

FLORIDA DEPARTMENT OF  
ENVIRONMENTAL PROTECTION  
OCT 07 2010  
SOUTHWEST DISTRICT  
TAMPA

**Report of  
Geotechnical Engineering Services  
Lena Road Landfill  
Stage 2  
Manatee County, Florida**

**September 30, 2010**



# Andreyev Engineering, Inc.

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▼ Groundwater ▼ Environmental ▼ Geotechnical ▼ Construction Materials Testing

Project No. CPGT-10-0062  
September 28, 2010

**TO: PBS&J**  
482 South Keller Road  
Orlando, FL 32810  
Attention: Mr. Joseph Miller, P.E.

**SUBJECT: Results of Geotechnical Investigation**  
Lena Road Landfill, Stage 2,  
Manatee County, Florida

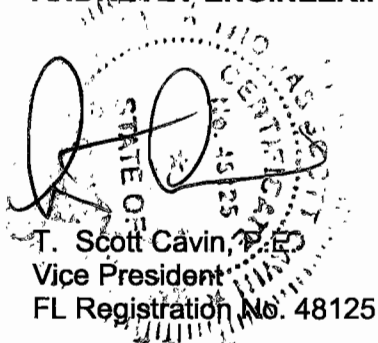
Dear Mr. Miller:

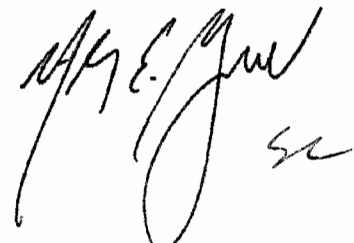
Andreyev Engineering Inc. has completed a geotechnical investigation for the Stage 2 portion of the Lena Road Class 1 Landfill operated by Manatee County. This report and the information contained are intended to address geotechnical assessment related items required for landfill design and construction.

We appreciate the opportunity to provide our services on the project and trust that this report is sufficient to address the geotechnical matters related to the project. Should you have any questions regarding this report, please feel free to contact the undersigned.

Sincerely,

**ANDREYEV ENGINEERING, INC.**

  
T. Scott Cavin, P.E.  
Vice President  
FL Registration No. 48125



Nicolas E. Andreyev, P.E.  
President

cc: Manatee County  
FDEP – Tampa District

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## 1.0 INTRODUCTION

This geotechnical investigation was conducted in support of renewal of the operating permit for the Lena Road Class 1 landfill in Manatee County. We understand the landfill is divided into 3 separate tracts, of which Stage 1 has been filled to capacity and Stage 3 is currently being filled. This work encompasses geotechnical assessment of the remaining stage (Stage 2). We further understand that the 3 stages contain perimeter slurry walls which are keyed into the top of the first confining layer beneath the property.

The investigation presented herein is intended to address FDEP review comments documented in the letter dated June 16, 2010 concerning renewal of the operating permit. Specifically, this investigation addresses items 3a through 3d of the letter, which request additional geotechnical and hydrogeologic information.

## 2.0 SCOPE OF INVESTIGATION

Our scope of investigation consisted of the following:

1. Conducted a detailed review of all previous geotechnical reports and landfill design drawings.
2. Investigated the deep subsurface conditions within Stage 2 by drilling nine (9) Standard Penetration Test borings. These additional borings were conducted to provide better coverage of the landfill footprint and investigate deep subsurface conditions in areas where this information is absent. The borings were drilled to depths ranging from 60 to 100 feet. The additional borings were drilled in the areas that were not drilled previously or where previous borings were not drilled sufficiently deep to allow proper assessment for foundation support and settlement analysis.
3. Conducted a series of engineering index property tests on the subsurface soils, including:
  - Moisture content
  - Percent fines content
  - Atterberg Limits
4. Evaluated the collected field and laboratory test data, prepared location plans, soil profiles, geologic cross sections through the soil boring alignments, presenting subsurface strata in elevation (ft-NGVD).
5. Conducted geotechnical evaluations of foundation bearing capacity including justification of selected parameters.
6. Conducted circular and block failure slope stability analyses. A total of four (4) slope conditions were be evaluated
7. Conducted analyses of immediate and long term settlement under the landfill and developed a settlement contour map using the settlement data points.

8. Evaluated the sinkhole potential using available published geologic maps and reports, FAVA report, sinkhole databases, photolineament analysis, and site specific boring data.
9. Prepared this comprehensive geotechnical report presenting the results of the testing, assessment of conditions, and engineering evaluations in support of landfill design and response to the FDEP RAI.

### **3.0 SITE LOCATION AND DESCRIPTION**

The site is located in Section 31, Township 34 South, Range 19 East and Section 6, Township 35 South, Range 19 East, Manatee County, Florida. It is approximately 1,500 feet south of Highway 64 and 3,500 feet east of Lena Road. An existing Class 1 landfill which is owned and operated by Manatee County is located immediately south of the project area. The subject property consists of approximately 115 acres and is designated as Stage 2.

Regionally, the site is located in a relatively flat, poorly drained low recharge area. Ground surface elevations occur at approximately +34 to +35 ft-NGVD. Based on review of the USGS quadrangle map (Lorraine FL) the subject property and surrounding area contain wetlands which discharge off-site via small creeks and sloughs which drain to the Manatee River. A site vicinity map is shown superimposed on the USGS quadrangle map on the attached **Figure 1**.

The project will consist of the Stage 2 area located immediately north of the existing Stage 1 landfill. Currently the property consists of a combination of vacant property, yard waste processing area, vehicle storage area, and a borrow pit and pile. An aerial photograph showing the Stage 2 landfill area and the various current uses is shown on the attached **Figure 3**.

We understand that a bentonite slurry wall is constructed around the entire perimeter of Stage 2. The wall extends to the first competent natural clay layer below the site and is intended to be a cutoff for horizontal flow outside the landfill boundaries. In addition, we understand that a series of leachate collection pipes are installed throughout the Stage 2 property and have inverts ranging from +16 to +27 ft-NGVD. The collection piles will also serve to control groundwater level below natural levels found outside the slurry wall.

This property has been the subject of geotechnical engineering studies in the past by Ardaman and Associates, including a comprehensive geotechnical study (reports dated August 29, 1985 and October 31, 1988), and progress reports during slurry wall construction (report dates ranging from June 1989 through August 1989).

#### 4.0 S.C.S. SOIL SURVEY

The "Soil Survey of Manatee County, Florida" published by the U.S. Department of Agriculture Soil Conservation Service (S.C.S.) was reviewed. The predominant shallow soil types identified at the site are as follows:

- **Eaugallie fine sand (20)**, which is a nearly level, poorly drained sand. The seasonal high groundwater table is between 10 and 40 inches deep. Permeability is rapid in the surface layer, moderate or moderately rapid in the subsoil, and rapid in the substratum.
- **Floridana-Immokalee-Okeelanta (26)**, which is a nearly level, poorly drained sand. The seasonal high groundwater table is between 25 and 40 inches deep. Permeability is very rapid.

A copy of the SCS Soil Survey is provided in **Figure 2**.

#### 5.0 PHOTOLINEAMENT STUDY AND SINKHOLE INVENTORY

Lineaments are defined as physical features of the earth's surface which are oriented in linear arrangements. Photolineaments are lineaments which are identified using aerial photographs in combination with topographic maps. These surface features typically represent underlying fractures of the limestone bedrock and are represented by trough like depressions, ridges marked by significant vegetation changes or changes in soil colorations. The enhanced topographical surface characteristics of fractures in the underlying limestone are typically caused by increased surface recharge which causes solution of overlying strata.

Vertical fracturing in a carbonate aquifer system can occur from propagation of basement structures through the overlying carbonates in response to crustal flexing caused by earth tides (Blanchet, 1957). Surface lineaments have been long recognized as surface manifestations of underlying vertical to near-vertical zones of fracture concentrations (Lattman and Parizek, 1964). Surface lineaments are typically orthogonally oriented with angles between 45 and 55 degrees east and west of north. In a karst carbonate aquifer system, fracture zones can be enlarged by chemical dissolution.

In order to examine photolineaments existing within and in the vicinity of the subject property, AEI utilized an aerial photograph with a scale of 1"=2,000' and a topographic map with a scale of 1"=2,000'. The photograph was inspected for soil colorations, natural drainage features, depression areas possibly indicating karst conditions and vegetation changes. In addition to the aerial photograph, a five foot contour topographic map was used to inspect the surface topography for depressions and sinks which may indicate surface subsidence caused by past karst activity.

Based on this analysis, there are no significant physical features which appear to represent potential fractures (photolineaments) within, the subject site. A map showing the results of the photolineament analysis is provided on **Figure 4**.

The Florida Geological Survey (FGS) Subsidence Incident Report database documenting sinkhole activity was reviewed and no new sinkholes in the vicinity of the subject property were identified. Based on this survey and the observed surficial topographic setting within the project area and immediate vicinity, the area has no reported sinkhole activity. In addition, PBS&J conducted an inventory of sinkhole occurrences from the Center for Instructional Technology sinkhole database at the University of South Florida. A copy of the Center's published map with the subject landfill superimposed is provided on **Figure 5**. The results indicate no sinkhole occurrences within a radius of 5 miles.

An evaluation of sinkhole potential was conducted by Ardaman and Associates and is documented in their report dated August 29, 1985. The results of the evaluation did not reveal evidence of sinkhole activity or sinkhole potential. The Ardaman findings are therefore consistent with this report.

## **6.0 SITE SPECIFIC INVESTIGATION**

A total of nine (9) SPT borings were drilled in the area of the Stage 2 property. The locations of the borings are presented on the attached **Figure 6**.

### **Natural Subsurface Conditions**

Borings B-1 through B-9 were drilled in the throughout the Stage 2 landfill area to depths ranging from 60 to 100 feet below existing ground. Subsoils at the boring locations were found to be relatively consistent. The encountered soils generally consisted of fine sands and slightly silty fine sands starting at ground surface and extending to depths of approximately 20 to 25 feet, followed by silty fine sand with phosphates to depths ranging from 25 to 30 feet. Below these surficial sands and silty sands the borings encountered alternating layers of sandy clay, silty clay and clay with phosphates extending to the boring termination depths of 60 to 100 feet. Impervious clay soils were consistently found in all borings drilled for this assessment.

Based on the SPT-N values, the surficial sands and slightly silty sands were generally found to be in a loose to medium dense state. The underlying silty sands were also found to be in a loose to medium dense state. The underlying sandy to silty clays and clays were generally found to be in a stiff to hard condition. Zones of very soft to soft clay were noted in a depth of approximately 2 feet in some of the borings.

Results of the borings are presented in profile form on **Figure 7** along with the results of soil classification tests and groundwater level measurements indicated adjacent to the associated borings and at the tested depths.

Borings drilled previously by Ardaman and Associates were generally consistent with these boring results.

### **Groundwater Conditions**

The groundwater table was measured in the open boreholes at the location of the borings. The groundwater table depths were found to range from 4.3 to 8.0 feet below existing grade. Based on surface elevations at the borings, these depths translate to groundwater elevations

ranging from +26.0 to +32.7 ft-NGVD. The following table provides a summary of the groundwater measurements and estimated elevations.

Well	Groundwater Depth (ft)	Groundwater Elevation (ft-NGVD)	Date of Reading
B-1	4.3	32.7	7/28/10
B-2	5.0	29.0	7/27/10
B-3	5.0	29.0	7/28/10
B-4	4.6	29.4	7/30/10
B-5	4.5	29.5	7/29/10
B-6	6.8	28.2	8/03/10
B-7	8.0	26.0	8/02/10
B-8	8.0	26.0	8/02/10
B-9	4.6	28.4	7/29/10

## 7.0 LABORATORY TESTING

A series of laboratory tests were conducted on the natural subsurface soils. The tests included natural moisture content, percent fines passing the number 200 sieve, and Atterberg Limits.

### Moisture and -200 Tests

The percent moisture content and percent of fines passing the number 200 U.S. Standard sieve were conducted on selected soil samples. A total of fourteen (14) tests were conducted on natural soils. The results of the tests are shown adjacent to the soil profiles and at the tested depths of the soil profiles on **Figure 7**. The visual soil classification was reviewed and revised after the laboratory tests were completed.

### Atterberg Limit Tests

Atterberg Limit tests were conducted on soft clay strata for the purpose of determining the liquid limit, plastic limit and plasticity index of the selected soil samples. A total of six (6) Atterberg Limit tests were conducted. The results of the tests are shown adjacent to the soil profiles and at the tested depths of the soil profiles on **Figure 7**.



## 8.0 GEOTECHNICAL ANALYSIS

### Bearing Capacity

Analysis of the foundation bearing capacity and subgrade settlement were based on a fill elevation of +135 ft-NGVD with side slopes of 4:1 (H:V), and an average fill density of 60 pounds per cubic foot. Based on ground surface elevations, the height of the landfill will be approximately 100 feet above natural grade. The bottom of the landfill will be a minimum of 3 feet below the lowest adjacent grade.

The bearing capacity of the landfill is a function of the density of the soils and the depths of the landfill materials below the adjacent ground surface. Soil density was defined by the Standard Penetration Test (SPT) N-value. Based on the assumptions stated above and on the data obtained from the borings, a net allowable foundation bearing pressure of 19,583 pounds per square foot was calculated. The net foundation load is estimated to be approximately 6,000 pounds per square foot, for a worst case area, which is well below the capacity of the foundation soils. The results of the evaluation are presented in **Attachment A**.

An additional bearing capacity analysis was conducted at the top of the first encountered clay layer. The purpose of this analysis was to verify sufficient bearing capacity at the clay interface and to ensure bearing pressure of the landfill material does not impact the slurry wall. For this analysis it was assumed that the clay depth is 20 feet below existing grade. Based on the assumptions stated above and on the data obtained from the borings, a net allowable foundation bearing pressure of 28,102 pounds per square foot was calculated, which is well above the estimated net foundation load. The results of the additional evaluation are also presented in **Attachment A**.

Based on the analysis, bearing failure is not a concern for this landfill design. As such, the perimeter slurry wall will not be impacted by vertical or lateral ground movements resulting from foundation bearing instability. The more critical stability component with regard to the existing slurry wall will be vertical settlement due to consolidation of the sands and clays underling the landfill.

### Slope Stability

The stability of the proposed Stage 2 landfill was evaluated along selected critical sections of the landfill profile. For each of the sections, the stability was analyzed for the end-of-construction conditions representing long term stability of the landfill. A total of four (4) landfill cross sections were evaluated. The cross section transect locations are presented on the attached **Figure 9**.

The long term stability analyses were performed using "Effective Stress Stability Analysis (ESSA)". The effective stress strength parameters for the various soil layers were assumed conservatively using the laboratory test data and empirical relationships.

The stability of the slopes was analyzed using STABL for Windows. The soft clay layer found at approximately 20 feet is the weakest layer in the soil profile and the minimum factor of safety for the slopes was analyzed using sliding block failure surfaces through the soft clay layer. A

critical failure surface searching method using a random technique for generating sliding block surfaces passing through the soft clay was used. The stability analyses were performed using Modified Janbu Method and the active and passive portions of the sliding surfaces were generated according to Rankine's theory.

The results of the stability analyses are presented in the plots and text outputs in **Attachment B**. The minimum factor of safety values for all sections are tabulated below:

Cross Section	Factor of Safety
A-A'	1.70
B-B'	1.90
C-C'	1.93
D-D'	1.68

The lowest resulting factor of safety of 1.68 is greater than 1.5, the required minimum factor of safety specified in 62-701.400 FAC. Thus, the landfill slopes are considered stable.

**Settlement**

To evaluate the impact of potential total settlement due to the loads to be placed in the Stage 2 landfill, settlement calculations were conducted for the encountered subsurface conditions at individual boring locations. The total settlement of the soil column for each boring location was calculated using elastic settlement equations for the sand layers and consolidation settlement methods for cohesive material. Settlement calculations were conducted at each of the boring locations presented herein, and at two locations within the landfill footprint from the previous geotechnical studies. The total settlement calculated for each boring location is summarized below:

Settlement Calculation Results	
Boring	Settlement (ft)
B-1	0.90
B-2	1.15
B-3	0.72
B-4	0.67
B-5	0.75

B-6	0.74
B-7	0.39
B-8	0.98
B-9	0.36
TH-16	0.80
TH-17	0.77

The results of the evaluation are presented in **Attachment C** along with supporting references and additional information regarding assumptions.

### **Settlement Contouring**

The GMS computer model was utilized to import the coordinates of the settlement calculation points. The model allows generation of contour maps, color flood maps and 3-D surface maps using the imported data. The areas between data points are interpolated/extrapolated by the model. The model has several interpolative and smoothing methods to create the data sets for mapping. To minimize model related distortions and over-smoothing appearance of the data, we have selected a method that is relatively linear with minimal distortion or smoothing of the data.

The method used to grid the landfill area and to interpolate/extrapolate the data between the boring locations is the Natural Neighbor Method using a constant nodal function. Natural neighbor interpolation is based on the Thiessen polygon network of the scatter point set. The Thiessen polygon network can be constructed from the Delauney triangulation of a scatter point set. A Delauney triangulation is a TIN that has been constructed so that the Delauney criterion has been satisfied.

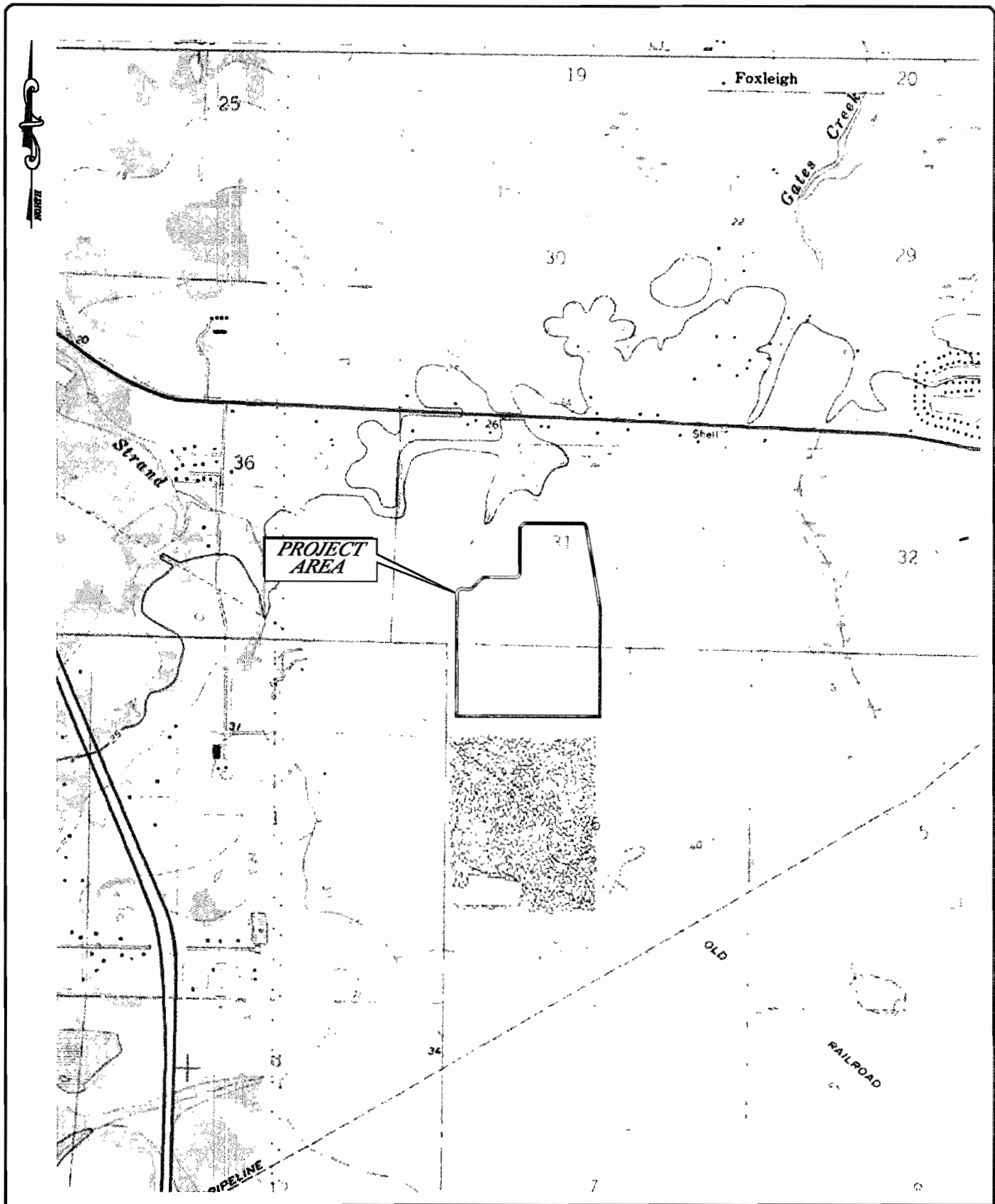
These generated contours are presented on the attached **Figure 10**, and may be used for evaluation of slurry wall impacts and/or leachate pipe slopes.

## **9.0 SUMMARY AND CONCLUSIONS**

The results of the field and laboratory investigations indicate that the subsurface soils across the project area are relatively consistent from one location to the next and are in a dense and stable condition for the purposes of landfill bearing, slope stability and settlement.

Based on review of available literature, survey information, and site specific explorations the sinkhole potential at this site is classified as low.

## FIGURES



**REFERENCE:**  
 U.S.G.S. LORRAINE, FLA.  
 QUADRANGLE MAP  
 DATED 1973  
 PHOTOREVISED 1987  
 SECTIONS 6 & 31  
 TOWNSHIP 34 & 35 SOUTH  
 RANGE 19 EAST



**Andreyev  
 Engineering,  
 Inc.**

GEOTECHNICAL INVESTIGATION  
**LENA ROAD LANDFILL  
 STAGE II**  
 MANATEE COUNTY, FL

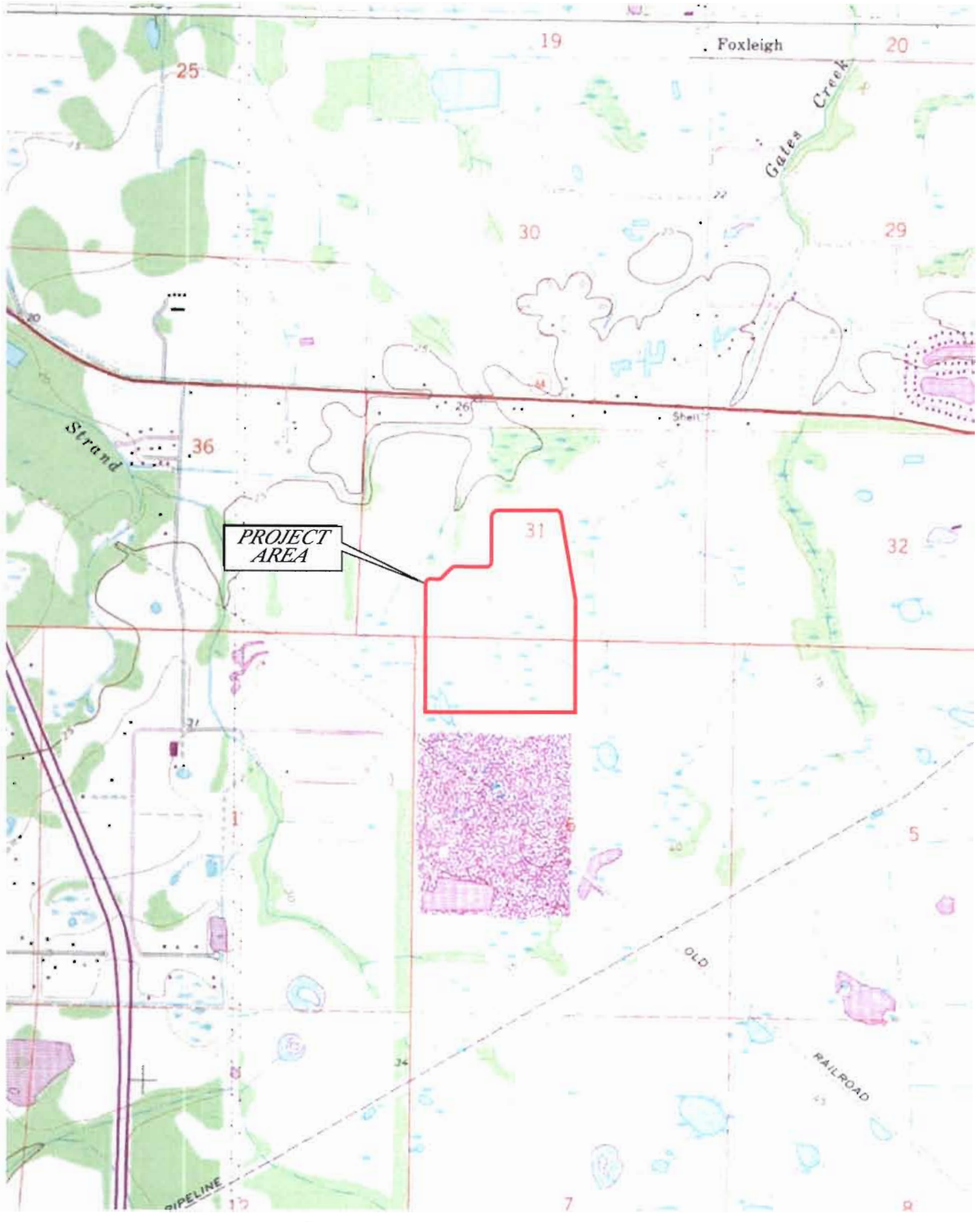
APPROXIMATE SCALE:  
 1" = 2000'

DATE: 08/27/10  
 PN: CPGT-10-0062

ENGINEER: SC  
 DRAWN BY: DLS

VICINITY MAP

FIGURE 1



REFERENCE:  
 U.S.G.S. LORRAINE, FLA.  
 QUADRANGLE MAP  
 DATED 1973  
 PHOTOREVISED 1987  
 SECTIONS 6 & 31  
 TOWNSHIP 34 & 35 SOUTH  
 RANGE 19 EAST



