"		84°			81°		N/A			
	Air Content (%		Molded and Cured * to ASTM C-31				Tested to ASTM C-39				
	N/A Yes					□ No □ Unknown					
	Location of Concrete Placement:  SOUTHEAST QUARTER OF CELL 'P'.										
SET NO.	DATE DATE AGE TEST SPECIMEN SIZE TOTAL TEST TYPE SPECIMEN							SPECIMEN WEIGHT			
321 110.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ:1N)	LOAD (LBS)	STRENGTI (PSI)	OF FRAC	(AIR DRY - LBS)		
LDSB-15	9-08	9-12	7	6.00	28.27	117,750	4160	2	CAB		
2		9-12	7	6.00	28.27	125,500	4440	2	CAD		
3		10-03	28								
4		10-03	28								
5		10-03	SP								
REMARKS: *Concrete Test Specimen Cured in Accordance with ASTM C-31 After Being Received in Laboratory											
						1 2	3	4	5		
·					Ċ	one Cone-Shea	r Shear	Spli	t Cone & Split		
V5111 (9/91)						ARDA	MAN & AS	SOCIATES	, INC.		
Florida Registra	ation No				Ву	/:					

-74 THIS FORM CONFORMS TO ASTM-C39

Florida Registration No	B <sub>1</sub>	



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

DATE:

FILE NO.: 97-9036/B





#### **CONCRETE DATA RECORD**

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

9-05-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
1	4252	12388	7:22	8:03	5	9	4 / 5½	N/A
2	LOAD WAS	S TESTED - C	YLINDERS	MOLDED,	SET #15.			
3	4578	12391	7:57	9:11	5	9	7	N/A
4	4357	12392	8:15	9:33	0	9	4 ½	N/A
5	3505	12396	9:30	10:18	0	9	5	N/A
6	4357	12399	10:15	10:40	0	7	8	N/A
		NDICATED FOR ASTICIZER AT		ARE BEE	ORE & AFT	ER ADDITION OF		1
								<u> </u>
								_
					-			

FLORIDA REGISTRATION NO.	. BY	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC. DATE						
Project I Project Loc Project Cont Concrete Su	cation: ractor:	LAIDLAW DRUM BARTOW AIR BA SEMCO CONSTRU FLORIDA ROCK	SE JCTION		ING	LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON VIROGROUP, INC. ATTN: JOHN BALE, P.E.					
DESIGN DATA 25606	Mix Type:	Strength: 4000 p.s.i. @ ormal wt. \( \square\) Lightv	veight [	28 (	Slump (inches) 7" unite Grou		Air Conten N/A				
FIBER	<sub>∑</sub> Tr	ansit Mixed:	Other 5	UPER PLA	ASTICIZER						
FIELD and LAB DATA	Concrete		7 : Ticket N	•		ime Concrete 8:30 Size of Load (C		Weather C	Y PURVIS		
		3505 led At Job Site:	1	2390		9		1	r Authorized By:		
	Valer Add		Yes	Ga	al. To	Extra Water Autho					
	Slump: (in	ches): 7"	Air Temp	Temperature (°F): Concrete Temperature (°F): 81°				Wet Weight (P.C.F.): N/A			
	Air Conter	nt (% by Vol.):	i	and Cured *	to ASTM	l C-31			Tested to ASTM C-39		
		N/A	X	Yes	□No	Unk	nown	X Ye	s 🗌 No		
	Location of	of Concrete Placem	ent:								
				SOUTHEAS	T QUA	RTER OF C	ELL 'P'.				
									1		
	DATE	DATE	AGE	TEST SPECI	IMEN SIZE	TOTAL	TEST	TYPE	SPECIMEN		
SET NO.	RECEIVE IN LAB	D TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO/IN	LOAD	STRENGTI (PSI)		WEIGHT (AIR DRY - LBS)		
						(650)	(, 0,)		2		
LDSB-15	9-08	9-12	7	6.00	28.2	7 117,7	50 4160	2	CAS		
2		9-12	7	6.00	28.2	7 125,50	00 4440	2	(M)		
3		10-03	28	6.00	28.2	7 162,00	5730	2	CAD		
4		10-03	28	6.00	28.2	7 161,0	5690	2	CAD		
5		10-03	SP								
REMARKS:	*Concre	te Test Specimen	Cured i	n Accorda	nce wit	h ASTM C-3	_	Received	in Laboratory		
	. '					Cone Cone-		Spl	it Cone & Split		
5111 (9/91)		····									

41986 Florida Registration No.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

<del>,                                      </del>													
	TO:				CC.				DATE:				
Project Project Lo Project Cont	cation:	LAIDLAW DRUM BARTOW AIR BE SEMCO CONSTRI	ASE	GE BUILD	ING	LAIDLAW EI ATTN: DENI BOYI		ON	RVICES				
Concrete Su		LORIDA ROCK	INDUS	TRIES		VIROGROUP, INC.							
Ouriere de	ppiici		111200	111200		ATTN: JOHN		ਜ਼ ਰ					
						1,111. 00111	, DALL,	1.11.					
DESIGN	Specified S	trength:			S	Slump (inches):		Air Conten	t (percent):				
DATA	4	1000 p.s.i. @		28 d	days	5"		N/A					
	Mix Type:												
	Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other 6" BOOM PUMP												
25606		FIBERMESH WITH											
FIELD	Date:		Time Co	ncrete Batcl	ned: T	ime Concrete Sar	npled:	Sampled E	By:				
and LAB		0-09-97		: 43		8:06		I	Y PURVIS				
DATA	Concrete Tr		Ticket N		S	ize of Load (C.Y.)	:	Weather C	onditions:				
	1	252	1.	2445		9			& MILD				
		ed At Job Site:		_		_		1	r Authorized By:				
	Ye (		Yes		I. To	9	C.Y.						
	Slump: (inc	nes): - 1/2"	Air iemp	erature (°F):	: 10	Concrete Tempera	ure (°F):	Wet Weight (P.C.F.):					
		(% by Vol.):		and Cured *	IO A STA	80°		N/I Tested to A					
	1	(/a by voi.). //A	l	Yes	IU ASTIVI ∏No	Unknov	'n	Tested to A					
		Concrete Placem		103		OTIKITOV	V1.1	[X] 16	5 110				
	2004	0011010101111100111		ID HALF	OF CET	II. TI.T	,						
				THILL .	or cur	ם עו							
			19	T HALF	OF K 8	J							
			ΕÆ	ST END	OF CET	J. 'F'							
	DATE	DATE	AGE	TEST SPECIF		TOTAL .	TEST	TYPE	SPECIMEN				
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ/IN	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY-LBS)				
						1230/	(1 0.7	11140	(AATOTT-200)				
LLSB-16	9-10	0.76	_						ans				
1		9-16	7	6.00	28.27	135,000	4770	2	200				
2		9-16	7	6.00	28.27	138,500	4900	3	CAD				
3		10-07	28										
4		10-07	28										
4			20										
5		10-07	SP										
REMARKS:	*Concrete	Test Specimen	Cured in	n Accordai	nce with	1 ASTM C-31 At	ter Being	Received	in Laboratory				
						1 2	3	4	5				
			,			one Cone-Shea	Shear	Spli	t Cone & Split				
<b>\</b> 5111 (9/91)													
						AHDA	MAN & AS	SOCIATES,	INC.				

A THIS FORM CONFORMS TO ASTM-C39

erioa registration 140.	 y	



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			(	CC.				DATE:	
Project Project Lor Project Cont Concrete Su	cation: BAI ractor: SEM	DLAW DRUM RTOW AIR BA MCO CONSTRU DRIDA ROCK	ASE JCTION	SE ATTN: DENNIS				ROBERTSON INC.		
DESIGN	Specified Stre	ngth:		<del> </del>	S	lump (inches):		Air Content	(percent):	
DATA		00 p.s.i. @		28 c	days	5" -		N/A		
	Mix Type:			7 4 44 4 4 i		nite Cl Croud	Other	W 500W 5		
25606	K Norm:	al wt. Lightv	veignt [	_ Mortar Mix	( []Gu	nite U Grout		" BOOM F IBERMESH		
23000		t Mixed:		Pump Mix					STICIZER	
FIELD	Date:	I		ncrete Batch	ned: T	ime Concrete San		Sampled B		
and LAB	B	9-97	1	: 43	1	8:06			PURVIS	
DATA	Concrete Truck	(No.:	Ticket N	0.:	S	ize of Load (C.Y.):		Weather Co	onditions:	
	425		1:	2445		9			& MILD	
	Water Added A		\/a a	- Co	ı To	9	C.Y.		r Authorized By:	
]	X Yes Slump: (inches		Yes Air Temo	5 Ga erature (°F):	II. To	oncrete Temperat		Wet Weight		
		./2"		73° 80°			۵.٥ ( ۱ ).	N/F	` '	
	Air Content (%		Molded	and Cured *	to ASTM	C-31		Tested to A	STM C-39	
	N/A			Yes	□No	Unknow	/n	X Ye	s 🗌 No	
	Location of Co	oncrete Placem								
			21	ND HALF	OF CEI	L'L'				
			15	ST HALF	OF K 8	J				
- · · · · · · · · · · · · · · · · · · ·			E <i>I</i>	AST END	_					
SET NO.	DATE RECEIVED	DATE TESTED	AGE (DAYS)	TEST SPECI	T	TOTAL LOAD	TEST STRENGTH		SPECIMEN WEIGHT	
	. IN LAB			DIAMETER (IN.)	AREA (SQ-IN	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)	
LLSB-16	9-10	0.16	_			125 222	4770		100	
1		9-16	7	6.00	28.27	135,000	4770	2	210	
2		9-16	7	6.00	28.27	138,500	4900	3	CAD	
3		10-07	28	6.00	28.27	153,000	5410	3		
4		10-07	28	6.00	28.27	155,500	5500	3	Rhw	
5		10-07	SP							
REMARKS:	*Concrete Te	st Specimen	Cured i	n Accorda	nce witl	h ASTM C-31 Af	ter Being	Received	in Laboratory	
						1 2	3	4	5	
						one Cone-Shea	r Sheal	Spli	t Cone & Split	
A5111 (9/91)			_			ARDA	MANRAS	SOCIATES,	INC.	
		1.00					/ /	JOURIES,	////	
Florida Registr	ation No.	41980	9		В	v: _ ( 1 ox C	wh	an 1	10/8/9/	



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

DATE:

FILE NO.: 97-9036/B



#### **CONCRETE DATA RECORD**



PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

9-09-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%)
3505	12442	7:15	8:05	0	9	4 3/4	N/A
LOAD WAS	TESTED - CY	LINDERS M	OLDED, S	ET #16.			<u> </u>
8875	12446	8:10	9:30	0	9	5	N/A
4252	12449	9:28	10:01	0	9	6	N/A
8999	12451	9:50	10:32	5 *	9	$4\frac{1}{2}$ / $5\frac{1}{2}$	N/A
8875	12452	10:03	10:47	0	9	5	N/A CA
8999	12455	11:00		3	4	5 1/2	N/A
AFTER 1ST	SLUMP.						
	8875 4252 8999 8875 8999	8875 12446 4252 12449 8999 12451 8875 12452	8875     12446     8:10       4252     12449     9:28       8999     12451     9:50       8875     12452     10:03       8999     12455     11:00	8875     12446     8:10     9:30       4252     12449     9:28     10:01       8999     12451     9:50     10:32       8875     12452     10:03     10:47       8999     12455     11:00	4252     12449     9:28     10:01     0       8999     12451     9:50     10:32     5 *       8875     12452     10:03     10:47     0       8999     12455     11:00     3	8875     12446     8:10     9:30     0     9       4252     12449     9:28     10:01     0     9       8999     12451     9:50     10:32     5 *     9       8875     12452     10:03     10:47     0     9       8999     12455     11:00     3     4	8875     12446     8:10     9:30     0     9     5       4252     12449     9:28     10:01     0     9     6       8999     12451     9:50     10:32     5 *     9     4½ / 5½       8875     12452     10:03     10:47     0     9     5       8999     12455     11:00     3     4     5 1/2

ELOPIDA REGISTRATION NO	8Y	



1525 Centennial Drive Bartow, Florida 33830



	TO:	·	<u> </u>	(	CC.					DATE:
Project Project Lo Project Cont Concrete Su	cation: BA	AIDLAW DRUM ARTOW EMCO CONSTRU LORIDA ROCK				LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON BOYD ROBERTSON VIROGROUP, INC. ATTN: JOHN BALE, P.E.				VICES
DESIGN	Specified St	trenath:		,	s	lump (i	nches):		Air Conten	t (percent):
DATA	1 '	000 p.s.i. @	28 days				¹" MAX.		N/A	
	Mix Type:	rmal wt. Light	weight [			,		Other Fi	IBER	
25606 MI	1	nsit Mixed:		Pump Mix			(	Other W/S	SUPER PL	ASTICIZER
FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Co	ncrete Sam	pled:	Sampled E	By:
and LAB	9-	-11-97	8:	30			: 58		C.A. B	EST
DATA	Concrete Tr	uck No.:	Ticket N	o.:	S	ize of L	oad (C.Y.):		Weather C	onditions:
		505	12	510			9		CLEAR	
		d At Job Site:								r Authorized By:
	☐ Ye:		Yes		I. To			C.Y.		(5.0.5)
	Slump: (incl	•	Air Temp	erature (°F):	C		e Temperati	ire (°F):	Wet Weigh	t (P.C.F.):
	6 }					86°			Tested to ASTM C-39	
		(% by Vol.):	1	and Cured * 1					Yes □ No	
	N/			∑ Yes  □ No  □ Unknown					[X Ye	s [] No
	Location of	Concrete Placen		LOOR SLA						
				ROM 100'			VEST OF	EAST		
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECIF	MEN SIZE		TOTAL LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT
	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ IN	)	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)
LDSB-17		0.10						4620		PaB
1		9-18	7	6.00	28.2	- 1	30,500	4620	2 2	1241
2		9-18	7	6.00	28.2	1 13	31,000	4630	2	
3		10-09	28						į	
4	1	. 10-09	28							
5		10-09	SP							
6		10-09	SP							
REMARKS	: *Concrete	Test Specimen	Cured i	n Accorda	nce wit	h AST	M C-31 Af	ter Being	Received	in Laboratory
						Cone	Cone-Shear	Shea	Spl	it Cone & Split
A5111 (9/91)						•	ARDA	MAN & AS	SOCIATES	, INC.
<b></b>					_					

orida Registration No.	Оу	·	



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			-	CC.					DATE:	
Project ( Project Loc Project Cont Concrete Su	cation: BAI ractor: SEN	IDLAW DRUM RTOW MCO CONSTRU DRIDA ROCK				LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON FOREST KIRKLAND VIROGROUP, INC. ATTN: JOHN BALE, P.E.				VICES	
DESIGN	Specified Stre	ength:			S	Slump (inches):			Air Conten	t (percent):	
DATA		00 p.s.i. @		28 c	lays	7	MAX.	·	N/A		
	Mix Type:	<del>_</del>						<b></b>		ł	
25606 MIX		nal wt. Lightv	veight [	_ Mortar Mix	< □Gu	inite (	Grout	Other F3	IBER		
23600 WIY		sit Mixed:		Pump Mix				Other w/s	SUPER PL	ASTICIZER	
FIEL D	Date:			ncrete Batch	ned T	ime Co	ncrete Sam		Sampled B		
FIELD and LAB		1-97	1	30			: 58	.р.оо.	C.A. B	•	
DATA	Concrete Truc		Ticket N		s		oad (C.Y.):		Weather C		
	350		12	510			9		CLEAR		
	Water Added						·		i	r Authorized By:	
	☐ Yes		Yes		I. To			C.Y.			
!	Slump: (inche	•	Air Temperature (°F):				e Temperati	ure (°F):	Wet Weight (P.C.F.):		
	6½"		Molded and Cured * to AST			86°			Tested to ASTM C-39		
	Air Content (%		1					_		3	
	N/A	Concrete Placem		Yes	□No		Unknow	(1	∑ Ye	5 110	
	Location of C	oncrete i lacem		LOOR SLA	B. FO	RK LI	דר אוואש	YAY			
			<del>-</del>	DOOK OLL	, 10	100 11	II I KOKK	***			
		•	F	ROM 100'	TO 1	25' V	VEST OF	EAST			
			E	ND OF BU	ILDIN	G.					
057.110	DATE	DATE	AGE	TEST SPECIF			TOTAL	TEST	TYPE	SPECIMEN	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO:IN	t)	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)	
LDSB-17										2.2	
1		9-18	7	6.00	28.2	7 13	30,500	4620	2	CA79	
2		9-18	7	6.00	28.2	7 13	31,000	4630	2	CAQ	
3		10-09	28	6.00	28.2		51,000	5340	2	CAG	
4		10-09	28	6.00	28.2	7 15	3,000	5410	2	CAD	
5		10-09	SP		İ						
6		10-09	SP				ļ				
REMARKS:	*Concrete T	est Specimen	Cured i	n Accordai	nce witl	h AST		_	Received	in Laboratory	
					L/ <sub>2</sub>	1 77∕⊓	2 N T T T T T	3 [	4 1 ⊓⊡		
					,	A Cone	Cone-Shear	Shear	Spli	t Cone & Split	
A5111 (9/91)								7.	șoci∌tes,	,	
		1 -					PHUAL	XIAKIN/& AS	SUCIALES,	""Y / -	

FORM 1001 D-9-74 THIS FORM CONFORMS TO ASTM-C39

Florida Registration No. 4198 C

By: 1. (5drey Man 10/9/9



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.: 97-9036/B





#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

7-11-97

PROJECT LOCATION:

BARTOW, FLORIDA

(9-11-97)

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	CONCRETE TEMP.
1	4252	12506	7:25	8:10	0	9	1½ / 7	86°
2	4578	12507	7:43	8:25	0	9	5 3/4	86° C
3	LOAD WAS	TESTED - CY	LINDERS MO	DLDED, SI	ET #17.			
4	3508	12511	8:42	9:18	0	9	7 .	86° O
5	4252	12512	8:50	9:30	0	9	6 1/2	86° C
6	8875	12513	9:00	9:45	0	9	5 1/2	87°
7	4578	12514	9:10	9:55	0	9	6	87°
8	8999	12519	10:15	11:15	0	5	7	87°
	ватсн сом	PUTER SET FO				FINE AGGREGATE.	E.	
		SLUP ON 1S	C LOAD ARE	BEFORE	& AFTER A	DDITION OF SUP	ER PLASTIC	IZER
	AT PLANT.							
		•						



1525 Centennial Drive Bartow, Florida 33830



	TO:	·			CC.		-			DATE:		
Project I Project Loc	cation: BAF	IDLAW DRUM		GE BUILD	ING		DLAW ENV	S WALTO	N	ICES		
Project Cont	ractor: SEM	ICO CONSTRU	ICTION				FORES'	r Kirkl	AND			
Concrete Su	Supplier: FLORIDA ROCK INDUSTRIES VIROGROUP, INC.											
	ATTN: JOHN BALE,											
DESIGN	Specified Stre	ngth:			S	Slump	(inches):		Air Conten	(percent):		
DATA	400	00 p.s.i. @		28 (	days		7"		N/A			
	Mix Type:											
		al wt.   Lightv	veight [	Mortar Min	x □Gu	ınite	Grout	Other				
25606												
MIX		it Mixed:		Pump Mix				Other				
FIELD	Date:		l	ncrete Batcl	hed: T		oncrete Sam	ipled:	Sampled B			
and LAB		.6-97		3:05			8:32		C.A.			
DATA	Concrete Trucl	k No.:	Ticket N	o.:	ĮS	ize of	Load (C.Y.):		Weather Co	onditions:		
	457	'8		L2605	ŀ		9		CLEAF	R & WARM		
	Water Added A	At Job Site:							Extra Wate	r Authorized By:		
	☐ Yes	No If '	Yes	Ga	ıl. To			C.Y.		,		
	Slump: (inches			erature (°F):	: 10	oncre	te Temperati	re (°F):	Wet Weight	: (P.C.E.):		
	6"	-,.		78°			89°					
	Air Content (%	by Vol 1:		and Cured *	to ASTM				Tested to ASTM C-39			
	1			Yes	∏No	0 01	Unknow	n	∑ Ye			
	N/A	oncrete Placem		162					(X) ie	5 110		
	Location of Co	uncrete Placem										
			<u>F</u>	FLOOR SL	AB							
				10000111100	m			> D 3 3 1 m C	OB OBIT	1,,,,		
			1	ORTHWES	T & SC	OTH	EAST QUAI	JRANTS	OF CELL	'H'.		
										İ		
	DATE	DATE	AGE	TEST SPECI	MEN SIZE	1	TOTAL	TEST	TYPE	SPECIMEN		
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN		LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)		
	III CAB					+	(003)	(e.20)	FRAC	(AIA DAT - LBS)		
LDSB-18	9-17									11/2		
1		9-23	7	6.00	28.27	7   - :	132,500	4690	2	CAL		
. 2		9-23	7	6.00	28.27	7   :	135,000	4770	2	(A)		
3		10-14	28			-						
4		10-14	28									
5		10-14	SP									
		10-14										
6		10-14	SP							ŀ		
								•				
REMARKS:	*Concrete Te	st Specimen	Cured i	n Accorda	nce wit	h ASI	TM C-31 Aft	ter Beina	Received	in Laboratory		
		•				1	2	3	4	5		
					€72	7/1	N	<u> </u>	ı Firi	7 ED ED		
					[::\s	Y I	\\\	//	1 (3)(1)			
						)[ ]			1 11 18			
					- - - - - - - - - - - - - - - - -	$\Lambda \setminus I$	[//\\]		]			
						one (	Cone-Shear	Shear	الناليا لـ Spli	Cone & Split		
A5111 (0/20)	<del> </del>	· · · · · · · · · · · · · · · · · ·			<u>~</u>		Cons-oneal	Oncar				
<b>45</b> 111 (9/91)							ARDA	MAN & AS	SOCIATES,	INC.		

forida Registration No By:	
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1525 Centennial Drive Bartow, Florida 33830



	TO:			•	CC.				DATE:		
•							/ICES				
DESIGN	Specified:	Strength:			S	Slump (inches):		Air Conten	t (percent):		
DATA	<b>}</b> '	4000 p.s.i. @		28 0	days	7"		N/A	,		
DAIA	Mix Type:	4000 p.s.i. @				<u>-</u>		1			
		ormal wt. Light	weiaht [	☐ Mortar Mix	к ПGu	ınite □Grout	Other				
25606	10.11								, r <sub>s</sub> = 1.4.		
MIX	₹∏Tr	ansit Mixed:		Pump Mix			Other				
FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Concrete Sar	npled:	Sampled E	By:		
and LAB	1	9-16-97	8	3:05		8:32	·	C.A.	BEST		
DATA	Concrete	Fruck No.:	Ticket N	o.:	S	Size of Load (C.Y.)		Weather C	onditions:		
		4578		12605		9		CLEA	R & WARM		
		led At Job Site:	.L					Extra Wate	er Authorized By:		
		es 🗓 No If	Yes	Ga	ıl. To		C.Y.				
	Slump: (in	ches):	Air Temp	erature (°F):	: C	Concrete Temperat	ure (°F):	Wet Weigh	t (P.C.F.):		
		6"		78°		89°					
	Air Conter	nt (% by Vol.):	Molded	and Cured *	to ASTM	C-31					
		N/A	X	Yes	□No	Unknov	vn				
	Location of	of Concrete Placem	nent:								
		•		FLOOR SL	AB						
SET NO.	DATE RECEIVE	DATE	AGE	TEST SPECI		OUTHEAST QUA	TEST STRENGTI	TYPE	SPECIMEN WEIGHT		
3E1 NO.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ.IN		(PSI)	FRAC	(AIR DRY - LBS)		
LDSB-18 1 2 3 4 5	9-17	9-23 9-23 10-14 10-14 10-14 10-14	7 7 28 28 SP SP	6.00 6.00 6.00 6.00	28.27 28.27 28.27 28.27	135,000	4690 4770 5910 5960	2 2 2 2 2	CAB CAB CAB		
REMARKS	: *Concret	e Test Specimen	Cured i	n Accorda	nce wit	h ASTM C-31 A	fter Beind	Received	in Laboratory		
						1 2	3	4	5		
		·				Cone Cone-Shea	r Shea	r Spl	it Cone & Split		
A5111 (9/91)				•				SOCIATES	,		
Florida Registr	ration No	41986			В	y: Plok	MAN & AS	Man	10/14/97		
_	•	IENTS, THE PUBLIC AND (	THRSELVES	ALL REPORTS A	ARE SURMIT	TTED AS THE CONFIDER	ITIAL PROPER	TY OF CHENTS	AND AUTHORIZATION FO		
UBLICATION OF S	TATEMENTS, CO	NCLUSIONS OR EXTRACT	S FROM OR	REGARDING OL	IR REPORT	S IS RESERVED PENDIN	IG OUR WAITT	EN APPROVAL			



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO .: 97-9036/B





#### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

DATE: 9-16-97

PROJECT LOCATION:

BARTOW, FLORIDA

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

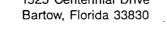
FLORIDA ROCK INDUSTRIES

NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)		
_1	6011	12601	7:28	8:10	0	9	1 3/4&6 1/	′2 89°	
2	4489	12604	7:45	8:25	0	9	5 1/2	89°	(
3	LOAD WAS	TESTED - CY	LINDERS N	OLDED, S	ET #18.				
4	5110	12607	8:30	9:06	0	9	7	89°	0
5	6011	12608	8:50	9:23	0	9	7	89°	6
6	4252	12609	9:05	9:33	0	9	7 1/4	88°	0
7	8875	12612	9:55	10:25	0	9	4 1/2	89°	Û
	INDICATE	1	1ST LOAD	IS BEFOR	E & AFTER	ADDITION OF S	UPER PLASTI	CIZER	
	COMPUTER	SET AT 3.0	% FREE MO	ISTURE I	N FINE AGO	GREGATE.			
	AND 0.0%	FREE MOIST	RUE IN CO	ARSE AGGI	REGATE.				
								·	
	_								

FLORIDA REGISTRATION NO.	BY
--------------------------	----



1525 Centennial Drive





	TO: CC. DATE:									
Project Project Lo Project Cont Concrete Su	pocation: BARTOW ATTN: DENNIS WALTON  tractor: SEMCO CONSTRUCTION, INC. FOREST KIRKLAND									
DESIGN	Specified Stre	nath:			S	Slump (inches):		Air Conten	t (percent):	
DATA		000p.s.i. @		28 d	lays	7"		N/		
DAIL	Mix Type:				<del>.::2                                   </del>					
		alwt. 🗀 Light	weight [	Mortar Mix	c □ Gu	unite Grout	Other 1	FIBERMES	H WITH	
25606		,				-				
23000		t Mixed:		Pump Mix			Other :	SUPERPLA	STICIZER	
FIELD	Date:		Time Co	ncrete Batch	ned: T	ime Concrete S	ampled:	Sampled E	By:	
and LAB	9-	-19-97	7	:50		8:38		C. AL	AN BEST	
DATA	Concrete Truck		Ticket N		S	Size of Load (C.)	<u>(.):</u>	Weather C	onditions:	
	4:	578	1	2742		9		CLEAR	& WARM	
	Water Added A		·	-				Extra Wate	er Authorized By:	
	X Yes	☐ No If	Yes	10 Ga	I. To	9	C.Y.	M.D.	MERIT	
	Slump: (inches	s):	Air Temp	erature (°F):	C	Concrete Temper	ature (°F):	Wet Weigh	t (P.C.F.):	
		1/2"		0°		86°				
	Air Content (%	by Vol.):	Molded	and Cured *	to ASTM	l C-31		Tested to A	ASTM C-39	
	N,	/A	<u>[</u> ]	Yes	□No	Unkn	own	∑ Ye	s 🗌 No	
	Location of Co	oncrete Placem	nent:							
				FLOOR S	LAB					
				NORTHEA	ST &	SOUTHWEST (	QUADRANT	S OF CEL	L 'H'.	
	DATE	DATE	AGE	TEST SPECIA	MEN SIZE	TOTAL	TEST	TYPE	SPECIMEN	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN	LOAD (LBS)	STRENGTI (PSI)	H OF FRAC	WEIGHT (AIR DRY - LBS)	
						(555)	1		1	
LDSB-19					İ				nos	
1		9-26	7	6.00	28.2	•	4540	2	Siz	
2		9-26	7	6.00	28.2	7 131,000	4630	2	CAO	
3		10-17	28							
4		10-17	28							
5		10-17	SP					ł		
6		10-17	SP							
REMARKS:	*Concrete Te	st Specimen	Cured i	n Accorda	nce wit	h ASTM C-31	After Being	Received	in Laboratory	
						1 2	3	4	5	
	<del></del>				c	one Cone-Sh	ear Shea	r Spli	it Cone & Split	
A5111 (9/91)						ARD	AMAN & AS	SOCIATES	, INC.	
Florida Registra	ation No				В	v:				

Florida Registration No.	Ву:
AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE S PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR RE	



1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.:

97-9036/B



#### **CONCRETE DATA RECORD**

DATE:

9-19-97

PROJECT NAME:

PROJECT LOCATION:

BARTOW

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LAIDLAW DRUM STORAGE BUILDING

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED		CUBIC YARDS CONCRETE	SLUMP (inches)	CONCRETE TEMP.
1	4252	12740	7:28	8:20	0	9	2 / 5	86° C
2	LOAD WAS	TESTED - C	LINDERS	MOLDED,	SET #19.			
3	8999	12743	8:16	9:30	0	9	6 3/4	86° C
4	4489	12748	9:30	10:15	0	6.5	6 1/2	87° (
		ED SLUMP OF LASTICIZER A		IS BEFO	RE & AFTER	ADDITION OF		
		R SET FOR 3.		NOISTURE	IN FINE A	GGREGATE		
		AND O.	0% FREE	MOISTRUE	IN COARSE	AGGREGATE.		·
				1	1			



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			<del> </del>	CC.					DATE:		
Project Project Lo Project Con Concrete Su	cation: B tractor: S	AGE BUII ON, INC. ISTRIES	LDING	LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON FOREST KIRKLAND VIROGROUP, INC. ATTN: JOHN BALE, P.E.								
DESIGN	Specified Stre	ength:			5	Slump	(inches):		Air Conter	Air Content (percent):		
DATA		000p.s.i. @		28	days		7"		N/	A		
25606	Mix Type:	al wt. Light	weight (	☐ Mortar Mi	x □Gι	unite	Grout	Other F	TIBERMES	H WITH		
25606	▼ Trans	it Mixed:		Pump Mix			,	Other S	SUPERPLA	STICIZER		
FIELD	Date:	<del></del>	Time Co	oncrete Batc	hed: 1	Γime C	oncrete Sam	pled:	Sampled E	By:		
and LAB		-19-97	1	:50			8:38			AN BEST		
DATA	Concrete Truc		Ticket N		S	Size of	Load (C.Y.):		Weather C			
ĺ	Water Added	578	<u>; 1</u>	2742			9		1	& WARM		
1	X Yes		Yes	10 Ga	ıl. To		9	C.Y.	l .	er Authorized By:		
	Slump: (inche			perature (°F)		Oncre	te Temperatı		M.D. MERIT Wet Weight (P.C.F.):			
	1	1/2"	1	.0°		3011010	86°	210 ( 1 ).	Tree vieign	it (1.0.1. <i>)</i> .		
	Air Content (%			and Cured *	to ASTM	1 C-31			Tested to A	ASTM C-39		
	N	/A		Yes	□No	Unknown			[X] Ye	🛚 Yes 🗌 No		
	Location of C	oncrete Placem	ent:	FLOOR S	ממז:							
				THOON	מאם		<del></del>					
				NORTHEA	ST &	SOUT	HWEST QU	ADRANTS	OF CEL	L 'H'.		
				•								
SET NO.	DATE RECEIVED	DATE TESTED	AGE	TEST SPECI	MEN SIZE		TOTAL LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT		
	INLAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (\$Q IN	0	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)		
LDSB-19										ack		
1		9-26	7	6.00	28.2	7 1	28,500	4540	2	CA-7		
2		9-26	7	6.00	28.2		31,000	4630	2	CAO2		
3		10-17	28	6.00	28.2	7 1	58,000	5590	2	(2)		
4		10-17	28	6.00	28.2	7 1	60,000	5660	2	(49)		
5		10-17	SP									
6		10-17	SP									
REMARKS:	*Concrete Te	st Specimen	Cured i	n Accorda	l nce wit	h AST	M C-31 Aft	er Being	Received	in Laboratory		
		1				1	2	3	4	5		
					c	one	Cone-Shear	Shear	Spli	t Cone & Split		

A5111 (9/91)

Florida Registration No.

D-9-74 THIS FORM CONFORMS TO ASTM-C39

ARDAMAN & ASSOCIATES, INC.

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED STHE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:			(	CC.				DATE:	
Project i Project Loc Project Cont Concrete Su	ontractor: SEMCO CONSTRUCTION - FORES							ON LAND	/ICES	
DESIGN	Specified Stre	ngth:			s	lump (inches):		Air Content	(percent):	
DATA	4000	0 p.s.i. @		28 d	ays	7"		N/A		
	Міх Туре:									
	X Norm	al wt. ☐ Lightv	weight [	Mortar Mix	□Gu	nite Grout	Other	FIBERMES	SH	
25606		ia Balissandi.	_	Duman Miss			Other			
		it iviixed.		Pump Mix	ا اند	: Conservato Con			LASTICIZER	
FIELD	Date:	4-97		ncrete Batch 8 : 05	iea:	ime Concrete Sar 8:21	npiea:	Sampled B	y: L TADLOCK	
and LAB DATA	Concrete Truck		Ticket N		-	ize of Load (C.Y.)	•	Weather Co		
DAIA	601		ł	o 192825		9	•	P/C 8		
	Water Added A		I						Authorized By:	
	☐ Yes	No If	Yes	Gal	. To		C.Y.		´	
	Slump: (inches	s):	Air Temp	erature (°F):	C	oncrete Temperat	ure (°F):	Wet Weight	(P.C.F.):	
	7 3,			87°		90°				
	Air Content (%	•		and Cured * t				Tested to ASTM C-39		
	N/A		1	Yes	□No	Unknov	<u>vn</u>			
	Location of Co	oncrete Placem								
			S	LAB 45'	EAST	& 12' NORTH	ł			
			O	F SOUTHWI	EST CO	ORNER.				
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECIA	IEN SIZE	TOTAL	TEST STRENGTH	TYPE	SPECIMEN	
3E1 NO.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO/IN)	LOAD (LBS)	(PSI)	H OF FRAC	WEIGHT (AIR DRY - LBS)	
LDS-20	9-25	}								
1	7 23	10-01	7	6.00	28.27	132,000	4670	2	CAS)	
2		10-01	7	6.00	28.27		4690	2	CHO	
3		10-22	28							
4		10-22	28				İ			
5		10-22	SP				,			
. 6		10-22	SP							
							İ			
REMARKS:	*Concrete Te	st Specimen	Cured in	a Accordar	ice with	n ASTM C-31 At	ter Reinc	Received	in Laboratory	
		от орошнон		.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1 2	3	4	5	
		•				one Cone-Shea		Split	Cone & Split	
A5111 (9/91)						ARDA	MANRAS	SOCIATES,	INC	
						ANUA	MIAIT & AS	JOUINI ES,	INC.	
Florida Registra	ation No				Ву	/:				

FORM 10c. 0-9-74 THIS FORM CONFORMS TO ASTM-C39

lorida Registration No.	By:
-------------------------	-----



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.				DATE:		
Projec Project Lo Project Cor Concrete S	ocation: BA ntractor: SE	AIDLAW DRUM ARTOW AIR B EMCO CONSTR LORIDA ROCK	ASE UCTION		DING	LAIDLAW E ATTN: DEN FOR VIROGROUP ATTN: JOH	NIS WALT EST KIRK , INC.	ON LAND	RVICES		
DESIGN	Specified Strength: Slump (inches): Air Content (page)										
DATA		•			1	Slump (inches):		i .	nt (percent):		
DAIA		00 p.s.i. @		28_	days	7"		N/7	<u>A</u>		
	Mix Type:  ☑ Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other FIRERMESH										
05505	X Nor	mai wt. Ligh	tweight	☐ Mortar M	lix 🔲 G	unite Grout	Other	FIBERM	ESH		
25606	Trac	nsit Mixed:	٠,	I Domen Adding							
		isit wiixed.		Pump Mix			Other W	SUPER I	PLASTICIZER		
FIELD	Date:	24 05	Time C	oncrete Bat	ched:	Time Concrete S	ampled:	Sampled	Ву:		
and LAB		24-97		8:05		8:21		DARY	L TADLOCK		
DATA	Concrete Tru		Ticket I		:	Size of Load (C.Y	<b>(.)</b> :	Weather (	Conditions:		
	60			192825		9		P/C	& HOT		
	Water Added	d At Job Site:		-					er Authorized By:		
	Yes		Yes	G	al. To		C.Y.		- viewonada by.		
	Slump: (inch	es):	Air Tem	perature (°F	): (	Concrete Temper		Wet Weigh	ot (PC E):		
	7 :	3/4"		87°		90°	4.0.0	11.0.1.j.			
	Air Content (		Molded	and Cured *	to ASTA	4 C-31		Tested to ASTM C-39			
	N/A	, ,	1	Yes	□No	□Unkno					
	Location of	Concrete Placen	nent:				OWIT	X Ye	es No		
	SLAB 45' EAST & 12' NORTH										
			^	F SOUTHV	IDCE O	001100					
				F SOUTH	VESI C	ORNER.					
						•					
	DATE	DATE	AGE	TEST SPECI	MEN CIZE	TOTAL	TECT	7/05			
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	·	LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT		
	ii V BAB	<del></del>	<del> </del>	DIAMETER (IN.)	AREA (SO.IN	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)		
LDS-20	9-25	1	1						10		
1		10-01	7	6.00	28.2	7 132,000	4670	2	CAL		
2		10-01	7	6.00	28.2			2	M.		
3		10-22	28	6.00	28.2	,	1	1	2003		
4		10-22	28	6.00	28.2		1	2	CAR		
5		10-22	SP	0.00	20.2	164,000	5800	2			
6		i	l				1				
6		10-22	SP			7					
REMARKS:	*Concrete To	est Specimen	Cured in	Accorda	nce with	ASTM C-31 A	ftor Boing	Dogoived	in Laboratory		
		•				1 · 2	nter being i	neceivea	in Laboratory		
					0.4		S	5.			
						One Cone-Shea					
11 (9/91)						one Cone-Shea	r Shear	Split	Cone & Split		
(0.0.7)						ARDA	MATO & ASS	OCIATES	INC. / / /		
		41980				1511	//	, 77	////////		
rida Dogietro	At	4/49(				1-11-	1/	, //	I = I = I = I = I = I = I = I = I = I =		

Florida Registration No. 7170 0

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.: 97-9036/B





DATE:

#### **CONCRETE DATA RECORD**

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

9-24-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	CONCRETE TEMP.
1	3505	192818	7:10	7:45	0	9	6 1/2	84°
2	8999	192822	7:45	8:11	5	9	6	83° C
3	LOAD WAS	TESTED - C	LINDERS 1	OLDED,	ET #20.			
4	8808	192829	8:48	9:20	0	9	4 3/4	88° C
5	6011	192831	9:05	10:00	0	9	3 1/2	86° C
	* #1 LOAD	WAS 1 3/4"	SLUMP AT	PLANT B	FORE SUPE	R PLASTICIZER	ADDED.	
	·							
								-

FLORIDA REGISTRATION NO.	8Y	-
	THE PARTY OF THE P	21750



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

							<del></del>				
	TO:				CC.				DATE:		
Project		LAIDLAW DRUM	STORA	GE BUIL	DING						
Project Lo		BARTOW AIR B	ASE			ATTN: DE	NNIS WA	LTON			
Project Cont	ractor:	SEMCO CONSTR	UCTION	1		FO	REST KI	RKLAND			
Concrete Su	ipplier:	FLORIDA ROCK	INDUS	STRIES		VIROGROU	P, INC.				
				ATTN: JO	HN BALE	, P.E.					
DESIGN	Specified S	Strength:			s	llump (inches):		Air Conten	t (percent):		
DATA		4000 p.s.i. @		28 (	days	5"		N/	Α ΄ ΄		
	Mix Type:			,				<u> </u>			
	I No	ormal wt. 🔲 Lighty	veight [	Mortar Mi	x □Gu	inite Grout	Other 6	" BOOM P	UMP		
25606				·							
		ansit Mixed:		Pump Mix					STICIZER		
FIELD	Date:		Time Co	oncrete Batc	hed: T	ime Concrete Sa	mpled:	Sampled B	•		
and LAB		9-30-97		7:30		7:55		1	Y PURVIS		
DATA	Concrete T		Ticket N		S	ize of Load (C.Y.)	:	Weather C			
		4578	1	.2916		9		l	& COOL		
	]	ed At Job Site:						I .	r Authorized By:		
	X Y∈		Yes * 10 Gal. To			9	C.Y.				
	Slump: (inc	•	1			oncrete Tempera	ture (°F):	Wet Weight (P.C.F.):			
		/ . 7"		72°		75°		N/A			
	Air Content	t (% by Vol.):		and Cured *				Tested to A	i		
		N/A	·	Yes	□No	Unknov	vn	X Ye	s 🗍 No		
	Location o	f Concrete Placem	ent:								
		<del></del>		CONCRE	re pav	EMENT					
				Fእርጥ C1	IDE OE	BUILDING.					
				LEGI 31	LDD OI	DOILDING:	<del>.</del>				
SET NO.	DATE	DATE	AGE	TEST SPECI	MEN SIZE	TOTAL	TEST	TYPE	SPECIMEN		
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SQ/IN)	LOAD (LBS)	STRENGTH (PSI)	FRAC	WEIGHT (AIR DRY - LBS)		
LDSB-21											
1		10-07	7	6.00	28.27	143,500	5080	2	(Plan		
2		10-07	7	6.00	28.27	1	5130	2	7811.		
3		10-28	28				1		(ru)		
4		10-28	28								
		10-28	SP				İ				
5		10-28	SP						,		
6		10-20	SE						1		
REMARKS:	*Concrete	Test Specimen	Cured i	n Accorda	nce with	ASTM C-31 A	fter Being	Received	in Laboratory		
						1 2	3	4	5		
* ADI	DED AFTE	R 1ST SLUMP.			1/2						
					[-]			1 1/1/1			
					1/2		//.	.			
					$\cup L$	2M $MY$	V/				
<del></del>				· · · · · · · · · · · · · · · · · · ·	C	one Cone-Shea	r Shear	Spli	Cone & Split		

A5111 (9/91)

ARDAMAN & ASSOCIATES, INC.

orida Registration No.	By:



# Ardaman & Associates, Inc. 1525 CENTENNIAL DRIVE

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO.: 97-9036/B





DATE:

### CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

9-30-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

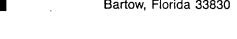
FLORIDA ROCK INDUSTRIES

NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inches)	AIR CONTENT (%
1	8999	12914	7:05	7:43	0	9	8"	N/A
2	LOAD WAS	TESTED - C	LINDERS 1	OLDED,	ET #21.			
3	6289	12917	7:40	8:33	0	9	6	N/A
4	6011	12919	7:53	8:44	10	9	6 1/2	
5	5110	12920	8:03	9:00	7	9	7	N/A
6	LOAD WAS	TESTED - CY	LINDERS N				/	
7	8875	12922	8:15	9:32	0	9	6	NI / D
8	6289	12925	9:05	9:45	0	9	7	N/A
9	6011	12926	9:18	10:11	. 0 -	9	7 1/2	N/A
10	3505	12927	9:20	10:30	12	9	4 1/2	N/A
11	5110	12929	9:50	11:00	5	9	7	N/A N/A
								N/A
						·		

FLORIDA REGISTRATION NO. 41986	ex ///0/11.1/1/c / 12/0/67
A HUTUU COOTCOTIO H	BY/ [8/4/4] M/an / 13/8/91



1525 Centennial Drive Bartow, Florida 33830





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:
Project Project Lo Project Cont Concrete Su	ocation: B tractor: S	AIDLAW DRUM ARTOW AIR E EMCO CONSTR LORIDA ROCK	ASE UCTIO	N	LDING	NG LAIDLAW ENVIROMENTAL SERVICES ATTN: DENNIS WALTON HORACE KIRKLAM VIROGROUP, INC. ATTN: JOHN BALE, P.E.				
DESIGN DATA	Specified Strength:  4000 p.s.i. @ 28 day:  Mix Type:  Normal wt. □ Lightweight □ Mortar Mix						(inches): 5"	Other 6	Air Conter N/	
25606	∏ Tran	sit Mixed:		Pump Mix				Other Si	יוסדים סד.ע	ASTICIZER
FIELD and LAB	Date:	-30-97	Time Co	oncrete Bato 7:30			Concrete San 7:55	npled:	Sampled E JOHNN	By: IY PURVIS
DATA	Concrete True	ck No.: 578	Ticket N	lo.: L2916		Size o	f Load (C.Y.): 9		Weather C	Conditions:
	Water Added	At Job Site:	1	V					Extra Wate	er Authorized By:
	X Yes Slump: (inche		Yes Air Toma	* 10 G perature (°F	al. To	Canar	9	C.Y.		RACTOR
	3 3/4	/ . 7"	An lemp	72°	).	Concre	ete Temperat 75°	ure (*F):	Wet Weigh	
	Air Content (9	% by Vol.):	ł	and Cured *		И C-31				ASTM C-39
	Location of C	/A Concrete Placem		Yes	□No		Unknow	'n	X Ye	s No
		onerete i lacem	CIII.	CONCRE	TE PAV	VEME	T			
					TDD 01		TT D T M C			
		- Man	·	EAST S	IDE OF	: BU.	LLDING.			
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	TEST SPEC	IMEN SIZE	N)	TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY - LBS)
LDSB-21										(20)
1		10-07	7	6.00	28.27	1	L43,500	5080	2	The second
2 3		10-07 10-28	7 28	6.00	28.27	1	.81,500	5130 6420	2 2	(history)
4		10-28	28	6.00	28.27	1	.83,500	6490	2	ANTO I
5	•	10-28	SP							
6		10-28	.SP							
REMARKS:	*Concrete Te	est Specimen	Curedia	Accorda	nco wit	h A C	TNA C 21 A44	or Boine	Danima	in Laboratory
			ourcu II	TACCOIGA	IICE WIL	1	2	er being	Heceivea 4	in Laboratory 5
* ADD	DED AFTER	1ST SLUMP.				Cone	Cone-Shear	Shear	Sali	
5111 (9/91)				<del>.</del>					Split	

FORM . A. Z. TUIS

Florida Registration No.