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GEOTECHNICAL INVESTIGATION  
**LENA ROAD LANDFILL  
 STAGE II**  
 MANATEE COUNTY, FL

APPROXIMATE SCALE:	DATE: 08/27/10	ENGINEER: SC
1" = 2000'	PN: CPGT-10-0062	DRAWN BY: DLS

VICINITY MAP  
 FIGURE 1



**LEGEND:**

- APPROXIMATE SUBJECT PROPERTY BOUNDARY
- 11 CASSIA FINE SAND
- 20 EAUGALLIE FINE SAND
- 26 FLORIDANA-IMMOKALEE-OKEELANTA ASSOCIATES
- 99 WATER



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GEOTECHNICAL INVESTIGATION  
**LENA ROAD LANDFILL  
STAGE II**  
MANATEE COUNTY, FL

APPROXIMATE SCALE:

1"=1000'

DATE: 08/27/10

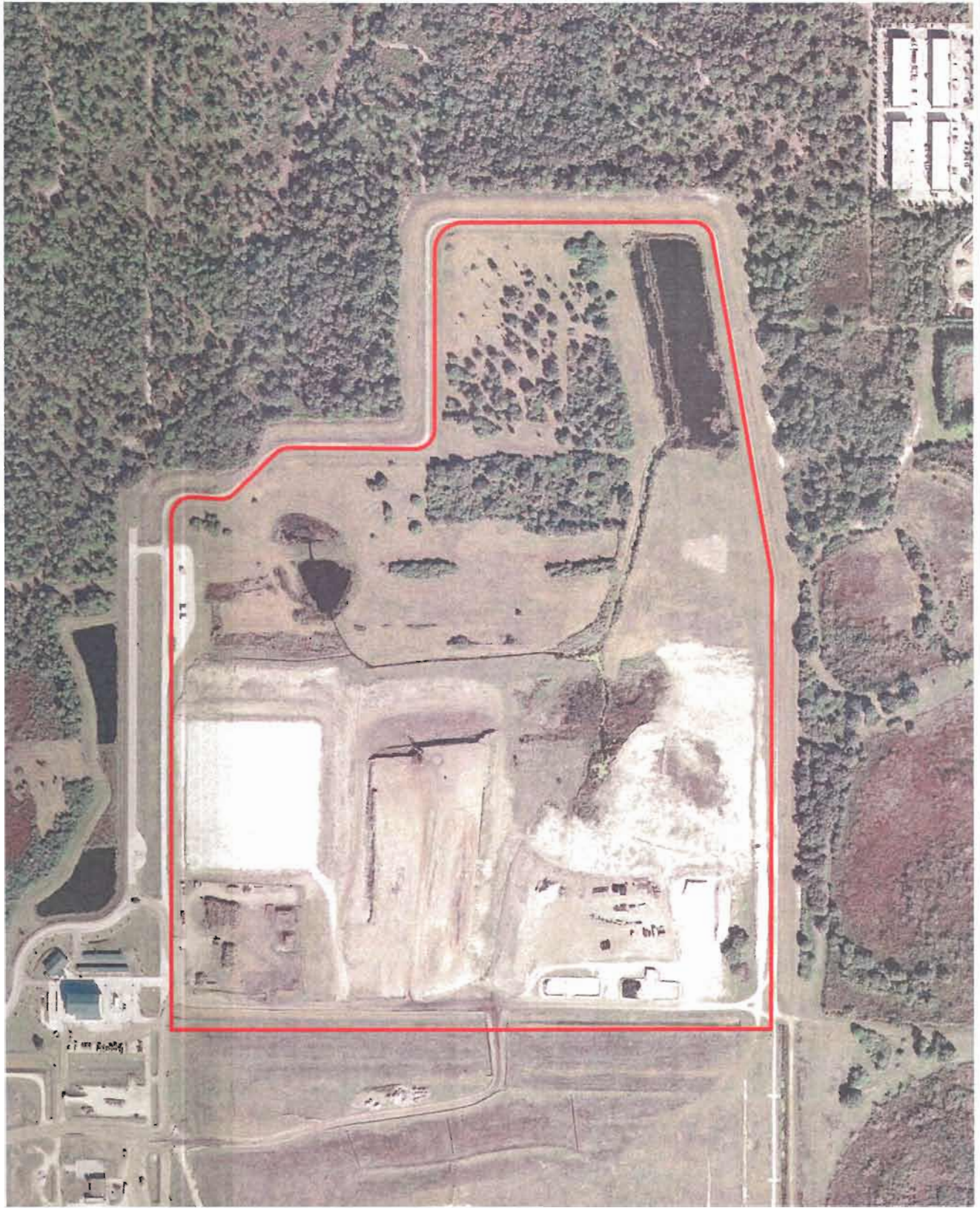
PN: CPGT-10-0062

ENGINEER: SC

DRAWN BY: DLS

SCS SOIL SURVEY

FIGURE 2



**LEGEND:**

— APPROXIMATE SUBJECT PROPERTY BOUNDARY



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APPROXIMATE SCALE:

1" = 500'

DATE: 08/27/10

ENGINEER: SC

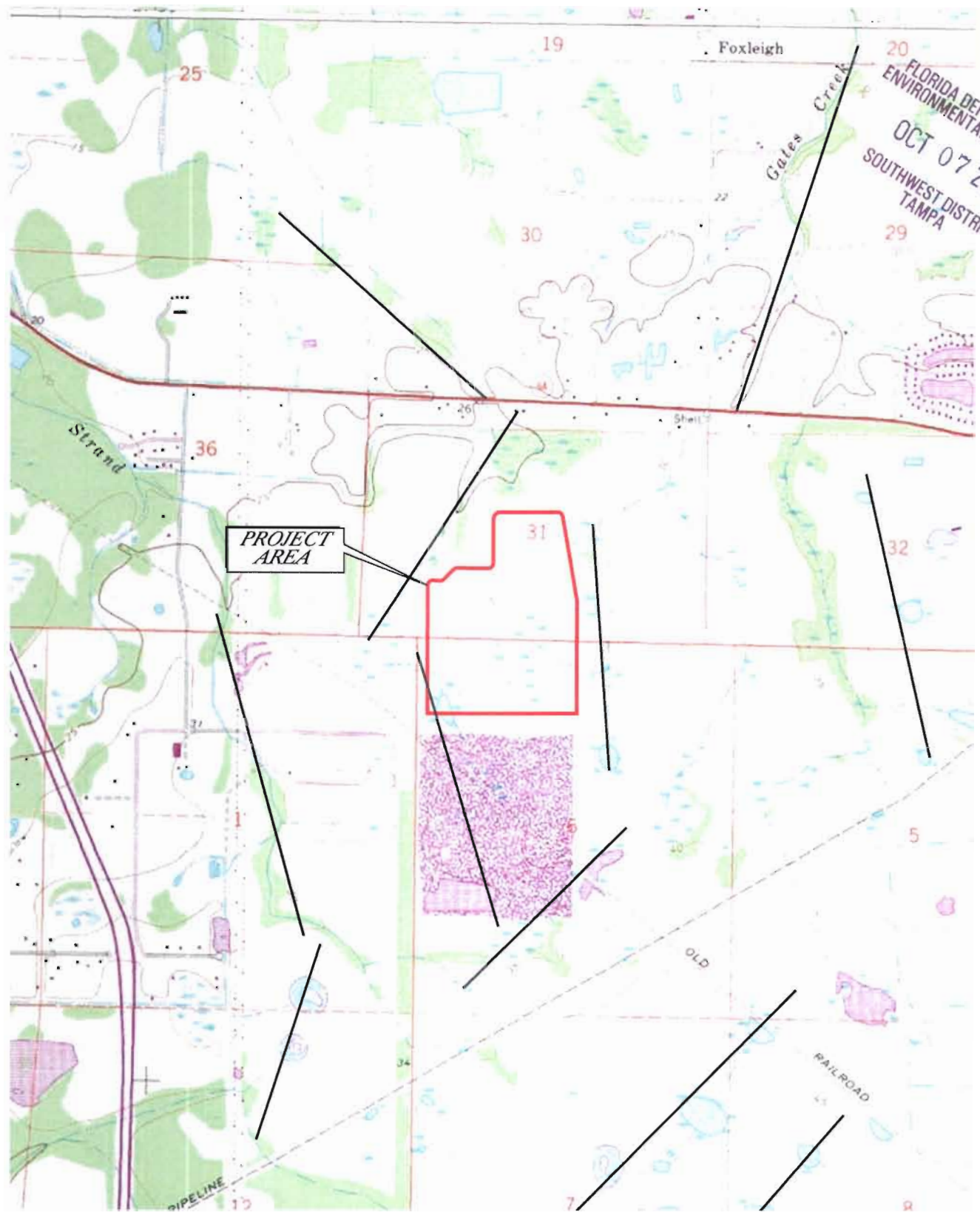
PN: CPGT-10-0062

DRAWN BY: DLS

2009 AERIAL PHOTOGRAPH

FIGURE 3





REFERENCE:  
 U.S.G.S. LORRAINE, FLA.  
 QUADRANGLE MAP  
 DATED 1973  
 PHOTOREVISED 1987  
 SECTIONS 6 & 31  
 TOWNSHIP 34 & 35 SOUTH  
 RANGE 19 EAST



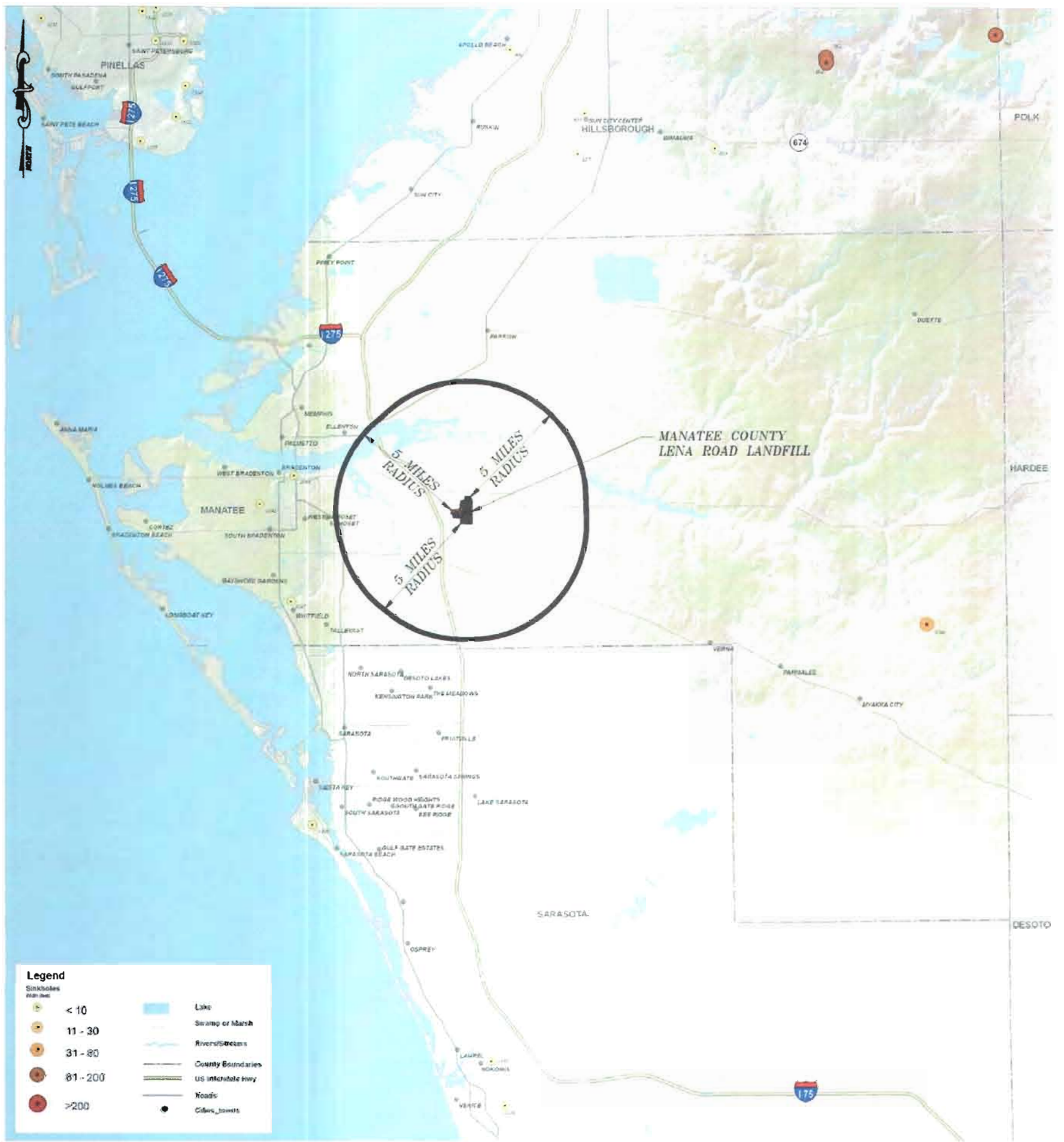
**Andreyev  
 Engineering,  
 Inc.**

GEOTECHNICAL INVESTIGATION  
**LENA ROAD LANDFILL  
 STAGE II**  
 MANATEE COUNTY, FL

APPROXIMATE SCALE:	DATE: 09/24/10	ENGINEER: SC
1" = 2000'	PN: CPGT-10-0062	DRAWN BY: DLS


PHOTOLINEAMENT MAP

FIGURE 4





REFERENCE:  
 SINKHOLES OF MANATEE COUNTY, FLORIDA, 2008  
 FLORIDA CENTER FOR INSTRUCTIONAL TECHNOLOGY, SINKHOLES  
 (TAMPA, FL: UNIVERSITY OF SOUTH FLORIDA, 2008)  
 DOWNLOADED FROM MAPS ETC. ON THE WEB AT [HTTP://ETC.USF.EDU/MAPS](http://etc.usf.edu/maps)  
 [MAP#11142]

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 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION <b>LENA ROAD LANDFILL          STAGE II</b> MANATEE COUNTY, FL
	DOCUMENTED SINKHOLE MAP FIGURE: 5
APPROXIMATE SCALE: <b>1" = 5 MILES</b>	DATE: 09/24/10 ENGINEER: SC PN: CPGT--10--0062 DRAWN BY: OLS



**LEGEND:**

-  APPROXIMATE LOCATION OF SPT BORING
-  APPROXIMATE LOCATION OF PREVIOUS SPT BORING DRILLED BY ARDAMAN & ASSOCIATES (REFER TO REPORT DATE AUGUST 29, 1985).



**Andrey Engineering, Inc.**

APPROXIMATE SCALE: 1" = 300'

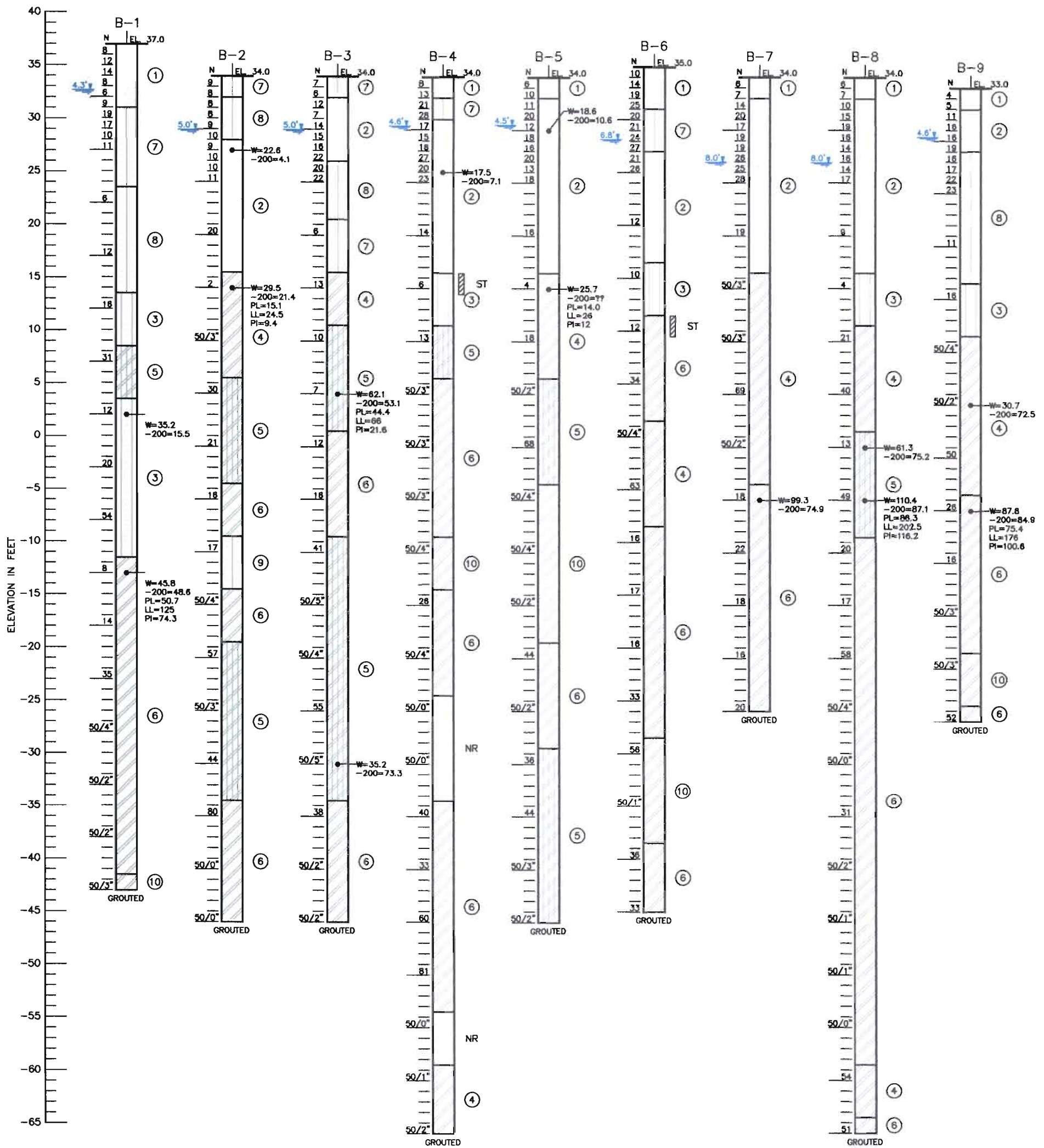
DATE: 08/27/10  
DRAWN BY: J. B. ...

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OC 10 7 2010  
SOUTH FLORIDA DISTRICT

GEOTECHNICAL INVESTIGATION  
**LENA ROAD LANDFILL  
STAGE II**  
MANATEE COUNTY, FL

**BORING LOCATION PLAN**

FIGURE: 5



**LEGEND:**

- ① LIGHT GRAY TO GRAYISH-BROWN FINE SAND (SP)
- ② LIGHT BROWN TO BROWN FINE SAND (SP)
- ③ GRAY SILTY FINE SAND WITH TRACES OF PHOSPHATES (SM)
- ④ LIGHT BROWN TO BROWN SANDY CLAY WITH TRACES OF PHOSPHATES (CL)
- ⑤ GREENISH-GRAY SILTY TO SANDY CLAY WITH TRACES OF PHOSPHATES (SM)(CL)
- ⑥ GREENISH-GRAY CLAY WITH TRACES OF PHOSPHATES (CL)
- ⑦ DARK REDDISH-BROWN SLIGHTLY SILTY FINE SAND, WEAKLY CEMENTED (SP-SM)
- ⑧ BROWN SLIGHTLY SILTY FINE SAND (SP-SM)
- ⑨ GRAYISH-BROWN SLIGHTLY SILTY FINE SAND WITH TRACES OF SHELL & PHOSPHATES (SP-SM)
- ⑩ BROWN HIGHLY CEMENTED CLAY WITH PHOSPHATES (CL)

(SP) UNIFIED SOIL CLASSIFICATION SYSTEM GROUP SYMBOL

1.0' DEPTH TO GROUNDWATER, JULY, 2010

N STANDARD PENETRATION RESISTANCE, IN BLOWS PER FOOT

50/1" 50 BLOWS OF HAMMER TO ADVANCE SAMPLING TOOL ONE INCH

NR NO SAMPLE RECOVERY

ST SHELBY TUBE

W MOISTURE CONTENT, IN PERCENT

-200 PERCENT OF FINES PASSING THE U.S. No. 200 SIEVE

PL PLASTIC LIMIT, IN PERCENT

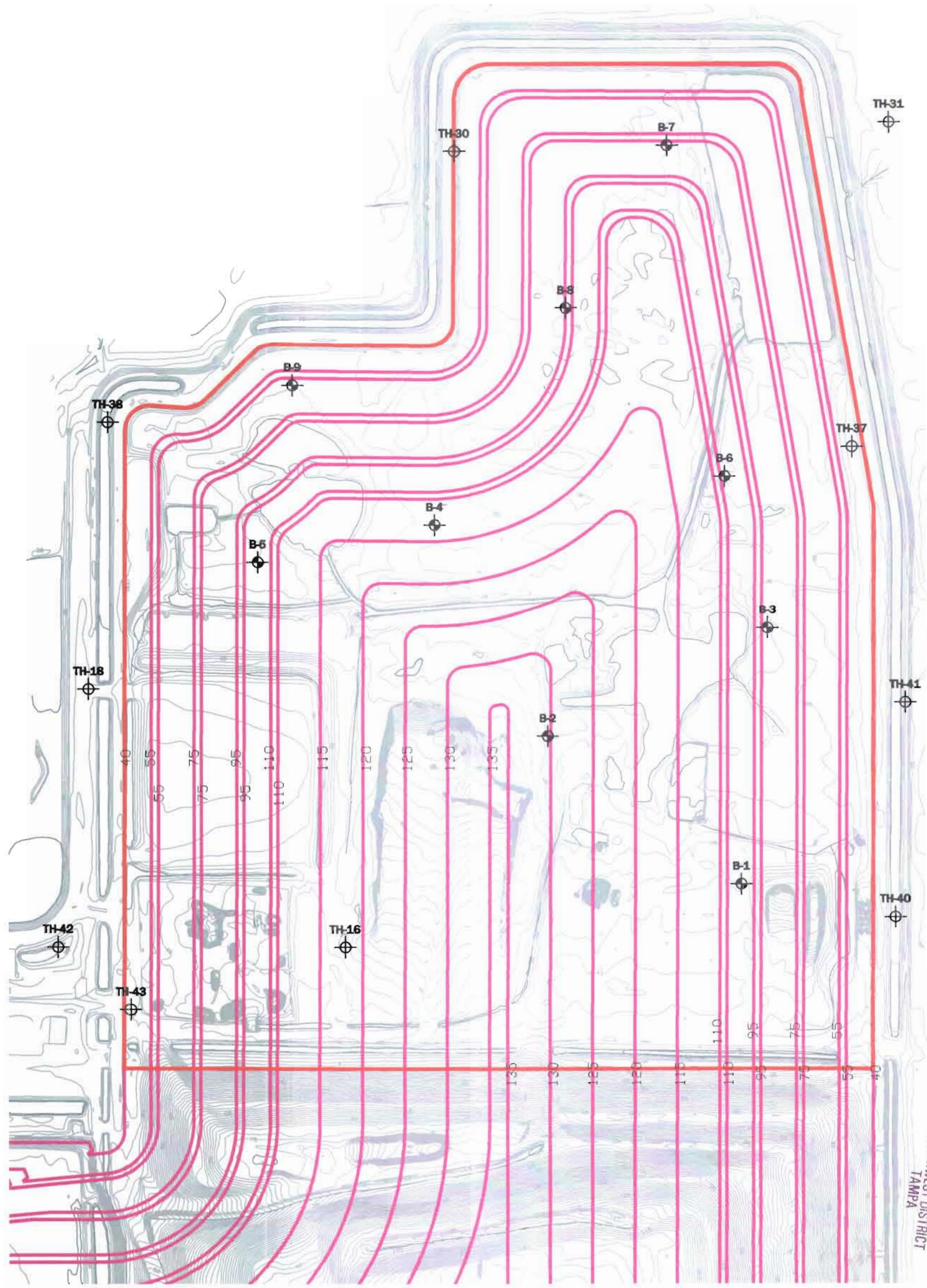
LL LIQUID LIMIT, IN PERCENT

PI PLASTICITY INDEX, IN PERCENT

EL. GROUND ELEVATION AT BORING LOCATION (FT - STATE PLANE FLORIDA EAST ZONE NAT 83)

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	<b>Andreyev Engineering, Inc.</b>		GEOTECHNICAL INVESTIGATION <b>LENA ROAD LANDFILL          STAGE II</b> MANATEE COUNTY, FL	
	APPROXIMATE SCALE: 1" = 10' DATE: 08/30/10 ENGINEER: SC PN: CPGT-10-0062		SOIL PROFILES DRAWN BY: DLS FIGURE 7	