41986

ARDAM

MAN ASSOCIATES AND 10/28/9



1525 Centennial Drive Bartow, Florida 33830



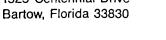


									· · · · · · · · · · · · · · · · · · ·		
!	TO:				CC.					DATE:	
Project	Namo: T	AIDLAW DRUM	STORA	CF BUILD	TNG	Τ.Δ	IDLAW EN	IVT RONME	ENTAL SE	RVICES	
Project Lo		ARTOW AIR B		OL DOLLD	1110		TN: DENN				
Project Cont		EMCO CONSTRI						ST KIRK			
Concrete Su		LORIDA ROCK				VI	ROGROUP,				
00110101010	ipplier. 2	DOTALDIT TOOK	211200	11(120			TN: JOHN		P.E.		
								,			
DESIGN	Specified St				5	Slump	(inches):		Air Content (percent):		
DATA		000 p.s.i. @		28 c	lays		5"		N/A		
	Mix Type:										
	X Nor	mal wt. Lighty	veight [	Mortar Mix	c ∏Gı	unite	Grout	Other 6	BOOM	PUMP .	
25606	   √∏rar	nsit Mixed:		Pump Mix				Other s	ום משמווי	ASTICIZER	
E1E1 5	Date:	ion mixed:		ncrete Batch	and: IT	Cime C	oncrete Sam		Sampled E		
FIELD and LAB		<del>-</del> 30-97		8:08	160.		9:00	ipieo.		NY PURVIS	
DATA	Concrete Tru		Ticket N				Load (C.Y.):		Weather C		
מוא	1	999	1	2921		J120 01	9		ſ	R & WARM	
		At Job Site:	L	2,721						r Authorized By:	
	X Yes		Yes	7 Ga	I. To		9	C.Y.		RACTOR	
	Slump: (inch			perature (°F):		Concre	te Temperati		Wet Weigh		
	8" 83°						84°	( · / ·		. (	
	Air Content (% by Vol.): Molded and Cured * to AS								Tested to A	STM C-39	
	N	/A		Yes	☐ No		Unknow	n	[X Ye	s □ No	
	Location of	Concrete Placem	ent:								
				CONCRETE	PAVE	MENT					
				EAST SID	E OF	BUIL	DING.				
	DATE	DATE	AGE	TEST SPECIA	AEN SIZE	1	TOTAL	TEST	TYPE	SPECIMEN	
SET NO.	RECEIVED IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN		LOAD	STRENGTH	OF	WEIGHT	
	111 DAO		· · · · · · · · · · · · · · · · · · ·	ONAIC ICISTAL.	ANER(30 III	"	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)	
LDSB-22		10.05	_		00 -		41 00-	40-0		(Phu)	
1		10-07	7	6.00	28.2	ſ	41,000	4990	2		
2		10-07	7	6.00	28.2	1 1	38,000	4880	2	ruw 1	
3		10-28	28								
4		10-28	28								
5		10-28	SP								
6		10-28	SP								
REMARKS:	*Concrete	Test Specimen	Cured in	n Accordar	nce witl	h AST	M C-31 Aft	ter Being	Received	in Laboratory	
		•				1	2	3	4	5	
						$\mathbb{V}/\mathbb{I}$		· //			
					[::	$\mathbb{N}$					
					1.7			///.			
					IJ,		Cons State	V <u>/</u>	البالنا ا		
5111 (9/91)				<del></del>	Ç	one	Cone-Shear	Shear	Split	Cone & Split	
2111 (A(A1)							ARDAN	MAN & ASS	SOCIATES,	INC.	

unda negistration ivo.	Ву:



1525 Centennial Drive





#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.					DATE:	
					0.5.					DATE.	
Project Project Lo Project Cont Concrete Su	cation: BA tractor: SE	IDLAW DRUM RTOW AIR B MCO CONSTR ORIDA ROCK	ASE UCTION	ı	DING	G LAIDLAW ENVIRONMENTAL SERVICES ATTN: DENNIS WALTON HORACE KIRKLAM VIROGROUP, INC. ATTN: JOHN BALE, P.E.					
DESIGN	Specified Stre	ngth:	<del></del>	<del></del>		Slump (inche	es):		Air Content (percent):		
DATA	400	00 p.s.i. @		28	days	5'			N/A	(10000000000000000000000000000000000000	
	Mix Type:										
05505	Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other 6" BOOM PUMP										
25606	☐ ☐ Transi	it Mixed:		Pump Mix			Other		HIDER DI.	ASTICIZER	
FIELD	Date:			ncrete Batc	hed:	Time Concre	te Sampled:		Sampled B		
and LAB	9-:	30-97		8:08		9:00	•			NY PURVIS	
DATA	Concrete Truck		Ticket N			Size of Load	(C.Y.):		Weather C	onditions:	
	899		1	2921		:	9			R & WARM	
	Water Added A 		Yes	7 Ga	il. To	Ć	)	C.Y.	1	r Authorized By: RACTOR	
	Slump: (inches			erature (°F)			nperature (°F		Wet Weight		
	8"			83°	1	849		,		. (1.1511.).	
	Air Content (%	by Vol.):	1	and Cured *					Tested to ASTM C-39		
	N/A	A oncrete Placem		Yes	□No	U	nknown		∑ Ye	s 🗌 No	
	Location of Ct	oncrete Placen		CONCRETE	י אמי	MENT				1	
			<del></del> -	CONCRETE	FAVL	SPIENT			,		
				EAST SID	E OF	BUILDING	· .				
									,		
	DATE	DATE	465	TEST SPECI	4EN 617E	TOTAL		ST	TYPE	SDECU151	
SET NO.	RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	DIAMETER (IN.)	AREA (SO II	→ LOAD	STRE	NGTH SI)		SPECIMEN WEIGHT	
LDSB-22						(683)		311	FRAC	(AIR DRY+LBS)	
1		10-07	7	6.00	28.2	7 141,0	00 49	90	2	(Phu)	
2		10-07	7	6.00	28.2			-	2	(OLL)	
3		10-28	28	6.00	28.2	1	1	40	2		
4		10-28	28	6.00	28.2	7 169,0	00 59	80	2	(772W)	
5		10-28	SP							(I)	
6		10-28	SP							-	
										İ	
REMARKS:	*Concrete Te	st Specimen	Cured in	n Accordar	nce wit	h ASTM C-	31 After Be	ing	Received	in Laboratory	
						1	2	3	4	5	
						Cone Cone	e-Shear S	hear	Split	Cone & Split	
5111 (9/91)							ARDAMAN &	Δςς	SOCIATES	ING 1 2	
Torida Registra	tion No	4986			В	P	Www	1 1	Wan	10/28/97	

9-74 THIS FORM CONFORMS TO ASTM-C39

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



	TO.		<del></del>		CC.			·	DATE:
	TO:				<i>.</i> .				DATE.
Project I Project Loc Project Cont Concrete Su	cation: BAF ractor: SEM	DLAW DRUM RTOW AIR BA MCO CONSTRI DRIDA ROCK	ASE UCTION		ING	LAIDLAW EN ATTN: DEN HOR. VIROGROUP ATTN: JOH	NIS WALT ACE KIRK , INC.	CON CLAM	RVICES
DESIGN	Specified Stren	ngth:			SI	ump (inches):		Air Conten	t (percent):
DATA		00 p.s.i. @	28 days			6" MAX.		N/A	
	Mix Type:	ix Type:  ⊠ Normal wt. ☐ Lightweight ☐ Mortar Mix ☐ Gunite ☐ Grout Other							
#525217	X  Transi			Pump Mix			Other 4	1" TO 2"	DIMP
51515	Date:	i wiixeu.		ncrete Batch	ed: Ti	me Concrete Sa		Sampled B	
FIELD and LAB	1	-27-97	!	9:57		10:45		DAN P	EMBLE
DATA	Concrete Truck				ze of Load (C.Y.)	:	Weather C	onditions: UNDER	
	899		1.	3493		9.5			IN/MAIN ROOF
	Water Added A				<u>.</u>		0.14		r Authorized By:
	☐ Yes	٠	Yes		l. To	9.5	C.Y.	Wet Weigh	/A
	Slump: (inches	s): *		erature (°F):	10	oncrete Tempera 85°	ture (*F):		· · · · •
	5" Air Content (%			73° and Cured *1	OASTM			Tested to A	/A ASTM C-39
	N/A	-, -,	x 3		□No	Unkno	wn	∑ Ye	
	Location of Co	oncrete Placem						<u> </u>	
			]	ROOF SLA	B , CE	LL 'L'			
			7	JNDER MA	TN ROC	)F			
				ONDER THE	277 1100	<u> </u>			
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECI	MEN SIZE	TOTAL LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT
SET NO.	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SO IN)		(PSI)	FRAC	(AIR DRY - LBS)
LL-23									as
1		11-03	7	6.00	28.27		3940	2	SAB
2		11-03	7	6.00	28.27	113,500	4010	2	CAL
3		11-24 11-24	28 28						
4		11-24	SP						
5		11-24	SP						
6		11 24							
REMARKS	: *Concrete Te	st Specimen	Cured in	n Accorda	nce with	1 ASTM C-31 A	fter Being	Received	I in Laboratory
i	PLED FROM (					1 2	3	4	5
SAM	PLED FROM (	CHOIL OF I	NOCK.						it Cone & Split
A5111 (9/91)					C	one Cone-She	-		
W(II (2/21)						ARD	AMAN & AS	SOCIATES	, INC.

unua negistration ivo.	O).	



-9-74 THIS FORM CONFORMS TO ASTM-C39

Florida Registration No.

## 🕶 Ardaman & Associates, Inc.

1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

	TO:				CC.				DATE:
Project Project Lo Project Cont Concrete Su	cation: BA	IDLAW DRUM RTOW AIR B MCO CONSTR ORIDA ROCK	ASE UCTION	ſ	DING	LAIDLAW EN ATTN: DENN HORA VIROGROUP, ATTN: JOHN	NIS WALT ACE KIRI INC.	FON KLAM	RVICES
DESIGN	Specified Stre	ngth:			S	lump (inches):		Air Conten	t (percent):
DATA	40	00 p.s.i. @		28 (	days	6" MAX.		N/A	
	Mix Type:								
	∑ Norm	al wt. Light	weight [	Mortar Mix	< □Gu	nite Grout	Other		
#525217	X Trans	it Miyed:	(J	Pump Mix			Other 2	1" TO 2"	DUMD
EIEL D	Date:	WINCU.		ncrete Batci	ned: IT	ime Concrete San		Sampled E	
FIELD and LAB	1	-27 <b>-</b> 97	1	9:57		10:45	ipied.	DAN P	•
DATA	Concrete Truc		Ticket N		s	ize of Load (C.Y.):		Weather C	onditions: UNDER
	89	99	1	3493		9.5			IN/MAIN ROOF
	Water Added A							Extra Wate	r Authorized By:
	Yes		Yes		1. To	9.5	C.Y.		/A
	Slump: (inche:	•		erature (°F):	C	oncrete Temperati	ure (°F):	Wet Weigh	
	Air Content (%			73° and Cured*:	to ASTM	85°		Tosted to A	/A STM C-39
	N/Z		1		□No	Unknow	'n	∑ Ye	
		oncrete Placem			<u> </u>			<u> </u>	
				ROOF SLA	B , CI	ELL 'L'			
			1	UNDER MA	IN ROO	OF.			
			1						]
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPECI	MEN SIZE	TOTAL LOAD	TEST STRENGTH	TYPE OF	SPECIMEN WEIGHT
	IN LAB	TESTED	(DAYS)	DIAMETER (IN.)	AREA (SOIN)	(LBS)	(PSI)	FRAC	(AIR DRY - LBS)
LL-23									
1		11-03	7	6.00	28.27	111,500	3940	2	(A)
2		11-03	7	6.00	28.27	· · ·	4010	2	CADA
3		11-24	28	6.00	28.27	1 '	5800	2	Coll
4		11-24	28	6.00	28.27	168,000	5940	2	CA
5		11-24	SP						
6		11-24	SP						
DE114 DV0		L			L				
HEMARKS:	*Concrete Te	st Specimen	Cured in	n Accordar	nce with	ASTM C-31 Af	_	Received	in Laboratory
* SAMP	LED FROM C	HUTE OF TR	RUCK.		0.4	1 2	3	4 1 Exca	ا التاليا 2
					c c	one Cone-Shear	Shear	Spli	Cone & Split
S111 (9/91)							· ·		
						ARDA/	VIA,NI,&AS∶	SOCIATES	JNC. // /

AS A MUTUAL PROTECTION TO CLIENTS, THE PUBLIC AND OURSELVES, ALL REPORTS ARE SUBMITTED AS THE CONFIDENTIAL PROPERTY OF CLIENTS AND AUTHORIZATION FOR PUBLICATION OF STATEMENTS, CONCLUSIONS OR EXTRACTS FROM OR REGARDING OUR REPORTS IS RESERVED PENDING OUR WRITTEN APPROVAL.



1525 Centennial Drive Bartow, Florida 33830



	TO:				CC.				DATE:
Project Project Lo Project Cont	cation: B	AIDLAW DRUM ARTOW AIR BA EMCO CONSTRU	ASE		ING	LAIDLAW ENV ATTN: DENNI HORAG		N	VICES
Concrete Su		LORIDA ROCK	INDUS	TRIES		VIROGROUP, ATTN: JOHN		.E.	·
DESIGN DATA	Mix Type:	000 p.s.i. @			days	Slump (inches): 6"		N/.	
25606	[X]Tra	rmal wt. Light		Pump Mix			Other 6"	BOOM P	STICIZER UMP
FIELD and LAB DATA	Concrete Tr	1				Fime Concrete Sa 7:45 Size of Load (C.Y.) 10	,	Weather C	By: NY PURVIS Conditions: R & COOL
			Yes	3671 	al. To	10 Concrete Tempera	C.Y.	Extra Wate	er Authorized By:
	7 Air Content	1/2" (% by Vol.):	Molded	63° and Cured *	to ASTM	79°		i	ASTM C-39
		/A Concrete Placem	ent:	Yes O' WEST	□No & 10'	Unknow		∑ Y€ CORNER	es No
			OI	F WEST R	AMP.				
SET NO.	DATE RECEIVED IN LAB	DATE TESTED	AGE (DAYS)	TEST SPECII DIAMETER (IN.)	MEN SIZE AREA(SO:IN	TOTAL LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT (AIR DRY - LBS)
LDSB-24 1	11-06	11-12	7	6.01	28.37	137,000	4830	2	esB
2		11-12	7 28	6.01	28.37	138,500	4880	2	CAR
4		12-13	28						
FEMARKS:	*Concrete	12-13 Test Specimen	SP Cured in	n Accorda	nce wit	h ASTM C-31 At	ter Beina	Received	in Laboratory
			· ·			1 2	3	4	5
5111 (9/91)		· · · · · · · · · · · · · · · · · · ·					MAN & ASS		

iorida negistration No	Зу	у:
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# Ardaman & Associates, Inc. 1525 CENTENNAL DRIVE

1525 CENTENNIAL DRIVE BARTOW, FLORIDA 33830 (813) 533-0858

FILE NO .:

97-9036/B



# CONCRETE DATA RECORD

PROJECT NAME:

LAIDLAW DRUM STORAGE BUILDING

DATE:

11-05-97

PROJECT LOCATION:

BARTOW AIR BASE

PROJECT CONTRACTOR:

SEMCO CONSTRUCTION

CONCRETE SUPPLIER:

FLORIDA ROCK INDUSTRIES

LOAD NO.	TRUCK NO.	TICKET NO.	TIME BATCHED	TIME POURED	WATER ADDED (gal.)	CUBIC YARDS CONCRETE	SLUMP (inchés)	AIR CONTENT (%)
1	3507	13670	6:53	7:40	o	10	5 1/4	N/A
2	LOAD WA	S TESTED - C	YLINDERS	MOLDED,	SET #24.			N/A G
3	7292	13674	7:55	8:27	10 *	10	5 3/4 / 7	N/A
4	4578	13676	8:25	9:11	10	10	7	N/A
5	3507	13677	8:42	9:45	5 *	10	5 1/2 / 7	N/A
6	LOAD WAS	TESTED - C	YLINDERS	MOLDED,	SET #25.			
7	4242	178099	9:42	10:40	5 / 5	10	5 / 6	N/A
8	8999	193677	9:55	10:55	5	10	6 1/2	N/A
9	4489	178100	9:54	11:10	5	10	5 3/4	N/A
10	4578	178103	10:24	11:25	10	10	6 1/2	N/A
11	LOAD WAS	TESTED - C	LINDERS (	MOLDED,	SET #26.			.,,,,,
12	4489	13687	11:50	12:15	5	10	7 1/2	N/A
13	4578	13688	12:00	12:39	0	10	7 1/4	N/A
14	4489	13691	12:55	1:20	5	10	7	N/A
15	LOAD WAS	TESTED - CY	LINDERS !	OLDED,	SET #27.			11/11
16	8999	13695	1:38	2:09	5	10	7 3/4	N/A
17	4578	13698	2:10	2:45	5	10	7 1/4	N/A
18	5110	13699	2:22	3:05	5	10	. 6	N/A
	* AFTER 1	ST SLUMP.						

FLORIDA REGISTRATION NO.	DV	

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1525 Centennial Drive Bartow, Florida 33830



#### COMPRESSIVE STRENGTH OF CONCRETE CYLINDERS

							, LINDER		·
	TO:				CC.				DATE:
Project Project L Project Cor Concrete S	ocation: Bantractor: SI	AIDLAW DRUM ARTOW AIR M EMCO CONSTM LORIDA ROCM	BASE RUCTIO	N	DING	LAIDLAW EN ATTN: DENN HORA VIROGROUP, ATTN: JOHN	IIS WALTO CE KIRKI INC.	ON LAM	RVICES
DESIGN	Specified St	renath:			<del></del>	Clump (in the -)		T	
DATA		000 p.s.i. @		28	days	Slump (inches): 6"		Air Conte	ent (percent): 'A
ľ	3	mal wt. Ligh	itweight	☐ Mortar N	Mix Па	unițe 🗌 Grout	Other SI	יות משמו	STICIZER
25606	TVTit Minut								
FIELD	Date:	Sit Wilded.		Pump Mix			Other 6"		
and LAB	1 -	-05-97	Time	Concrete Bat	ched:	Time Concrete Sa	impled:	Sampled	Ву:
DATA	Concrete Tru	ck No.:	Ticket	9:23 No:		10:05 Size of Load (C.Y.)	· · · · · · · · · · · · · · · · · · ·		NY PURVIS
ļ	601	1	78098	(	10	).		Conditions: .R & COOL	
ą.	Water Added	At Job Site:	1						er Authorized By:
•	Yes		Yes	5 G		10	C.Y.		.D.
	Slump: (inche	•	Air Tem	perature (°F	):	Concrete Tempera	ture (°F):	Wet Weigh	nt (P.C.F.):
	Air Content (%	. / 4" 6 by Vol ):	Moldad	66° and Cured	145 A O TA	79°		N/	<u>'A</u>
	N/	• •		Yes	□ No			Tested to ASTM C-39	
	Location of C	oncrete Placen	nent:	, .00		Unknov	vn	X Ye	es 🗌 No
				10' WES'	T OF S	OUTHWEST CO	RNER		
							· ·		
				OF WEST	RAMP.				
SET NO.	DATE RECEIVED	DATE TESTED	AGE	TEST SPECI	MEN SIZE	TOTAL	TEST	TYPE	SPECIMEN
	INLAB	123120	(DAYS)	DIAMETER (IN.)	AREA (SO:IN)	LOAD (LBS)	STRENGTH (PSI)	OF FRAC	WEIGHT (AIR DRY - LBS)
LDSB-25	11-06								
1		11-12	7	6.01	28.37	159,250	5610	2	CAB
2		11-12	7	6.01	28.37	165,000	5820	2	CAB CAB
3		12-13	28						
4		12-13	28						
5		12-13	SP						
REMARKS: *	Concrete Te	st Specimen (	Cured in	Accordar	ice with	ASTM C-31 Aft	er Beina F	eceived	in Laboratory
					1	2	3	4.	5
11 (9/91)		** · · · · · · · · · · · · · · · · · ·			Cor	ne Cone-Shear	Shear	Split	Cone & Split
						ARDAM	IAN & ASSC	CIATES, I	NC.
orida Registrati	ion No				D.			•	

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1525 Centennial Drive Bartow, Florida 33830



TO:					DATE:						
Project Name: LAIDLAW DRUM Project Location: BARTOW AIR B Project Contractor: SEMCO CONSTR Concrete Supplier: FLORIDA ROCK			BASE RUCTION	UCTION HORACE KIRKL					ON LAM		
DESIGN	Specified Str	enath:			10	Slump (inches):		la: o :			
DATA	,	000 p.s.i. @		28	days	6"		Air Conte	ent (percent): 'A	:	
	Mix Type:										
25606	Norr	nal wt. ☐ Ligh	tweight	☐ Mortar M	lix 🔲 Gu	unite Grout	Other SU	PER PLA	STICIZER	{	
25606	[XTran	sit Mixed:	Г	Pump Mix			Other 6"	POOM T	TIMD		
IELD	Date:			oncrete Bate	ched I	ime Concrete Sa				_	
ind LAB		-05-97	1	10:37		11:40	impied.	Sampled	by: INY PURVI	c	
DATA	Concrete True		Ticket I	Vo.:	S	ize of Load (C.Y.	):		Conditions:		
	Water Added	292	178104			10		CLEA	R & COOL		
	Yvater Added		Yes	5 G	al. To	,	0.11		er Authorize	d E	
	Slump: (inche			perature (°F				CONTRACTOR Wet Weight (P.C.F.):			
		3/4"		72°		80°	.tare ( 1 ).	vvet vveigi	it (P.C.F.):		
	Air Content (%	6 by Vol.):	1	and Cured *	to ASTM	C-31		Tested to	ASTM C-39		
			]	l Voo		- I Interes		600.14	_		
	N/A Location of C	A Concrete Placen	l <u>lx</u> nent:	Yes	No TH & 15	Unknow		T CORNE		] 1	
	N/i Location of C	A Concrete Placen	l IX		TH & 15					] 1	
SET NO.	DATE RECEIVED	Concrete Placen	AGE (DAYS)	10' SOUT	TH & 15  RAMP.  MEN SIZE	TOTAL LOAD			ER SPECIME	N	
	DATE RECEIVED INLAB	oncrete Placen	nent:	10' SOU	TH & 15	5' WEST OF	SOUTHWES	T CORNE	CR .	N	
SET NO.  LDSB- 26	DATE RECEIVED	oncrete Placen	nent:	OF WEST  TEST SPECI	RAMP.  MEN SIZE  AREA(SO IN)	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)	T CORNE	SPECIME WEIGHT	N	
LDSB- 26	DATE RECEIVED INLAB	DATE TESTED	AGE (DAYS)	OF WEST  TEST SPECI DIAMETER (IN.)  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)  5270	T CORNE	SPECIME WEIGHT	N	
LDSB- 26 1 2	DATE RECEIVED INLAB	DATE TESTED  11-12 11-12	AGE (DAYS)	OF WEST  TEST SPECI	RAMP.  MEN SIZE  AREA(SO IN)	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)	T CORNE	SPECIME WEIGHT	N	
LDSB- 26	DATE RECEIVED INLAB	DATE TESTED	AGE (DAYS)	OF WEST  TEST SPECI DIAMETER (IN.)  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)  5270	T CORNE	SPECIME WEIGHT	N	
LDSB- 26 1 2	DATE RECEIVED INLAB	DATE TESTED  11-12 11-12	AGE (DAYS)	OF WEST  TEST SPECI DIAMETER (IN.)  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)  5270	T CORNE	SPECIME WEIGHT	N	
LDSB- 26 1 2 3	DATE RECEIVED INLAB	DATE TESTED  11-12 11-12 12-13	AGE (DAYS) 7 7 28	OF WEST  TEST SPECI DIAMETER (IN.)  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)  5270	T CORNE	SPECIME WEIGHT	N	
LDSB- 26 1 2 3 4 5	DATE RECEIVED IN LAB	DATE TESTED  11-12 11-12 12-13 12-13 12-13	AGE (DAYS)  7 7 28 28 SP	OF WEST  TEST SPECI DIAMETER (IN.)  6.01  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37  28.37	TOTAL LOAD (LBS) 149,500 150,750	SOUTHWES  TEST STRENGTH (PSI)  5270 5310	T CORNE	SPECIME WEIGHT (AIR DRY-L	N BS)	
LDSB- 26 1 2 3 4 5	DATE RECEIVED IN LAB	DATE TESTED  11-12 11-12 12-13 12-13 12-13	AGE (DAYS)  7 7 28 28 SP	OF WEST  TEST SPECI DIAMETER (IN.)  6.01  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37  28.37	TOTAL LOAD (LBS)	SOUTHWES  TEST STRENGTH (PSI)  5270 5310	T CORNE	SPECIME WEIGHT (AIR DRY-L	BS)	
LDSB- 26 1 2 3 4 5	DATE RECEIVED IN LAB	DATE TESTED  11-12 11-12 12-13 12-13 12-13	AGE (DAYS)  7 7 28 28 SP	OF WEST  TEST SPECI DIAMETER (IN.)  6.01  6.01	RAMP.  MEN SIZE  AREA(SO IN)  28.37  28.37	TOTAL LOAD (LBS)  149,500 150,750  ASTM C-31 Af	TEST STRENGTH (PSI) 5270 5310	T CORNE	SPECIME WEIGHT (AIR DRY-L	or)	

3	ву:
A MUTUAL PROTECTION TO CLIENTS THE PUBLIC AND OURSELVED ALL PERSONS	



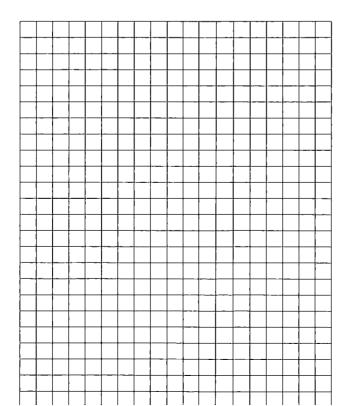
1525 Centennial Drive Bartow, Florida 33830



Proje	TO:				CC.				DATE:				
	_ocation: E entractor: S	AIDLAW DRI BARTOW AIR BEMCO CONST LORIDA ROC	BASE TRUCTIO	ON	LDING	LAIDLAW E ATTN: DEN HOR VIROGROUP ATTN: JOH	NIS WALT ACE KIRK , INC.	'ON LAM	RVICES				
DESIGN	Specified S		<del></del>			Slump (inches):		Air Content (percent):					
DATA	Mix Type:	000 p.s.i. @		28 days 6" N/A									
25606	XNor	mal wt. Lig	htweight	☐Mortar	Mix 🗆 G	Sunite Grout	Other S	UPER PLA	ASTICIZER				
23000		nsit Mixed:		Dump Mi				' BOOM B					
FIELD and LAB	Date:	L-05-97	Time (	Concrete Ba	atched:	Time Concrete S		Sampled					
DATA	Concrete Tru		Ticket	1:13 No:		1:35		JOHN	NY PURVIS				
	45	78	Honet	13693		Size of Load (C.Y. 10	.):	Weather (	Conditions: R & COOL				
	Water Added	_			<u></u>				er Authorized B				
	Slump: (inche		If Yes Air Tem		Gal. To	10 Concrete Tempera	C.Y.	CON'	TRACTOR				
		1/2"		73°			ature (°F):	Wet Weight (P.C.F.):					
	Air Content (9			and Cured		81° 1C-31	Tested to ASTM C-39						
	N/A								X Yes No				
				25' SOL	JTH & 2	0' WEST OF	SOUTHINE	m					
		25' SOUTH & 20' WEST OF SOUTHWEST  CORNER OF WEST RAMP.											
				CORNER	OF WE	ST RAMP.							
SET NO.	DATE RECEIVED	DATE	AGE	TEST SPEC	IMEN SIZE	TOTAL	T						
	INLAB	TESTED	(DAYS)	DIAMETER (IN.)		LOAD (LBS)	TEST STRENGTH (PSI)	TYPE OF FRAC	SPECIMEN WEIGHT				
LDSB- 27	11-06	11 10						- Thac	(AIR DRY - LBS)				
		11-12	7	6.01	28.37	132,250	4660	2	CAD				
2		11-12	7	6.01	28.37	132,500	4670	2	CAB				
3		12-13	28		]								
4		12-13	28										
5		12-13	SP										
MARKS: *	Concrete Tes	t Specimen	Cured in	Accorda	ice with	ASTM C-31 Aft							
				- I o o i dui	1	A31WC-31 Aπ 2	er Being R 3	eceived in 4	Laboratory				
							Γ. 7/1	neid	3 [1]				
					一样			17 11					
9/91)		<del></del>		<del></del>	Con	e Cone-Shear	Shear	Split	Cone & Split				
						ARDAM	AN & ASSO	CIATES, IN	IC.				
la Registratio	in No		<del></del>		Ву: _	AS THE CONFIDENTIA	_						



# Effects of Polypropylene Fibers in Reducing Corrosion of Rebar in Concrete



A Summary of a Report presented at the ACI Conference Hong Kong, Dec. 5, 1991

Included in ACI Publication SP-128

The right to reprint this report has been authorized by American Concrete Institute

#### **Effects of Polypropylene Fibers in Reducing Corrosion of Rebar in Concrete**

A. L. Landau

FIBERMESH COMPANY

T.E. Webster

WEBSTER ENGINEERING ASSOCIATES

In early 1986, Webster Engineering Associates, Inc initiated an investigation into the effect of polypropylene fibers on the corrosion of reinforcing steel in concrete. The results of those first tests were reported in 1987 by Webster and Vondron at the International Bridge Conference in Pittsburg, Pennsylvania and by Landau at the Research Institute Conference in Hong Kong.

Webster Engineering continued the test program. In August, 1988, Webster and Landau reported on the data and results that could then be developed from the continuing study. This report was included in the Post-OWIC Conference Symposium on Concrete and Structures on August, 1988 at Kuala Lumpur, Malaysia.

This current report was presented on December 6, 1991 at the ACI International Conference on Rehabilitation of Concrete Structures in Hong Kong. It is based on a further examination of the same concrete prisms studied and produced in 1987 and reported upon in 1988.

## THE CAUSES OF CORROSION

Most corrosion of reinforcing steel in concrete is caused by the migration of chloride ions reaching the surface of the steel. Marine environments, industrial processes, and deicing salts are the most common sources of such alien chloride ions. The steel in concrete is protected from corrosion by a combination of the chemical reactions at the steel surface, known as passivation, and by the protection from the environment provided by the cover of the concrete

#### **PASSIVATION**

Hydration of Portland cement releases alkalis (the hydroxides of sodium,

calcium, and potassium). The water in the pores of new concrete will have a high pH in the range of 13.6 - 13.9. At this high pH level chemical reactions that occur on the surface of the steel rapidly create a condition in which the steel surface is described as being passive. This passivation layer inhibits the electrochemical reaction of the corrosion process. In ordinary concrete the surface of the steel will remain passive as long as the pH level is maintained even though oxygen and moisture contact the steel.

Oxygen in small quantities is required to maintain the passivity of the surface of the steel, but normally there is enough oxygen in the concrete.

There are two common conditions which cause the loss of passivity of steel reinforcement in concrete and therefore permit corrosion. The first is the concentration of a significant number of free chloride ions in the pore water adjacent to the steel. The second is the reduction of the alkalinity of the concrete



1. Corrosion pumping to the surface



2. Example of spalling



3. Rusting at roadside caused by deicing salts, Montreal, Canada

aujacent to the steel, normally attributed to the carbonation of the concrete. Any reduction in the passivity of the steel will permit corrosion to occur.

Free chloride ions are the most common cause of the deterioration of the protective passivation of steel. Usually there are small amounts of chlorides in concrete present from the time of mixing but they are generally bound into the solid paste. These chlorides originate in the aggregate, water content, and admixtures

but do not create any problems when the amount is small and they are firmly anchored.

Because carbonation involves reactions with carbon dioxide in the air, it proceeds from the outer surface to the interior of the concrete. The rate of penetration depends upon a number of factors and, most importantly with respect to fibers in concrete, this includes humidity and the permeability of the concrete. Surface defects such as honeycombing, air

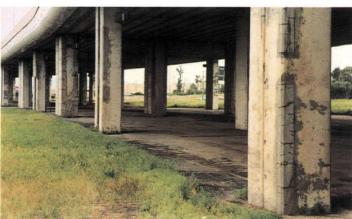
bubbles or cracks will enable carbon dioxide to proceed into the concrete at a greater rate.

Moisture is required for the carbonation reaction, which occurs as a gas dissolved in a moisture film reacting with alkalis in solution. Carbonation occurs most rapidly at humidities ranging from 50 to 75 percent. At lower humidity levels moisture films do not tend to form on the surface of the pores; while at higher levels water tends to block the penetration of additional carbon dioxide. If the concrete in contact with the steel becomes carbonated it no longer protects the steel through the passivation process. Corrosion will then commence whenever moisture becomes available. From that point on, the rate of corrosion will depend upon the quality of the concrete and degree of cracking, in addition to moisture availability.

4. Spalling of the same area, Montreal, Canada



5. Repair of overpass, without fibers, Montreal, Canada



**6.** Close-up of failed repair, without fibers



#### **OXYGEN**

Oxygen can migrate through even the highest quality of concrete, either as a gas or dissolved in liquid. It will move quicker in gaseous form than in a liquid, but it will still move if there is a moving force such as the consumption of oxygen by corrosion or if there are cycles of wetting and drying. The damage by corrosion is usually worse in areas subjected to cycles of wetting and drying and this is partially related to the increased movement of oxygen under these conditions.

The quality of concrete has an influence on the degree and rate of corrosion. As the quality of concrete improves, the movement of oxygen is increasingly restricted. Therefore the early stages of corrosion of steel reinforcement will be very slow for a period of years due mainly to the limited amount of oxygen present at the steel. Cracks in the concrete, poor workmanship or insufficient cover over the reinforcing steel allow easier access of the oxygen and, therefore, will allow the rate of corrosion to increase.

#### RUST

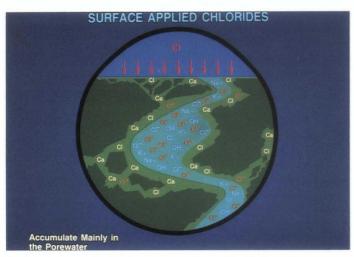
Rust is commonly recognized as the expansive by-product of the corrosion of steel. As the rust, or expansive by-product of corrosion, continues to be produced, there is a progressively greater

expansive force developed between the reinforcing steel and the concrete. Cracks in the concrete will develop as the concrete fails in tension because the expansive forces exceed the tension strength of the concrete.

Cracking and spalling at the surface are the visible symptoms of active corrosion at this stage and this is not necessarily accompanied by rust staining. In some circumstances there will be horizontal cracking between reinforcing steel members which will develop small to large areas of delamination within the concrete without signs of distress on the surface.

#### CHLORIDE IONS

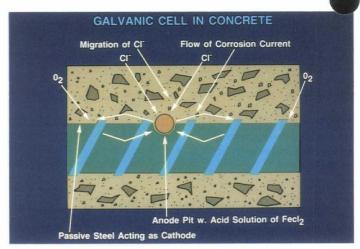
The chloride ions which create damage are the alien chlorides from marine exposure, deicing salts and similar environments which tend to accumulate in the pores of the concrete. While some of these alien chloride ions will become loosely combined with the crystalline hydration products of cement, the remainder will concentrate in the pore water and will be relatively free to move. (See Illustration 7).



7. Chloride Ions in the Porewater. Alien chloride ions from marine environments, deicing salts, or industrial processes enter the concrete as part of the pore water. Upon reaching the steel reinforcement they become a primary cause of corrosion.

The mechanism of corrosion of steel in concrete containing chlorides is complex and is really beyond the scope of this report. The chloride ions disrupt the passivating reactions that occur on the surface of the steel in the highly alkaline environment within an uncarbonated concrete. If the concrete is partially or totally carbonated, even smaller concentrations of free chlorides may initiate corrosion. (See Illustration 8).

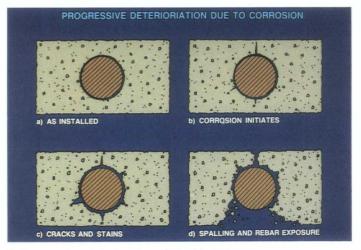
The access of chlorides into concrete is controlled by the quality of concrete, the thickness of cover and sometimes the presence of an effective chloride retarding surface sealer. Unless the concrete surface is completely sealed by an impermeable coating, the chloride ions will penetrate the concrete. The concentration of chlorides will tend to be greatest at the surface and will be gradually reduced at increasing depths within the concrete.



8. Galvanic Cell in Concrete. The uneven concentration of alien chlorides at the surface of the steel will create an anode-cathode relationship resulting in the formation and flow of a corrosive electrical current.

#### CARBONATION

The second means by which loss of alkalinity occurs in concrete is by carbonation, which is the reaction of the alkaline materials in the concrete with the carbon dioxide in the atmosphere. The reaction reduces the alkalinity of the pore water. When the plant the pore water becomes less than approximately 11.5, the processes that cause and maintain the passivation layer no longer occur and the passivation protection is destroyed. The steel is then free to corrode exactly as if exposed to the open atmosphere. (See Illustration 9).



9. Progressive deterioration of steel in concrete.

#### THE ROLE OF FIBERS IN CONCRETE

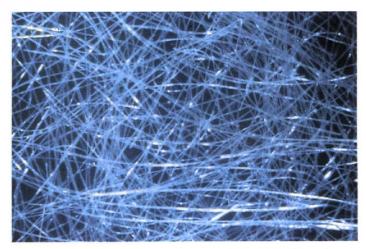
Fibers in concrete have two major functions. The first is to prevent plastic shrinkage cracking. The second is to reduce the segregation of the components of the concrete. There are a number of other physical properties which are improved by the addition of fibers to concrete. The reduction in permeability of the concrete is an attribute of prime importance with regard to the protection against corrosion. The high Toughness Index, which is the ability of concrete to sustain a load after initial crack, is also important as it relates both to spalling and to a continuing bond to the steel reinforcement.

Polypropylene fibers are considered the best type of fibers to be placed in concrete. Polypropylene is inert and is not affected by either acids or the alkalis found in concrete. It will not degrade in concrete. It is not subject to any form of corrosion. It is light, with a specific gravity of .91 and, therefore, there is a large volume of fibers for a given weight. It is strong, with a tensile strength of over 50 Ksi. It is an economical fiber and so can be used in adequate quantities without a large expenditure of money. Normally, for slabs and other horizontal concrete flat work, polypropylene fibers are found to be more satisfactory in use than wire mesh or other steel members used for secondary reinforcement and for these reasons can replace these steel units. The fibers cannot replace primary steel reinforcement.

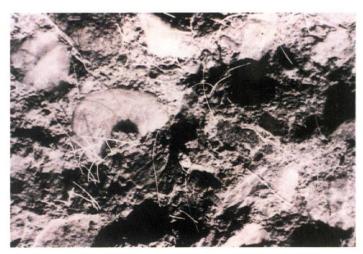
The normal dosage of polypropylene fibers is .9 kilos per cubic reter of concrete (1-1/2 pounds per cubic yard). The fiber this usually 19mm (3/4"). The fibrillated bundles of fibers event balling and during mixing are separated into individual fibers and become evenly distributed throughout the concrete. There are approximately 7,100,00 individual fibers per cubic meter or about 7 fibers per cubic centimeter. (See Illustrations 10, 11, 12).



10. Groups of fibrillated fibers. The polypropylene fibers are fed into the concrete in fibrillated bundles in order to prevent balling during mixing. The mixing cycle breaks the bundles into idual fibers as shown in Illustration #12.



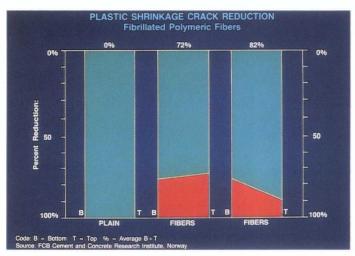
**11.** A demonstration of fiber distribution. This block of acrylic simulates the manner in which the fibers are located throughout the entire mass of concrete.



**12.** Micro-photo of fibers in concrete. This 50x photograph shows the manner in which the fibers are evenly distributed throughout the concrete in a tri-dimensional plane to assure firm anchorage.

#### PLASTIC SHRINKAGE CRACKING

It has been noted that cracks in concrete allow ready access to the reinforcing steel of rust-inducing elements such as moisture, chlorides, carbon dioxide, and oxygen. Fibers are able to reduce this type of cracking by 95% to 100% in a slab composed of good quality concrete, placed and cured following recommended concrete practices. The Norwegian Cement and Concrete Research Institute, in testing the control of plastic shrinkage cracks, found that approximately 80% of all plastic shrinkage cracks extended completely through the concrete. Therefore cracks of this type must be regarded as a major source of damage. If such cracks were superficial, penetrating only slightly into the concrete, then the incidence of plastic shrinkage cracks would not be serious as the integrity of the concrete would not be affected. (See Illustrations 13 & 14).



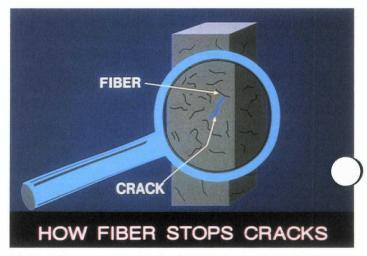
13. Most plastic shrinkage cracks extend through the concrete. Tests by the Norwegians proved that approximately 80% of all plastic shrinkage cracks extend throughout the thickness of the concrete.



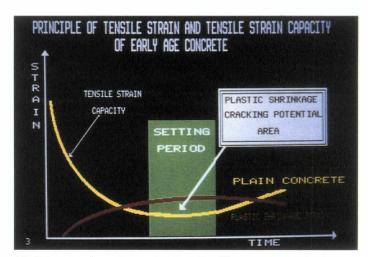
**14.** Typical plastic shrinkage crack. Plastic shrinkage cracks destroy the integrity of the concrete and permit easy access of destructive elements to the reinforcing steel.

In concrete without fibers, removal of the bleed water is basically responsible for causing plastic shrinkage cracking. As the bleed water moves to the surface of the concrete, microscopic capillary canals are formed. Throughout the concrete a multitude of microscopic cracks are developed and these begin to meet, join and become larger cracks, known as macro-cracks. The macro-cracks also meet, join and grow into major damaging plastic shrinkage cracks.

When fibers are introduced into the concrete, the micro-cracks begin to form. However, when a micro-crack reaches a fiber it is prevented from further growth. The tiny micro-crack remains in its initial small size. Somewhere adjacent to the first crack another micro-crack appears and it also is intersected by another fiber and prevented from further growth. In this manner the micro-cracks are not allowed to develop into cracks which could create a reduction in the concrete's integrity. (See Illustration 15 & 16).



**15.** How fibers stop cracks. A micro-crack, developed by the bleed water, is stopped and prevented from growing when it intersects a fiber.



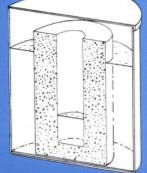
**16.** Principle of tensile strain capacity. Fibers prevent plastic shrinkage cracks during the critical stage prior to final set by increasing the resistance to the internal stresses created by plastic shrinkage of the concrete.

#### FERMEABILITY OF CONCRETE

The permeability of concrete will vary widely for a number of reasons. The addition of fibers will also vary in the degree of the reduction in permeability they will provide in a given application. The amount of fiber in the concrete has a great effect upon the improvement to be expected. In the Von Test, as a part of this report, there was a 44% reduction in permeability when the equivalent of 593 grams of polypropylene per cubic meter was added to the plain concrete. This improvement was increased to 79% when the equivalent of 1187 grams per cubic meter was included in the mix. (See Illustration 17 and 18).

#### Permeability-Von Test Method-B

Sealed 5 gallon vessel containing 6" x 12" concrete cylinder. Specimen has 2" x 11" inner bore. Permeability is tested by measuring the milliliters of water migrating into the inner bore.



17. The Von Test for permeability. The Von Test truly measures the permeability of concrete and is preferred to methods which measure absorption.

# EFFECT OF FIBER ON CONCRETE PERMEABILITY NON FIBER CONCRETE 1.0 LB. FIBERMESH/YD<sup>3</sup> 2.0 LB. FIBERMESH/YD<sup>3</sup> AGE-DAYS

Effect of fiber on permeability. The Von Test shows that the ee of permeability is affected by the amount of fiber in the concrete.

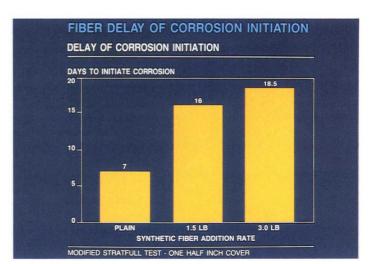
#### INITIAL TEST PROGRAM — 1986

The initial test program by Webster Engineering to evaluate the effect of fibers on the corrosion of steel in concrete began in April, 1986 and a report indicated that, on a preliminary basis, the addition of fibers in concrete could significantly prolong the time before the occurrence of corrosion of steel in concrete.

The program consisted of two separate sets of tests. In both stages the procedure of testing was the same and followed the Stratful method. In the first test, the test units consisted of four (4) single #4 reinforcing bars cast in 38mm (1-1/2") diameter cylinders of concrete. The first bar was cast in plain concrete. The second bar was in concrete containing polypropylene fibers at the rate of 890 grams per cubic meter (1-1/2 pounds per cubic yard). The third bar was in plain concrete with the addition of 10% of calcium chloride by weight of cement. The fourth bar was cast in concrete which contained both the addition of 10% of calcium chloride and also the equivalent of 890 grams per cubic meter (1 1/2 pounds per cubic yard) of polypropylene fiber.

After curing for 28 days, the specimens were then submerged to 2/3 of their length in water containing 15% sodium chloride. Each specimen was then examined for corrosion by measuring the electrical potential of the reinforcing bar with a copper/copper sulfate electrode. When the observed potential exceeded 350 mV, the specimens were also examined for cracks due to internal pressure created by the steel corrosion .

The second set of tests were then performed with the only difference being the doubling of the amount of fiber in the two appropriate specimens. In this test, the two plain concrete specimens attained a corrosive potential of negative 500 mV at five (5) and seven (7) days, respectively, while the specimens with fibers did not attain the same negative 500 mV potential until the sixteenth (16) and twenty-first (21) days. These tests indicated that the addition of fibers reduces the rate of ion diffusion and thus delays the initiation of corrosion. (See Illustration 19).



**19.** Fibers delay corrosion. The Stratful tests by Webster showed that the addition of fibers doubled the time before corrosion began.

#### PRESENT TEST PROGRAM — 1987

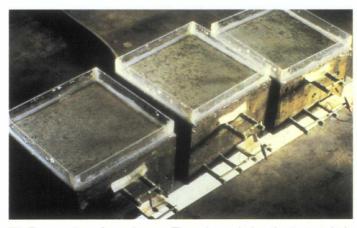
In January 1987, Webster Engineering began the test program still underway to evaluate the long-term effects of adding polypropylene fibers to concrete with relation to the protection of steel reinforcement against corrosion. The specimens were 300mm x 300mm x 175mm prisms (approximately 12" x 12" x 7"). Polypropylene fibers were included in selected prisms. The specimens contained an upper mat of "anodic steel" consisting of a 25mm (1") cover over two (2) reinforcing bars in a location that eventually became chloride contaminated and moist from salt water ponding. (See Illustration 20).

The lower mat remained in a chloride free environment and became cathodic. This lower mat consisted of a 25mm cover over either four (4) reinforcing bars, a double layer of welded wire mesh, or no reinforcing steel at all. All exposed ends of steel were epoxy coated to prevent any end corrosion. The upper and lower mats were electrically connected so that the flow of macrocell corrosion current between the cathoodic and anodic mats was isolated and could be measured. Other corrosion parameters such as linear polarization, copper/copper sulfate half-cell potential at the top surface and concrete electrical resistance could also be measured.

After 21 days of air curing, the specimens began a cycle of 92 hours of ponding of 15% sodium salt water solution at a depth of 13mm (1/2") in the laboratory at 15 to 21 degrees Celsius (60 - 70°F.). At the end of the 92 hours exposure, the salt water was removed, the slabs were rinsed with fresh water, and then placed in a heating chamber at 38 degrees Celsius (100°F.) for a period of 68 hours. After the specimens were removed from the heating chamber, the ponding cycle was resumed.

It is estimated that 24 weeks of this cyclic treatment represents 10 to 20 years of chloride penetration in a typical northern climate, for bridges and parking decks.

Two variables were to be tested in this program. The first was the length and amount of polypropylene fiber. The second was the type and placement of the reinforcing steel. The detailed description of each specimen follows:



**20.** Preparation of specimens. The prisms during the test period of 48 weeks, prepared for the salt water ponding.

#### SPECIMEN DESIGN

#### MIX DESIGNS FOR VARIOUS VOLUMES OF 19.1mm FIBRILLATED POLYMERIC FIBERS

Note: Batch weights are given for a volume of 0.055 m³, sufficient to cast 3 beam specimens.