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**LEGEND:**

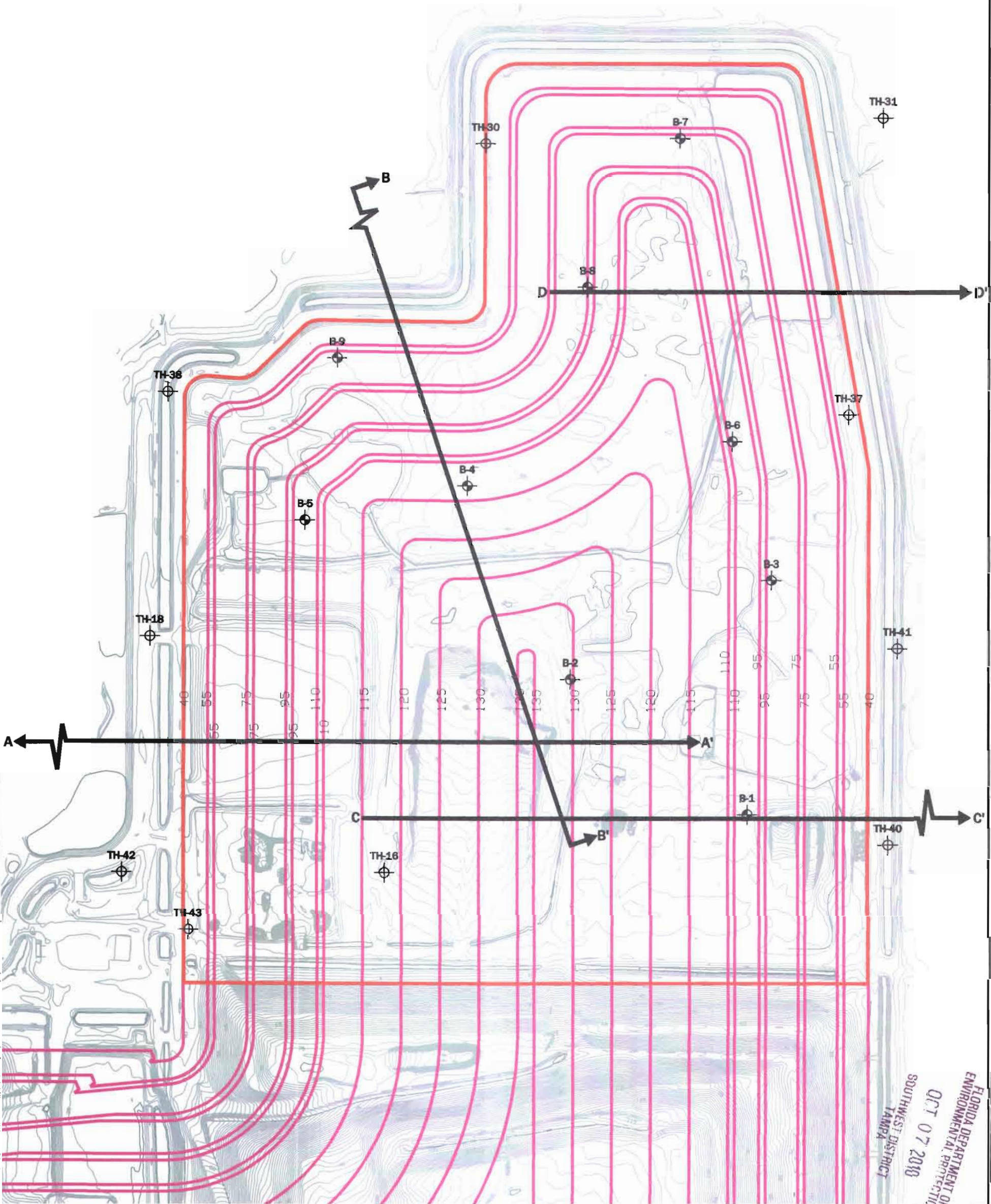
- APPROXIMATE LOCATION OF SPT BORING
- APPROXIMATE LOCATION OF PREVIOUS SPT BORING DRILLED BY ARDAMAN & ASSOCIATES (REFER TO REPORT DATE AUGUST 29, 1985)



GEOTECHNICAL INVESTIGATION  
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APPROXIMATE SCALE: 1"=300'  
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**LANDFILL GRADING PLAN**  
 FIGURE 8

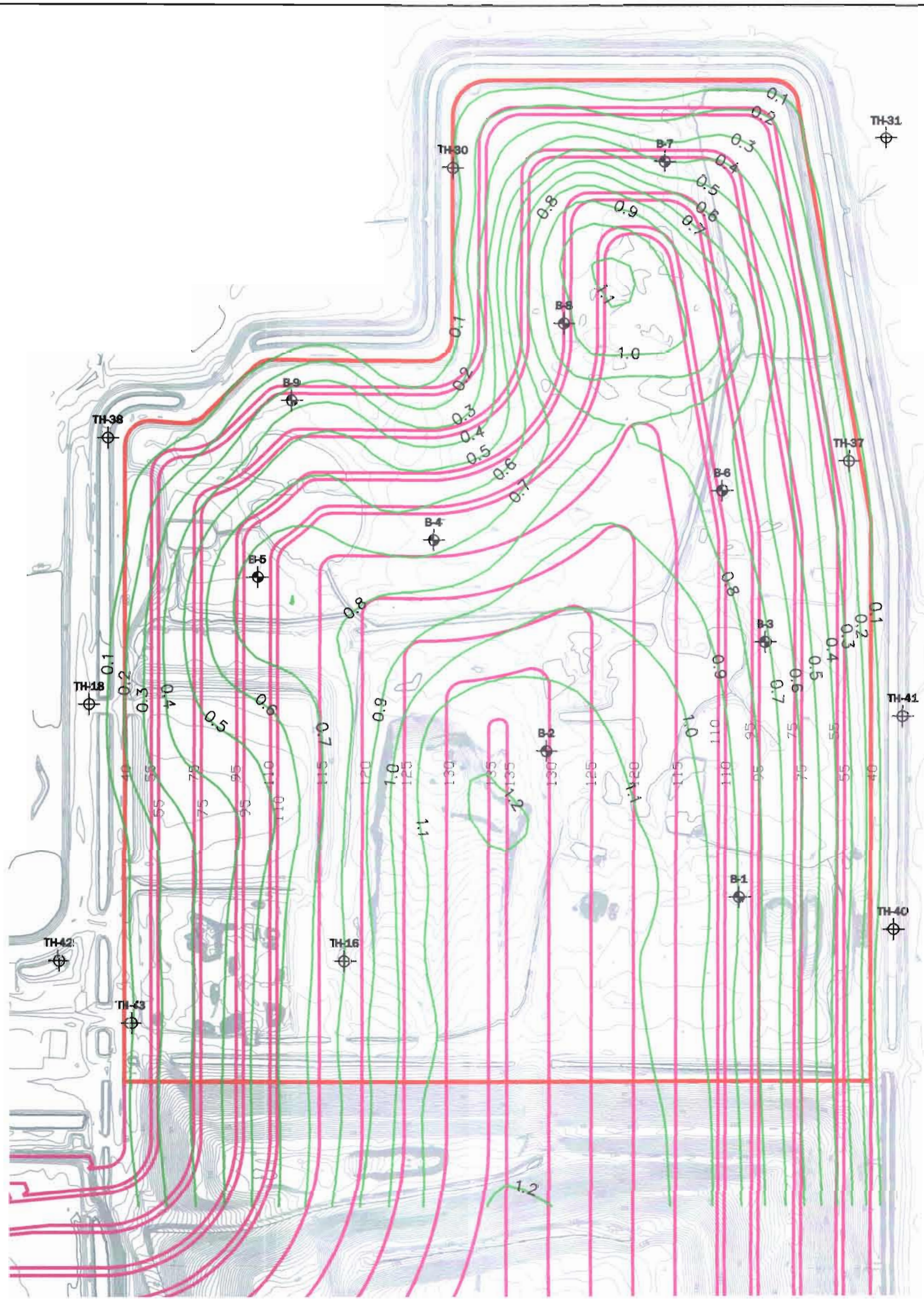


FLORIDA DEPARTMENT OF  
 ENVIRONMENTAL PROTECTION  
 OCT 07 2010  
 SOUTHWEST DISTRICT  
 TAMPA




**LEGEND:**  
  
 SLOPE TRANSECT ANALYZED FOR  
 SLOPE STABILITY

<b>Andreyev Engineering, Inc.</b>		GEOTECHNICAL INVESTIGATION <b>LIENA ROAD LANDFILL STAGE II</b> MANATEE COUNTY, FL
APPROXIMATE SCALE: 1" = 300'	DATE: 09/24/10 PN: CPGT-1J--0062	ENGINEER: SC DRAWN BY: CLS


SLOPE STABILITY TRANSECTS  
 FIGURE 9



**LEGEND:**

-  APPROXIMATE LOCATION OF SPT BORING
-  APPROXIMATE LOCATION OF PREVIOUS SPT BORING DRILLED BY ARDAMAN & ASSOCIATES (REFER TO REPORT DATE AUGUST 29, 1985)
-  SETTLEMENT CONTOUR (FT)

FLORIDA DEPARTMENT OF  
 ENVIRONMENTAL PROTECTION  
 OCT 07 2010  
 SOUTHWEST DISTRICT  
 TAMPA

 <b>Andreyev Engineering, Inc.</b>		GEOTECHNICAL INVESTIGATION <b>LENA ROAD LANDFILL STAGE II</b> MANATEE COUNTY, FL	
		<b>SETTLEMENT CONTOURS</b> FIGURE 10	
APPROXIMATE SCALE: <b>1" = 300'</b>	DATE: 09/16/10 PN: CPGT-10-0962	ENGINEER: SC DRAWN BY: DLB	

**ATTACHMENT A**  
**BEARING CAPACITY ANALYSIS RESULTS**



## BEARING CAPACITY ANALYSIS

**PROJECT: LENA ROAD LANDFILL, STAGE 2**

**Enter soil characteristics**

Cohesion,  $c = 0$  psf  
Friction angle,  $\phi = 29$  degrees (whole degrees, <50, preferably)  
Unit weight,  $\gamma = 100$  pcf

The above entries yield the following factors:

$c' = 0.00$	
$\phi' = 20.3$	
$*N_q' = 6.58$	$**N_q' = 7.5$
$*N_c' = 15.10$	$**N_c' = 18.1$
$*N_\gamma' = 5.60$	$**N_\gamma' = 5.2$
$*N_q = 16.44$	$**N_q = 20.4$
$*N_c = 27.86$	$**N_c = 33.4$
$*N_\gamma = 19.34$	$**N_\gamma = 17.8$
$*N$ factors from Eqs. 10-32,34,36. (Method 1)	$**N$ factors from fig. 10.7 & 10.8 (Method 2)

Determine whether footing is a strip (length to width ratio  $\geq 5$ ); square; circular; or rectangular.

Enter St for strip, Sq for square, C for circular, or R for rectangular.

Enter here  $\rightarrow$  sg

Footing shape is: square

---

**Enter smallest lanfill dimension**

$B = 1000$  feet  
 $D_f = 36$  inches

**FOR LOCAL SHEAR FAILURE:**

$q_u' = 20,650$  psf  
Method 1

$q_u' = 19,583$  psf  
Method 2

**FOR GENERAL SHEAR FAILURE:**

$q_u = 69,393$  psf  
Method 1

$q_u = 65,453$  psf  
Method 2

Note: The above values for  $q_u'$  and  $q_u$  have been calculated by selective use of the following formulae.

$q_u' = c' N_c' + q N_q' + 0.5 \gamma B N_\gamma'$  (strip ftg.)  
 $q_u' = 1.3 c' N_c' + q N_q' + 0.4 \gamma B N_\gamma'$  (square ftg.)  
 $q_u' = 1.3 c' N_c' + q N_q' + 0.3 \gamma B N_\gamma'$  (circular ftg.)  
 $q_u = c N_c + q N_q + 0.5 \gamma B N_\gamma$  (strip ftg.)  
 $q_u = 1.3 c N_c + q N_q + 0.4 \gamma B N_\gamma$  (square ftg.)  
 $q_u = 1.3 c N_c + q N_q + 0.3 \gamma B N_\gamma$  (circular ftg.)

**Terzaghi's Ultimate Bearing Capacity Equation**

Reference: Principles of Geotechnical Engineering, Das, section 10 - 2

## BEARING CAPACITY ANALYSIS

**PROJECT: LENA ROAD LANDFILL, STAGE 2 - Deeper clay stratum**

### Enter soil characteristics

Cohesion,  $c = 1000$  psf  
Friction angle,  $\phi = 22$  degrees (whole degrees, <50, preferably)  
Unit weight,  $\gamma = 110$  pcf

The above entries yield the following factors:

$c' = 666.67$	
$\phi' = 15.1$	
$*N_q' = 3.97$	$**N_q' = 4.3$
$*N_c' = 11.02$	$**N_c' = 13$
$*N_\gamma' = 2.68$	$**N_\gamma' = 2.1$
$*N_q = 7.82$	$**N_q = 9.1$
$*N_c = 16.88$	$**N_c = 20.2$
$*N_\gamma = 7.13$	$**N_\gamma = 6.66$
$*N$ factors from Eqs. 10-32,34,36. (Method 1)	$**N$ factors from fig. 10.7 & 10.8 (Method 2)

Determine whether footing is a strip (length to width ratio  $\geq 5$ ); square; circular; or rectangular.

Enter St for strip, Sq for square, C for circular, or R for rectangular.

Enter here  $\rightarrow$  sq

Footing shape is: square

---

### Enter smallest landfill dimension

$B = 1000$  feet  
 $D_f = 240$  inches

### FOR LOCAL SHEAR FAILURE:

$q_u' = 28,102$  psf  
Method 1

$q_u' = 28,427$  psf  
Method 2

### FOR GENERAL SHEAR FAILURE:

$q_u = 65,290$  psf  
Method 1

$q_u = 70,700$  psf  
Method 2

Note: The above values for  $q_u'$  and  $q_u$  have been calculated by selective use of the following formulae.

$q_u' = c' N_c' + q N_q' + 0.5 \gamma B N_\gamma'$  (strip ftg.)  
 $q_u' = 1.3 c' N_c' + q N_q' + 0.4 \gamma B N_\gamma'$  (square ftg.)  
 $q_u' = 1.3 c' N_c' + q N_q' + 0.3 \gamma B N_\gamma'$  (circular ftg.)  
 $q_u = c N_c + q N_q + 0.5 \gamma B N_\gamma$  (strip ftg.)  
 $q_u = 1.3 c N_c + q N_q + 0.4 \gamma B N_\gamma$  (square ftg.)  
 $q_u = 1.3 c N_c + q N_q + 0.3 \gamma B N_\gamma$  (circular ftg.)

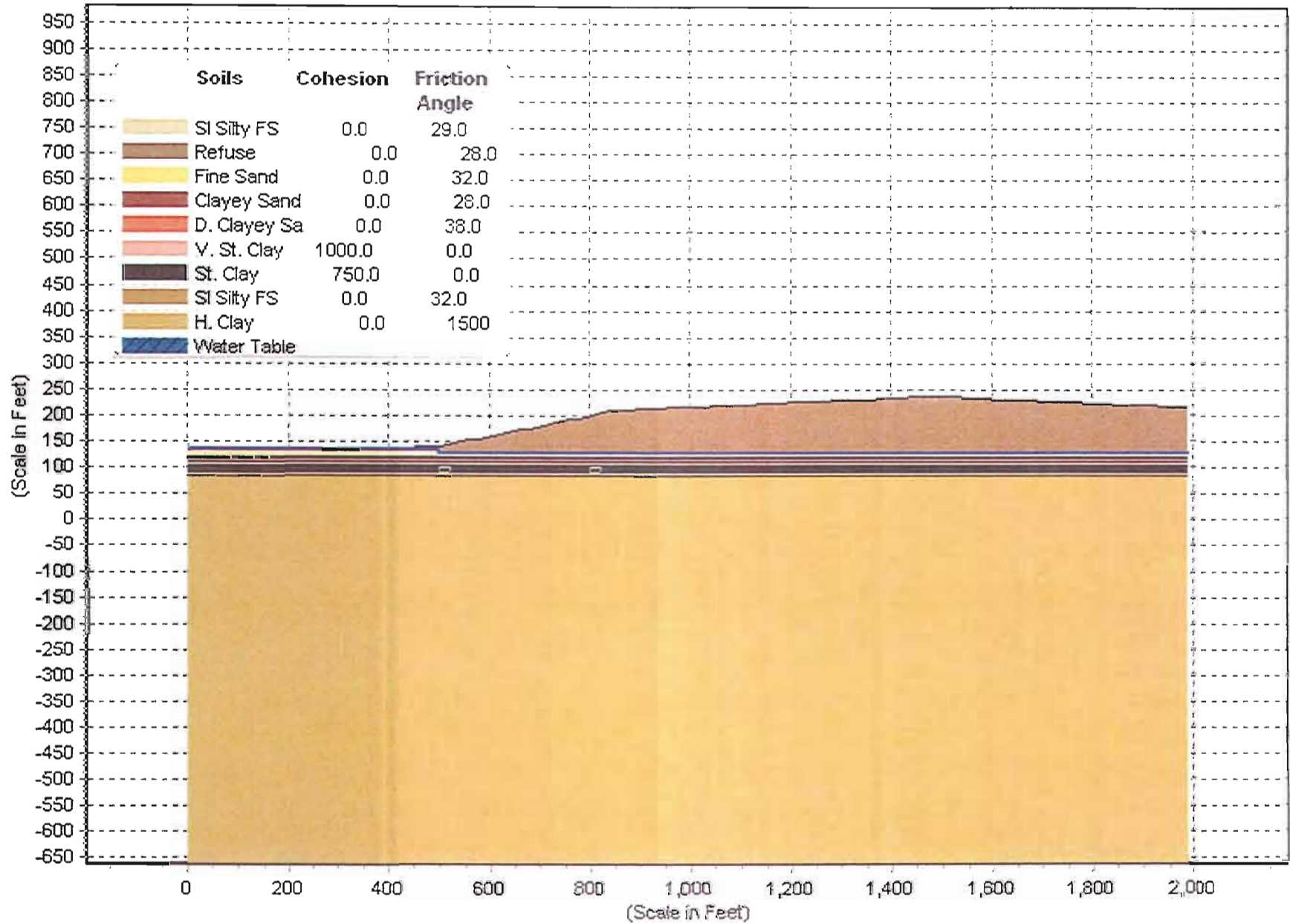
**Terzaghi's Ultimate Bearing Capacity Equation**

**Reference: Principles of Geotechnical Engineering, Das, section 10 - 2**

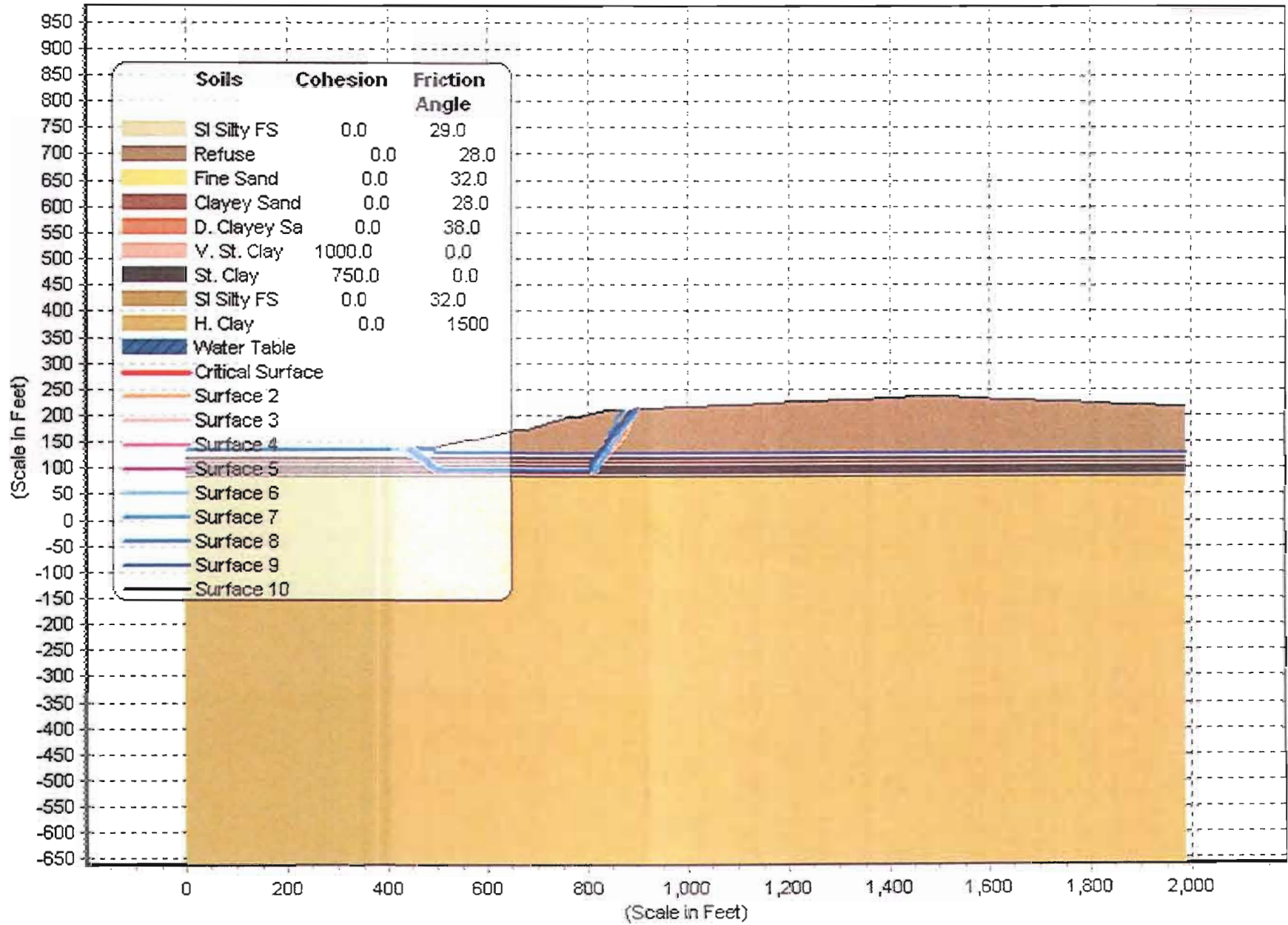
**ATTACHMENT B**

**SLOPE STABILITY ANALYSIS RESULTS**

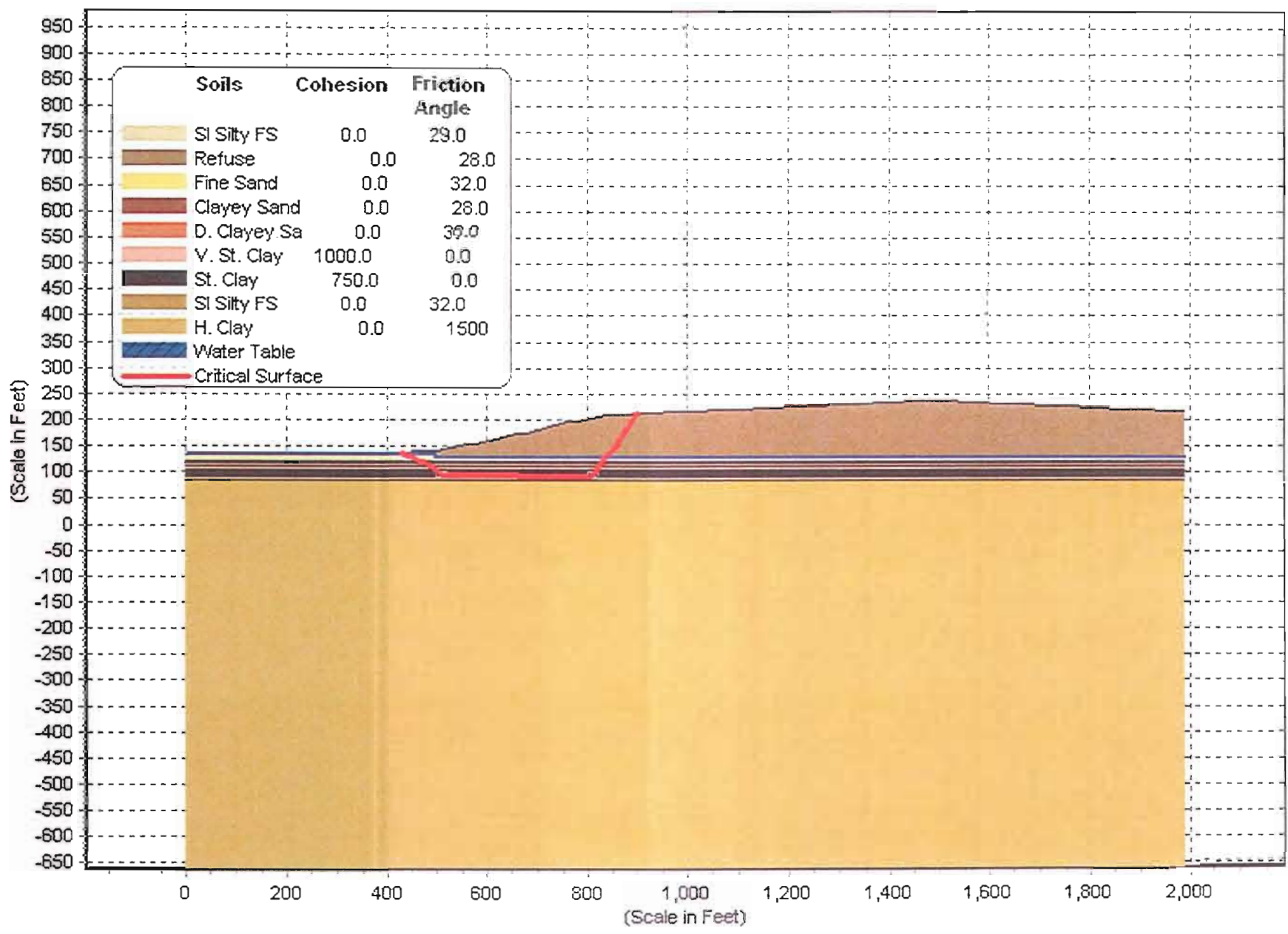
# LENA ROAD LANDFILL - X-SEC A - A'



LENA ROAD LANDFILL - X-SEC A - A' - FS Min- Janbu = 1.702



LENA ROAD LANDFILL - X-SEC A - A' - FS Min- Janbu = 1.702



result.out  
 \*\* STABL for WINDOWS \*\*  
 by  
 Geotechnical Software Solutions

1

--Slope Stability Analysis--  
 Simplified Janbu, Simplified Bishop  
 or Spencer's Method of Slices

Run Date: 9/27/10  
 Time of Run: 14:00  
 Run By: Shawkat Ali  
 Input Data Filename: run.in  
 Output Filename: result.out  
 Unit: U.S.C.  
 Plotted Output Filename: result.plt

PROBLEM DESCRIPTION LENA ROAD LANDFILL - X-SEC A - A'

BOUNDARY COORDINATES

20 Top Boundaries  
 29 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	135.00	300.00	135.00	2
2	300.00	135.00	500.00	140.00	2
3	500.00	140.00	560.00	155.00	1
4	560.00	155.00	580.00	155.00	1
5	580.00	155.00	660.00	175.00	1
6	660.00	175.00	680.00	175.00	1
7	680.00	175.00	760.00	195.00	1
8	760.00	195.00	780.00	195.00	1
9	780.00	195.00	840.00	210.00	1
10	840.00	210.00	860.00	210.00	1
11	860.00	210.00	980.00	215.00	1
12	980.00	215.00	1100.00	220.00	1
13	1100.00	220.00	1220.00	225.00	1
14	1220.00	225.00	1340.00	230.00	1
15	1340.00	230.00	1460.00	235.00	1
16	1460.00	235.00	1510.00	235.00	1
17	1510.00	235.00	1630.00	230.00	1
18	1630.00	230.00	1750.00	225.00	1
19	1750.00	225.00	1870.00	220.00	1
20	1870.00	220.00	1990.00	215.00	1
21	500.10	127.00	500.20	140.00	1
22	500.10	127.00	1990.00	127.00	2
23	0.00	121.50	1990.00	121.50	3
24	0.00	116.50	1990.00	116.50	4
25	0.00	111.50	1990.00	111.50	5
26	0.00	105.50	1990.00	105.50	6
27	0.00	100.50	1990.00	100.50	7

1

			result.out			
28	0.00	90.50	1990.00	90.50	8	
29	0.00	85.50	1990.00	85.50	9	

ISOTROPIC SOIL PARAMETERS

9 Type(s) of soil

1

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	70.0	80.0	0.0	28.0	0.00	0.0	1
2	95.0	105.0	0.0	29.0	0.00	0.0	1
3	105.0	115.0	0.0	32.0	0.00	0.0	1
4	95.0	110.0	0.0	28.0	0.00	0.0	1
5	115.0	125.0	0.0	38.0	0.00	0.0	1
6	110.0	125.0	1000.0	0.0	0.00	0.0	1
7	105.0	120.0	750.0	0.0	0.00	0.0	1
8	105.0	115.0	0.0	32.0	0.00	0.0	1
9	115.0	130.0	0.0	1500.0	0.00	0.0	0

1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED

Unit Weight of Water = 62.40

Piezometric Surface No. 1 Specified by 4 Coordinate Points

1

Point No.	X-Water (ft)	Y-Water (ft)
1	0.00	133.00
2	500.00	133.00
3	500.10	127.00
4	1990.00	127.00

A Critical Failure Surface Searching Method, Using A Random Technique For Generating Sliding Block Surfaces, Has Been Specified.