	Conventional Water Reducer			Superplasticize	
	0.1%	0.3%	0.5%	0.3%	0.5%
Cement Fly ash Sand+ 5-10 mm aggregate++ 10-20 mm aggregate++ Added water TOTAL			12.55 kg 3.15 kg 48.60 kg 10.45 kg 48.40 kg 8.34 kg 131.49 kg	for all	mixes
19.1 mm Fibers	49.5 gms	148.5 gms		148.5 gms	247.5 gms
Air entrainment Water reducer	4 ml 40 ml	4 ml 40 ml	4 ml 40 ml		_
Superplasticizer	40 1111	_	40 1111	25 ml	150 ml
Slump (cm)	18	13	5	6	5
Unit weight (kg/m³)	2381	2345	2361	*	*
% Air	2.5	5.4	4.2	*	*

- \* Not measured
- + Moisture content of sand = 2.14%
- ++ Moisture content of combined coarse aggregate = 1.16%

	00 0
Specimen	Description
100 A & B	Plain Portland Cement Concrete Rebar top & bottom
101 A & B	.890 kg/m³, 38mm fiber Rebar top & bottom
102 A & B	.890 kg/m³, 38mm fiber Rebar top, mesh bottom
103 A & B	.890 kg/m³, 38mm fiber Rebar top, no bottom steel
104 A & B	1.780 kg/m³, 19mm fiber Rebar top & bottom
105 A & B	3.560 kg/m³, 19mm fiber Rebar top & bottom
106 A & B	1.780 kg/m³, 38mm fiber

Rebar top & bottom

(Note — The amount of fiber is the equivalent per cubic meter)

### PARAMETERS TO BE MEASURED

The following five (5) parameters were measured, with the exception of Specimen #103, which did not have any bottom steel. Only half-cell potentials and visual appearance could be evaluated for Specimen #103.

Half Cell Potential	Millivolts to copper sulfate electrode (250 mV = active corrosion)
Corrosion Current	Macro currrent between upper and lower mats
Resistance	. Electrical resistance in ohms
Linear Polarization	. Rate of corrosion
Appearance	Visual, as per Item E, chart, page 9: (1) No cracking, no spalling (2) No cracking, spalling with minimal oxidation

- (3) No cracking, minimal spalling and oxidation
- (4) Minimal cracking, spalling and oxidation
- (5) Cracking, spalling and oxidation

#### **CORROSION RESISTANCE RATINGS**

	100 <u>A&amp;B</u>	101 <u>A&amp;B</u>	102 <u>A&amp;B</u>	103 <u>A&amp;B</u>	104 <u>A&amp;B</u>	105 <u>A&amp;B</u>	106 <u>A&amp;B</u>
Α	5	4	3	5	4	3	3
В	3	2	2	-	5	4	3
С	5	3	3		3	3	3
D	2	5	1	-	3	3	4
E	5	4	3	1	2	3	3
F	20	18	12	*	17	15	16
G		10%	40%		15%	25%	20%

\* - Due to no bottom steel, several tests were not performed

A = Half-cell potentials B = Corrosion current

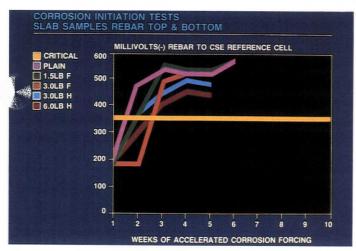
C = Resistance

D = Linear polarization

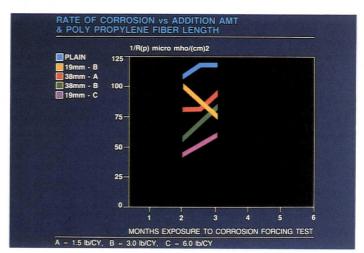
E = Appearance

F = Point total

G = Percent reduction



**21.** 1988 test results. Basically, the tests pointed out that an increase in the amount of fiber would result in an increase in the amount of time before corrosion would commence.



**22.** 1988 test results. The tests also confirmed that it was the amount of fiber, not fiber length, that controlled the delay in corrosion.

#### SURVEY OF SPECIMENS — 1991

Since the end of the active period taking readings from the prisms in 1987, the specimens have been stored outside at the location of Webster Engineering at Cleveland, Ohio. Therefore the prisms have been subjected to typical northern climatic conditions. The specimens have been stored on a paved uncovered surface subject to rain, the heat of the sun in the summer and the cold temperatures of ice and snow in the winter.

Duplicate prisms of each configuration had been made. Webster Engineering has completed a visual inspection in one of each set of prisms by sawing into the prism to the point of revealing 'ocation of the steel reinforcement in order to evaluate the eof corrosion of the steel. Also, the amount of decamination, if any, would then be noted.

The photographs reproduced here show the condition of the steel rebar after over 4 years of being embedded in concrete that has been subjected to a simulated marine environment. There is every indication that the addition of polypropylene fibers will benefit concrete which is exposed to the possibility of excessive corrosion. The authors stress that there is a difference between laboratory testing and performance in the field. Probably, due to more varied conditions of concrete, workmanship, and environment, the benefical effect of the addition of fibers may be greater in the field. The present series of tests are being carried out to simulate field conditions and the results are presented to stimulate interest in finding economical means of reducing the massive damage to concrete structures by corrosion, the world over.



23. This photograph was taken in 1987 after aging the prisms for 48 weeks

From left to right, top row:

 100B
 101B
 106B

 Plain concrete
 .890 kg, 38mm fiber
 1.780 kg, 38mm fiber

 Rebar Top & Bottom
 Rebar Top & Bottom
 Rebar Top & Bottom

From left to right, bottom row:

100A 101A 106A
Plain concrete .890 kg, 38mm fiber 1.780 kg, 38mm fiber
Rebar Top & Bottom Rebar Top & Bottom Rebar Top & Bottom
(Note — the amount of fiber is the equivalent per cubic meter)



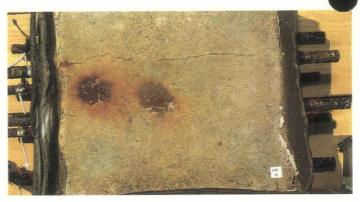
24. Prism 100A Year 1987 No fiber

A close-up of Prism 100A . Plain concrete with rebar top and bottom. Showing the surface staining from interior corrosion of the steel.



25. Prism 100A Year 1991 No fiber

A significant amount of delamination can be seen as a direct result of corrosion crossing from one steel member to another.



26. Prism 101A Year 1987 .890 kg, 38mm fiber

Prism 101A, with the equivalent of .890 kilos of 38mm fiber per cubic meter of concrete and rebar top and bottom, shows considerable staining from internal corrosion. There is a crack in the concrete which is not from plastic shrinkage but developed at a later period during testing. This crack is probably mainly responsible for the degree of corrosion which has occurred at one side of the specimen during the 48 week test period.



27. Prism 101A Year 1991 .890 kg, 38mm fiber

As suspected from the visual examination of the surface, this prism has also undergone considerable delamination as a result of corrosion from rebar to rebar. However, as noted, on the opposite side from the crack there has been very little corosion of the steel.



28. Prism 101A Year 1991 .890 kg, 38mm fiber

As noted above, the steel in the prism on the side opposite from the crack has suffered only slight damage from corrosion.



29. Prism 106A Year 1987 1.780 kg, 38mm fiber

This prism has the equivalent of 1.780 kilos of 38mm polypropylene fiber added to the mix. There is rebar on top and bottom. Visually, there seems to be a large amount of corrosion present.



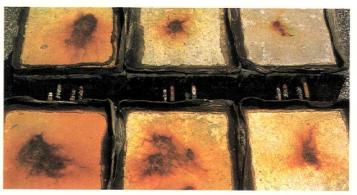
30. Prism 106A Year 1991 1.780 kg, 38mm fiber

It is interesting to note the small amount of corrosion of the steel that has occurred and which is responsible for the staining of the surface.



31. Prism 106A Year 1991 1.780 kg, 38mm fiber

A close-up of the single small area of the prism that shows any indication of corrosion.



32. This photograph was taken in 1987, after 48 weeks of aging.

_	-				
From	left	to	right.	top	row:

From left to right, top ro	w:	
100B	104B	105B
Plain concrete	1.780 kg, 19mm fiber	3.560 kg, 19mm fiber
Rebar Top & Bottom	Rebar Top & Bottom	Rebar Top & Bottom

#### From left to right, bottom row:

100A	104A	105A
Plain concrete	1.780 kg, 19mm fiber	3.560 kg, 19mm fiber
Rebar Top & Bottom	Rebar Top & Bottom	Rebar Top & Bottom
(Note — the amount of fibe	r is the equivalent per cubic	meter)



33. Prism 104A 1987 1.780 kg, 19 mm fiber

This prism has the equivalent of 1.780 kilos of 19mm polypropylene fiber per cubic meter, with rebar top and bottom. This photograph was taken in 1987, after the specimen had undergone 48 weeks of aging under extreme laboratory conditions. Compare the condition of this prism to its duplicate, Prism 104B, in illustration # 32.



34. Prism 104A 1991 1.780 kg, 19mm fiber

The specimen after being sawn to examine the two sections of rebar. Note that only minimal corrosion has occurred and the rebar appears to be in excellent condition.



35. Prism 104A 1991 1.780 kg, 19mm fiber

The same prism as shown in Illustration #34, showing the single small area in which corrosion has taken place.



36. Prism 105A 1987 3.560 kg, 19mm fiber

This specimen, with the equivalent of 3.5 kilos of 19mm polypropylene fiber and rebar top and bottom, has a moderate amount of staining showing on the surface. Its duplicate, Prism 105B, upper row in Illustration 32, appears to have less internal corrosion. Prism 105A was therefore selected in 1991 for disassembly to evaluate the degree corrosion had taken place.

#### CONCLUSION-

It is not claimed that the addition of polypropylene fibers will prevent the corrosion of steel in concrete. The tests shown in this report show that there continues to be corrosion, even with relatively large amounts of fiber present. There are many alternative methods to reduce corrosion. The major point of consideration is that the addition of fibers to concrete provides valuable improvements to a number of the physical properties of concrete, without regard to the effect on corrosion control. If, in addition to these advantages, the time before corrosion commences in a concrete structure and if the rate of corrosion is reduced, then the use of polypropylene fibers becomes a long-term economical and technical alternative worthy of serious consideration.

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Mindess,S., Properties of Concrete Reinforced with Fibrillated Polypropylene Fibers Under Impact Loading. Cement and Concrete Research Volume #18, Vancouver, British Columbia, Canada August 10, 1987



Fibermesh Company Division of Synthetic Industries, Inc. 4019 Industry Drive, Chattanooga, TN 37416 USA Phone 615/892-7243

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37. Prism 105A 1991 3.560 kg, 19mm fiber

Sawing to the rebar reveals only a minor amount of corrosion of the steel. The surface of the rebar is only slightly corroded.



38. Prisms 100, 102, and 103

This photograph was taken in 1987 at the completion of the 48 weeks of initial aging under test conditions.

From left to right, top row:

 100B
 102B
 103B

 Plain concrete
 .890 kg, 38mm fiber
 .890 kg, 38mm fiber

 Rebar Top & Bottom
 Rebar Mesh bottom
 Rebar No Bottom

From left to right, bottom row:

100A 102A 103A
Plain concrete 890 kg, 38mm fiber 8ebar Top & Bottom Rebar Top & Bottom Rebar Top & Bottom (Note — the amount of fiber is the equivalent per cubic meter)

The prisms with mesh bottom show indications of corrosion, as there is still an anode-cathode relationship to promote corrosion. As expected, the prisms without bottom layers of steel do not show any signs of corrosion.

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LETTER OF TRANSMITTAL

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### A & S LABORATORIES, INC.

2165 Sunnydale Blvd., Suite Q Clearwaler, FL 34625 (813) 441-2044

Customer:

FLORIDA ROCK INDUSTRIES, INCORPORATED

Attention:

David McFall

A & S Sample Number:

550628

Date Sampled:

06/10/97

Date Tested:

06/15/97

Reference:

Well Water

Sample Location

Bartow

The results of tests performed in accordance with FDOT Test Method PM1-T 026, Quality of Water to be Used in Concrete are as follows:

Parameter	Specification Limits	Results
Aikalinity (as CaCO <sub>2</sub> )	0.05%	0.017%
Total Organic Solids	0.05%	0.009%
Total Inorganic Solids	0.08%	0.019%
Total Chlorides	0.05%	0.003%

The water sample <u>meets or exceeds</u> specifications in Section 923-1 of FDOT Standard Specifications for Road and Bridge Construction.

Very truly yours,

Gregory P. Allen

Laboratory Director

Quality Control Manager

25	<u> </u>
55525	SANFORD SCALE CO., INC.
35255	Certificate of Inspection
55	THIS CERTIFIES THAT THE SCALES LOCATED
2525	FI. ROCK - Bartow, FI
2525	HAVE BEEN TESTED AND APPROVED THIS DATE 3 - 21 - 97
3525	SCALE TEST BASED ON STANDARDS SET BY U.S. GOVERNMENT AND FLORIDA DEPT. OF AGRICULTURE AND THIS TEST COMPLIES WITH D.O.T. SPECIFICATIONS AND FLA. STATUTE CHAPTER 531.
35555	SANFORD SCALE CO., INC. P. O. BOX 1388 SANFORD, FLORIDA 32772-1388
5252	S C L E  SERVICE DEPT. TECHNICIAN
5	

2525	SANFORD SCALE CO., INC.
125252	Certificate of Inspection This certifies that the scales located
252525	HIS CERTIFIES THAT THE SCALES LOCATED  F. ROCK  Bartew, F.
32525	HAVE BEEN TESTED AND APPROVED THIS DATE  SCALE TEST BASED ON STANDARDS SET BY U.S. GOVERNMENT AND FLORIDA DEPT. OF AGRICULTURE
25255	AND THIS TEST COMPLIES WITH D.O.T. SPECIFICATIONS AND FLA. STATUTE CHAPTER 531.  SANFORD SCALE CO., INC.  P. O. BOX 1988
555555	SANFORD, FLORIDA 32772-1388  SC LE  SERVICE DEPT. TECHNICIAN
[] []	

rs-s-s-s-s-s-s-s-s-s-s-s-s-s-s-s-s-s-s-	
SANFORD SCALE CO., INC.	
Tus centificate of Inspection	
THIS CERTIFIES THAT THE SCALES LOCATED	
HAVE BEEN TESTED AND APPROVED THIS DATE  SCALE TEST BASED ON STANDARDS SET BY U.S. GOVERNMENT AND FLORIDA DEPT. OF AGRICULTURE  AND THIS TEST COMPLIES WITH D.O.T. SPECIFICATIONS AND FLA. STATUTE CHAPTER 531	
SANFORD SCALE CO., INC.  P. O. BOX 1398 SANFORD, FLORIDA 32772-1388	
SERVICE DEPT. TECHNICIAN  3 C	

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## Concrete Products Performance Evaluation



### Mix Design Information

### General Mix Design Information

Mix Design Number: 52-5217

Mix Design Class: 4000 PSI 2" Pump Mix

Specified Strength (psi): 4000

Slump (in.): 6.0 + -1.5

Air Content (%): 3.5 + -2.0

Water/Cementitious Ratio: 0.44

Unit Weight (pcf): 137.0

### Mix Design Proportions

Material	Weight (lb.)	Volume (cu. ft.)
Type I Portland	520	2.65
Fly Ash (2.20)	160	1.17
Silica Sand	1372	8.36
S FL Lmstn. FRI, #89	1350	9.13
Water	296	4.74
Air Entrainment, oz.	6.8	0.95
Lignosulfonate Admix, oz.	13.6	

SEMCO Construction

P.06





### Collected Data and Preliminary Analysis

Seq.	طحا	LabStrength Specimens (psi)				Air	Unit	Conc	Amb.	Woter	Plastic		Moving	Range			
Tail	Test	Date	3 day	7 day	28 4ey	28 day	S6 day	Sirab	Content	Weight	Tourup.	Тетр.	Added	Age	Test	Avg of	of
			4x12 Cyl	6x12 Cyl	feel 2 Cyl	GE12 Cyl	6±12 Cyl	(in.)	(%)	(bc()	(deg F)	(deg F)	(zVyd)	(min.)	<u>(psi)</u>	3 Tests	Tat
<u>Num.</u> 1	Num.	Made 09-12-95	MIZ CH	4420	5274	5550		\$.0	N/A		N/A	N/A	0		5410		280
. 2		10-17-95		4650	6120	5946		4.0	N/A		24	N/A	0		6034)	~~~	180
3	3	10-24-95		3920	4270	4940		7.0	N/A		80	76	1		4590	5340	630
4	4	10-26-95		4460	5394	5744		4.5	N/A		· AS	82	1		5650	5420	110
5	5	11-01-95		3750	5114	4978		8.0	N/A		75	80	5		5040	5090	140
4	7	11.02-95		5580	6470	6610		6.0	N/A		78	52	.7		6540	5740	140
7	ĸ	11-43-96		4340	6030	5700		7.0	N/A		79	RA	.5		5990	5860	180
8	9	11-07-95		3920	5434	5000		6.0	N/A		82	87	.7		5020	5850	30
9	10	11-14-95		3540	4746	5300		7.25	NA		79	45	1		5120	5380	360
10	11	11-14-95		3890	4544	5054		7.5			79	65	1		5000	5040	110
11		12-01-95		3900	5.584	5000		\$.5			75	62	0		5330	5150	500
17	13			3580	51,34	5040		7.5			79	77	1		5090 4740	5140 5050	90 0
13	14			3250 3980	4740	4740		6.0 6.0			74 75	84 60	.6		5460		٥
14		12-14-95 12-19-95		3780 4200	5468 6222	5464 5470		6.0			74				5430		90
15 16	17			4450	5444	571.0		9.0			57				5690		50
17		01-05-96		3130	4620	5000		 ده			63				4910		180
18	20			3760	\$010	501.0		7.0			67	\$5	1		5010	5200	0
19	21	01-17-96		3600	4350	4490		7.0	N/A		77	74	.\$		4360	4770	so
20	22	01-18-96		4100	5179	\$1,70		7.5	N/A		76	74	0		5170	4850	Q
21	23	01-24-96		3920	4900	5350		6.25	N/A		68	. 70	0		5060	4870	550
22	24	01-25-96		3400	\$340	5060		5.0	N/A		72	58	• •		5200	5150	280
23	25	01-25-96		4030	\$520	4634		7.5	N/A		77	59	0		5070	5120	900
24	26	01-29-96		3400	4640	4640		10.0	N/A	<u>i</u>	74	64	.6		4640	4970	0
25	27	01-29-96	2630	3760	5270	5340		7,5	N/A	,	76	66	1		5320	5010	90
26	28	<b>91-31-96</b>		1130	5440	3640		E.C	N/A		82	. 74	1		\$640	5200	0
27	29	02-01-96		3600	4704	\$220		N/A	, N/A		N/A	. 69	0		\$060	5340	320
28	50	02-07-96		4250	4300	5740		7.5	N/A		74	56	. 1		6020	- 5570	560
29	31	92-09-94		3820	5760	6330		6.5	N/A		64	52	. 0		6050	\$710	570
30	32			3940	5490	\$550		7.5	N/A		65	38	0		5520	5860	60
91		021496		3480	4760	S1.30		8.0			67				5060		
32		02-16-96		4100		6204		8.0	•		72		• 0	•	6100		
33		02-16-96		4280		6178		6.3			70	6)	6		6030	5730	
34		02-20-96		3560		4790		9.0	N/A		73	64	1		4950	5690	320
35		02-21-96		4360		5620		8.3	N/A		72	. 58	• •	١	\$\$70	5520	100
36	38			4450		55.30		7.0			64	64		)	3530	5350	0
37		03-14-96		4270		5520		6.			69	66	s 0	)	5430	5510	
36	40	<b>4,</b>		3220		5250		7.0			7.	•			\$340		
39	41	01-72-46	•	5740	6108	6446		8.0	N/A		80	65	. 2	:	6270	5680	340

Filename: 2N Mix Number: 52-5217 Print Date: 12-24-1996

### Concrete Products Performance Evaluation



### **American Concrete Institute Analysis**

Average	Strength:	5370	psi
ZZVOLUGO			•

Number of Tests: 39

Design Strength: 4000 psi

Standard Deviation: 492 psi

Correction Factor (ACI 301-89 Table 3.9.1.2): 1.00

Adjusted Standard Deviation 492 psi

#### Determination of Required Average Strength

(ACI 301-89 Section 3.9.2.1 Equation 3-3): 4659 psi

(ACI 301-89 Section 3.9.2.1 Equation 3-4): 4646 psi

Minimum Required Average Strength (the larger of above equations) 4659 psi

Performance Above ACI 301/318 Minimum Required: 711 psi

Meets ACI 301-89 Section 17.2 and ACI 318-89 Section 5.6.2.3 for the acceptance of concrete strength (no single test < f'c - 500 psi and no average of 3 consecutive tests < f'c): YES

#### Control Standards (ACI 214-77{89} Table 3.5)

Class of Operation: General Construction/Field Control Testing

Concrete Performance: Very Good Adj. Standard Deviation 492 psi

Laboratory Testing Proficiency: Very Good Within Test C.V.: 3.5

As per ACI 301-89 Section 3.9.1.1 and  $\Lambda$ CI 318 Section 4.3.1.1, the above information also qualifies these mix designs:

Signature

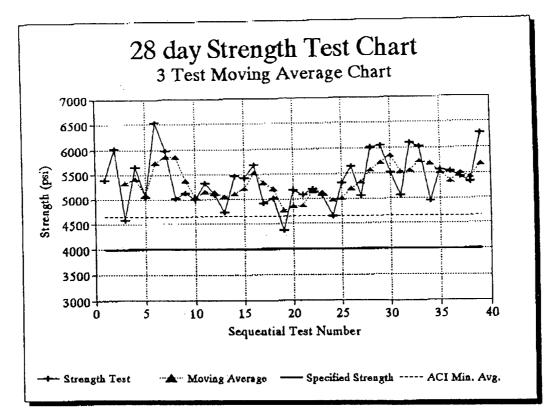
Title

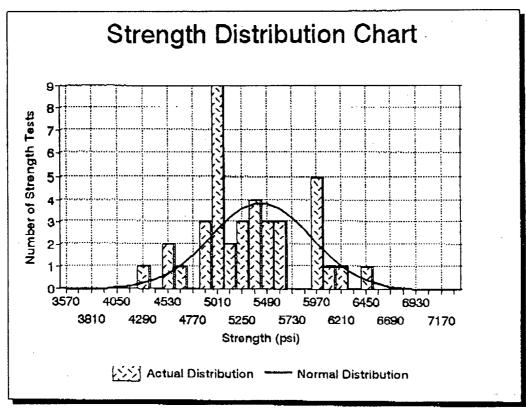
Filename: 2N Mix Number: 52-5217

## uction Fax:941-533-3376 Jun 17 '97 10:49 Concrete Products Performance Evaluation



### **Control Chart Summary**







### A & S LABORATORIES, INC.

2165 Sunnydale Blvd., Suite Q Clearwater, FL 34625 (813) 441-2044

Customer:

FLORIDA ROCK INDUSTRIES, INCORPORATED

Attention:

David McFall

A & S Sample Number:

550628

Date Sampled:

06/10/97

Date Tested:

06/15/97

Reference;

Well Water

Sample Location

Bartow

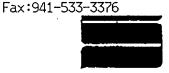
The results of tests performed in accordance with FDOT Test Method IM1-T 026, Quality of Water to be Used in Concrete are as follows:

Parameter	Specification Limits	Results
Alkalinity (as CaCO <sub>2</sub> )	0.05%	0.017%
Total Organic Solids	0.05%	0.009%
Total Inorganic Solids	0.08%	0.019%
Total Chlorides	O.U.S.W.	0.003%

The water sample <u>meets or exceeds</u> specifications in Section 923-1 of FDOT Standard Specifications for Road and Bridge Construction.

Very truly yours,

Gregory P. Allen Laboratory Director



### SOUTHDOWN, INC. BROOKSVILLE CEMENT LABORATORY TEST CERTIFICATE

16301 Ponce de Leon Boulevard - Brooksville, Florida 34614

(352) 796-7241

CONSIGNED TO: FL Rock

DATE: MAY 1997 COUNTITY 27,40 TYPE I/II

, -									
<del>-</del> . [ [			SPECIFICATION LIMITS						
TATT			TYPE	El Caya	TYPE	11			
	TEST		ASTM	AASHTO	ASTM	AASHTO			
Chemical Composition	RESULT		C-150	M-85	C-150	M-85			
% Silicon Dioxide (SiO2)	20.75	Min %			20.0	20.0			
% Aluminum Oxide (Al2O3)	5.01	Max %		7.5	6.0	6.0			
% Ferric Oxide (Fe2O3)	3.84	Max %	1 44.00	6.0	6.0	6.0			
% Calcium Oxide (CaO)	63.99	_	** <del>***</del> **;;;;	<u></u>					
% Magnesium Oxide (MgO)	0.77	Max %	6.0	6.0	6.0	6.0			
% Sulfur Trioxide (SO3):	2.91		J. 73.5	19 18 X 1 ( )					
When C3A is 8.0% or less		Max %	3.0	3.0	3.0	3.0			
When C3A is over 8.0%		Max %	3.5	3.5					
% Tricalcium Silicate (C3S)	52.96	Max %				55.0			
% Tricalcium Aluminate (C3A)	7.71	Max %			8.0	8.0			
% Alkalis (Na2O+0.658K2O)	0.51	Max %	A 10.5 i	0.60		0.60			
% Insoluble Residue	0.36	Max %	0.75	0.75	0.75	0.75			
% Loss on Ignition	1.68	Max %	3.0	3.0	3.0	3.0			
Physical Properties	31-2.10		The same of the	1,340	2 př. 3 A.	4			
Fineness: Blaine (m2/kg)	391	Min	280	280	280	280			
		Max	A A	400		400			
Time of Setting (Gillmore):			25 8 9935	7.77		1			
Initial (hours:mins)	1:57	Min	1 hour	1 hour	1 hour	1 hour			
Final (hours:mins)	3:59	Max	11.0	10 hours	i .	10 hours			
%Air Content	7.17	Max %	12.0	12.0	12.0	12.0			
Compressive Strength (PSI):		1	1.17	1 1 1 1 1	12.0	12.0			
1 Day:	2,140								
3 Day:	3,583	Min	1800	1800	1500	1500			
7 Day:	4,561	Min	2800	2800	2800	2800			
%Autoclave Expansion	0.010	Max %	0.80	0.80	0.80	0.80			
Heat of Hydration (cal/g)	77.84	1	0.00	0.00	0.60	0.60			
We certify that the cement contains		<u>.                                    </u>	1	L	L	L			

We certify that the cement contained in this shipment complies with the following current applicable specifications:

ASTM C150

[X]

AASHTO M-85 TYPE I

[X] ·

Consignee's Specs

Fed.SS-C-1960/3

[X]

AASHTO M-85 TYPE II

[X]

Cement covered by this Mill Certificate has been produced in the U.S.A.

#### **BEST AVAILABLE COPY**



## LETTER OF TRANSMITTAL

205 CENTURY BLVD., P.O. BOX 706		07/07/97 JOB NO 97086
CGC 009876 • PHONE 941 / 533-7	7193 • FAX 941 / 533-3376	ATTENTION  John Bale
TO ViroGroup, Inc.		Laidlaw Environmental Services, Inc.
P.O. Box 1867		
Lexington, S.C. 29072		Concrete submittal
Via Fax: 803-957-3845		
GENTLEMEN:		
- WE ARE SENDING YOU	X Attached Under separate c	over via the following items:
☐ Shop drawings		Samples
Copy of letter	Change order	
COPIES DATE NO.		DESCRIPTION
1 07/03/97 - #5	7 Straight cement 4000PS	I_concrete
Su	bmittal_complete	
		<del></del>
THESE ARE TRANSMITTED as checked	below:	
☐ For approval		Resubmit copies for approval
K For your use	☐ Approved as noted	Submit copies for distribution
As requested	<ul> <li>Returned for corrections</li> </ul>	Return corrected prints
☐ For review and comment		
	19	PRINTS RETURNED AFTER LOAN TO US
EMARKS	. 7	
-		
	·	
mank you		
Ed Locke		
<sub>OPY TO</sub> File		

SIGNED: Fd Locke

GENERAL OFFICE: 155 East 21st Street / P.O. Box 4667 / Jacksonville, Florida 32201 / (904) 355-1781

### FLORIDA ROCK INDUSTRIES INC Mining, Ready Mix Concrete and Construction Products

Reply To: CENTRAL FLORIDA DIVISION
P.O. BOX 119

Bartow, Florida 33830



July 3, 1997

Semco Construction Ed Locke P.O.Box 706 Bartow, FL 33831

Dear Ed,

As requested enclosed is the new mix design for your Laidlaw Project at the Bartow Airport.

After researching our file the only data we found was poured in 1995. As we discussed the use of straight cement in our mix designs is hardly ever used.

As far as the dosage rate of W.R.D.A. 64, we will adjust the amount depending on the job conditions and weather to meet your project requirements. This amount will be adjusted if ambient temperature is 90 degrees and rising.

Thank You,

Charles D. Kreitner



### MATERIALS TESTING LABORATORY

5109 Carder Road / P.O. Box 547819 Orlando, Florida 32854-7819 (407) 298-1900





#### CONCRETE MIX DESIGN

CLASS OF CONCRETE:

4000 PSI

MIX NO.:

2-5602

PROJECT:

Laidlaw at Bartow Airbase

ARCHITECT:

ENGINEER:

CONTRACTOR:

Semco Construction

DATE:

07-01-97

REPORT NO .:

**MATERIALS** 

CEMENT:

Type I/II

ASTM C 150 Broco (Florida Mining)

FINE AGGREGATE:

COARSE AGGREGATE I:

CEMENTITIOUS MATERIAL:

Silica Sand #57 Cr. Limestone ASTM C 33 ASTM C 33

Florida Rock Industries Inc Florida Rock Industries Inc

1

COARSE AGGREGATE II:

Darex AEA

AIR-ENTRAINING AGENT: CHEMICAL ADMIXTURE:

WRDA - 64

ASTM C 260 W. R. Grace & Company ASTM C 494 W.R. Grace & Company

TESTS ON AGGREGATES

FINE	Specific	Unit	Colorim	Colorimetric		GRADATION (% PASSING U.S. SIEVE)											
AGGREGATE	Gravity	Weight	Test Lighter Than Std.		Test .		Test .		3/8"	#4	#8	#16	#30	#50	#100	#200	F.M.
	2.63	102				100	99	91	62	20	3		2.25				
ARSE	Specific	Unit	L.A.	GRADATION (% PASSING U.S. SIEVE)													
AGGREGATE	Gravity	Weight	Abrasion	2"	1 1/2"	]"	3/4"	1/2"	3/8"	#4	#8	#16	F.M.				
I	2.37	84.2	35		100	100	83	34	13	4	3		6.97				
II																	

MIX DESIGN FOR

4000 PSI CONCRETE AT

28 DAYS

Cement Content*: 5.6 cwt/cu. yd.	Stump:	3.0 + - 1.5	in.	Fine Agg. Volume:	42.1	%
Water/Cement (by weight)*: 0.45	Air:	3.0 + -2.0	<b>%</b>	Unit Weight:	140.6	PCF

Based on total cementitious material.

MATERIALS	QUANTITIES (SSD BASIS)	VOLUME (CU. FT.)
Type I/N Silica Sand #57 Cr. Limestone Water Darex AEA, oz. WRDA • 64, oz.	560 1331 1650 254 1.7 11.2	2.85 8.11 11.16 4.07 .81
		<del>27.00</del>



Contractor assumes responsibility for ordering and placing mixes by Mix No. as approved by Architect/Engineer.

### Concrete Products Performance Evaluation

FEERIDA ROCK IND.



### Mix Design Information

### General Mix Design Information

Mix Design Number: 2-5402

Mix Design Class: 4000 PSI

Specified Strength (psi): 4000

Slump (in.): 4.0 + -1.0

Air Content (%): 3.0 + -2.0

Water/Cementitious Ratio: 0.48

Unit Weight (pcf): 140.2

### Mix Design Proportions

Material	Weight (lb.)	Volume (cu. ft.)
Type I Portland	540	2.75
Silica Sand	1338	8.15
S FL Lmstn. FRI, #57	1650	11.16
Water	258	4.13
Air Entrainment, oz.	1.6	0.81
Lignosulfonate Admix, oz.	10.8	





### Collected Data and Preliminary Analysis

Seq.	Lab			გი <del>ი</del>	igto Spedime	va ([w]) —			Air	Unit	Cosc	Amb.	Woter	Plaatic		Moving	Range
Test	Tat	Date	3 day	7 day	28 day	28 day	56 day	Slump	Content	Weight	Тевер.	Tomp.	Added	Age	T¢st	Avg. of	<b>્</b>
Num.	Nucs.	Made	6x12.Cyt	6x12 Cyt	6x12 Cyl	6x12 Cyl	6x12 Cy1	<u>(in.)</u>	(%)	(ka)	(deg P)	(deg F)	(FI/A)	(min.)	(psi)	3 Tests	Test
1	1	3-24-95		4680	\$790	5810		5.25	N/A		73	70	3		5800		20
2	2	4-24-95		4400	6060	5800		5.0	N/A		<b>84</b>	71	Q		5930		260
3	3	4-25-95		4910	6070	<b>61.60</b>		5.75	N/A		76	72	0		6120	5950	90
4	4	4-25-95		4100	51.94	5280		5.75	N/A		76	63	0		5240	5760	90
5	5	5-01-95		`4750	5780	5500		1.25	S/A		84	72	0		5640	5660	250
6	6	5-01-95		4960	6170	5600		4.5	N/A		83	72	0		5890	5590	\$70
7	9	5-11-95		2990	5370	1460		N/A	N/A		N/A	N/A	N/A		5420	5650	90
8	1.8	<b>9-28-9</b> 5		5370	6060	6060		60	N/A		80	74	0		4060	5790	0
9	19	9-28-95		4670	5810	5740		۵Ş	N/A		81	76	1.5		3760	5750	70
ιο	20	9-28-95		\$190	6160	6230		ş.s	N/A		93	79	0		6200	6010	70
11	21	9-28-95		ទំរួកប	6340	6270		\$.\$	N/A		93	80	Ó		6310	6090	70
12	23	10-03-95		\$120	\$ <del>99</del> 0	6110		40	N/A		92	75	ō		6050	6180	120
13	24	10-03-05		4930	5640	\$740		<del>ፈ</del> \$	NA		91	78	Q		5690	6020	100
14	25	10-03-95		4560	5340	\$430		6.0	N/A		95	50	0		5390	5710	90
15	29	10-30-95		4660	5760	58L0		4,0	N/A		86	80	0		5790	5670	50
17		10 21 00		45.00	5440	6700		4 5	\$1/A		£3	76	0		5720	4630	40

Filename: 3T Mix Number: 2-5402 Print Date: 07-01-1997



### **Concrete Products Performance Evaluation**

## American Concrete Institute Analysis

Average Strength: 5810 psi

Number of Tests: 16

Design Strength: 4000 psi

Standard Deviation: 300 psi

Correction Factor (ACI 301-89 Table 3.9.1.2): 1.16

Adjusted Standard Deviation 348 psi

Determination of Required Average Strength

(ACI 301-89 Section 3.9.2.1 Equation 3-3): 4466 psi

(ACI 301-89 Section 3.9.2.1 Equation 3-4): 4311 psi

Minimum Required Average Strength (the larger of above equations) 4466 psi

Performance Above ACI 301/318 Minimum Required: 1344 psi

Meets ACI 301-89 Section 17.2 and ACI 318-89 Section 5.6.2.3 for the acceptance of concrete strength (no single test < f'c - 500 psi and no average of 3 consecutive tests < f'c): YES

Control Standards (ACI 214-77{89} Table 3.5)

Class of Operation: General Construction/Field Control Testing

Concrete Performance: Excellent

Adj. Standard Deviation 348 psi

Laboratory Testing Proficiency: Excellent

Within Test C.V.: 1.9

As per ACI 301-89 Section 3.9.1.1 and ACI 318 Section 4.3.1.1, the above information also qualifies these mix designs:

2-5602 4000 PSI 0.45 W/C Ratio

John Ruehlen

Signature

Quality Control Manager

Title

Filename: 3T

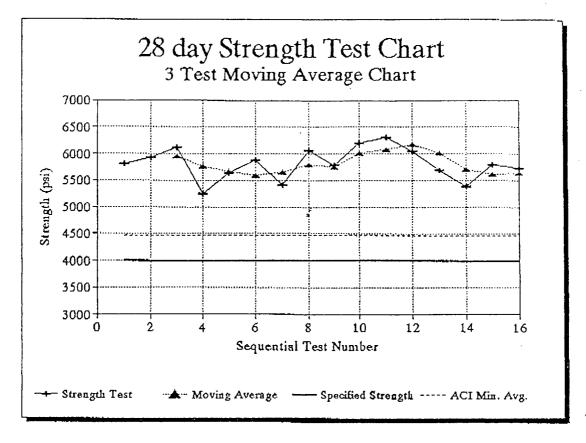
Mix Number: 2-5402

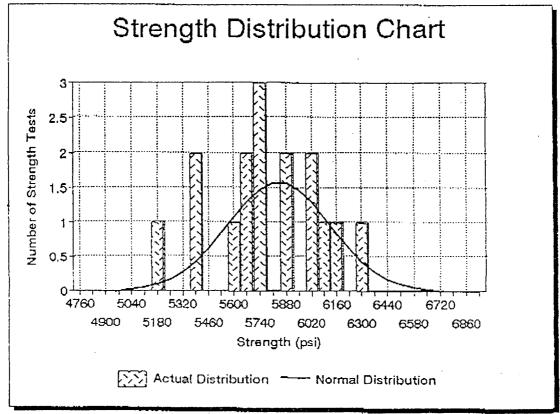
Print Date: 07-01-1991





### Control Chart Summary





Florida Rock Industries P.O. Box 547819 Orlando, FL 32854

#### Gentlemen:

This letter is to certify that Broco Type I and Type II portland cement, when shipped, is guaranteed to meet current ASTM Designation C-150.

Sincerely,

Paul H. Owen, Jr.

Manager, Technical Services

PHO/db

GENERAL OFFICE: 155 East 21st Street / P.O. Box 4667 / Jacksonville, Florida 32201 / (904) 355-1781 FLORIDA ROCK INDUSTRIES ING Mining, Ready Mix Concrete, and Construction Products

REPLY TO: Sales Office 8500 Florida Rock Road Orlando, Florida 32824-7824 407-858-0455 FAX #407-856-6255



#### LETTER OF CERTIFICATION

Mr. John Ruehlen Florida Rock Industries, Inc. P. O. Box 547819 Orlando, FL 32854-7819

Dear John:

This letter is to certify that the materials produced at our Sandland Sand Mine, FDOT Pit# 16-077, Lake Wales, Florida, meets specifications as set forth in current ASTM C-33 and/or the applicable State Department of Transportation (FDOT) Specifications for road and bridge construction as contained in the applicable State DOT book of Standard Specifications, latest edition. Also wil meet ASTM C-144 specifications for use as Masonry Sand for Masonry purposes.

If any further information is needed please let us know.

FLORIDA ROCK INDUSTRIES, INC. AGGREGATES DIVISION

e) mefeel/nw

Walter A. McFall Vice President Sales State of Florida

WAM/mm

GENERAL OFFICE: 155 East 21st Street / P.O. Box 4667 / Jacksonville, Florida 32201 / (904) 355-1781

FURIDA ROCK INDUSTRIES INC Mining, Ready Mix Concrete, and Construction Products

REPLY TO: Sales Office 8500 Florida Rock Road Orlando, Florida 32824-7824 407-856-0455 FAX #407-856-6255



#### LETTER OF CERTIFICATION

Mr. John Ruehlen Florida Rock Industries, Inc. P. O. Box 547819 Orlando, FL 32854-7819

Dear John:

This letter is to certify that the #57 and S-1-B (#89) stone distributed from our Auburndale Distribution Terminal, #TM-478, Winter Haven, Florida, meets specifications as set forth in current ASTM C-33 and/or the applicable State Department of Transportation (FDOT) Specifications for road and bridge construction as contained in the applicable State DOT book of Standard Specifications, latest edition.

If any further information is needed please let us know.

FLORIDA ROCK INDUSTRIES, INC. AGGREGATES DIVISION

ed. Mfel/m

Walter A. McFall Vice President Sales State of Florida

WAM/mm



### A & S LABORATORIES, INC.

2165 Sunnydale Blvd., Suite Q Clearwater, FL 34625 (813) 441-2044

RELORIDA ROCK TIND

Customer:

FLORIDA ROCK INDUSTRIES, INCORPORATED

Attention:

David McFall

A & S Sample Number:

550628

Date Sampled:

06/10/97

Date Tested:

06/15/97

Reference:

Well Water

Sample Location

Bartow

The results of tests performed in accordance with FDOT Test Method FMI-T 026, Quality of Water to be Used in Concrete are as follows:

<u>Parameter</u>	Specification Limits	Results
Alkalinity (as CaCO <sub>3</sub> )	0.05%	0.017%
Total Organic Solids	0.05%	0 009%
Total Inorganic Solids	0.08%	0.019%
Total Chlorides	0.05%	0.003%

The water sample <u>meets or exceeds</u> specifications in Section 923-1 of FDOT Standard Specifications for Road and Bridge Construction.

Very truly yours,

Gregory P. Allen Laboratory Director GRACE

February 6, 1997

Grace Construction Products

W.R. Grace & Co.-Conn. 1200 N.W. 15th Avenue Pompano Beach, FL 33069

(800) 433-0020 (954) 974-6700 Fax (954) 968-5586

Florida Rock Industries 5109 Carder Rd. Orlando, FL 32810

Attn: John Ruchlen

This is to certify that DAREX AEA, an air-entraining admixture, as manufactured and supplied by the Construction Products Division, W. R. Grace & Co.-Conn., is formulated to comply with Specification for Air-Entraining Admixtures for Concrete, ASTM Designation: C- 260 (AASHTO M 154).

DAREX AEA does not contain calcium chloride or chloride containing compounds as a functional ingredient. There are trace amounts of chloride present contributed from domestic water supply during manufacturing.

This is in addition to and not in substitution for our standard Condition of Sale printed on the reverse side hereof.

DLB:de

D. L. Bobolts Regional Manager

STATE OF FLORIDA : COUNTY OF BROWARD :

Swom to and subscribed, before me, this Thursday, February 06, 1997.

Av. 1997 Sended from Awy, and Desching Against

GRACE

February 6, 1997

**Grace Construction Products** 

W.R. Grace & Co.-Conn. 1200 N.W. 15th Avenue Pompano Beach, FL 33069

(800) 433-0020 (954) 974-6700 Fax (954) 968-5586

Florida Rock Industries 5109 Carder Rd. Orlando, FL 32810

Attn: John Ruehlen

This to certify that WRDA-64, a water-reducing and water-reducing retarder admixture, as manufactured and supplied by the Construction Products Division, W. R. Grace & Co.-Conn., is formulated to comply with Specifications for Chemical Admixtures for Concrete, ASTM Designation: C 494-92, Type A & D (AASHTO M194, Types A &D).

WRDA-64 does not contain calcium chloride. There are trace amounts of chloride present contributed from domestic water supply during manufacturing.

The foregoing is in addition to and not in substitution for our standard Condition of Sale printed on the reverse side hereof.

DLB:de

D. L. Bobolts Regional Manager

STATE OF FLORIDA : COUNTÝ OF BROWARD :

Sworn to and subscribed, before me, this Thursday, February 06, 1997.

Junif Contractor of Larger

## WRDA®-64

#### Water Reducing Admixture ASTM C494 Types A & D



#### **DESCRIPTION:**

WRDA® -64 is a polymer based aqueous solution of complex organic compounds. WRDA-64 is a ready-to-use low viscosity liquid which is factory pre-mixed in exact proportions to minimize handling, eliminate mistakes and guesswork.

WRDA-64 contains no calcium chloride. One gallon weighs approximately 10.1 lbs.

#### USES:

WRDA-64 produces a concrete with lower water content (typically 8 to 10% reduction), greater plasticity and higher strength. It is used in ready-mix plants, block and concrete product plants, in lightweight and prestressed work . . . wherever concrete is produced.

#### ADVANTAGES:

WRDA-64 offers significant advantages over single component water reducers. Water reduction and setting times are more consistent due to the polymer components. WRDA-64 also performs especially well in concrete containing fly ash and other pozzolans.

The use of WRDA-64 produces a plastic concrete that is more workable, easier to place and more finishable than plain or other admixtured concrete. In the hardened state, WRDA-64 concrete has higher compressive and flexural strengths at all ages than untreated or conventional admixtured concrete.

The greater degree of plasticity achieved, compared with conventional water reducing admixtures, allows improved finishability.

#### FINISHABILITY:

Finishers have stated that the cement paste, or mortar, in WRDA-64 admixtured concrete has improved trowelability. The influence of WRDA-64 on the finishability of lean mixes has been particularly noticeable. Floating and troweling, by machine or hand, imparts a smooth, close tolerance surface.

#### **ADDITION RATE:**

The addition rate range of WRDA-64 is 3 to 6 fluid ounces per 100 pounds of cement. Pretesting is required to determine the appropriate addition rate for Type A and Type D performance. Optimum addition depends on the other concrete mixture components, job conditions, and desired performance characteristics.

#### DISPENSING EQUIPMENT:

A complete line of accurate, automatic dispensing equipment is available. WRDA-64 may be introduced to the mix on the sand or in the water.

#### **COMPATIBILITY WITH OTHER ADMIXTURES:**

WRDA-64 is compatible in concrete with all air entraining admixtures such as DAREX® AEA and Daravair®. Due to the slight air entraining properties of WRDA-64, itself, the addition rate of air entraining admixture may be reduced by about 25%. By combining the separate effects of air entraining and dispersion, the water requirement of concrete may be reduced up to 15%. Each admixture should be added separately. While WRDA-64 contains no calcium chloride, it is compatible with calcium chloride in concrete mixes. Again, each should be added separately.

#### PACKAGING:

WRDA-64 is available in bulk, delivered by metered tank trucks, and in 55-gallon drums. WRDA-64 contains no flammable ingredients. It will freeze at about 28°F, but will return to full strength after thawing and thorough agitation.

### ARCHITECT'S SPECIFICATION FOR CONCRETE WATER REDUCING ADMIXTURE:

Concrete shall be designed in accordance with ACI Standard Recommended Practice for Selecting Proportions for Concrete, ACI 211.

The water reducing (or water reducing and retarding) admixture shall be WRDA-64, as manufactured by Grace Construction Products, or equal. The admixture shall not contain calcium chloride. It shall be used in strict accordance with the manufacturer's recommendations. The admixture shall comply with ASTM Designation C494, Type A water reducing (or Type D water reducing and retarding) admixtures. Certification of compliance shall be made available on request.

The admixture shall be considered part of the total water. The admixture shall be delivered as a ready-to-use liquid product and shall require no mixing at the batching plant or job site.





### GRACE CONCRETE ADMIXTURES

#### **DESCRIPTION:**

DAREX® AEA® admixture is an aqueous solution of a complex mixture of organic acid salts. It contains a catalyst for more rapid and complete hydration of portland cement. DAREX AEA is specially formulated for use as an air entraining admixture for concrete and is manufactured under rigid control which provides uniform, predictable performance. It is supplied ready-to-use and does not require premixing with water. One gallon weighs approximately 8.5 lbs.

#### **USES:**

DAREX AEA is used in ready-mix, block, and concrete products plants. It is also used on the job with job-site mixers, highway pavers. . . . wherever concrete is mixed and there is a need for purposeful air entrainment.

Because DAREX AEA plasticizes or "fattens" the mix, it is particularly effective with slag, lightweight, or manufactured aggregates which tend to produce harsh concrete. It also makes possible the use of natural sand deficient in fines

#### AIR ENTRAINING ACTION:

Air is entrained by the development of a semi-microscopic bubble system—introduced into the mix by agitation and stabilized by DAREX AEA—in the mortar phase of the concrete.

Workability is Improved. Millions of tiny air bubbles entrained with DAREX AEA act as flexible ball bearings, lubricating and plasticizing the concrete mix. This permits a substantial reduction in mixing water with no loss in slump. Placeability is improved...bleeding, green shrinkage and segregation are minimized.

**Durability is Increased.** DAREX AEA concrete is extremely durable, particularly when subjected to freezing and thawing. It has resistance to frost and deicing salts, as well as to sulfate, sea and alkaline waters.

#### COMPATIBILITY WITH OTHER ADMIXTURES:

DAREX AEA is compatible in concrete with all known accelerating admixtures, water reducing admixtures and water reducing retarders. By combining the separate effects of air entrainment with the dispersion of a water reducing admixture, the water requirement of concrete may be reduced with proportional increases in strength and improvement in durability. EACH ADMIXTURE SHOULD BE ADDED SEPARATELY TO THE MIX.