100 Trial Surfaces Have Been Generated.

2 Boxes Specified For Generation Of Central Block Base

Length Of Line Segments For Active And Passive Portions Of Sliding Block Is 10.0

Box	X-Left	Y-Left	X-Right	Y-Right	Height
-----	--------	--------	---------	---------	--------



No.	(ft)	(ft)	result.out (ft)	(ft)	(ft)
1	500.00	95.00	520.00	95.00	10.00
2	800.00	95.00	820.00	95.00	10.00

1

Following Are Displayed The Ten Most Critical Of The Trial Failure Surfaces Examined. They Are Ordered - Most Critical First.

\* \* Safety Factors Are Calculated By The Modified Janbu Method \* \*

Failure Surface Specified By 28 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	430.66	138.27
2	437.61	133.90
3	447.33	131.55
4	455.94	126.46
5	464.33	121.02
6	474.22	119.59
7	481.75	113.01
8	491.57	111.12
9	499.78	105.42
10	507.00	98.50
11	516.48	95.30
12	808.13	90.55
13	814.38	98.35
14	821.36	105.52
15	825.28	114.72
16	831.81	122.29
17	838.64	129.60
18	844.03	138.02
19	851.09	145.10
20	858.10	152.23
21	864.73	159.72
22	868.90	168.81
23	873.70	177.58
24	879.53	185.71
25	885.94	193.38
26	891.28	201.84
27	897.96	209.27
28	900.16	211.67

\*\*\* 1.702 \*\*\*

Individual data on the 50 slices

Slice No.	width (ft)	weight (lbs)	Water Force		Force Norm (lbs)	Force Tan (lbs)	Earthquake Force		surcharge Load (lbs)
			Top (lbs)	Bot (lbs)			Hor (lbs)	Ver (lbs)	

				result.out					
1	6.9	1497.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	3.7	1781.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	6.0	3652.0	0.0	279.2	0.0	0.0	0.0	0.0	0.0
4	8.6	8346.3	0.0	2492.2	0.0	0.0	0.0	0.0	0.0
5	7.6	11600.4	0.0	5131.6	0.0	0.0	0.0	0.0	0.0
6	0.7	1342.1	0.0	645.9	0.0	0.0	0.0	0.0	0.0
7	9.9	19169.5	0.0	7920.8	0.0	0.0	0.0	0.0	0.0
8	3.5	7815.3	0.0	4380.7	0.0	0.0	0.0	0.0	0.0
9	4.0	10344.5	0.0	6040.8	0.0	0.0	0.0	0.0	0.0
10	7.8	22609.3	0.0	10346.2	0.0	0.0	0.0	0.0	0.0
11	2.0	5915.0	0.0	2718.2	0.0	0.0	0.0	0.0	0.0
12	8.1	27407.9	0.0	15183.7	0.0	0.0	0.0	0.0	0.0
13	0.1	444.7	0.0	248.0	0.0	0.0	0.0	0.0	0.0
14	0.2	826.0	0.0	524.1	0.0	0.0	0.0	0.0	0.0
15	0.1	317.4	0.0	107.4	0.0	0.0	0.0	0.0	0.0
16	0.1	342.0	0.0	189.6	0.0	0.0	0.0	0.0	0.0
17	4.7	17676.5	0.0	9874.9	0.0	0.0	0.0	0.0	0.0
18	2.1	8794.0	0.0	4962.0	0.0	0.0	0.0	0.0	0.0
19	9.5	43816.8	0.0	18783.0	0.0	0.0	0.0	0.0	0.0
20	43.5	231696.8	0.0	87073.0	0.0	0.0	0.0	0.0	0.0
21	20.0	115325.5	0.0	40656.7	0.0	0.0	0.0	0.0	0.0
22	80.0	525118.9	0.0	*****	0.0	0.0	0.0	0.0	0.0
23	20.0	147233.9	0.0	42689.3	0.0	0.0	0.0	0.0	0.0
24	80.0	652752.2	0.0	*****	0.0	0.0	0.0	0.0	0.0
25	20.0	179142.2	0.0	44721.9	0.0	0.0	0.0	0.0	0.0
26	28.1	260222.0	0.0	63592.1	0.0	0.0	0.0	0.0	0.0
27	6.3	56944.2	0.0	20310.1	0.0	0.0	0.0	0.0	0.0
28	2.1	17923.3	0.0	5150.0	0.0	0.0	0.0	0.0	0.0
29	4.9	39923.0	0.0	10447.9	0.0	0.0	0.0	0.0	0.0
30	0.0	167.6	0.0	40.6	0.0	0.0	0.0	0.0	0.0
31	2.5	19311.3	0.0	7497.2	0.0	0.0	0.0	0.0	0.0
32	1.4	9697.5	0.0	3034.9	0.0	0.0	0.0	0.0	0.0
33	1.5	10465.8	0.0	1669.8	0.0	0.0	0.0	0.0	0.0
34	4.3	27982.3	0.0	3297.6	0.0	0.0	0.0	0.0	0.0
35	0.7	4230.7	0.0	332.8	0.0	0.0	0.0	0.0	0.0
36	4.4	26187.8	0.0	946.9	0.0	0.0	0.0	0.0	0.0
37	2.4	13771.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
38	1.4	7554.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
39	4.0	21180.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
40	7.1	33850.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
41	7.0	30073.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
42	1.9	7549.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
43	4.7	17568.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
44	4.2	13434.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
45	4.8	12533.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
46	5.8	11838.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
47	6.4	9604.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48	5.3	5081.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
49	6.7	2754.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50	2.2	177.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Failure Surface Specified By 25 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	453.72	138.84
2	460.97	133.30
3	469.35	127.85
4	476.88	121.26
5	485.96	117.07
6	493.04	110.00

		result.out
7	500.81	103.71
8	508.06	96.82
9	516.26	91.10
10	815.85	95.51
11	822.39	103.07
12	829.13	110.46
13	835.55	118.13
14	842.56	125.26
15	849.29	132.66
16	855.06	140.82
17	861.92	148.10
18	868.72	155.43
19	875.40	162.88
20	881.15	171.05
21	884.74	180.39
22	888.24	189.75
23	889.10	199.72
24	895.03	207.77
25	897.34	211.56

\*\*\* 1.707 \*\*\*

1

Failure Surface Specified By 26 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	438.25	138.46
2	447.00	135.30
3	455.48	130.01
4	462.69	123.07
5	469.80	116.04
6	479.79	115.77
7	488.43	110.74
8	496.83	105.30
9	504.26	98.61
10	511.39	91.61
11	804.09	94.58
12	811.14	101.66
13	817.97	108.97
14	822.01	118.12
15	828.75	125.51
16	833.83	134.12
17	840.49	141.58
18	846.14	149.83
19	853.21	156.91
20	859.11	164.98
21	865.05	173.02
22	872.12	180.09
23	872.78	190.07
24	877.46	198.91
25	881.20	208.18
26	883.66	210.99

\*\*\* 1.740 \*\*\*

result.out

Failure Surface Specified By 26 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	443.53	138.59
2	444.99	137.41
3	454.95	136.47
4	463.74	131.70
5	470.81	124.64
6	478.55	118.31
7	487.17	113.24
8	495.25	107.34
9	503.27	101.36
10	512.34	97.16
11	806.86	96.42
12	813.88	103.54
13	820.15	111.33
14	826.41	119.13
15	832.60	126.98
16	839.36	134.35
17	846.11	141.73
18	851.12	150.39
19	857.03	158.45
20	864.10	165.53
21	868.07	174.71
22	874.55	182.31
23	877.38	191.91
24	880.61	201.37
25	884.55	210.56
26	884.79	211.03

\*\*\* 1.747 \*\*\*

1

Failure Surface Specified By 26 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	434.29	138.36
2	441.29	132.24
3	449.59	126.65
4	458.57	122.26
5	466.89	116.71
6	474.38	110.09
7	483.69	106.43
8	490.95	99.56
9	500.32	96.06
10	509.34	91.74
11	816.16	90.55
12	820.01	99.78
13	826.52	107.37
14	831.95	115.77

		result.out
15	838.79	123.06
16	843.32	131.98
17	847.89	140.87
18	849.44	150.75
19	856.27	158.06
20	862.97	165.48
21	870.04	172.55
22	874.37	181.56
23	879.17	190.34
24	885.68	197.93
25	892.59	205.16
26	896.01	211.50

\*\*\* 1.750 \*\*\*

Failure Surface Specified By 28 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	427.36	138.18
2	432.74	134.16
3	439.86	127.14
4	447.37	120.54
5	457.26	119.03
6	466.08	114.31
7	475.14	110.07
8	482.78	103.63
9	491.54	98.81
10	498.63	91.75
11	508.57	90.72
12	806.03	91.14
13	812.49	98.77
14	819.53	105.88
15	821.22	115.73
16	826.75	124.06
17	831.87	132.66
18	838.87	139.79
19	845.85	146.96
20	852.11	154.75
21	858.64	162.33
22	865.22	169.86
23	872.08	177.13
24	879.15	184.20
25	882.28	193.70
26	889.15	200.97
27	896.11	208.15
28	899.37	211.64

\*\*\* 1.756 \*\*\*

result.out

Point No.	X-Surf (ft)	Y-Surf (ft)
1	411.20	137.78
2	417.82	135.05
3	426.90	130.85
4	436.88	130.21
5	444.83	124.15
6	453.74	119.60
7	463.69	118.64
8	471.13	111.96
9	479.80	106.98
10	488.98	103.00
11	497.29	97.44
12	505.46	91.68
13	816.50	96.03
14	821.86	104.48
15	828.06	112.32
16	835.01	119.51
17	838.06	129.03
18	844.09	137.01
19	850.92	144.31
20	855.92	152.97
21	862.91	160.12
22	867.31	169.10
23	873.12	177.24
24	879.10	185.25
25	886.17	192.32
26	892.80	199.82
27	898.51	208.02
28	900.99	211.71

\*\*\* 1.760 \*\*\*

Failure surface Specified By 25 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	448.92	138.72
2	451.48	137.33
3	458.82	130.54
4	467.86	126.27
5	475.88	120.30
6	483.39	113.69
7	491.60	107.98
8	499.59	101.97
9	508.04	96.62
10	517.34	92.95
11	803.55	93.01
12	808.25	101.84
13	815.30	108.94
14	819.71	117.91
15	826.65	125.11
16	831.79	133.69
17	837.72	141.74
18	843.00	150.23

		result.out
19	844.86	160.05
20	846.84	169.86
21	852.79	177.89
22	858.12	186.35
23	861.33	195.82
24	866.83	204.18
25	872.10	210.50

\*\*\* 1.768 \*\*\*

1

Failure Surface Specified By 26 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	441.52	138.54
2	445.48	134.68
3	454.43	130.22
4	461.83	123.50
5	469.72	117.36
6	476.80	110.29
7	485.45	105.27
8	494.98	102.24
9	503.06	96.35
10	802.53	95.45
11	807.87	103.90
12	812.21	112.91
13	817.93	121.11
14	822.84	129.83
15	829.90	136.91
16	836.26	144.63
17	843.27	151.75
18	850.10	159.06
19	857.12	166.18
20	862.37	174.69
21	869.43	181.78
22	876.47	188.88
23	883.23	196.24
24	890.22	203.39
25	896.75	210.97
26	897.32	211.55

\*\*\* 1.774 \*\*\*

Failure Surface Specified By 25 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	443.21	138.58
2	448.08	136.03
3	455.31	129.12

		result.out
4	462.83	122.53
5	470.74	116.42
6	479.01	110.79
7	487.85	106.12
8	495.01	99.14
9	502.41	92.41
10	802.44	93.90
11	806.15	103.19
12	809.01	112.77
13	816.06	119.85
14	821.55	128.21
15	827.28	136.41
16	834.30	143.54
17	837.95	152.85
18	844.94	160.00
19	850.22	168.49
20	855.41	177.04
21	862.46	184.13
22	869.23	191.49
23	875.53	199.26
24	882.57	206.36
25	886.82	211.12

\*\*\* 1.785 \*\*\*

1

	Y	A	X	I	S	F	T
	0.00	248.75	497.50	746.25	995.00	1243.75	
X	0.00	***	-----	-----	-----	-----	-----
	248.75	+	*				
		61					
A	497.50	+	512				
		1**	.	*			
		*					
X	746.25	+	*	*			
		1	1118*	.11*			
		11					
I	995.00	+	*				
		*					

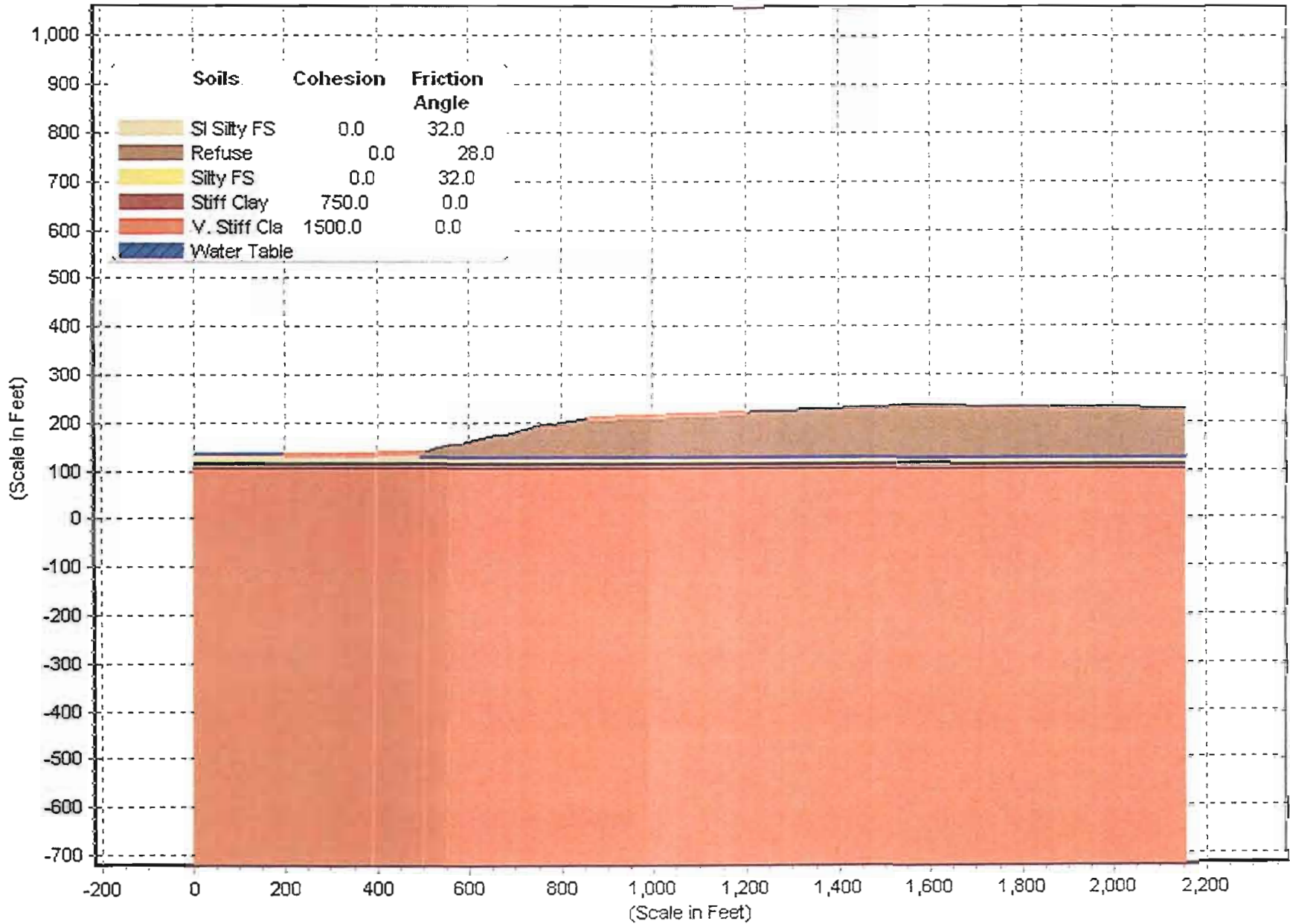


result.out

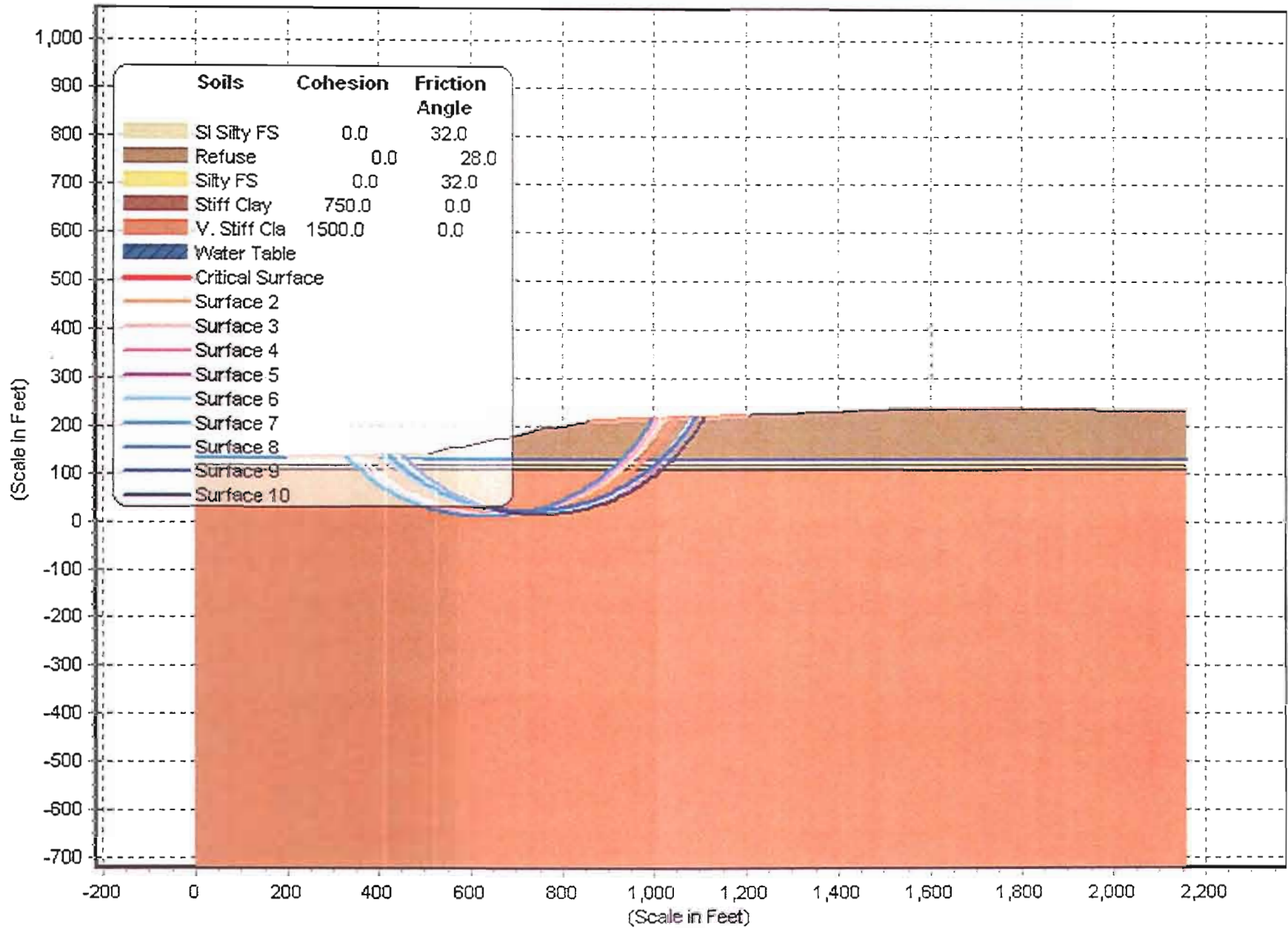
```

-
S 1243.75 + *
-
-
-
1492.50 + *
-
-
-
F 1741.25 + *
-
-
-
T 1990.00 + *** *
```

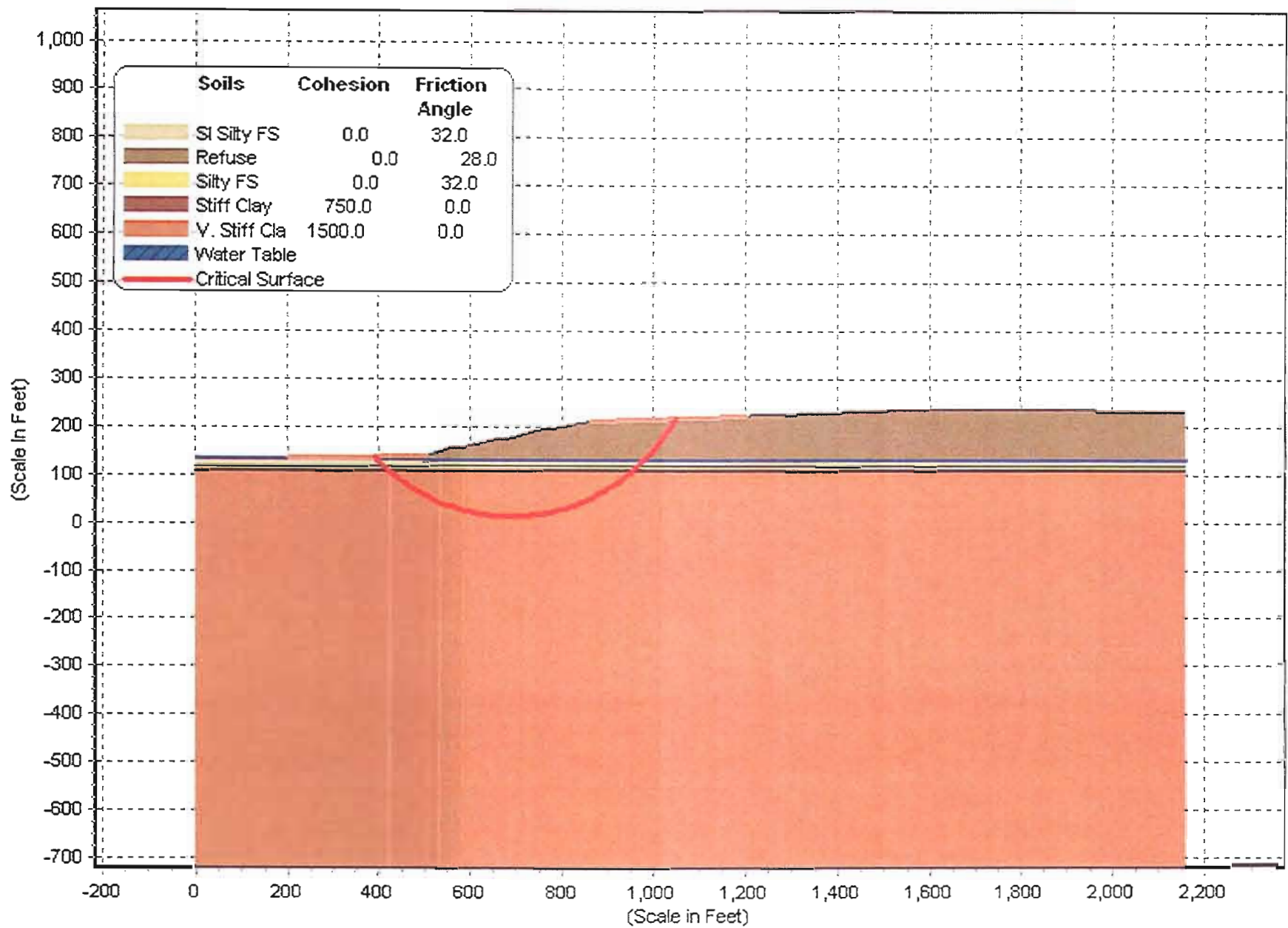
# LENA ROAD LANDFILL - X-SEC B - B'