#### ADDITION RATES:

There is no standard addition rate for DAREX AEA. The amount to be used will depend upon the amount of air required under job conditions, usually in the range of 4 to 8%. Typical factors which might influence the amount of air entrained are: temperature, cement, sand gradation, and use of extra fine materials such as fly ash. Typical DAREX AEA addition rates range from 3/4 to 3 fluid ounces per 100 lbs. of cement.

The air entraining efficiency of DAREX AEA becomes even greater when used with water reducing and set retarding agents. This may allow a reduction of up to two-thirds in the amount of DAREX AEA required for the specified air content.

#### MIX ADJUSTMENT:

Entrained air results in increased yields with a consequent decrease in the cement content of the placed concrete. This condition calls for a mix adjustment, usually accomplished by reducing the fine aggregate content. This is in addition to the reduction in water content brought about by the increase in plasticity.

#### DISPENSING EQUIPMENT:

A complete line of automatic DAREX AEA dispensers is available. Accurate and simple, these dispensers are easily adapted to existing facilities on paving mixers and in batching plants.

#### PACKAGING:

DAREX AEA is available in bulk, delivered in metered tank trucks, and 55-gallon drums. DAREX AEA contains no flammable ingredients. IT FREEZES AT ABOUT 30°F, BUT ITS AIR ENTRAINING PROPERTIES ARE COMPLETELY RESTORED BY THAWING AND THOROUGH AGITATION.

### ARCHITECTS' SPECIFICATION FOR CONCRETE AIR ENTRAINING ADMIXTURE:

Concrete shall be air entrained concrete, containing 4 to 8% entrained air. The air contents in the concrete shall be determined by the pressure method (ASTM Designation C 231) or gravimetric method (ASTM Designation C 138). The air entraining admixture shall be a purified hydrocarbon type with a cement catalyst, such as DAREX AEA, as manufactured by the Construction Products Division of W.R. Grace & Co.-Conn., or equal. The air entraining admixture shall be added at the concrete mixer or batching plant at approximately 34 to 3 fluid ounces per 100 lbs. of cement, or in such quantities as to give the specified air contents.



Laidlaw Environmental Services of Bartow Florida, Inc. Add at the ndix 9 end of Appendix 9

Bartow, Florida

Drum Storage Building

Project № 12-32803.D1 Date of Issue: August 19, 1996

#### 1.5 SUPERVISION

1.5.1 All concrete work indicated on the Drawings and specified herein shall be performed under the personal and constant supervision of a competent construction superintendent or foreman experienced in this class of work.

#### CORRECTION OF CONCRETE WORK 1.6

The Contractor is responsible for correcting concrete work that does not conform to the specified requirements, including requirements for strength, tolerances, and finishes. Correct deficient concrete as directed by the Engineer.

#### PART 2 - PRODUCTS

#### 2.1 **MATERIALS:**

- 2.1.1 Water Potable and free of deleterious substances per ACI 318.
- Cement Portland Cement, ASTM C-150, Type 1, Gray, only one brand permitted throughout work.

#### 2.1.3 Admixtures -

- 2.1.3.1 Air Entraining agent per ASTM C-260. Air content shall be given percent plus or minus one percent.
- 2.1.3.2 Water reducing agent per ASTM C494, Type A, and contain not more chlorideions than are present in municipal drinking water.
- 2.1.3.3 High range water reducing admixture (superplasticizer): Per ASTM C494, Type F or G, and contain not more chloride ions than are present in municipal drinking water.
- 2.1.4 Prohibited Admixtures: Calcium chloride, thiocyanates, or admixture containing more than .05% chloride ions are not permitted.

#### 2.1.5 Aggregates -

- 2.1.5.1 Fine aggregate shall be sand conforming to ASTM C-33.
- 2.1.5.2 Coarse aggregate shall be gravel or crushed stone conforming to ACI 318, and ASTM C-33, Size #57.
- 2.1.6 Curing and Sealing Compounds per ASTM C309, minimum 30% solids content. Sodium silicate compounds are not permitted. Compounds must be non-toxic and free of taste and color. Provide "Master-cure" as manufactured by Master Builders, Inc., or an approved equal.
- 2.1.7 Polymer bonding agent shall be Weld Crete by Larsen Products Corporation or an approved equal.

Project № 12-32803.D1
Date of Issue: August 19, 1996

- 2.1.8 Epoxy Adhesive (Bonding Agent) shall be Sikadur Hi-Mod by the Sika Chemical Corporation or an approved equal. Formulation to suit application.
- 2.1.9 Non-Shrink Cement Grout: Masterflow 713 as manufactured by Master Builders or approved equal.
- 2.1.10 Vapor Barrier and Moist Curing Sheeting shall be per ASTM C171, minimum 6 mil polyethylene clear plastic sheets by Visking Company or approved equal.
- 2.1.11 Polymer Patching Mortar shall be SikaTop by the Sika Chemical Corporation. Formulation to suit application.
- 2.1.12 Cement Grout Patch Mix: Equal parts of cement and sand and sufficient water to attain workability to patch honeycombed areas and fill form tie holes solid and permanently bond to concrete.
- 2.1.13 Cement Grout Slurry Mix: Equal parts of cement and sand and sufficient water to attain consistency of heavy paint. Alternate slurry mixes and may be used by the Contractor, subject to Engineer's approval.

#### PART 3 - EXECUTION

#### 3.1 INSTALLATION:

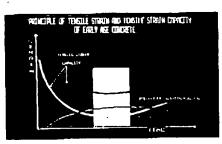
- 3.1.1 Concrete mixes shall be designed to meet the required strength qualities as noted on the structural plans by the approved testing laboratory, or use standard performance tested mix design of supplier subject to approval by the Engineer for each strength of concrete required.
  - 3.1.1.1 Class A: 4,000 psi minimum compressive strength at 28 days
     minimum 5.5 bags of cement per cubic yard, air entrained,
    with max. water: cement ratio of 0.45. Class A concrete to
    be used in all structure, including base slabs on grade, tanks,
    basins, footings, foundations, wells, trench drains, and sumps.
    Class A concrete may be used throughout the work at the
    Contractor's option.
  - 3.1.1.2 Class B: 4,000 psi minimum compressive strength at 28 days
     minimum 5.5 bags of cement per cubic yard with max.
    water: cement 0.45. Class B concrete to be used in all
    structures, including base slabs on grade, trench drains, and
    sumps not exposed to the elements.
- 3.1.2 Allowable slumps: 3 to 4-1/2 inches at delivery point
- 3.1.3 Air entrained concrete shall be used for all work exposed to the elements.
- 3.1.4 Workability of concrete shall be such that concrete can be handled, placed, and worked into angles and corners of forms, around reinforcing steel and inserts without segregation and without water and fine material rising to the surface.

### FIBERMESH ENGINEERING DATA

#### IMPORTANT

All test data reported on the following pages apply only and strictly to Fibermesh fibers.

### PROVED to Reduce Plastic Cracking and Concrete Permeability



Testing at Webster Engineering & Associates, Inc. has shown that the addition of Fibermesh fibers to plastic concrete substantially increases the resistance of the concrete to early age plastic shrinkage cracking and cracking in response to vibrations at early ages. The addition at the rate of 1.5 lb/yd3 (0.9 Kg/m3) of Fibermesh polypropylene fibers increases the tensile strain capacity (ability to resist strain without developing visible cracking) of the Immature concrete (see graph). This is particularly important since a large amount of the cracking of concrete occurs during the first 24 hours after placement, when the concrete is most susceptible to vibrations, plastic shrinkage and settlement cracking. Early age cracks, if they develop, have an effect of increasing the net permeability of the concrete and exposing substantially greater surface areas of the concrete to the detrimental environment, thus prematurely aging the concrete and shortening its performance life.

#### **CRACK PANEL STUDIES**

Tests run at San Jose State University and the University of Callfornia, Berkeley, clearly show the beneficial effect of Fibermesh fibers in controlling the magnitude of concrete cracking under adverse curing conditions. The crack inhibiting action of Fibermesh became evident in the first 4 hours of the tests and was

maintained as the concrete aged through 28 days. Tests were conducted with numerous sources of materials and mix proportions, with and without wire mesh. Without exception, the Fibermesh concrete inhibited cracking typically in the range of 90% to 100% over the non-fiber control specimen.





These accelerated test photos show a comparison between the two slabs at 24 hours. The cracking in the control slab without fiber started at 2.6 hours — most of the cracking patterns were developed at 4 hours. At 24 hours, and even after 28 days, the Fibermesh slab had virtually no cracking.

"The cycle of cracking, agents permeating and steel corroding can be somewhat interrupted or reduced by using Fibermesh polypropylene fibers."

Webster Engineering & Associates, Inc. Cleveland, Ohio

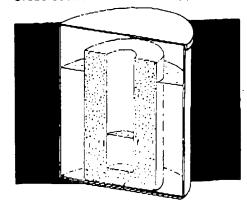
#### Water Migration/Permeability

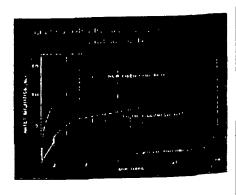
The Von Test Method of water migration measurement was used at San Jose State University to compare plain concrete with concrete reinforced with various amounts of Fibermesh.

Migration of water rates indicated reduction in permeability of 33-14% at 1.0 lb/yd³ (0.593 Kg/m³) and as high as 79% at 2.0 lb/yd³ (1.186 Kg/m³)

Note: Deneral reduction of permeability

#### Cross section of Von Test Apparatus





### FIBERMESH ENGINEERING DATA

### PROVED to Increase Concrete Abrasion Resistance

A test program designed to evaluate relative abrasion resistance was developed to measure the effect of Fibermesh fibers in concrete when exposed to excessive wear. The Army Corps of Engineers' "Method of Test for Resistance of Concrete or Mortar Surfaces to Abrasion" (Rotating Cutter Method CRD-C52-54) was used.

#### **CONCLUSION:**

"Based on the data derived from the rotating-cutter method of testing, the use of Fibermesh will increase the abrasion resistance by 105%. This added toughness with the use of Fibermesh will double the serviceable life of concrete exposed to similar wear conditions."

Paul P. Kraal, P.E. State of California

Tests were also run in cooperation with the Norwegian Highways Laboratories. Tests were

conducted on Norcem Cement's studded tire, abrasion test machine. At 42 MPH utilizing steel studded tires and 10 ton axle loads the equipment can accurately demonstrate the effects of 10 years of highway wear at the rate of 15,000 vehicles per day.

#### **CONCLUSION:**

The Fibermesh C-75 specimen exhibited a 52% increase in abrasion resistance by sustaining 34.4% less material loss than the control specimen without fibers.

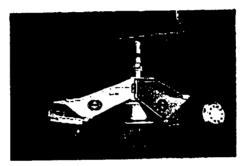
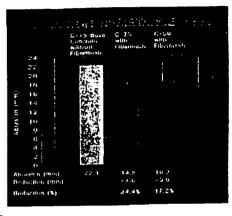


Photo and graph courtesy Norcem Cement A/S.

Significantly, the C-50 Fibermesh specimen, containing less cement, still exhibited a 20% increase in abrasion resistance over the C-75 control specimen by sustaining 17.2% less material loss.

The C-50 concrete has a base design strength of 7,252 psl while the C-75 concrete has a design strength equivalent to 10,878 psi.



## **PROVED** in Static Load Test as Alternate to Welded Wire Fabric

A comprehensive study was conducted in the laboratories of Wiss, Janney, Elstner & Associates, Inc., Consulting & Research Engineers by registered Professional Engineers. Results apply only to Flbermesh.

#### **PURPOSE OF THE TEST**

This test program compared on a large scale the flexural capacity and deflections of concrete slabs containing the recommended quantity of Fibermesh polypropylene fibers to a plain concrete slab and a concrete slab

Photo courtesy Wiss, Janney, Elstner & Assoc.

containing a typical amount of welded wire fabric (WWF) for drying shrinkage crack control purposes. All three slabs were cast from one batch of concrete.

#### **CONCLUSIONS:**

The results of the study reported herein indicate that substituting welded wire fabric with Fibermesh at a rate of 1.5 lbs. per cubic yard (0.9 kilograms/cubic meter) of concrete yields:

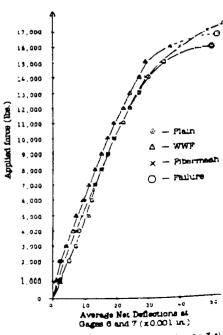
- Equivalent flexural strength capacity of the slab.
- Equivalent load-deflection relationship.

The flexural capacity of the slab containing Fibermesh was 2% higher than the slab containing welded wire fabric and 8% higher than the plain concrete slab.

The load-deflection data indicate that, with respect to flexural response characteristics, Fibermesh fibers can be used as a practical alternative to welded wire fabric which is commonly used for

shrinkage crack control purposes essentially unreinforced concrete.

Direct excerpts from the Wiss, Janney, Eistner & Associates rep



Force-versus deflection ourves for the 3 st

### FIBERMESH ENGINEERING DATA

## **PROVED** as Alternate to Welded Wire Fabric in Composite Deck Systems

### LOAD TESTS AND ENGINEERING STUDY

An engineering study based on load tests conducted by recognized authorities compared the Fibermesh micro-reinforcement system to welded wire fabric in composite metal decks.

#### **CONCLUSION:**

"As all the tests using the Fibermesh fiber reinforced concrete were equal or better than the welded wire fabric reinforced concrete tests, an equivalency for structural performance in composite slabs has been demonstrated for use of Fibermesh fibers in lieu of the normally required welded wire fabric. Also, equivalency of the diaphragm behavior with the use of Fibermesh fibers has been demonstrated." Clarkson W. Pinkham, S.E., President, S.B. Barnes Associates, Consulting Structural Engineers.

#### HEADED STUD SHEAR CONNECTOR STRENGTH TEST

As a follow-up to the load tests, a test program was conducted on the strengths of headed stud shear connectors in concrete comparing the use of Fibermesh micro-reinforcing system to the use of welded wire fabric.

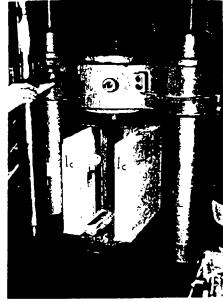
The use of welded wire fabric with metal decking has always been a problem because the correct position of the mesh is difficult to maintain in a slab that is only 2 to 3 inches (51 mm -75 mm) thick above the ribs.

The use of fiber reinforced concrete in place of welded wire fabric eliminates the construction problems and provides a consistent solution to the problems concerning the amount and location of the reinforcement.

The results of the Pushout Tests show that the strength and ductility of shear connectors in steel mesh and Fibermesh reinforced concrete are comparable.

#### **CONCLUSION:**

"Fibermesh may be substituted for weided wire fabric in composite beams with no change in the shear connector design. Shear connector values given in the AISC Specifica-

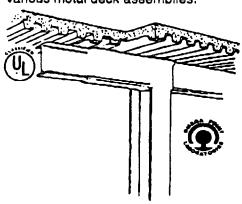


Slab Testing Machine

tion Manual of Steel Construction may be used for Fibermesh Concrete." Roger G. Slutter, Fritz Engineering Laboratory, Lehigh University, Bethlehem, Pennsylvania.

# PROVED by Underwriters Laboratories and Omega Point Laboratories as Acceptable Alternate to Welded Wire Fabric in Metal Deck Assemblies

A series of fire tests was conducted at these facilities using standard ASTM Tests E84, E119 (UL263) on various metal deck assemblies.



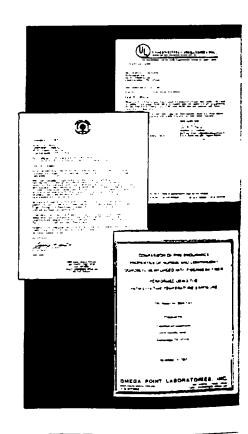
CONCLUSION OF UNDERWRITERS LABORATORIES:

"... based upon the full-scale fire test data developed with the use of

your product in a protected concretesteel form unit assembly, it is our conclusion that your polymeric fiber reinforcement would be a suitable alternate to welded wire fabric in similar type constructions. That is, concrete-steel form unit floor assemblies with protection material directly applied to the steel form unit. These constructions are currently described in the Fire Resistance Directory as D700 Series or D800 Series Designs."

### CONCLUSION OF OMEGA POINT LABORATORIES

"The results presented herein have convinced Omega Point Laboratories [O ISSUE & DIANKE! IBCOGN!!!ON IOI Fibermesh fiber as a substitution for weided wire mesh in concrete walls, flooricelling and rooficelling assemblies."



A sophisticated study of the impact resistance of concrete

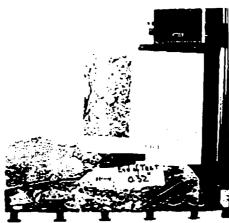
# FIBERMESH ENGINEERING DATA

# PROVED to Increase Shatter Resistance of Concrete

A test program evaluated the shatter resistance of Fibermesh increte and plain concrete when rposed to crushing loads. The specimens were 21" x 6" x 6" (525 mm x 150 mm x 150 mm) giving a height/thickness (H/T) ratio of 3½ to 1 in order to simulate a column in a high rise building. All columns were tested in a standard compression strongth machine. The rate of compression was .025" (0.635 mm) in rininute and was automatically the content of the standard compression.

#### **CONCLUSION:**

Results show the ability of Fibermesh concrete to sustain Itself and not shatter after more than 10% compression as compared to plain concrete which shattered completely shortly after first crack. This characteristic of Fibermesh concrete is important to applications where there are impact or seismic concerns for safety to life and property.



Plain concrete falls at 0.32 (8 mm) compression



Research engineer removes Fibermesh specimen after test ended. Column was compressed 10% and still remained intact.

"During the fracture, fibers are exposed. The surface of the fibers are ploughed lengthwise during pull-out which indicates a good bond between fibers and cement paste."

G.M. Idorn Consult A/S Consulting and Research Engineers Denmark

# Fibermesh specimen is free-standing after 2.0" (51 mm) compression

### PROVED to Increase Impact Resistance

A sophisticated study of the Impact resistance of concrete containing Fibermesh was conducted at the University of British Columbia, utilizing an instrumented impact machine developed by Dr. Sidney Mindess.



The results indicate the foot counds of energy to fracture cams with and without rebar.

IMPACT FRACTURE ENERGY FIBERMESH FRC
BEAMS WITHOUT REBAR

20
0.0 0.1 0.3 0.5
PIBER CONTENT % VOLUME

IMPACT FRACTURE ENERGY FIBERMESH FRC
BEAMS WITH REBAR

200
0.0 0.1 0.3 0.5
FIBER CONTENT % VOLUME

100
0.0 0.1 0.3 0.5
FIBER CONTENT % VOLUME

CONCLUSION: The addition of Fibermesh fibers shows remarkable increases in energy absorption/impact of both plain and steel reinforced concrete.

The Fibermesh fibers act in two

ways. They "bridge" the cracks that develop, thereby inhibiting further crack growth and enhance the bond between the concrete and the reinforcing bars by inhibiting cracking of the concrete under bearing stresses in the vicinity of the bar deformations.

"It is worth emphasizing the point that there appears to be a synergistic effect when fibers are combined with conventional reinforcement; together, they are much more effective than when the effects of each are considered separately."

Sidney Mindess, Arnon Bentur, Department of Civil Engineering, University of British Columbia,

Vancouver, Canada

### FIBERMESH ENGINEERING DATA

#### PROVED-**Physical Properties** of Fibermesh

Absorption Spectic Gravity

- Nil -0.9

Fiber Length

- ¼″, ½″, ¾″, 1¼″ 2" and Multi-Design Gradations (nominal 3, 13, 19, 38, 51mm and Multi-Design Gradations)

Melt Point

- 320°F-340°F (160°C-170°C)

Ignition Point Thermal Conductivity - Low Electrical Conductivity - Low

- 1100°F (590°C)

Acid and Salt Resistance - High

10<sup>3</sup>kal

Modulus (Youngs) - 0.5 (3.5 kN/mm²)

The following test data were produced by Signet Laboratory from ready mixed concrete and issued in a report entitled "Evaluation of FIBERMESH Synthetic Fibers in Concrete," by P. Kraai, PE.

#### A. NORMAL WEIGHT CONCRETE

1. COMPRESSIVE STRENGTH ASTM C-39, psi (MPa) 1 psl = .006895 MPa

Control 7 days 2030 (14.0) 3905 (26.9) 28 days

**Fibermesh** 2270 (15.7) 4240 (29.2)

II. FLEXURAL STRENGTH ASTM C-78, psl (MPa) (6"x6"x18" Beams) (15×15×46cm) Modulus of Rupture

7 days 28 days

Control **Fibermesh** 258 (1.8) 288 (2.0) 358 (2.5) 390 (2.7)

III. SPLITTING TENSILE STRENGTH ASTM C-496, psi (MPa)

Control 7 days 178 (1.2) 275 (1.9) 28 days

**Fibermesh** 194 (1.3) 290 (2.0)

#### **B. LIGHTWEIGHT AGGREGATE** CONCRETE

I. COMPRESSIVE STRENGTH ASTM C-39, psi (MPa)

> Control Fibermesh 7 days 1295 (8.9) 1275 (8.8) 2655 (18.3) 28 days 2780 (19.2)

II. FLEXURAL STRENGTH ASTM C-78, psi (MPa)

> Control **Fibermesh** 3 days 315 (2.2) 300 (2.1) 28 davs 515 (3.6) 563 (3.9)

JIII. SPLITTING TENSILE STRENGTH ASTM C-496, pel (MPa)

> Control **Fibermesh** 7 days 248 (1.7) 215 (1.5) 28 days 303 (2.1) 310 (2.1)

#### FIBERMESH GUIDE SPECIFICATION

Use only 100 percent virgin polypropylene fibrillated, MD Graded, fibers containing no reprocessed olefin materials and specifically manufactured to an optimum gradation for use as concrete secondary reinforcement. Application per cubic yard shall equal a minimum of 1.5 pounds (0.9 Kg/m3). Fibers are for the control of cracking due to drying shrinkage and thermal expansion/contraction, to lower concrete permeability, to increase impact capacity, shatter resistance and abrasion resistance, while adding fibrillated toughness and residual strength. Fiber manufacturer must document evidence of 5 year satisfactory performance history, ISO 9002 certification of manufacturing facility, compliance with applicable building codes and centify performance in accordance with ASTM C-1116, Type III, 4.1.3 and ASTM C-1116 (Ref. ASTM C-1018) Performance Level 1, I<sub>s</sub> outlined in Section 21, Note 17 and a minimum average Residual Strength of 50 psi, of 4 beams from a single batch. Fibrous concrete reinforcement shall be manufactured by Fibermesh, 4019 Industry Drive, Chattanooga, Tennessee, USA, 37416, (423) 892-7243.

Available in The Construction Specifications institute format, both as printed hardcopy and as IBM-PC/DOS, MS/DOS computer software. Call your local Fibermesh representative.

#### **APPLICATION GUIDELINES**

#### Do specify Fibermeah for:

- The reduction of concrete cracking as a result of Intrinsic stresses.
- · A superior method and cost-effective alternate to welded wire fabric for secondary and/or temperature reinforcement.
- A reduction in the permeability of concrete.
- · Greater impact, abrasion, shatter and fatigue resistance in concrete.
- · Support and cohesiveness in the concrete on steep inclines and/or slipformed placements.
- · Provides Residual Strength.
- · Placements where all materials must be non-metallic.
- Areas requiring materials which are both alkaliproof and chemical resistant.
- · Improved durability.
- Fibrillated toughness.

#### Don't specify Fibermesh for:

- . The control of cracking as a result of external stresses.
- Increasing the structural number of PC concrete in pavement or slabs on grade.
- · Higher structural strength develop-
- The elimination or reduction In curling and/or creep.
- The justification for a reduction in the size of the support columns.
- · The replacement of any moment or structural steel reinforcement.
- Increasing of ACI and/or PCA control Joint guidelines.
- The thinning-out of bonded or unbonded overlay sections.
- . Decreasing the thickness of slabs on grade.