LENA ROAD LANDFILL - X-SEC B - B' - FS Min- Spencer = 1.901



LENA ROAD LANDFILL - X-SEC B - B' - FS Min- Spencer = 1.901



result.out  
 \*\* STABL for WINDOWS \*\*  
 by  
 Geotechnical Software Solutions

1

--Slope Stability Analysis--  
 Simplified Janbu, Simplified Bishop  
 or Spencer's Method of Slices

Run Date: 9/27/10  
 Time of Run: 13:00  
 Run By: Shawkat Ali  
 Input Data Filename: run.in  
 Output Filename: result.out  
 Unit: U.S.C.  
 Plotted Output Filename: result.plt

PROBLEM DESCRIPTION LENA ROAD LANDFILL - X-SEC B - B'

BOUNDARY COORDINATES

12 Top Boundaries  
 17 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	135.00	300.00	135.00	2
2	300.00	135.00	500.00	140.00	2
3	500.00	140.00	560.00	155.00	1
4	560.00	155.00	580.00	155.00	1
5	580.00	155.00	660.00	175.00	1
6	660.00	175.00	680.00	175.00	1
7	680.00	175.00	760.00	195.00	1
8	760.00	195.00	780.00	195.00	1
9	780.00	195.00	860.00	210.00	1
10	860.00	210.00	1560.00	235.00	1
11	1560.00	235.00	1760.00	235.00	1
12	1760.00	235.00	2160.00	230.00	1
13	500.10	127.00	500.20	140.00	1
14	500.10	127.00	2160.00	127.00	2
15	0.00	116.50	2160.00	116.50	3
16	0.00	111.50	2160.00	111.50	4
17	0.00	106.50	2160.00	106.50	5

1

ISOTROPIC SOIL PARAMETERS

5 Type(s) of Soil

soil	Total	Saturated	Cohesion	Friction	Pore	Pressure	Piez.
------	-------	-----------	----------	----------	------	----------	-------

Type No.	Unit Wt. (pcf)	Unit Wt. (pcf)	Intercept (psf)	Angle (deg)	Pressure Param.	Constant (psf)	Surface No.
1	70.0	80.0	0.0	28.0	0.00	0.0	1
2	100.0	110.0	0.0	32.0	0.00	0.0	1
3	95.0	105.0	0.0	32.0	0.00	0.0	1
4	105.0	120.0	750.0	0.0	0.00	0.0	1
5	115.0	130.0	1500.0	0.0	0.00	0.0	1

1

1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED

Unit weight of Water = 62.40

Piezometric Surface No. 1 Specified by 4 Coordinate Points

Point No.	X-Water (ft)	Y-Water (ft)
1	0.00	133.00
2	500.00	133.00
3	500.10	127.00
4	2160.00	127.00

1

A Critical Failure Surface Searching Method, Using A Random Technique For Generating Circular Surfaces, Has Been Specified.

400 Trial Surfaces Have Been Generated.

20 Surfaces Initiate From Each of 20 Points Equally Spaced Along The Ground Surface Between X = 200.00 ft. and X = 500.00 ft.

Each Surface Terminates Between X = 860.00 ft. and X = 1200.00 ft.

Unless Further Limitations Were Imposed, The Minimum Elevation At Which A Surface Extends Is Y = 0.00 ft.

10.00 ft. Line Segments Define Each Trial Failure Surface.

1

Following Are Displayed The Ten Most Critical Of The Trial Failure Surfaces Examined. They Are Ordered - Most Critical First.

\* \* Safety Factors Are Calculated By Spencer's Method \* \*

result.out

Number of convergent trials 324  
Number of non convergent trials 76

Failure Surface Specified By 78 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	389.47	137.24
2	396.57	130.19
3	403.83	123.31
4	411.25	116.61
5	418.84	110.09
6	426.57	103.76
7	434.46	97.61
8	442.49	91.65
9	450.66	85.88
10	458.96	80.31
11	467.40	74.94
12	475.96	69.78
13	484.65	64.82
14	493.45	60.07
15	502.36	55.53
16	511.38	51.21
17	520.49	47.10
18	529.71	43.22
19	539.01	39.55
20	548.40	36.11
21	557.87	32.90
22	567.41	29.91
23	577.02	27.15
24	586.70	24.62
25	596.43	22.32
26	606.22	20.26
27	616.05	18.43
28	625.92	16.84
29	635.83	15.49
30	645.77	14.37
31	655.73	13.49
32	665.71	12.85
33	675.70	12.45
34	685.70	12.28
35	695.70	12.36
36	705.69	12.67
37	715.68	13.23
38	725.65	14.02
39	735.59	15.05
40	745.51	16.32
41	755.40	17.83
42	765.24	19.57
43	775.05	21.55
44	784.80	23.76
45	794.50	26.21
46	804.13	28.88
47	813.70	31.79
48	823.20	34.92
49	832.62	38.28
50	841.95	41.86
51	851.20	45.67
52	860.35	49.70
53	869.41	53.94

		result.out
54	878.36	58.40
55	887.20	63.08
56	895.92	67.96
57	904.53	73.05
58	913.01	78.34
59	921.37	83.84
60	929.59	89.54
61	937.67	95.43
62	945.61	101.51
63	953.40	107.78
64	961.04	114.23
65	968.52	120.87
66	975.84	127.68
67	982.99	134.67
68	989.98	141.82
69	996.79	149.14
70	1003.43	156.62
71	1009.88	164.26
72	1016.15	172.05
73	1022.24	179.99
74	1028.13	188.07
75	1033.82	196.29
76	1039.32	204.64
77	1044.62	213.12
78	1046.71	216.67

Circle Center At X = 687.5 ; Y = 430.1 and Radius, 417.9

\*\*\* Factor of Safety = 1.901 \*\*\*

Individual data on the 95 slices

Slice No.	width (ft)	weight (lbs)	Water		Force Norm (lbs)	Force Tan (lbs)	Earthquake Force		Surcharge Load (lbs)
			Force Top (lbs)	Force Bot (lbs)			Hor (lbs)	Ver (lbs)	
1	4.3	926.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	2.8	1676.3	0.0	349.7	0.0	0.0	0.0	0.0	0.0
3	7.3	8262.0	0.0	3899.0	0.0	0.0	0.0	0.0	0.0
4	7.4	14126.0	0.0	8134.5	0.0	0.0	0.0	0.0	0.0
5	0.1	303.0	0.0	179.3	0.0	0.0	0.0	0.0	0.0
6	5.8	14902.6	0.0	9091.5	0.0	0.0	0.0	0.0	0.0
7	1.6	4774.4	0.0	2988.4	0.0	0.0	0.0	0.0	0.0
8	4.4	14155.8	0.0	8741.4	0.0	0.0	0.0	0.0	0.0
9	3.3	12158.8	0.0	7529.4	0.0	0.0	0.0	0.0	0.0
10	7.9	33296.7	0.0	20166.8	0.0	0.0	0.0	0.0	0.0
11	8.0	40389.0	0.0	23945.1	0.0	0.0	0.0	0.0	0.0
12	8.2	47487.3	0.0	27603.4	0.0	0.0	0.0	0.0	0.0
13	8.3	54566.0	0.0	31139.8	0.0	0.0	0.0	0.0	0.0
14	8.4	61600.3	0.0	34552.3	0.0	0.0	0.0	0.0	0.0
15	8.6	68565.2	0.0	37838.7	0.0	0.0	0.0	0.0	0.0
16	8.7	75436.7	0.0	40997.2	0.0	0.0	0.0	0.0	0.0
17	8.8	82191.1	0.0	44026.1	0.0	0.0	0.0	0.0	0.0
18	6.6	64775.1	0.0	34231.2	0.0	0.0	0.0	0.0	0.0
19	0.1	892.2	0.0	256.7	0.0	0.0	0.0	0.0	0.0
20	0.1	967.3	0.0	492.6	0.0	0.0	0.0	0.0	0.0
21	2.2	21077.5	0.0	10716.9	0.0	0.0	0.0	0.0	0.0
22	9.0	92128.7	0.0	45944.1	0.0	0.0	0.0	0.0	0.0



			result.out						
23	9.1	99601.8	0.0	48573.9	0.0	0.0	0.0	0.0	0.0
24	9.2	106910.9	0.0	51067.5	0.0	0.0	0.0	0.0	0.0
25	9.3	114034.3	0.0	53423.8	0.0	0.0	0.0	0.0	0.0
26	9.4	120949.2	0.0	55640.9	0.0	0.0	0.0	0.0	0.0
27	9.5	127634.9	0.0	57717.9	0.0	0.0	0.0	0.0	0.0
28	2.1	29468.3	0.0	13154.4	0.0	0.0	0.0	0.0	0.0
29	7.4	104122.0	0.0	46499.0	0.0	0.0	0.0	0.0	0.0
30	9.6	138183.9	0.0	61446.7	0.0	0.0	0.0	0.0	0.0
31	3.0	43457.7	0.0	19235.3	0.0	0.0	0.0	0.0	0.0
32	6.7	99353.1	0.0	43860.8	0.0	0.0	0.0	0.0	0.0
33	9.7	148290.0	0.0	64601.4	0.0	0.0	0.0	0.0	0.0
34	9.8	153527.3	0.0	65961.0	0.0	0.0	0.0	0.0	0.0
35	9.8	158431.5	0.0	67174.9	0.0	0.0	0.0	0.0	0.0
36	9.9	162988.1	0.0	68242.1	0.0	0.0	0.0	0.0	0.0
37	9.9	167182.3	0.0	69161.3	0.0	0.0	0.0	0.0	0.0
38	9.9	171004.9	0.0	69933.0	0.0	0.0	0.0	0.0	0.0
39	10.0	174444.3	0.0	70556.4	0.0	0.0	0.0	0.0	0.0
40	4.3	75665.7	0.0	30358.2	0.0	0.0	0.0	0.0	0.0
41	5.7	101539.9	0.0	40672.7	0.0	0.0	0.0	0.0	0.0
42	10.0	178264.2	0.0	71356.1	0.0	0.0	0.0	0.0	0.0
43	4.3	76860.8	0.0	30755.8	0.0	0.0	0.0	0.0	0.0
44	5.7	102175.7	0.0	40776.7	0.0	0.0	0.0	0.0	0.0
45	10.0	180699.3	0.0	71559.6	0.0	0.0	0.0	0.0	0.0
46	10.0	182108.4	0.0	71437.2	0.0	0.0	0.0	0.0	0.0
47	10.0	183100.1	0.0	71166.0	0.0	0.0	0.0	0.0	0.0
48	10.0	183671.6	0.0	70745.5	0.0	0.0	0.0	0.0	0.0
49	9.9	183822.3	0.0	70176.0	0.0	0.0	0.0	0.0	0.0
50	9.9	183554.2	0.0	69458.1	0.0	0.0	0.0	0.0	0.0
51	9.9	182868.2	0.0	68591.8	0.0	0.0	0.0	0.0	0.0
52	4.6	85027.8	0.0	31722.1	0.0	0.0	0.0	0.0	0.0
53	5.2	96502.4	0.0	35856.3	0.0	0.0	0.0	0.0	0.0
54	9.8	178523.1	0.0	66417.6	0.0	0.0	0.0	0.0	0.0
55	5.0	89207.0	0.0	33241.0	0.0	0.0	0.0	0.0	0.0
56	4.8	85899.1	0.0	31869.6	0.0	0.0	0.0	0.0	0.0
57	9.7	172248.6	0.0	63657.9	0.0	0.0	0.0	0.0	0.0
58	9.6	169176.9	0.0	62060.8	0.0	0.0	0.0	0.0	0.0
59	9.6	165738.2	0.0	60319.2	0.0	0.0	0.0	0.0	0.0
60	9.5	161948.0	0.0	58435.3	0.0	0.0	0.0	0.0	0.0
61	9.4	157816.8	0.0	56409.4	0.0	0.0	0.0	0.0	0.0
62	9.3	153359.1	0.0	54242.6	0.0	0.0	0.0	0.0	0.0
63	9.2	148591.6	0.0	51936.7	0.0	0.0	0.0	0.0	0.0
64	8.8	138091.0	0.0	47639.9	0.0	0.0	0.0	0.0	0.0
65	0.4	5439.1	0.0	1852.9	0.0	0.0	0.0	0.0	0.0
66	9.1	137722.9	0.0	46912.0	0.0	0.0	0.0	0.0	0.0
67	9.0	131276.4	0.0	44196.3	0.0	0.0	0.0	0.0	0.0
68	8.8	124621.3	0.0	41346.6	0.0	0.0	0.0	0.0	0.0
69	8.7	117780.9	0.0	38365.2	0.0	0.0	0.0	0.0	0.0
70	8.6	110776.0	0.0	35253.3	0.0	0.0	0.0	0.0	0.0
71	8.5	103631.3	0.0	32012.9	0.0	0.0	0.0	0.0	0.0
72	8.4	96370.2	0.0	28646.0	0.0	0.0	0.0	0.0	0.0
73	8.2	89016.1	0.0	25154.3	0.0	0.0	0.0	0.0	0.0
74	8.1	81594.4	0.0	21539.9	0.0	0.0	0.0	0.0	0.0
75	7.9	74129.9	0.0	17804.8	0.0	0.0	0.0	0.0	0.0
76	6.2	53573.0	0.0	11426.2	0.0	0.0	0.0	0.0	0.0
77	1.6	13085.4	0.0	2524.9	0.0	0.0	0.0	0.0	0.0
78	4.4	35033.3	0.0	6248.4	0.0	0.0	0.0	0.0	0.0
79	3.2	24553.0	0.0	3732.8	0.0	0.0	0.0	0.0	0.0
80	2.6	18771.7	0.0	2481.7	0.0	0.0	0.0	0.0	0.0
81	4.9	34418.6	0.0	3415.5	0.0	0.0	0.0	0.0	0.0
82	6.6	42355.4	0.0	1722.6	0.0	0.0	0.0	0.0	0.0
83	0.7	4435.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
84	7.2	41619.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85	7.0	37301.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0

				result.out					
86	6.8	33042.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
87	6.6	28857.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
88	6.5	24760.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
89	6.3	20766.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90	6.1	16889.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
91	5.9	13142.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
92	5.7	9540.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
93	5.5	6096.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
94	5.3	2824.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
95	2.1	254.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Failure Surface Specified By 79 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	357.90	136.45
2	365.08	129.49
3	372.42	122.70
4	379.92	116.09
5	387.57	109.65
6	395.37	103.39
7	403.32	97.32
8	411.40	91.43
9	419.62	85.74
10	427.97	80.23
11	436.45	74.93
12	445.05	69.82
13	453.76	64.92
14	462.59	60.22
15	471.52	55.73
16	480.56	51.45
17	489.69	47.38
18	498.92	43.52
19	508.24	39.88
20	517.63	36.46
21	527.11	33.26
22	536.65	30.28
23	546.27	27.53
24	555.94	25.00
25	565.67	22.70
26	575.46	20.63
27	585.28	18.78
28	595.15	17.17
29	605.06	15.78
30	614.99	14.63
31	624.95	13.71
32	634.92	13.02
33	644.91	12.57
34	654.91	12.35
35	664.91	12.36
36	674.91	12.61
37	684.90	13.09
38	694.87	13.80
39	704.83	14.75
40	714.76	15.93
41	724.66	17.34
42	734.52	18.98
43	744.34	20.85
44	754.12	22.95
45	763.85	25.27
46	773.52	27.83

		result.out
47	783.12	30.61
48	792.66	33.61
49	802.13	36.83
50	811.51	40.28
51	820.82	43.94
52	830.04	47.82
53	839.16	51.92
54	848.19	56.22
55	857.11	60.74
56	865.92	65.46
57	874.62	70.38
58	883.21	75.51
59	891.67	80.84
60	900.01	86.37
61	908.21	92.08
62	916.28	97.99
63	924.21	104.08
64	931.99	110.36
65	939.63	116.82
66	947.11	123.45
67	954.44	130.26
68	961.60	137.24
69	968.60	144.38
70	975.43	151.68
71	982.09	159.14
72	988.57	166.76
73	994.87	174.52
74	1000.99	182.43
75	1006.93	190.48
76	1012.67	198.67
77	1018.22	206.98
78	1023.58	215.43
79	1023.83	215.85

Circle Center At X = 659.4 ; Y = 440.5 and Radius, 428.1

\*\*\* Factor of Safety = 1.917 \*\*\*

1

Failure Surface Specified By 78 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	357.90	136.45
2	365.06	129.47
3	372.39	122.67
4	379.88	116.04
5	387.52	109.59
6	395.31	103.32
7	403.25	97.25
8	411.33	91.36
9	419.55	85.66
10	427.91	80.16
11	436.39	74.86
12	444.99	69.77
13	453.71	64.88
14	462.55	60.19

		result.out
15	471.49	55.72
16	480.54	51.46
17	489.69	47.42
18	498.93	43.60
19	508.26	39.99
20	517.67	36.61
21	527.16	33.45
22	536.72	30.52
23	546.34	27.82
24	556.03	25.34
25	565.78	23.10
26	575.57	21.09
27	585.41	19.31
28	595.29	17.76
29	605.21	16.45
30	615.15	15.38
31	625.11	14.54
32	635.10	13.94
33	645.09	13.57
34	655.09	13.44
35	665.09	13.55
36	675.08	13.90
37	685.06	14.48
38	695.03	15.30
39	704.98	16.36
40	714.89	17.65
41	724.77	19.18
42	734.62	20.94
43	744.42	22.93
44	754.17	25.16
45	763.86	27.62
46	773.49	30.30
47	783.06	33.22
48	792.55	36.36
49	801.97	39.72
50	811.30	43.31
51	820.55	47.11
52	829.71	51.14
53	838.76	55.38
54	847.71	59.84
55	856.56	64.50
56	865.29	69.38
57	873.90	74.46
58	882.39	79.74
59	890.76	85.23
60	898.99	90.91
61	907.08	96.78
62	915.03	102.84
63	922.84	109.09
64	930.49	115.53
65	937.99	122.14
66	945.33	128.93
67	952.51	135.90
68	959.52	143.03
69	966.36	150.32
70	973.02	157.78
71	979.51	165.39
72	985.81	173.15
73	991.93	181.07
74	997.86	189.12
75	1003.59	197.31
76	1009.13	205.64
77	1014.47	214.09

78            1015.34            result.out  
   215.55

Circle Center At X = 655.5 ; Y = 434.9 and Radius, 421.5

\*\*\* Factor of Safety = 1.925 \*\*\*

Failure surface specified By 79 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	342.11	136.05
2	349.23	129.04
3	356.52	122.19
4	363.97	115.52
5	371.57	109.02
6	379.33	102.71
7	387.23	96.58
8	395.27	90.63
9	403.45	84.88
10	411.76	79.32
11	420.20	73.96
12	428.77	68.80
13	437.45	63.84
14	446.25	59.09
15	455.16	54.54
16	464.17	50.21
17	473.28	46.09
18	482.49	42.18
19	491.78	38.50
20	501.16	35.03
21	510.62	31.78
22	520.15	28.76
23	529.75	25.96
24	539.42	23.39
25	549.14	21.05
26	558.91	18.93
27	568.73	17.05
28	578.60	15.40
29	588.49	13.98
30	598.42	12.79
31	608.38	11.84
32	618.35	11.12
33	628.34	10.64
34	638.34	10.39
35	648.34	10.37
36	658.33	10.60
37	668.32	11.05
38	678.30	11.75
39	688.26	12.67
40	698.19	13.83
41	708.09	15.23
42	717.96	16.85
43	727.78	18.71
44	737.56	20.80
45	747.29	23.12
46	756.96	25.66
47	766.57	28.44

		result.out
48	776.11	31.43
49	785.58	34.66
50	794.97	38.10
51	804.27	41.76
52	813.49	45.64
53	822.61	49.74
54	831.63	54.05
55	840.55	58.57
56	849.36	63.30
57	858.06	68.24
58	866.64	73.38
59	875.09	78.72
60	883.42	84.25
61	891.61	89.99
62	899.67	95.91
63	907.59	102.02
64	915.36	108.31
65	922.98	114.79
66	930.44	121.44
67	937.75	128.27
68	944.90	135.27
69	951.87	142.43
70	958.68	149.75
71	965.31	157.24
72	971.77	164.87
73	978.04	172.66
74	984.13	180.59
75	990.03	188.67
76	995.74	196.88
77	1001.26	205.22
78	1006.57	213.69
79	1007.51	215.27

Circle Center At X = 643.9 ; Y = 435.5 and Radius, 425.1

\*\*\* Factor of Safety = 1.927 \*\*\*

1

Failure Surface Specified By 78 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	436.84	138.42
2	443.94	131.38
3	451.21	124.51
4	458.64	117.82
5	466.23	111.30
6	473.97	104.97
7	481.86	98.83
8	489.90	92.88
9	498.08	87.13
10	506.39	81.57
11	514.84	76.22
12	523.41	71.06
13	532.10	66.12
14	540.91	61.39
15	549.83	56.86

		result.out
16	558.85	52.56
17	567.98	48.47
18	577.20	44.60
19	586.51	40.96
20	595.91	37.53
21	605.38	34.34
22	614.93	31.37
23	624.55	28.64
24	634.23	26.13
25	643.97	23.86
26	653.76	21.83
27	663.60	20.03
28	673.48	18.46
29	683.39	17.13
30	693.33	16.05
31	703.29	15.20
32	713.27	14.59
33	723.27	14.22
34	733.27	14.09
35	743.27	14.20
36	753.26	14.55
37	763.24	15.14
38	773.21	15.96
39	783.15	17.03
40	793.07	18.34
41	802.95	19.88
42	812.79	21.66
43	822.58	23.68
44	832.32	25.93
45	842.01	28.42
46	851.63	31.13
47	861.19	34.08
48	870.67	37.25
49	880.08	40.65
50	889.40	44.28
51	898.62	48.13
52	907.76	52.20
53	916.79	56.49
54	925.72	60.99
55	934.54	65.71
56	943.24	70.63
57	951.82	75.77
58	960.28	81.11
59	968.60	86.65
60	976.79	92.39
61	984.84	98.32
62	992.75	104.44
63	1000.50	110.76
64	1008.11	117.25
65	1015.55	123.93
66	1022.83	130.79
67	1029.94	137.81
68	1036.89	145.01
69	1043.66	152.37
70	1050.25	159.89
71	1056.66	167.57
72	1062.88	175.40
73	1068.91	183.37
74	1074.75	191.49
75	1080.39	199.75
76	1085.83	208.14
77	1091.07	216.66
78	1092.02	218.29

result.out

Circle Center At X = 733.7 ; Y = 430.6 and Radius, 416.5

\*\*\* Factor of Safety = 1.934 \*\*\*

Failure Surface Specified By 77 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	436.84	138.42
2	443.94	131.38
3	451.21	124.51
4	458.65	117.83
5	466.24	111.32
6	474.00	105.01
7	481.90	98.88
8	489.95	92.95
9	498.15	87.22
10	506.48	81.69
11	514.94	76.36
12	523.53	71.24
13	532.25	66.33
14	541.08	61.64
15	550.02	57.16
16	559.07	52.91
17	568.22	48.87
18	577.46	45.06
19	586.80	41.48
20	596.22	38.12
21	605.72	35.00
22	615.29	32.11
23	624.93	29.45
24	634.63	27.03
25	644.39	24.84
26	654.20	22.90
27	664.05	21.19
28	673.95	19.73
29	683.87	18.50
30	693.82	17.52
31	703.79	16.79
32	713.78	16.29
33	723.78	16.04
34	733.78	16.04
35	743.78	16.27
36	753.77	16.75
37	763.74	17.48
38	773.69	18.45
39	783.62	19.66
40	793.51	21.11
41	803.37	22.80
42	813.18	24.73
43	822.94	26.91
44	832.65	29.31
45	842.29	31.96
46	851.87	34.84
47	861.37	37.95
48	870.79	41.29



		result.out
49	880.14	44.87
50	889.39	48.66
51	898.54	52.69
52	907.59	56.93
53	916.54	61.40
54	925.38	66.08
55	934.10	70.98
56	942.70	76.08
57	951.17	81.40
58	959.50	86.92
59	967.71	92.64
60	975.77	98.56
61	983.68	104.68
62	991.44	110.98
63	999.04	117.48
64	1006.49	124.15
65	1013.77	131.01
66	1020.88	138.04
67	1027.81	145.25
68	1034.57	152.62
69	1041.15	160.15
70	1047.54	167.84
71	1053.74	175.69
72	1059.74	183.68
73	1065.56	191.82
74	1071.17	200.10
75	1076.57	208.51
76	1081.77	217.05
77	1082.29	217.94

Circle Center At X = 729.0 ; Y = 426.0 and Radius, 410.0

\*\*\* Factor of Safety = 1.936 \*\*\*

1

Failure Surface Specified By 80 Coordinate Points

Point No.	X-surf (ft)	Y-surf (ft)
1	405.26	137.63
2	412.70	130.94
3	420.28	124.42
4	428.00	118.06
5	435.86	111.88
6	443.85	105.87
7	451.97	100.03
8	460.22	94.38
9	468.59	88.91
10	477.07	83.62
11	485.68	78.52
12	494.39	73.61
13	503.20	68.89
14	512.12	64.37
15	521.14	60.04
16	530.25	55.91
17	539.44	51.99
18	548.72	48.26

		result.out
19	558.08	44.74
20	567.52	41.43
21	577.03	38.32
22	586.60	35.43
23	596.23	32.74
24	605.92	30.27
25	615.66	28.01
26	625.45	25.96
27	635.28	24.13
28	645.15	22.52
29	655.05	21.12
30	664.98	19.94
31	674.93	18.97
32	684.91	18.23
33	694.89	17.70
34	704.89	17.40
35	714.89	17.31
36	724.89	17.44
37	734.88	17.80
38	744.86	18.37
39	754.83	19.16
40	764.78	20.17
41	774.71	21.39
42	784.60	22.84
43	794.46	24.50
44	804.28	26.37
45	814.06	28.47
46	823.79	30.77
47	833.47	33.29
48	843.09	36.02
49	852.65	38.96
50	862.14	42.11
51	871.56	45.47
52	880.90	49.03
53	890.17	52.80
54	899.35	56.77
55	908.43	60.94
56	917.43	65.30
57	926.33	69.87
58	935.12	74.63
59	943.81	79.58
60	952.39	84.72
61	960.85	90.04
62	969.20	95.55
63	977.42	101.25
64	985.51	107.12
65	993.48	113.17
66	1001.31	119.39
67	1009.00	125.78
68	1016.55	132.34
69	1023.95	139.06
70	1031.20	145.94
71	1038.31	152.98
72	1045.25	160.18
73	1052.04	167.52
74	1058.66	175.02
75	1065.12	182.65
76	1071.40	190.43
77	1077.52	198.34
78	1083.46	206.38
79	1089.22	214.56
80	1091.72	218.28

result.out  
Circle Center At X = 713.8 ; Y = 473.1 and Radius, 455.8

\*\*\* Factor of Safety = 1.936 \*\*\*

Failure Surface Specified By 79 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	326.32	135.66
2	333.41	128.61
3	340.67	121.73
4	348.09	115.03
5	355.66	108.50
6	363.39	102.15
7	371.26	95.98
8	379.27	90.00
9	387.43	84.21
10	395.71	78.61
11	404.13	73.21
12	412.67	68.01
13	421.33	63.01
14	430.10	58.21
15	438.99	53.62
16	447.98	49.24
17	457.07	45.08
18	466.26	41.12
19	475.53	37.39
20	484.89	33.87
21	494.33	30.58
22	503.85	27.50
23	513.44	24.66
24	523.09	22.03
25	532.80	19.64
26	542.56	17.47
27	552.37	15.53
28	562.22	13.83
29	572.11	12.35
30	582.03	11.11
31	591.98	10.10
32	601.95	9.33
33	611.94	8.79
34	621.93	8.48
35	631.93	8.41
36	641.93	8.57
37	651.92	8.97
38	661.90	9.60
39	671.87	10.47
40	681.81	11.57
41	691.72	12.91
42	701.59	14.47
43	711.43	16.27
44	721.22	18.30
45	730.97	20.55
46	740.65	23.04
47	750.28	25.75
48	759.84	28.69
49	769.32	31.85

		result.out
50	778.73	35.23
51	788.06	38.84
52	797.30	42.66
53	806.45	46.69
54	815.50	50.94
55	824.45	55.41
56	833.30	60.08
57	842.03	64.95
58	850.64	70.03
59	859.13	75.31
60	867.50	80.79
61	875.73	86.47
62	883.83	92.33
63	891.79	98.39
64	899.60	104.63
65	907.27	111.05
66	914.78	117.65
67	922.14	124.42
68	929.33	131.37
69	936.36	138.48
70	943.22	145.76
71	949.91	153.19
72	956.42	160.78
73	962.75	168.52
74	968.90	176.41
75	974.86	184.43
76	980.64	192.60
77	986.21	200.90
78	991.60	209.33
79	994.92	214.82

Circle Center At X = 630.0 ; Y = 434.3 and Radius, 425.9

\*\*\* Factor of Safety = 1.940 \*\*\*

1

Failure Surface Specified By 78 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	421.05	138.03
2	428.48	131.33
3	436.06	124.81
4	443.79	118.46
5	451.65	112.28
6	459.66	106.29
7	467.79	100.47
8	476.06	94.85
9	484.45	89.40
10	492.96	84.15
11	501.59	79.10
12	510.32	74.24
13	519.17	69.57
14	528.12	65.11
15	537.17	60.85
16	546.31	56.80
17	555.54	52.95

		result.out
18	564.85	49.31
19	574.25	45.89
20	583.72	42.67
21	593.26	39.67
22	602.86	36.89
23	612.53	34.32
24	622.25	31.97
25	632.02	29.85
26	641.84	27.94
27	651.69	26.25
28	661.58	24.79
29	671.51	23.55
30	681.46	22.54
31	691.42	21.75
32	701.41	21.18
33	711.40	20.84
34	721.40	20.73
35	731.40	20.84
36	741.40	21.18
37	751.38	21.74
38	761.35	22.53
39	771.30	23.54
40	781.22	24.78
41	791.11	26.23
42	800.97	27.92
43	810.79	29.82
44	820.56	31.95
45	830.28	34.29
46	839.95	36.86
47	849.55	39.64
48	859.09	42.63
49	868.56	45.84
50	877.96	49.27
51	887.27	52.90
52	896.51	56.75
53	905.65	60.80
54	914.70	65.06
55	923.65	69.52
56	932.50	74.18
57	941.24	79.04
58	949.86	84.09
59	958.38	89.34
60	966.77	94.78
61	975.03	100.40
62	983.17	106.22
63	991.18	112.21
64	999.04	118.38
65	1006.77	124.73
66	1014.35	131.25
67	1021.78	137.94
68	1029.06	144.80
69	1036.19	151.82
70	1043.15	159.00
71	1049.95	166.33
72	1056.58	173.81
73	1063.04	181.45
74	1069.33	189.22
75	1075.44	197.14
76	1081.37	205.19
77	1087.12	213.37
78	1090.37	218.23

Circle Center At X = 721.5 ; Y = 464.0 and Radius, 443.3  
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result.out

\*\*\* Factor of Safety = 1.955 \*\*\*

Failure Surface Specified By 78 Coordinate Points

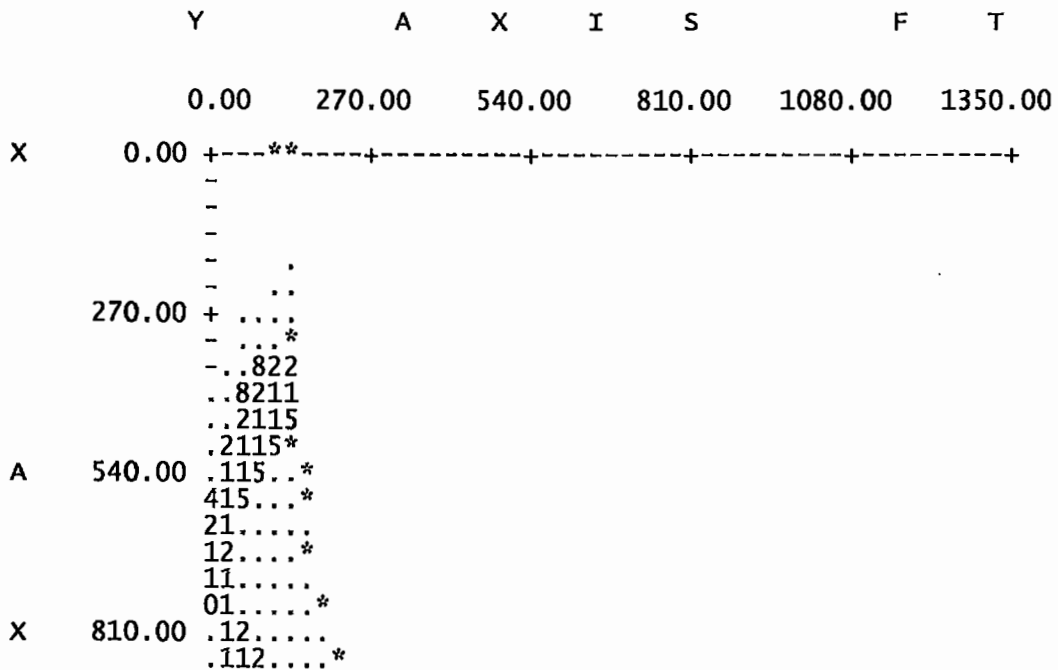
Point No.	X-Surf (ft)	Y-Surf (ft)
1	452.63	138.82
2	459.70	131.75
3	466.95	124.85
4	474.35	118.13
5	481.91	111.59
6	489.63	105.23
7	497.50	99.06
8	505.52	93.08
9	513.67	87.29
10	521.97	81.71
11	530.39	76.32
12	538.95	71.14
13	547.62	66.16
14	556.41	61.40
15	565.32	56.85
16	574.33	52.51
17	583.44	48.39
18	592.65	44.49
19	601.95	40.81
20	611.33	37.36
21	620.80	34.14
22	630.34	31.14
23	639.95	28.37
24	649.62	25.84
25	659.35	23.54
26	669.14	21.47
27	678.97	19.64
28	688.84	18.04
29	698.75	16.69
30	708.68	15.57
31	718.65	14.69
32	728.63	14.05
33	738.62	13.65
34	748.62	13.49
35	758.62	13.58
36	768.61	13.90
37	778.59	14.46
38	788.56	15.26
39	798.51	16.30
40	808.43	17.58
41	818.31	19.10
42	828.15	20.86
43	837.95	22.85
44	847.70	25.07
45	857.40	27.53
46	867.03	30.23
47	876.59	33.15
48	886.08	36.30
49	895.49	39.68
50	904.82	43.28

		result.out
51	914.06	47.11
52	923.20	51.16
53	932.25	55.43
54	941.18	59.91
55	950.01	64.61
56	958.73	69.52
57	967.32	74.63
58	975.79	79.95
59	984.12	85.48
60	992.32	91.20
61	1000.38	97.11
62	1008.30	103.22
63	1016.07	109.52
64	1023.68	116.00
65	1031.14	122.67
66	1038.43	129.51
67	1045.56	136.52
68	1052.52	143.71
69	1059.30	151.06
70	1065.90	158.57
71	1072.32	166.23
72	1078.56	174.05
73	1084.60	182.02
74	1090.45	190.13
75	1096.11	198.37
76	1101.57	206.75
77	1106.82	215.26
78	1108.94	218.89

Circle Center At X = 750.2 ; Y = 429.4 and Radius, 416.0

\*\*\* Factor of Safety = 1.956 \*\*\*

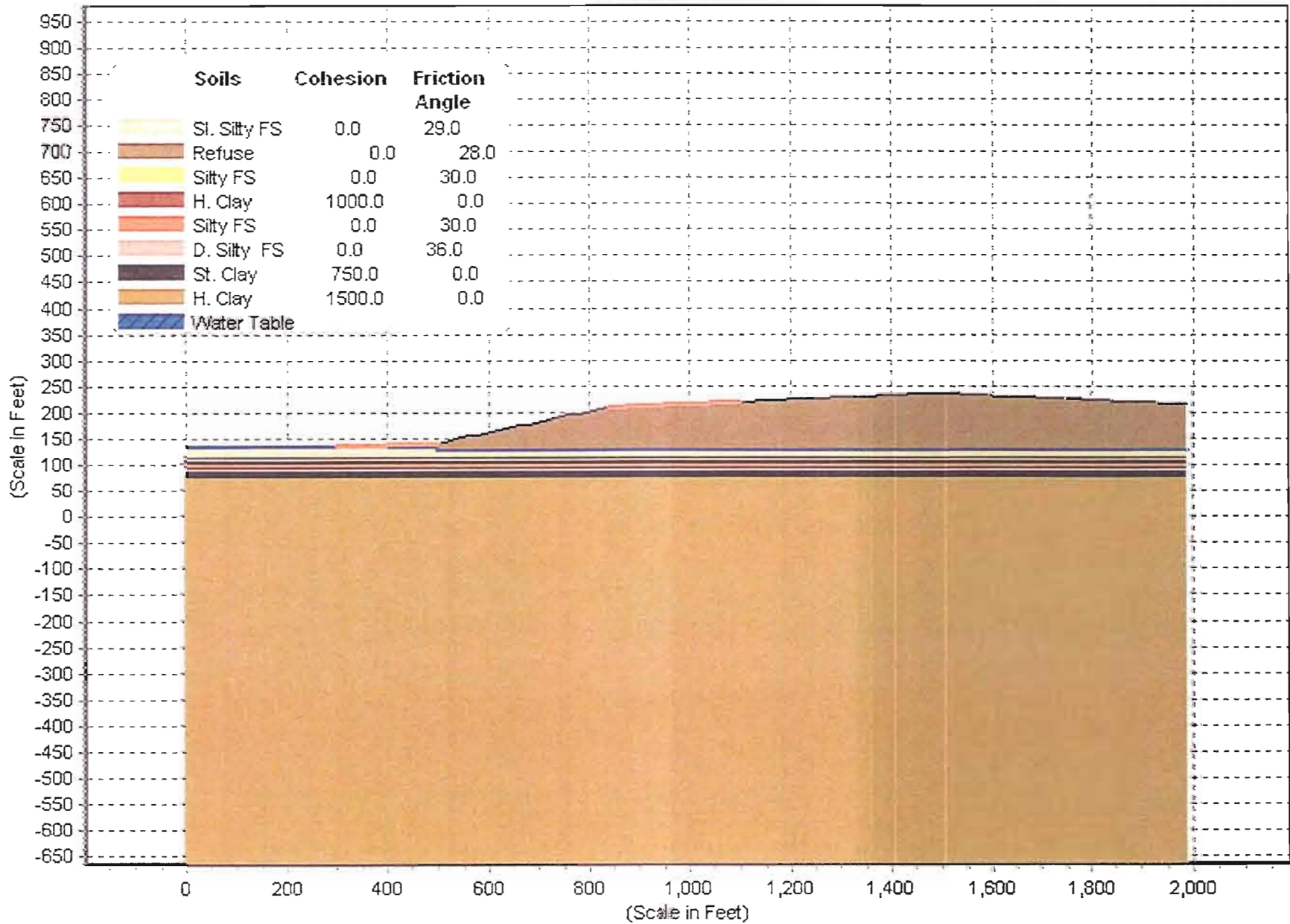
1



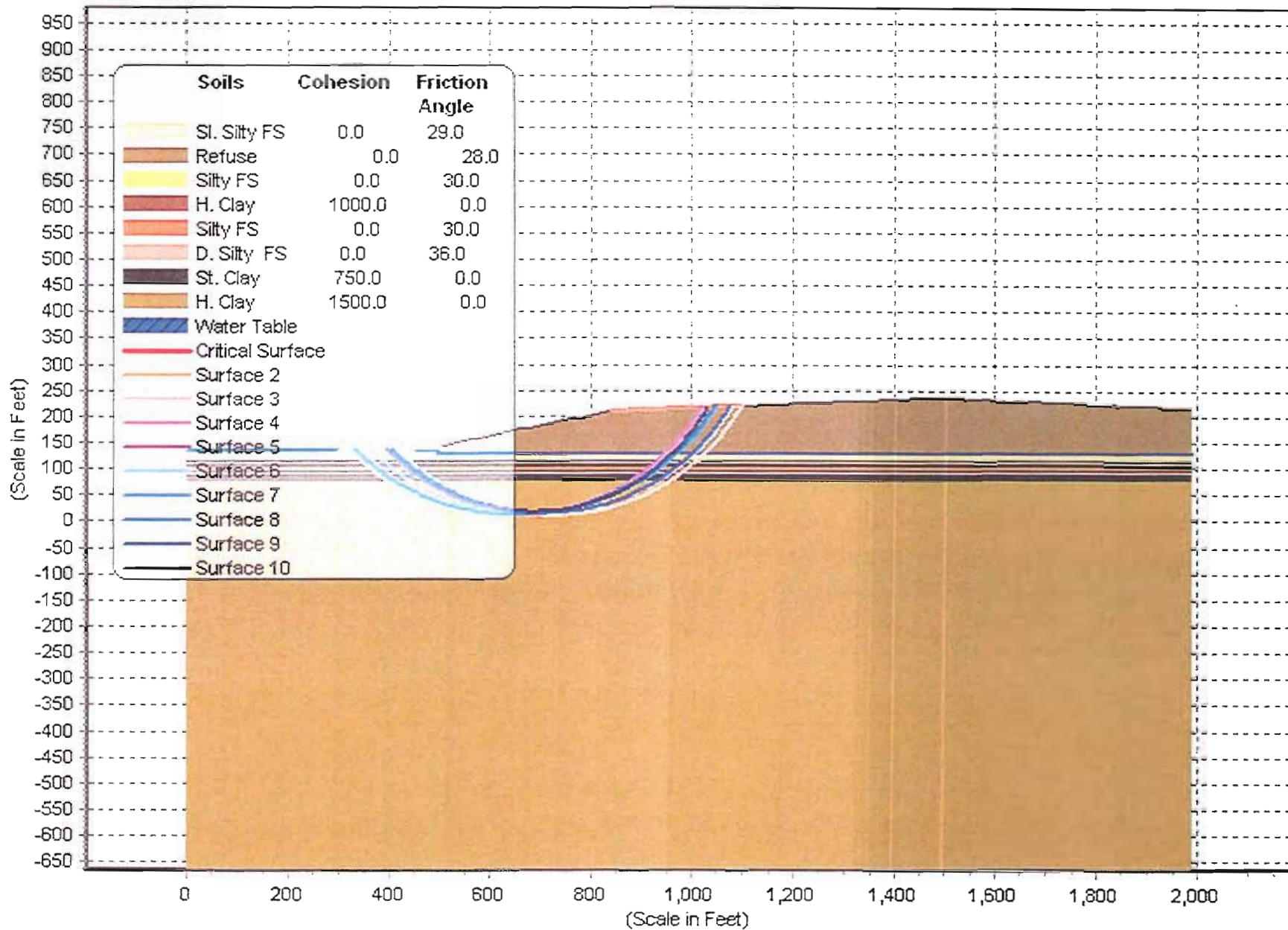




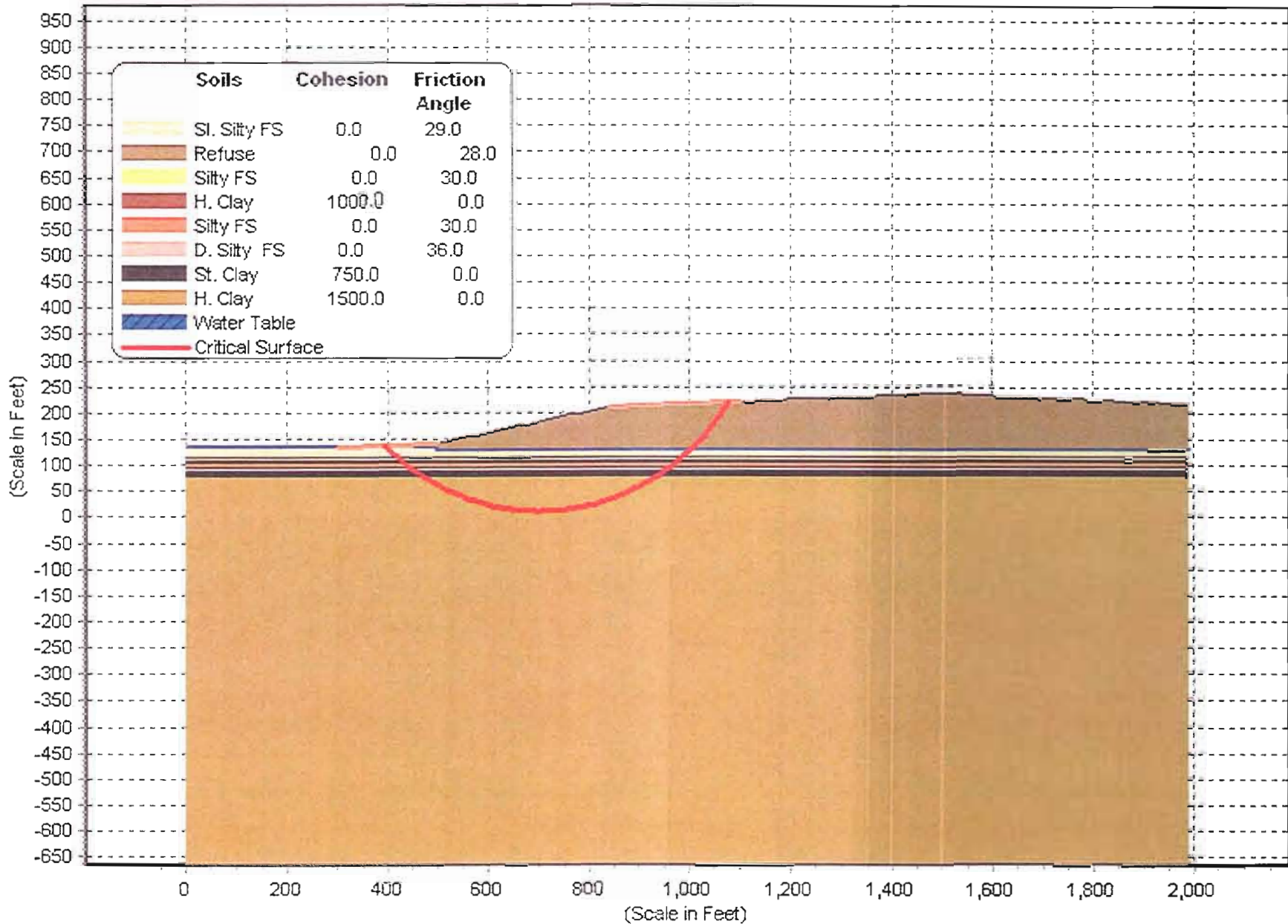
# LENA ROAD LANDFILL - X-SEC C - C'



LENA ROAD LANDFILL - X-SEC C - C' - FS Min- Spencer = 1.928



LENA ROAD LANDFILL - X-SEC C - C' - FS Min- Spencer = 1.928



result.out  
 \*\* STABL for WINDOWS \*\*  
 by  
 Geotechnical Software Solutions

1

--Slope Stability Analysis--  
 Simplified Janbu, Simplified Bishop  
 or Spencer's Method of Slices

Run Date: 9/27/10  
 Time of Run: 14:30  
 Run By: Shawkat Ali  
 Input Data Filename: run.in  
 Output Filename: result.out  
 Unit: U.S.C.  
 Plotted Output Filename: result.plt

PROBLEM DESCRIPTION LENA ROAD LANDFILL - X-SEC C - C'

BOUNDARY COORDINATES

20 Top Boundaries  
 28 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	135.00	300.00	135.00	2
2	300.00	135.00	500.00	140.00	2
3	500.00	140.00	560.00	155.00	1
4	560.00	155.00	580.00	155.00	1
5	580.00	155.00	660.00	175.00	1
6	660.00	175.00	680.00	175.00	1
7	680.00	175.00	760.00	195.00	1
8	760.00	195.00	780.00	195.00	1
9	780.00	195.00	840.00	210.00	1
10	840.00	210.00	840.00	210.00	1
11	840.00	210.00	980.00	215.00	1
12	980.00	215.00	1100.00	220.00	1
13	1100.00	220.00	1220.00	225.00	1
14	1220.00	225.00	1340.00	230.00	1
15	1340.00	230.00	1460.00	235.00	1
16	1460.00	235.00	1510.00	235.00	1
17	1510.00	235.00	1630.00	230.00	1
18	1630.00	230.00	1750.00	225.00	1
19	1750.00	225.00	1870.00	220.00	1
20	1870.00	220.00	1990.00	215.00	1
21	500.10	127.00	500.20	140.00	1
22	500.10	127.00	1990.00	127.00	2
23	0.00	113.00	1990.00	113.00	3
24	0.00	108.00	1990.00	108.00	4
25	0.00	103.00	1990.00	103.00	5
26	0.00	93.00	1990.00	93.00	6
27	0.00	88.00	1990.00	88.00	7

1 28 0.00 78.00 result.out 1990.00 78.00 8

ISOTROPIC SOIL PARAMETERS

8 Type(s) of Soil

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	70.0	80.0	0.0	28.0	0.00	0.0	1
2	95.0	105.0	0.0	29.0	0.00	0.0	1
3	100.0	110.0	0.0	30.0	0.00	0.0	1
4	110.0	125.0	1000.0	0.0	0.00	0.0	1
5	100.0	110.0	0.0	30.0	0.00	0.0	1
6	110.0	120.0	0.0	36.0	0.00	0.0	1
7	105.0	120.0	750.0	0.0	0.00	0.0	1
8	115.0	130.0	1500.0	0.0	0.00	0.0	1

1

1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED

Unit Weight of Water = 62.40

Piezometric Surface No. 1 Specified by 4 Coordinate Points

Point No.	X-Water (ft)	Y-Water (ft)
1	0.00	133.00
2	500.00	133.00
3	500.10	127.00
4	1990.00	127.00

1

A Critical Failure Surface Searching Method, Using A Random Technique For Generating Circular Surfaces, Has Been Specified.

400 Trial Surfaces Have Been Generated.

20 Surfaces Initiate From Each Of 20 Points Equally Spaced Along The Ground Surface Between X = 300.00 ft. and X = 500.00 ft.

Each Surface Terminates Between X = 840.00 ft. and X = 1100.00 ft.