#### Active member of

American Concrete Institute

National Ready Mixed

Concrete Association



ACPA - American Concrete Pavement Association

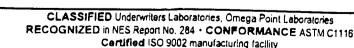
ARTBA - American Road & Transportation Builders Association

ACPA - American Concrete Pipe

ASCC - American Society for Concrete Construction

NPCA - National Precast Concrete Association

SFA - Synthetic Fiber Association



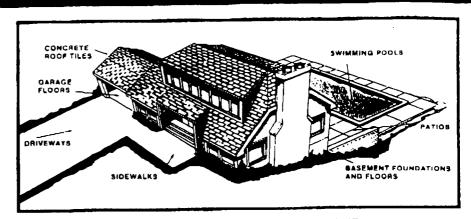




# FIBERMIX® and FIBERMIX® STEALTH® — for Concrete

FIBERMIX is 100% polypropylene synthetic fiber specially engineered to inhibit the formation of concrete plastic shrinkage cracking.

- Building Code Report NES No. 414
- · Distributes tens of millions of crack inhibiting engineered fibers
- · Achieves a superior concrete job
- · Safe and simple to use
- Easy to finish
- Pumpable
- · Rustproof and alkaliproof



DON'T GIVE CONCRETE CRACKS A HOME.

# HARBOURITE® - for Stucco, Precast Products, Shotcrete

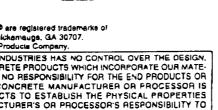
Harbourite® is 100% polypropylene fiber engineered for micro-reinforcement of stucco and shotcrete. Also used in precast concrete pipe, block and tile.

- · Inhibits cracking due to drying shrinkage
- · Provides new dimension in stucco toughness, shatter resistance
- Easy, safe to use—just add to mix
- · No corrosion or chemical reaction -alkaliproof
- Reduces rebound and material loss in gunite, shotcrete applica-
- Makes concrete pipe and precast products tougher, more durable with resistance to spalling and impact
- · Alternate system to non-structural wire mesh

Fibermestr®, Fibermid®, Steath® and Harbourite® are registered trademarks of Synthotic Industrios, Inc., 209 LaFeyette Road, Chickemauge, GA 30707. Microban® is a registered trademark of Microban Products Company.

THE FIBERMESH DIVISION OF SYNTHETIC INDUSTRIES HAS NO CONTROL OVER THE DESIGN. MANUFACTURE, OR TESTING OF THE CONCRETE PRODUCTS WHICH INCORPORATE OUR MATE-RIALS. THEREFORE, FIBERMESH ASSUMES NO RESPONSIBILITY FOR THE END PRODUCTS OR USES MADE OF OUR MATERIALS. THE CONCRETE MANUFACTURER OR PROCESSOR IS RESPONSIBLE FOR TESTING ITS PRODUCTS TO ESTABLISH THE PHYSICAL PROPERTIES THEREOF. IT IS THE CONCRETE MANUFACTURER'S OR PROCESSOR'S RESPONSIBILITY TO CERTIFY COMPLIANCE OF ITS PRODUCT, INCLUDING ANY FORMULATION WHICH MAY INCLUDE OUR SYNTHETIC FIBER MATERIALS.









#### Fibermesh® Division

Figermoon Europe I,Id Smeckley Wood Close,



# 1. PRODUCT NAME AQUA KURE WHITE

Liquid membrane forming concrete curing compound, WATER BASED, WHITE PIGMENTED.

2. MANUFACTURER
LAMBERT CORPORATION
20 N. COBURN AVENUE
ORLANDO, FLORIDA 32805
PHONE (407) 841-2940
TOLL FREE 800-432-4746
FAX (407) 839-1890

#### 3. PRODUCT DESCRIPTION

AQUA KURE - WHITE is a liquid membrane forming concrete curing compound. When applied to freshly placed concrete surfaces, it forms a surface membrane which prevents rapid evaporation of the mixing water necessary for proper concrete curing and strength development. AQUA KURE -WHITE when tested according to the water retention test ASTM C-156, will restrict the loss of water to not more than 0.55 kg/m² in 72 hours. The white pigmentation of AQUA KURE reflects the heatproducing rays of the sun, thereby helping to keep the concrete surface cooler. The white pigmentation will also help prevent excessive heat build-up and reduce the cause of thermal cracking during the curing period. AQUA KURE - WHITE is available in two groups of product, one for State Department of Transportation application (state certified), and the second for construction application meeting ASTM C-309.

The concrete curing state begins at the moment the cement hydration process begins and continues until hydration is complete, approximately 28 days. This is one of the most critical periods in concrete construction. The chemical reaction which takes place during the first few days after the pour will determine greatly the final quality of concrete. Concrete will

develop the majority of its strength in the first 7-14 days, but the hydration process must be allowed to continue if the concrete is to reach its planned strength. If the moisture content of the concrete is lost before the hydration is complete, the concrete cannot develop its maximum planned strength.

#### Advantages

Most economical of all curing

Permits proper hydration of cement. Assures concrete that is hard and highly resistant to deterioration.

Prevents scaling, hair checking, and dusting of concrete.

Excellent reflectance qualities.

Easy application by hand or power

Protects the surface of fresh concrete from damage resulting from early rainfall.

#### Basic Uses

Protection of concrete is considered vital in today's high tech world. This is particularly true of structures like bridges and highways which are subject to a variety of damaging chemicals and physical abuse. Most concrete engineers are unanimous in their insistence that fresh concrete be protected as quickly as possible with a concrete curing compound. The concept of a liquid membrane system for curing concrete was developed in the early 1950's. It was a great simplification over the previous curing methods. AQUA KURE -WHITE is a thoroughly tested water based liquid membrane curing compound that will conform to ASTM C-309, federal, state, county, and municipal specifications. It provides efficient, economical concrete curing for all types of construction.

#### Limitations

Do not use AQUA KURE - WHITE on surfaces to be covered by paint, resilient flooring or ceramic tile, or other subsequent products without removal of the AQUA KURE - WHITE residue. This may be done through a stiff wire brooming of the surface, a riding floor scrubber, water blast or sandblast. Around columns or perimeters near walls, removal may entail grinding, sandblasting or liquid strippers depending on the thickness of the compound. Good

concrete paints, epoxies, liquid floor hardeners, sealers, ceramic tile cements, are formulated to give maximum adhesion when applied to a clean concrete surface. Always follow the surface preparation requirements of the manufacturer of the subsequent product to be installed.

Test areas should be applied when uncertain of surface conditions or unfamiliarity of product exist. Tests will determine if the surface is properly prepared for adequate adhesion, best method of application, and probable coverage rate.

#### Applicable Standards

ASTM C-309-91, Type 2, Class A.B (Liquid Membrane Forming Compounds for Curing Concrete)

AASHTO-M148, Type 2, Class A, B (when light reflectance is waived)

#### Composition and Materials

Hydrocarbon resin emulsion, white pigment, suspended in water. Contains no wax, paraffin or oil.

#### 4. TECHNICAL DATA

Color	White
Solids	26-30%
Bulk Density	
Flash Point	
Freeze Point	
Dry Time	
Moistire Loss	37 Kg/M

#### 5. INSTALLATION

Before using this product, please refer to the Material Safety Data Sheet for additional handling instructions. Proper handling precautions MUST be taken.

#### When To Apply -Horizonial Surfaces

Curing compounds only work if they are on top of the concrete surface and do not penetrate. The timing of application is important. AQUA KURE-WHITE should be applied after setting of cement, immediately after evaporation of the surface water sheen and the concrete surface will not be marred by foot traffic. It is during this time that the concrete is most vulnerable to spalling, hairchecking, and other surface defects. If surface is dry, it should be completely dampened (no puddles) before applying AQUA KURE.

#### Vertical Surfaces

Application should be made immediately after the forms have been removed and walls are rewetted with clean water. Allow excess water to run off before applying AQUA KURE. WHITE. For uniform application on vertical surfaces, the specified rate of application may be achieved by two coats applied at an interval of approximately 4 hours. Do not apply to interfacing of channels to be caulked with elastomeric sealants. This can be avoided by masking.

#### **Application Methods**

Stir AQUA KURE - WHITE thoroughly prior to use. Do not dilute or alter product. Apply with spray, brush, roller, or lambswool applicator. On smooth concrete use spray, lambswool applicator or short-nap roller. On rough concrete (broomed or textured) use spray, brush, or long-nap roller. Apply uniformly to form a continuous film on the surface without thick or ponded areas. A power airless sprayer will give best results for large areas. Industrial low pressure type pump sprayer is recommended for small areas. To ensure proper application with sprayers, use only a clean or new industrial grade sprayer equipped with a non-adjustable fan tipped nozzle, neoprene hose and gaskets. Maintain sufficient pump pressure throughout application. Uniform surface coverage is essential, avoid puddling in low areas. If material starts to come out of nozzle in a stream, versus a fog, or starts to come out in spits and sputters, the nozzle has become clogged. Stop immediately and clean nozzle with lacquer thinner before proceeding. Clean the sprayer immediately after use with soap and water or lacquer thinner.

#### Cautions

Apply at temperatures above 50°F. Use adequate ventilation. For interior applications, ventilation system should be capable of exchanging total air volume in application area in 30 minutes or less. Avoid prolonged or repeated breathing of vapor or spray mist. KEEP OUT OF THE REACH OF CHILDREN. Contains a petroleum distillate.

#### Clean Up

Clean brushes, tools, sprayers, rollers and other equipment with soap and water, lacquer thinner, toluol, or xylol. First Aid

Eye Contact: Hold eyelids open and immediately flush with plenty of lukewarm water for at least 15 minutes and call a physician.

Skin Contact: Wash thoroughly with soap and water. If irritation persists, seek medical aid.

Inhalation: Remove from exposure, administer oxygen if breathing is difficult.

Ingestion: Do not induce vomiting. Small amounts of liquid aspirated into lungs may cause serious pulmonary injury.

#### Safety Equipment

Solvent resistant gloves, goggles and if applied in areas of poor or inadequate ventilation, use mine safety mask and canister (Organic Vapor Canister No. 77705 GMA).

#### 6. COVERAGE

Compliance with ASTM C-309 specification is an application rate of 200 square feet per gallon.

Dept. of Transportation coverage rate is 200 square feet per gallon.

#### 7. PACKAGING

55 gallon drums 5 gallon pails

#### 8. STORAGE

Store upright or on side away from excessive heart. Retighten bungs immediately after each use to avoid contamination.

#### 9. WARRANTY NOTICE

LAMBERT CORPORATION products are designed to be used in the construction industry and should be applied by competent persons in accordance with current published instructions. We cannot be held responsible for difficulty caused by inferior materials and conditions, or by inferior workmanship. LAMBERT reserves the right to have the true cause of any difficulty determined by accepted test

methods by an independent party. Any claim regarding product defect must be received in writing 1 year from day of shipment. No claim will be considered without such written notice or after the specified time interval.

DISCLAIMER OF WARRANTIES AND LIMITATION OF LIABILITY: LAMBERT CORPORATION, (Seller) warrants that if any goods supplied prove defective in workmanship or material, that Seller shall replace them or refund their purchase price. THIS WARRANTY IS MADE IN LIEU OF ANY AND ALL OTHER WARRANTIES, EXPRESSED OR IMPLIED, INCLUDING THE WARRANTIES OF MERCHANT-ABILITY AND/OR FITNESS WHICH ARE HEREBY DISCLAIMED. IT IS UNDERSTOOD AND AGREED THAT BUYER'S SOLE REMEDY, AND THEREFORE SELLER'S LIABILITY, WHETHER IN CONTRACT, TORT, UNDER ANY WARRANTY, IN NEGLIGENCE, OR OTHERWISE SHALL BE LIMITED TO THE RETURN OF THE PURCHASE PRICE PAID BY PURCHASER OR REPLACEMENT OF ANY DEFECTIVE GOODS SOLD BY SELLER AND UNDER NO CIRCUMSTANCES SHALL SELLER BE LIABLE FOR SPECIAL, INDIRECT OR CONSEQUENTIAL DAMAGES. THE PRICE STATED FOR THE GOODS IS A CONSIDERATION IN LIMITING SELLER'S LIABILITY. Any liability or risk resulting from the use of this product is assumed by the PURCHASER/USER except where a specific warranty is provided by the manufacturer in writing. Before application, the PURCHASER USER shall determine the suitability of the product for his intended use and PURCHASER/USER assumes all liabilities and risks whatsoever in connection therewith. THERE ARE NO WARRANTIES WHICH EXTEND BEYOND THE FACE HEREOF.

#### Vertical Surfaces

Application should be made mediately after the forms have been removed and walls are rewetted with clean water. Allow excess water to run off before applying AQUA KURE -WHITE. For uniform application on vertical surfaces, the specified rate of application may be achieved by two coats applied at an interval of approximately 4 hours. Do not apply to interfacing of channels to be caulked with elastomeric sealants. This can be avoided by masking.

#### Application Methods

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Ingestion: Do not induce vomiting. Small amounts of liquid aspirated into lungs may cause serious pulmonary injury.

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#### 7. PACKAGING

55 gallon drums 5 gallon pails

#### 8. STORAGE

Store upright or on side away from excessive heart. Retighten bungs immediately after each use to avoid contamination.

#### 9. WARRANTY NOTICE

LAMBERT CORPORATION products are designed to be used in the construction industry and should be applied by competent persons in accordance with current published instructions. We cannot be held responsible for difficulty caused by other materials and conditions, or by inferior workmanship. LAMBERT reserves the right to have the true cause of any difficulty determined by accepted test

methods by an independent party. Any claim regarding product defect must be received in writing I year from day of shipment. No claim will be considered without such written notice or after the specified time interval.

DISCLAIMER OF WARRANTIES AND LIMITATION OF LIABILITY: LAMBERT CORPORATION, (Seller) warrants that if any goods supplied prove defective in workmanship or material, that Seller shall replace them or refund their purchase price. THIS WARRANTY IS MADE IN LIEU OF ANY AND ALL OTHER WARRANTIES, EXPRESSED OR IMPLIED. INCLUDING THE WARRANTIES OF MERCHANT-ABILITY AND/OR FITNESS WHICH ARE HEREBY DISCLAIMED. IT IS UNDERSTOOD AND AGREED THAT BUYER'S SOLE REMEDY, AND THEREFORE SELLER'S LIABILITY. WHETHER IN CONTRACT, TORT. UNDER ANY WARRANTY, IN NEGLIGENCE, OR OTHERWISE SHALL BE LIMITED TO THE RETURN OF THE PURCHASE PRICE PAID BY PURCHASER OR REPLACEMENT OF ANY DEFECTIVE GOODS SOLD BY SELLER AND UNDER NO CIRCUMSTANCES SHALL SELLER BE LIABLE FOR SPECIAL, INDIRECT OR CONSEQUENTIAL DAMAGES. THE PRICE STATED FOR THE GOODS IS A CONSIDERATION IN LIMITING SELLER'S LIABILITY. Any liability or risk resulting from the use of this product is assumed by the PURCHASER/USER except where a specific warranty is provided by the manufacturer in writing. Before application, the PURCHASER USER shall determine the suitability of the product for his intended use and PURCHASER/USER assumes all liabilities and risks whatsoever in connection therewith. THERE ARE NO WARRANTIES WHICH EXTEND BEYOND THE FACE HEREOF.

## APPENDIX 10

**Secondary Containment Hydrostatic Test Results** 

Project № 12-32803.D1 Date of Issue: August 19, 1996

- specified strength, and not more than 10% of the strength tests shall have values less than the specified strength.
- 3.3.14 Additional tests (including coring) may be required if deemed necessary by the Engineer due to failure of any of the above tests, poor workmanship, questionable concrete, etc. These tests shall be paid for by the Contractor.
- 3.3.15 If core tests fall below the design specified strength, concrete represented by the weaker strength samples shall be removed and replaced.
- 3.3.16 Testing laboratory representative shall inspect all reinforcing steel placement prior to concrete placement and this inspection shall verify bar size, spacing, location in member and concrete cover is per the Plans and Specifications.
- 3.3.17 Copies of all inspection and test results shall be forwarded to the Gen. Contractor, Engineer, Concrete Subcontractor and Owner.

#### 3.4 REPAIR/REPLACEMENT OF DEFECTIVE CONCRETE

3.4.1 The Engineer may required the complete replacement of excessively defective concrete, and repairs as required to correct defective concrete.

#### 3.5 CLEAN-UP:

3.5.1 At the completion of the work, remove from the site all excess materials and debris. Leave entire area in a neat and broom clean condition. Throughout work, maintain areas free of materials and debris which would interfere or be dangerous to other trades.

#### 3.6 TESTING OF REQUIRED WATERTIGHT CONCRETE STRUCTURES

- 3.6.1 All concrete structures which are to hold stormwater, liquids, water and/or provide containment (tanks, basins, wells, sumps, trench drains, etc.) shall be tested by the Contractor prior to any backfilling for watertightness.
- 3.6.2 The test shall be hydrostatic test by filling the structure to maximum 1' above the operating level or to the top level with water and allowing to stand for a period of 48 hours. The level of the water shall be checked after 24 hours and at the end of the time period. Allowance for evaporation will be taken into account.
- 3.6.3 Any detectable leaks are to be repaired and the structure retested until a satisfactory test is made.
- 3.6.4 If the water level is lower at the end of the test period by a significant amount and no leaks are detected, the structure shall be drained and the bottom slab inspected for any leaks. After repair, the structure shall be retested until a satisfactory test is made.

-END OF SECTION-

Udd at start of appendix

03300 - 8

#### Water Levels for Cells with Fiber Concrete (1.5 lbs./cubic yard)

vater	20,000,000,000,000	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0	· , , , , , , , , , , ,			Water Loss - Evap.
Cell	Base Reading	24-hours	48-hours	Delta @ 24-hours	Delta @ 48-hours	Evaporation @ 48-hours (2.)	@ 48-hours
A	4 7/16	4 9/16	4 5/8	1/8	3/16	1/16	2/16
В	4 3/8	4 1/2	4 9/16	1/8	3/16	1/16	2/16
С	4 3/8	4 17/32	4 5/8	5/32	1/4	1/16	3/16
D	4 5/16	4 15/32	4 17/32	5/32	7/32	1/16	3/16
Ε	4 7/16	4 11/16	4 25/32	1/4	11/32	1/16	5/16
Н	4 3/4	4 15/16	5	3/16	1/4	1/16	3/16
1	4 1/8	4 3/8	4 3/8	1/4	1/4	1/16	3/16
J	4 1/2	4 1/2	4 5/8	0	1/8	1/16	1/16
К	4 23/32	4 25/32	4 13/16	1/16	3/32	1/16	1/16
L	4 3/16	4 5/16	4 7/16	1/8	1/4	1/16	3/16
М	4 3/8	4 7/16	4 1/2	1/16	1/8	1/16	1/16
Ν	4 3/8	4 7/16	4 7/16	1/16	1/16	1/16	0
0	3 7/8	3 29/32	4 3/32	1/32	7/32	1/16	3/16
P	4 11/16	4 25/32	4 13/16	3/32	1/8	1/16	1/16
Q Q	4 7/16	4 5/8	4 5/8	3/16	3/16	1/16	2/16

Average 2/16
Range 0 to 5/16
Standard Deviation 1/16

Average Permeability

1.92E-06 cm/sec

#### Water Levels for Cells without Fiber Concrete

Cell F G	Base Reading 5 5/32 4 13/16	24-hours 5 1/2 5 21/32	Delta @ 24-hours 11/32 27/32	Delta @ 48-hours 17/32 2 11/32	Evaporation @ 48-hours (2.) 1/16 1/16	Water Loss - Evap. <u>@ 48-hours</u> 8/16 2 5/16	Water Migration Rate (3.) Adjusted for Fiber 3/16 14/16
					Cell F Cell C		Adjusted Permeability (cm/sec) 2.66E-06 1.31E-05

Notes: 1. All readings reported to the nearest 1/32-inches and calculations to the nearest 1/16-inches.

- 2. Evaporation based on an average temperature of 73 F and a relative humidity of 46% for the first 24 hours and an average temperature 71 F and a relative humidity of 44% for the second 24 hours under the following conditions: no sunlight and no wind. This resulted in an evaporation of 1/16-inches over the 48-hour period.
- 3. Fiber assumed to result in a 61.5% reduction in water migration based on testing conducted by Dr. Paul P. Kraai, P.E. at San Jose State University in California.
- 4. The theoretical permeabilities of concrete without fiber and with 1.5 lbs of fiber per cubic yard are 5.21E-6 cm/sec and 8.68E-7 cm/sec respectfully based upon Dr. Kraai's research

Results of Previous Hydrostatic Test indicated that Cells F and G would require repair and retesting. Following is the results of the retest for Cells F and G performed after addition repairs where completed. Tests were conducted between December 4. 1997 to December 6, 1997 by Mr. Horace Kirklam (LES). Results of the retest indicate that Cells F and G are performing satisfactory.

#### Results of Hydrostatic Water Test for Cells F and G

Water Loss - Evap.

Cell	Base Reading	24-hours	48-hours	Delta @ 24-hours	Delta @ 48-hours	Evaporation @ 48-hours (2.)	@ 48-hours
F	5 7/16	5 17/32	5 5/8	3/32	3/16	1/16	2/16
G	5 3/32	5 5/32	5 1/4	1/16	5/32	1/16	2/16

**Actual Permeability** 

	(cm/sec)
Cell F	1.86E-06
Cell G	1.40E-06

Notes: 1. All readings reported to the nearest 1/32-inches and calculations to the nearest 1/16-inches.

- 2. Evaporation rate assumed to be the same as previous tests, 1/16 of an inch.
- 3. Fiber assumed to result in a 61.5% reduction in water migration based on testing conducted by Dr. Paul P. Kraai, P.E. at San Jose State University in California.
- 4. The theoretical permeabilities of concrete without fiber and with 1.5 lbs of fiber per cubic yard are 5.21E-6 cm/sec and 8.68E-7 cm/sec respectfully based upon Dr. Kraai's research

# LES FACILITY BARTOW, FL DRUM STORAGE BUILDING CELL VOLUMES

CELL	ACTUAL VOLUME (CUBIC FEET)	DESIGN VOLUME (CUBIC FEET)	REQUIRED VOLUME (CUBIC FEET)
Α	175.69	188.60	117.6
В	145.69	154.68	94.1
С	101.56	106.32	70.6
D	118.68	137.73	94.1
E	88.17	106.32	70.6
F	120.54	154.68	94.1
G	162.32	188.60	117.6
11	231.83	239.23	176.5
[	186.54	193.64	141.2
J	153.35	163.03	105.9
K	162.54	163.03	105.9
L	109.12	105.28	58.8
M	161.48	163.03	105.9
N	163.13	163.03	105.9
O	211.39	207.69	117.6
P	251.87	239.23	176.5
Q	199.88	193.64	141.2

- Notes: 1. Actual volume for each cell based on field measurements taken by Mr. Horace Kirkland, LES, on October 31, 1997.
  - Design and required volumes based on calculations performed by ViroGroup on January 22, 1997.
  - 3. Required volume is equal to 10 percent of the total volume to be stored in each cell with the exception of Cell O which requires a volume of 25 percent of the total volume to accommodate a planned future permit to store PCB's.
  - 4. A factor of 7.48 gallons per cubic foot was used.
  - 5. This table replaces an earlier version. This table contains no changes in "Actual Volumes" or "Design Volumes" columns. A review of the "Required Volumes" data revealed that a clerical error had been made in transferring this data from the planning and design effort to the preparation of design drawings.

Exchange for appendip

# LES FACILITY BARTOW, FL DRUM STORAGE BUILDING CELL VOLUMES

CELL	ACTUAL VOLUME (CUBIC FEET)	DESIGN VOLUME (CUBIC FEET)	REQUIRED VOLUME (CUBIC FEET)
A	175.69	188.60	70.6
В	145.69	154.68	94.1
C	101.56	106.32	94.1
D	118.68	137.73	94.1
E	88.17	106.32	94.1
F	120.54	154.68	94.1
G	162.32	188.60	94.1
Н	231.83	239.23	70.6
I	186.54	193.64	70.6
J	153.35	163.03	117.7
K	162.54	163.03	82.4
L	109.12	103.65	94.1
M	161.48	163.03	94.1
N	163.13	163.03	94.1
Ο	211.39	207.69	47.1
P	251.87	239.23	176.5
Q	199.88	193.64	141.2

- Notes: 1. Actual volume for each cell based on field measurements taken by Mr. Horace KirklaM, LES, on October 31, 1997.
  - 2. Design volumes based on calculations performed by ViroGroup on July 12, 1997.
  - 3. Required volume is equal to 10 percent of the total volume to be stored in each cell.