Unless Further Limitations Were Imposed, The Minimum Elevation At Which A Surface Extends Is Y = 0.00 ft.

result.out

10.00 ft. Line Segments Define Each Trial Failure Surface.

1

Following Are Displayed The Ten Most Critical Of The Trial Failure Surfaces Examined. They Are Ordered - Most Critical First.

\* \* Safety Factors Are Calculated By Spencer's Method \* \*

Number of convergent trials            379  
Number of non convergent trials       21

Failure surface specified by 80 coordinate points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	394.74	137.37
2	401.88	130.37
3	409.19	123.55
4	416.65	116.89
5	424.26	110.40
6	432.02	104.09
7	439.92	97.96
8	447.96	92.02
9	456.14	86.25
10	464.44	80.68
11	472.87	75.30
12	481.42	70.12
13	490.09	65.13
14	498.87	60.35
15	507.76	55.76
16	516.75	51.38
17	525.83	47.21
18	535.02	43.25
19	544.29	39.50
20	553.64	35.96
21	563.07	32.64
22	572.58	29.54
23	582.15	26.66
24	591.79	23.99
25	601.49	21.55
26	611.24	19.33
27	621.04	17.34
28	630.88	15.57
29	640.76	14.03
30	650.68	12.71
31	660.62	11.63
32	670.58	10.77
33	680.56	10.14
34	690.55	9.74
35	700.55	9.57
36	710.55	9.62
37	720.55	9.91
38	730.53	10.43
39	740.51	11.17

		result.out
40	750.46	12.15
41	760.38	13.35
42	770.28	14.78
43	780.14	16.44
44	789.96	18.32
45	799.74	20.43
46	809.46	22.76
47	819.13	25.32
48	828.74	28.09
49	838.28	31.09
50	847.75	34.30
51	857.14	37.73
52	866.46	41.38
53	875.68	45.24
54	884.82	49.30
55	893.86	53.58
56	902.79	58.06
57	911.63	62.75
58	920.35	67.64
59	928.96	72.73
60	937.45	78.01
61	945.82	83.49
62	954.06	89.16
63	962.16	95.01
64	970.13	101.05
65	977.96	107.27
66	985.65	113.67
67	993.18	120.25
68	1000.56	126.99
69	1007.79	133.91
70	1014.85	140.98
71	1021.75	148.22
72	1028.49	155.61
73	1035.05	163.16
74	1041.44	170.85
75	1047.64	178.69
76	1053.67	186.67
77	1059.51	194.79
78	1065.17	203.04
79	1070.63	211.41
80	1075.32	218.97

Circle Center At X = 703.0 ; Y = 445.2 and Radius, 435.7

\*\*\* Factor of safety = 1.928 \*\*\*

Individual data on the 104 slices

Slice No.	Width (ft)	Weight (lbs)	Water Force		Force Norm (lbs)	Force Tan (lbs)	Earthquake Force		Surcharge Load (lbs)
			Top (lbs)	Bot (lbs)			Hor (lbs)	Ver (lbs)	
1	4.5	949.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	2.7	1520.4	0.0	307.5	0.0	0.0	0.0	0.0	0.0
3	7.3	7852.5	0.0	3768.9	0.0	0.0	0.0	0.0	0.0
4	7.5	13432.3	0.0	7976.8	0.0	0.0	0.0	0.0	0.0
5	4.6	10804.2	0.0	6752.9	0.0	0.0	0.0	0.0	0.0
6	3.0	8308.5	0.0	5325.1	0.0	0.0	0.0	0.0	0.0

			result.out						
7	3.0	8877.8	0.0	5652.2	0.0	0.0	0.0	0.0	0.0
8	4.8	16300.6	0.0	10417.9	0.0	0.0	0.0	0.0	0.0
9	1.4	5224.6	0.0	3274.1	0.0	0.0	0.0	0.0	0.0
10	6.5	26407.2	0.0	16677.0	0.0	0.0	0.0	0.0	0.0
11	6.7	31077.1	0.0	19536.0	0.0	0.0	0.0	0.0	0.0
12	1.3	6620.1	0.0	4183.0	0.0	0.0	0.0	0.0	0.0
13	5.7	30097.1	0.0	18700.1	0.0	0.0	0.0	0.0	0.0
14	2.5	13960.1	0.0	8671.6	0.0	0.0	0.0	0.0	0.0
15	8.3	50567.0	0.0	30907.3	0.0	0.0	0.0	0.0	0.0
16	4.2	27749.8	0.0	16701.3	0.0	0.0	0.0	0.0	0.0
17	4.2	29345.8	0.0	17622.7	0.0	0.0	0.0	0.0	0.0
18	8.6	63903.7	0.0	37620.0	0.0	0.0	0.0	0.0	0.0
19	8.7	70684.0	0.0	40793.5	0.0	0.0	0.0	0.0	0.0
20	8.8	77358.5	0.0	43842.9	0.0	0.0	0.0	0.0	0.0
21	1.1	10383.4	0.0	5798.3	0.0	0.0	0.0	0.0	0.0
22	0.1	813.4	0.0	246.8	0.0	0.0	0.0	0.0	0.0
23	0.1	883.9	0.0	472.7	0.0	0.0	0.0	0.0	0.0
24	7.6	69224.5	0.0	36756.2	0.0	0.0	0.0	0.0	0.0
25	9.0	88510.0	0.0	45819.0	0.0	0.0	0.0	0.0	0.0
26	9.1	95964.9	0.0	48486.6	0.0	0.0	0.0	0.0	0.0
27	9.2	103272.0	0.0	51024.0	0.0	0.0	0.0	0.0	0.0
28	9.3	110410.8	0.0	53429.9	0.0	0.0	0.0	0.0	0.0
29	9.4	117360.9	0.0	55703.1	0.0	0.0	0.0	0.0	0.0
30	6.4	83054.5	0.0	38771.0	0.0	0.0	0.0	0.0	0.0
31	3.1	40965.4	0.0	19071.3	0.0	0.0	0.0	0.0	0.0
32	9.5	129315.0	0.0	59846.4	0.0	0.0	0.0	0.0	0.0
33	7.4	103519.0	0.0	47672.0	0.0	0.0	0.0	0.0	0.0
34	2.2	30497.8	0.0	14042.4	0.0	0.0	0.0	0.0	0.0
35	9.6	139519.0	0.0	63445.3	0.0	0.0	0.0	0.0	0.0
36	9.7	145225.7	0.0	65038.1	0.0	0.0	0.0	0.0	0.0
37	9.8	150640.2	0.0	66492.3	0.0	0.0	0.0	0.0	0.0
38	9.8	155746.4	0.0	67806.5	0.0	0.0	0.0	0.0	0.0
39	9.8	160531.0	0.0	68980.3	0.0	0.0	0.0	0.0	0.0
40	9.9	164982.6	0.0	70013.5	0.0	0.0	0.0	0.0	0.0
41	9.9	169087.9	0.0	70904.8	0.0	0.0	0.0	0.0	0.0
42	9.3	162017.6	0.0	67186.8	0.0	0.0	0.0	0.0	0.0
43	0.6	10816.7	0.0	4467.7	0.0	0.0	0.0	0.0	0.0
44	10.0	175245.3	0.0	72261.6	0.0	0.0	0.0	0.0	0.0
45	9.4	166580.3	0.0	68632.8	0.0	0.0	0.0	0.0	0.0
46	0.6	9934.1	0.0	4093.4	0.0	0.0	0.0	0.0	0.0
47	10.0	178360.9	0.0	73047.3	0.0	0.0	0.0	0.0	0.0
48	10.0	180599.1	0.0	73226.0	0.0	0.0	0.0	0.0	0.0
49	10.0	182445.5	0.0	73261.1	0.0	0.0	0.0	0.0	0.0
50	10.0	183897.2	0.0	73153.2	0.0	0.0	0.0	0.0	0.0
51	10.0	184951.3	0.0	72902.2	0.0	0.0	0.0	0.0	0.0
52	10.0	185604.9	0.0	72507.8	0.0	0.0	0.0	0.0	0.0
53	10.0	185859.8	0.0	71971.2	0.0	0.0	0.0	0.0	0.0
54	9.5	178509.4	0.0	68541.0	0.0	0.0	0.0	0.0	0.0
55	0.4	7203.2	0.0	2750.4	0.0	0.0	0.0	0.0	0.0
56	9.9	184247.6	0.0	70469.9	0.0	0.0	0.0	0.0	0.0
57	9.7	178975.2	0.0	68500.2	0.0	0.0	0.0	0.0	0.0
58	0.1	2633.0	0.0	1006.1	0.0	0.0	0.0	0.0	0.0
59	9.8	179468.0	0.0	68401.6	0.0	0.0	0.0	0.0	0.0
60	9.8	177771.5	0.0	67156.5	0.0	0.0	0.0	0.0	0.0
61	9.7	175697.4	0.0	65771.1	0.0	0.0	0.0	0.0	0.0
62	9.7	173253.7	0.0	64246.5	0.0	0.0	0.0	0.0	0.0
63	9.6	170449.5	0.0	62583.6	0.0	0.0	0.0	0.0	0.0
64	9.5	167294.1	0.0	60783.1	0.0	0.0	0.0	0.0	0.0
65	1.7	29919.7	0.0	10834.2	0.0	0.0	0.0	0.0	0.0
66	7.8	133427.2	0.0	48011.4	0.0	0.0	0.0	0.0	0.0
67	9.4	158218.9	0.0	56772.9	0.0	0.0	0.0	0.0	0.0
68	9.3	152785.8	0.0	54565.3	0.0	0.0	0.0	0.0	0.0
69	9.2	147088.5	0.0	52224.7	0.0	0.0	0.0	0.0	0.0



				result.out					
70	9.1	141141.1	0.0	49751.7	0.0	0.0	0.0	0.0	0.0
71	9.0	134963.6	0.0	47148.0	0.0	0.0	0.0	0.0	0.0
72	8.9	128573.7	0.0	44414.9	0.0	0.0	0.0	0.0	0.0
73	8.8	121990.0	0.0	41553.6	0.0	0.0	0.0	0.0	0.0
74	8.7	115234.4	0.0	38566.0	0.0	0.0	0.0	0.0	0.0
75	8.6	108325.7	0.0	35453.4	0.0	0.0	0.0	0.0	0.0
76	8.5	101070.1	0.0	32150.5	0.0	0.0	0.0	0.0	0.0
77	0.0	215.2	0.0	66.8	0.0	0.0	0.0	0.0	0.0
78	8.4	94366.4	0.0	28859.9	0.0	0.0	0.0	0.0	0.0
79	6.6	70149.5	0.0	20488.9	0.0	0.0	0.0	0.0	0.0
80	1.7	17435.7	0.0	4893.5	0.0	0.0	0.0	0.0	0.0
81	5.3	53614.8	0.0	14711.4	0.0	0.0	0.0	0.0	0.0
82	2.8	27153.1	0.0	7075.8	0.0	0.0	0.0	0.0	0.0
83	8.0	74252.9	0.0	18075.7	0.0	0.0	0.0	0.0	0.0
84	2.5	21788.9	0.0	4878.3	0.0	0.0	0.0	0.0	0.0
85	5.4	45855.7	0.0	9371.9	0.0	0.0	0.0	0.0	0.0
86	0.9	7168.1	0.0	1370.9	0.0	0.0	0.0	0.0	0.0
87	1.2	9484.4	0.0	1755.0	0.0	0.0	0.0	0.0	0.0
88	4.8	38008.4	0.0	6289.5	0.0	0.0	0.0	0.0	0.0
89	0.8	6152.4	0.0	897.0	0.0	0.0	0.0	0.0	0.0
90	7.5	54568.0	0.0	6264.7	0.0	0.0	0.0	0.0	0.0
91	7.4	48459.1	0.0	2109.1	0.0	0.0	0.0	0.0	0.0
92	0.0	47.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
93	7.2	43227.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
94	7.1	39001.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
95	6.9	34777.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
96	6.7	30617.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
97	6.6	26534.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
98	6.4	22540.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
99	6.2	18649.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100	6.0	14875.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
101	5.8	11228.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
102	5.7	7724.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
103	5.5	4373.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
104	4.7	1207.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Failure surface Specified By 81 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	415.79	137.89
2	422.92	130.88
3	430.20	124.03
4	437.64	117.35
5	445.23	110.84
6	452.97	104.50
7	460.85	98.35
8	468.87	92.38
9	477.03	86.59
10	485.31	80.99
11	493.73	75.58
12	502.26	70.37
13	510.91	65.35
14	519.67	60.54
15	528.55	55.92
16	537.52	51.51
17	546.59	47.31
18	555.76	43.31
19	565.02	39.53
20	574.36	35.96
21	583.78	32.61

		result.out
22	593.27	29.47
23	602.84	26.55
24	612.47	23.85
25	622.16	21.37
26	631.90	19.11
27	641.69	17.08
28	651.52	15.27
29	661.40	13.69
30	671.31	12.34
31	681.24	11.21
32	691.20	10.31
33	701.18	9.64
34	711.17	9.20
35	721.17	8.99
36	731.17	9.00
37	741.16	9.25
38	751.15	9.72
39	761.13	10.43
40	771.09	11.36
41	781.02	12.52
42	790.92	13.91
43	800.79	15.52
44	810.62	17.36
45	820.40	19.42
46	830.14	21.71
47	839.82	24.22
48	849.44	26.95
49	858.99	29.90
50	868.48	33.07
51	877.89	36.46
52	887.22	40.06
53	896.46	43.87
54	905.62	47.90
55	914.68	52.13
56	923.64	56.57
57	932.49	61.21
58	941.24	66.06
59	949.87	71.10
60	958.39	76.34
61	966.79	81.78
62	975.05	87.40
63	983.19	93.22
64	991.19	99.22
65	999.05	105.40
66	1006.77	111.75
67	1014.34	118.29
68	1021.76	124.99
69	1029.02	131.87
70	1036.12	138.91
71	1043.06	146.11
72	1049.84	153.46
73	1056.44	160.97
74	1062.87	168.63
75	1069.12	176.44
76	1075.19	184.38
77	1081.08	192.47
78	1086.78	200.68
79	1092.29	209.03
80	1097.61	217.50
81	1099.08	219.96

Circle Center At X = 725.5 ; Y = 445.3 and Radius, 436.3

result.out

\*\*\* Factor of Safety = 1.942 \*\*\*

1

Failure surface Specified By 81 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	415.79	137.89
2	422.92	130.89
3	430.21	124.04
4	437.66	117.37
5	445.26	110.87
6	453.00	104.54
7	460.89	98.39
8	468.92	92.43
9	477.08	86.65
10	485.37	81.06
11	493.79	75.66
12	502.33	70.46
13	510.99	65.45
14	519.75	60.65
15	528.63	56.04
16	537.61	51.65
17	546.69	47.45
18	555.86	43.47
19	565.13	39.70
20	574.47	36.14
21	583.90	32.80
22	593.40	29.68
23	602.96	26.77
24	612.60	24.08
25	622.29	21.62
26	632.03	19.38
27	641.83	17.36
28	651.67	15.57
29	661.54	14.00
30	671.45	12.67
31	681.39	11.55
32	691.35	10.67
33	701.33	10.02
34	711.32	9.59
35	721.32	9.40
36	731.32	9.43
37	741.32	9.69
38	751.30	10.19
39	761.28	10.91
40	771.23	11.86
41	781.16	13.04
42	791.06	14.44
43	800.93	16.08
44	810.76	17.93
45	820.54	20.02
46	830.27	22.32
47	839.94	24.85
48	849.56	27.61
49	859.10	30.58
50	868.58	33.77

		result.out
51	877.98	37.17
52	887.31	40.79
53	896.54	44.63
54	905.69	48.67
55	914.74	52.92
56	923.69	57.38
57	932.53	62.05
58	941.27	66.91
59	949.89	71.98
60	958.40	77.24
61	966.78	82.69
62	975.03	88.34
63	983.16	94.17
64	991.14	100.19
65	998.99	106.39
66	1006.69	112.77
67	1014.24	119.32
68	1021.64	126.05
69	1028.89	132.94
70	1035.97	140.00
71	1042.89	147.21
72	1049.65	154.59
73	1056.23	162.12
74	1062.64	169.79
75	1068.87	177.62
76	1074.92	185.58
77	1080.78	193.68
78	1086.46	201.91
79	1091.95	210.27
80	1097.24	218.75
81	1097.93	219.91

Circle Center At X = 724.8 ; Y = 445.3 and Radius, 435.9

\*\*\* Factor of Safety = 1.944 \*\*\*

Failure surface Specified By 82 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	321.05	135.53
2	328.33	128.67
3	335.76	121.98
4	343.34	115.45
5	351.05	109.08
6	358.90	102.89
7	366.88	96.87
8	375.00	91.02
9	383.24	85.35
10	391.60	79.87
11	400.07	74.56
12	408.66	69.44
13	417.36	64.51
14	426.17	59.77
15	435.08	55.23
16	444.08	50.88
17	453.18	46.72

		result.out
18	462.36	42.77
19	471.63	39.01
20	480.98	35.46
21	490.40	32.12
22	499.90	28.98
23	509.46	26.04
24	519.08	23.32
25	528.76	20.81
26	538.49	18.51
27	548.27	16.42
28	558.09	14.54
29	567.95	12.88
30	577.85	11.43
31	587.77	10.20
32	597.72	9.19
33	607.69	8.39
34	617.67	7.81
35	627.66	7.45
36	637.66	7.31
37	647.66	7.38
38	657.66	7.67
39	667.65	8.18
40	677.62	8.91
41	687.57	9.85
42	697.51	11.01
43	707.41	12.39
44	717.28	13.98
45	727.12	15.79
46	736.91	17.81
47	746.66	20.04
48	756.36	22.49
49	766.00	25.14
50	775.58	28.01
51	785.10	31.08
52	794.54	34.36
53	803.92	37.85
54	813.21	41.53
55	822.42	45.42
56	831.55	49.51
57	840.58	53.80
58	849.52	58.28
59	858.36	62.96
60	867.09	67.83
61	875.72	72.89
62	884.24	78.13
63	892.63	83.56
64	900.91	89.17
65	909.07	94.96
66	917.09	100.92
67	924.99	107.06
68	932.74	113.37
69	940.36	119.85
70	947.84	126.49
71	955.17	133.29
72	962.35	140.25
73	969.37	147.37
74	976.24	154.64
75	982.95	162.05
76	989.50	169.61
77	995.88	177.31
78	1002.09	185.15
79	1008.13	193.12
80	1013.99	201.22

		result.out
81	1019.68	209.45
82	1024.57	216.86

Circle Center At X = 639.3 ; Y = 466.3 and Radius, 459.0

\*\*\* Factor of Safety = 1.946 \*\*\*

1

Failure surface Specified By 80 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	342.11	136.05
2	349.28	129.09
3	356.62	122.30
4	364.11	115.67
5	371.75	109.22
6	379.54	102.95
7	387.47	96.86
8	395.54	90.95
9	403.75	85.23
10	412.08	79.70
11	420.54	74.37
12	429.11	69.23
13	437.81	64.29
14	446.61	59.55
15	455.53	55.01
16	464.54	50.69
17	473.65	46.57
18	482.86	42.66
19	492.15	38.96
20	501.52	35.48
21	510.98	32.21
22	520.50	29.17
23	530.09	26.34
24	539.75	23.74
25	549.46	21.36
26	559.23	19.20
27	569.04	17.27
28	578.89	15.57
29	588.78	14.09
30	598.70	12.84
31	608.65	11.82
32	618.62	11.03
33	628.60	10.47
34	638.60	10.13
35	648.60	10.03
36	658.60	10.16
37	668.59	10.52
38	678.57	11.11
39	688.54	11.93
40	698.48	12.98
41	708.40	14.25
42	718.29	15.76
43	728.14	17.49
44	737.94	19.45
45	747.70	21.63

		result.out
46	757.41	24.04
47	767.06	26.67
48	776.64	29.53
49	786.16	32.60
50	795.60	35.89
51	804.96	39.40
52	814.25	43.12
53	823.44	47.05
54	832.54	51.20
55	841.54	55.55
56	850.44	60.11
57	859.23	64.88
58	867.92	69.84
59	876.48	75.00
60	884.92	80.36
61	893.24	85.92
62	901.43	91.66
63	909.48	97.59
64	917.39	103.70
65	925.16	109.99
66	932.79	116.46
67	940.26	123.11
68	947.58	129.92
69	954.74	136.91
70	961.73	144.05
71	968.56	151.36
72	975.22	158.82
73	981.71	166.43
74	988.02	174.18
75	994.15	182.09
76	1000.09	190.13
77	1005.85	198.30
78	1011.42	206.61
79	1016.80	215.04
80	1017.73	216.57

Circle Center At X = 648.0 ; Y = 444.3 and Radius, 434.2

\*\*\* Factor of Safety = 1.947 \*\*\*

Failure surface specified By 80 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	394.74	137.37
2	402.03	130.52
3	409.47	123.84
4	417.05	117.33
5	424.79	110.98
6	432.66	104.82
7	440.67	98.83
8	448.80	93.02
9	457.07	87.39
10	465.46	81.95
11	473.98	76.70
12	482.60	71.65
13	491.34	66.78

		result.out
14	500.18	62.12
15	509.13	57.65
16	518.17	53.38
17	527.31	49.32
18	536.54	45.46
19	545.85	41.81
20	555.24	38.37
21	564.70	35.14
22	574.24	32.12
23	583.83	29.32
24	593.49	26.73
25	603.21	24.36
26	612.97	22.21
27	622.79	20.28
28	632.64	18.56
29	642.53	17.07
30	652.44	15.80
31	662.39	14.75
32	672.36	13.93
33	682.34	13.32
34	692.33	12.94
35	702.33	12.79
36	712.33	12.86
37	722.32	13.15
38	732.31	13.67
39	742.28	14.40
40	752.24	15.37
41	762.17	16.55
42	772.07	17.96
43	781.93	19.59
44	791.76	21.43
45	801.55	23.50
46	811.28	25.79
47	820.96	28.29
48	830.59	31.01
49	840.14	33.95
50	849.64	37.09
51	859.06	40.45
52	868.40	44.02
53	877.66	47.80
54	886.83	51.78
55	895.91	55.97
56	904.89	60.36
57	913.78	64.95
58	922.56	69.74
59	931.23	74.72
60	939.78	79.90
61	948.22	85.26
62	956.54	90.82
63	964.73	96.55
64	972.79	102.47
65	980.71	108.57
66	988.50	114.85
67	996.14	121.30
68	1003.64	127.91
69	1010.99	134.69
70	1018.18	141.64
71	1025.22	148.75
72	1032.10	156.01
73	1038.81	163.42
74	1045.35	170.98
75	1051.73	178.69
76	1057.93	186.53



		result.out
77	1063.95	194.52
78	1069.79	202.63
79	1075.45	210.88
80	1080.90	219.20

Circle Center At X = 704.3 ; Y = 459.6 and Radius, 446.8

\*\*\* Factor of Safety = 1.947 \*\*\*

1

Failure surface Specified By 80 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	363.16	136.58
2	370.50	129.78
3	377.98	123.15
4	385.61	116.69
5	393.39	110.40
6	401.30	104.28
7	409.34	98.35
8	417.52	92.59
9	425.82	87.01
10	434.24	81.62
11	442.79	76.42
12	451.44	71.41
13	460.20	66.60
14	469.07	61.98
15	478.04	57.56
16	487.11	53.34
17	496.27	49.32
18	505.51	45.50
19	514.84	41.90
20	524.24	38.50
21	533.72	35.31
22	543.27	32.33
23	552.88	29.57
24	562.55	27.02
25	572.27	24.69
26	582.04	22.57
27	591.86	20.67
28	601.72	18.99
29	611.61	17.53
30	621.53	16.29
31	631.48	15.27
32	641.45	14.47
33	651.43	13.89
34	661.43	13.54
35	671.43	13.41
36	681.43	13.50
37	691.42	13.81
38	701.41	14.35
39	711.38	15.10
40	721.33	16.08
41	731.26	17.28
42	741.16	18.70
43	751.02	20.34

		result.out
44	760.85	22.20
45	770.63	24.28
46	780.36	26.57
47	790.04	29.08
48	799.66	31.81
49	809.22	34.74
50	818.71	37.89
51	828.13	41.25
52	837.47	44.82
53	846.73	48.60
54	855.91	52.58
55	864.99	56.76
56	873.98	61.15
57	882.87	65.73
58	891.65	70.51
59	900.33	75.48
60	908.89	80.65
61	917.33	86.00
62	925.66	91.54
63	933.86	97.27
64	941.93	103.17
65	949.86	109.26
66	957.66	115.52
67	965.32	121.95
68	972.83	128.55
69	980.20	135.31
70	987.41	142.24
71	994.47	149.32
72	1001.37	156.56
73	1008.10	163.96
74	1014.67	171.50
75	1021.07	179.18
76	1027.29	187.01
77	1033.35	194.97
78	1039.22	203.06
79	1044.91	211.28
80	1049.27	217.89

Circle Center At X = 672.3 ; Y = 463.0 and Radius, 449.6

\*\*\* Factor of Safety = 1.949 \*\*\*

Failure surface Specified By 83 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	331.58	135.79
2	339.01	129.09
3	346.57	122.56
4	354.28	116.18
5	362.12	109.97
6	370.08	103.92
7	378.17	98.05
8	386.39	92.34
9	394.72	86.81
10	403.17	81.46
11	411.72	76.29

		result.out
12	420.39	71.30
13	429.16	66.49
14	438.03	61.87
15	446.99	57.44
16	456.04	53.19
17	465.19	49.14
18	474.41	45.28
19	483.72	41.62
20	493.10	38.16
21	502.55	34.89
22	512.07	31.82
23	521.65	28.96
24	531.29	26.30
25	540.98	23.84
26	550.72	21.59
27	560.51	19.54
28	570.34	17.70
29	580.21	16.07
30	590.11	14.64
31	600.03	13.43
32	609.98	12.43
33	619.95	11.63
34	629.93	11.05
35	639.93	10.67
36	649.92	10.51
37	659.92	10.56
38	669.92	10.82
39	679.91	11.29
40	689.89	11.97
41	699.85	12.86
42	709.79	13.96
43	719.70	15.27
44	729.58	16.79
45	739.43	18.52
46	749.24	20.45
47	759.01	22.59
48	768.73	24.94
49	778.40	27.49
50	788.02	30.25
51	797.57	33.20
52	807.06	36.36
53	816.48	39.72
54	825.82	43.27
55	835.09	47.02
56	844.28	50.97
57	853.38	55.11
58	862.40	59.44
59	871.32	63.96
60	880.14	68.67
61	888.86	73.56
62	897.48	78.63
63	905.99	83.89
64	914.38	89.32
65	922.66	94.93
66	930.82	100.71
67	938.85	106.67
68	946.76	112.79
69	954.54	119.08
70	962.18	125.53
71	969.68	132.14
72	977.05	138.90
73	984.27	145.82
74	991.34	152.89

		result.out
75	998.26	160.11
76	1005.02	167.48
77	1011.63	174.98
78	1018.08	182.62
79	1024.37	190.40
80	1030.49	198.31
81	1036.44	206.34
82	1042.23	214.50
83	1044.38	217.68

Circle Center At X = 652.6 ; Y = 484.5 and Radius, 474.0

\*\*\* Factor of Safety = 1.952 \*\*\*

1

Failure Surface Specified By 79 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	405.26	137.63
2	412.48	130.71
3	419.86	123.96
4	427.38	117.38
5	435.07	110.97
6	442.89	104.75
7	450.86	98.70
8	458.97	92.85
9	467.21	87.18
10	475.58	81.71
11	484.07	76.43
12	492.68	71.35
13	501.41	66.48
14	510.25	61.80
15	519.20	57.33
16	528.25	53.07
17	537.39	49.02
18	546.63	45.19
19	555.95	41.57
20	565.35	38.16
21	574.83	34.98
22	584.38	32.01
23	594.00	29.27
24	603.67	26.75
25	613.41	24.46
26	623.19	22.39
27	633.02	20.55
28	642.89	18.94
29	652.79	17.55
30	662.73	16.40
31	672.68	15.48
32	682.66	14.79
33	692.65	14.33
34	702.65	14.10
35	712.65	14.10
36	722.64	14.34
37	732.63	14.80
38	742.61	15.50

		result.out
39	752.56	16.43
40	762.50	17.59
41	772.40	18.98
42	782.27	20.60
43	792.10	22.45
44	801.88	24.52
45	811.61	26.82
46	821.29	29.35
47	830.90	32.10
48	840.45	35.07
49	849.93	38.26
50	859.33	41.67
51	868.65	45.30
52	877.88	49.14
53	887.02	53.19
54	896.06	57.46
55	905.01	61.94
56	913.84	66.62
57	922.57	71.50
58	931.18	76.59
59	939.67	81.87
60	948.03	87.35
61	956.27	93.02
62	964.37	98.88
63	972.34	104.93
64	980.16	111.16
65	987.84	117.57
66	995.36	124.15
67	1002.73	130.91
68	1009.94	137.84
69	1016.99	144.93
70	1023.88	152.19
71	1030.59	159.60
72	1037.13	167.16
73	1043.49	174.88
74	1049.67	182.74
75	1055.67	190.74
76	1061.48	198.88
77	1067.10	207.15
78	1072.53	215.55
79	1074.61	218.94

Circle Center At X = 707.5 ; Y = 445.5 and Radius, 431.4

\*\*\* Factor of Safety = 1.952 \*\*\*

Failure surface specified By 76 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	394.74	137.37
2	401.81	130.30
3	409.06	123.41
4	416.47	116.70
5	424.05	110.18
6	431.79	103.85
7	439.69	97.71

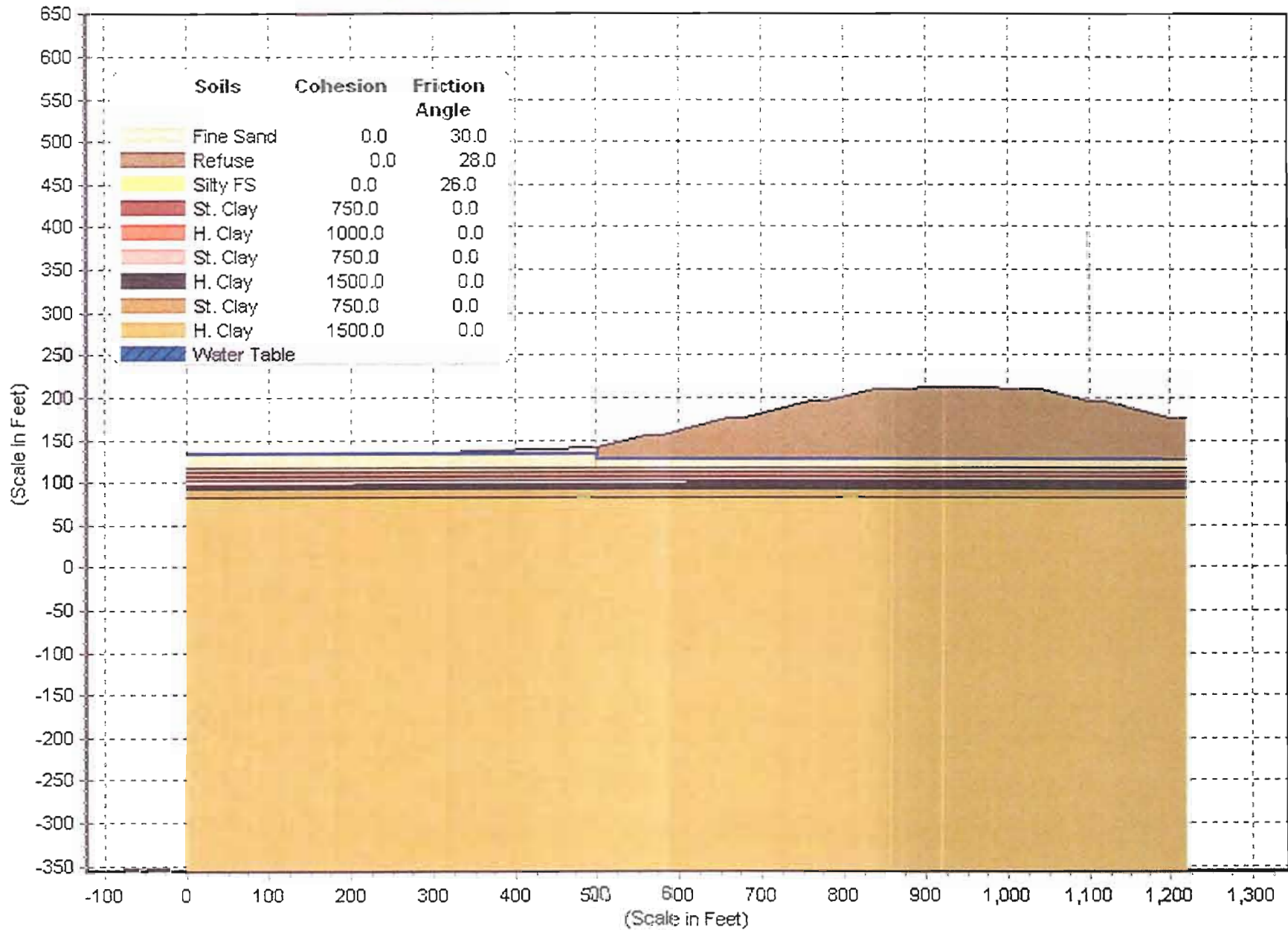
		result.out
8	447.74	91.77
9	455.93	86.04
10	464.26	80.50
11	472.72	75.18
12	481.32	70.07
13	490.04	65.18
14	498.88	60.50
15	507.83	56.04
16	516.89	51.81
17	526.05	47.81
18	535.31	44.03
19	544.67	40.49
20	554.10	37.18
21	563.62	34.10
22	573.21	31.27
23	582.86	28.67
24	592.58	26.31
25	602.36	24.20
26	612.18	22.33
27	622.05	20.70
28	631.95	19.32
29	641.89	18.19
30	651.85	17.30
31	661.83	16.66
32	671.82	16.27
33	681.82	16.13
34	691.82	16.24
35	701.81	16.60
36	711.79	17.20
37	721.76	18.05
38	731.69	19.15
39	741.60	20.50
40	751.48	22.09
41	761.31	23.93
42	771.09	26.01
43	780.81	28.34
44	790.48	30.90
45	800.08	33.71
46	809.60	36.75
47	819.05	40.03
48	828.41	43.54
49	837.68	47.29
50	846.86	51.26
51	855.94	55.46
52	864.90	59.89
53	873.76	64.54
54	882.49	69.40
55	891.11	74.48
56	899.59	79.78
57	907.94	85.28
58	916.15	90.99
59	924.22	96.90
60	932.13	103.01
61	939.89	109.32
62	947.50	115.81
63	954.93	122.50
64	962.20	129.36
65	969.30	136.41
66	976.22	143.63
67	982.96	151.02
68	989.51	158.57
69	995.87	166.29
70	1002.04	174.16



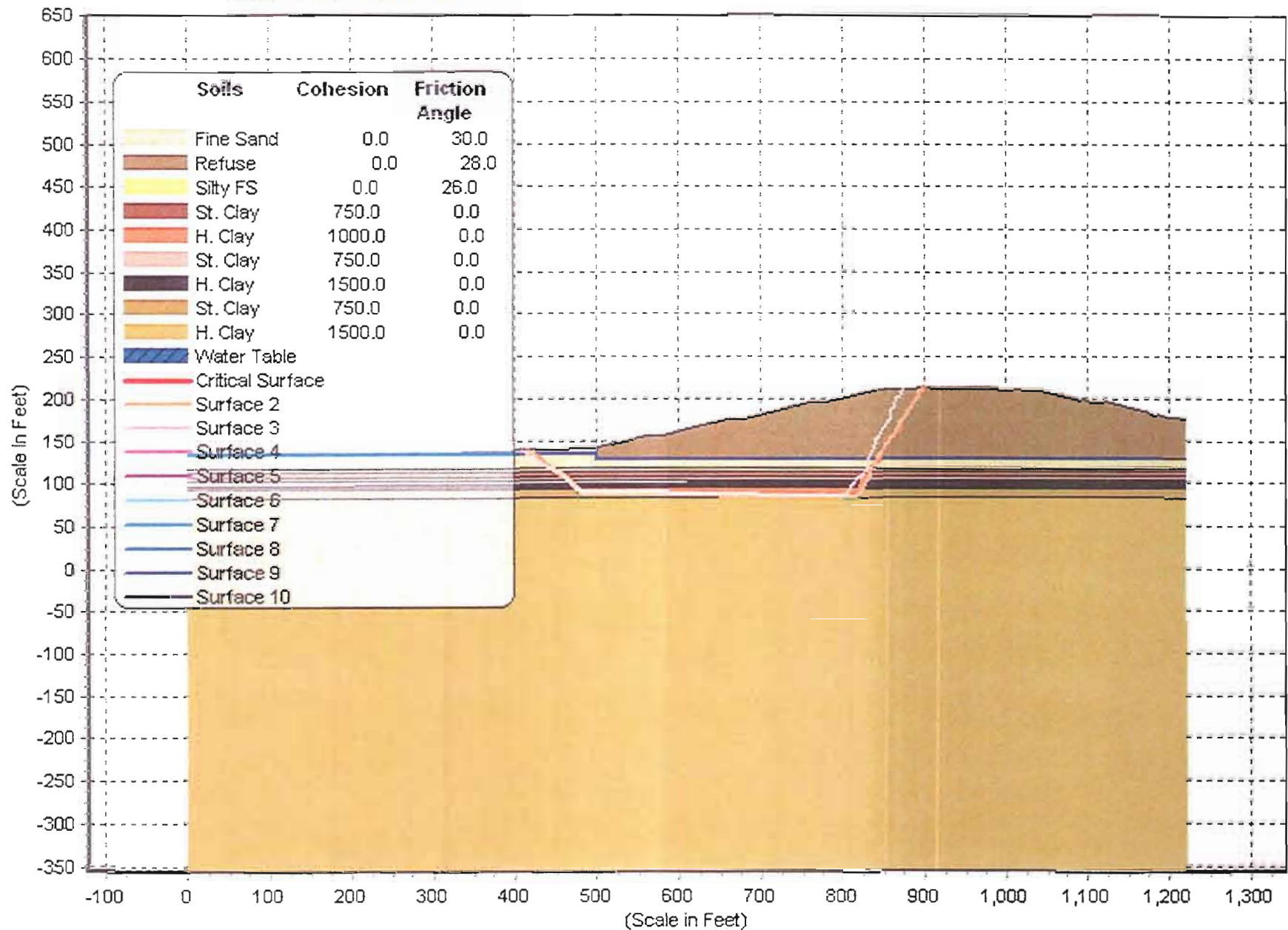
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F 1741.25 + * result.out
      -
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      - *
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T 1990.00 + *** *
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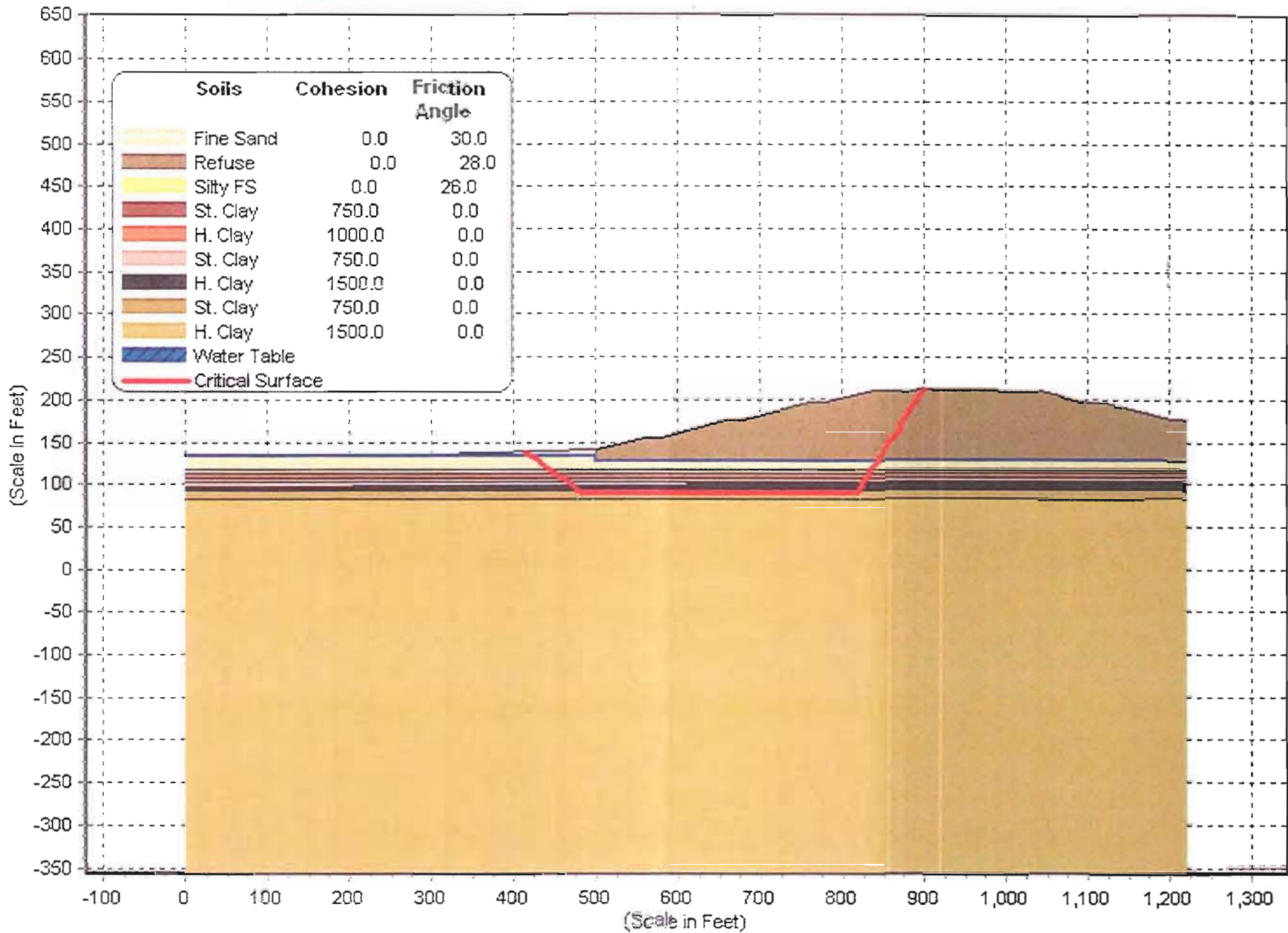
# LENA ROAD LANDFILL - X-SEC D - D'



LENA ROAD LANDFILL - X-SEC D - D' - FS Min- Janbu = 1.684



LENA ROAD LANDFILL - X-SEC D - D' - FS Min- Janbu = 1.684



result.out  
 \*\* STABL for WINDOWS \*\*  
 by  
 Geotechnical Software Solutions

1

--Slope Stability Analysis--  
 Simplified Janbu, Simplified Bishop  
 or Spencer's Method of Slices

Run Date: 9/27/10  
 Time of Run: 16:00  
 Run By: Shawkat Ali  
 Input Data Filename: run.in  
 Output Filename: result.out  
 Unit: U.S.C.  
 Plotted Output Filename: result.plt

PROBLEM DESCRIPTION LENA ROAD LANDFILL - X-SEC D - D'

BOUNDARY COORDINATES

15 Top Boundaries  
 24 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	135.00	300.00	135.00	2
2	300.00	135.00	500.00	140.00	2
3	500.00	140.00	560.00	155.00	1
4	560.00	155.00	580.00	155.00	1
5	580.00	155.00	660.00	175.00	1
6	660.00	175.00	680.00	175.00	1
7	680.00	175.00	760.00	195.00	1
8	760.00	195.00	780.00	195.00	1
9	780.00	195.00	840.00	210.00	1
10	840.00	210.00	940.00	212.00	1
11	940.00	212.00	1040.00	210.00	1
12	1040.00	210.00	1100.00	195.00	1
13	1100.00	195.00	1120.00	195.00	1
14	1120.00	195.00	1200.00	175.00	1
15	1200.00	175.00	1220.00	175.00	1
16	500.10	127.00	500.20	140.00	1
17	500.10	127.00	1220.00	127.00	2
18	0.00	117.00	1220.00	117.00	3
19	0.00	112.00	1220.00	112.00	4
20	0.00	107.00	1220.00	107.00	5
21	0.00	102.00	1220.00	102.00	6
22	0.00	97.00	1220.00	102.00	7
23	0.00	92.00	1220.00	92.00	8
24	0.00	82.00	1220.00	82.00	9

1

ISOTROPIC SOIL PARAMETERS

9 Type(s) of Soil

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	70.0	80.0	0.0	28.0	0.00	0.0	1
2	100.0	110.0	0.0	30.0	0.00	0.0	1
3	95.0	105.0	0.0	26.0	0.00	0.0	1
4	105.0	120.0	750.0	0.0	0.00	0.0	1
5	110.0	125.0	1000.0	0.0	0.00	0.0	1
6	105.0	120.0	750.0	0.0	0.00	0.0	1
7	115.0	130.0	1500.0	0.0	0.00	0.0	1
8	105.0	120.0	750.0	0.0	0.00	0.0	1
9	115.0	130.0	1500.0	0.0	0.00	0.0	1

1

1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED

Unit Weight of Water = 62.40

Piezometric Surface No. 1 Specified by 4 Coordinate Points

Point No.	X-Water (ft)	Y-Water (ft)
1	0.00	133.00
2	500.00	133.00
3	500.10	127.00
4	1190.00	127.00

1

A Critical Failure Surface Searching Method, Using A Random Technique For Generating Sliding Block Surfaces, Has Been Specified.

200 Trial Surfaces Have Been Generated.

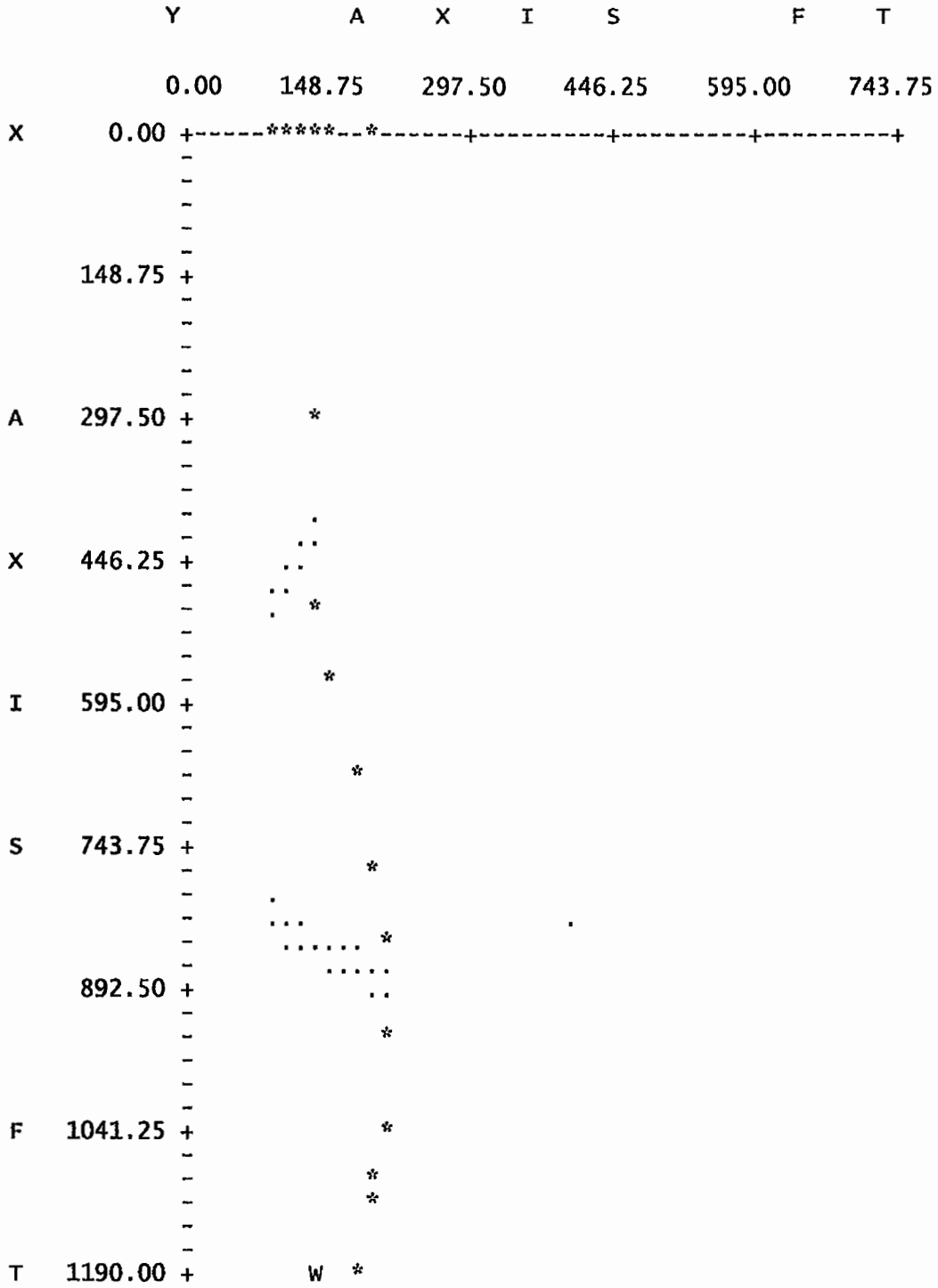
2 Boxes Specified For Generation Of Central Block Base

Length Of Line Segments For Active And Passive Portions Of Sliding Block Is 5.0

Box No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Height (ft)
1	475.00	86.00	495.00	86.00	10.00
2	800.00	86.00	820.00	86.00	10.00

\*\*\*\* ERROR - BK10 \*\*\*\*

1



\*\*\*\*\*  
 \*\*\*\*\* EXECUTION OF STABL ABORTED \*\*\*\*\*  
 \*\*\*\*\*

result.out

1

Following Are Displayed The Ten Most Critical Of The Trial Failure Surfaces Examined. They Are Ordered - Most Critical First.

\* \* Safety Factors Are Calculated By The Modified Janbu Method \* \*

Failure Surface Specified By 50 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	412.71	137.82
2	415.70	134.84
3	419.99	132.27
4	424.88	131.23
5	429.13	128.60
6	432.70	125.09
7	436.53	121.89
8	440.42	118.74
9	445.01	116.77
10	448.59	113.27
11	452.51	110.17
12	456.13	106.72
13	461.01	105.63
14	464.63	102.18
15	469.25	100.26
16	472.95	96.91
17	476.63	93.52
18	480.94	90.98
19	485.89	90.29
20	817.56	90.67
21	819.97	95.04
22	823.06	98.98
23	824.90	103.63
24	828.23	107.36
25	831.39	111.23
26	833.45	115.79
27	836.03	120.07
28	839.49	123.68
29	843.02	127.22
30	844.99	131.82
31	847.79	135.96
32	850.96	139.83
33	852.83	144.46
34	856.16	148.20
35	859.68	151.74
36	863.21	155.28
37	866.75	158.82
38	868.68	163.43
39	870.30	168.16
40	872.32	172.73
41	875.56	176.54
42	877.94	180.94
43	879.67	185.63
44	882.07	190.02
45	885.59	193.56

		result.out
46	889.03	197.19
47	891.52	201.53
48	894.31	205.68
49	897.76	209.30
50	899.40	211.19

\*\*\* 1.684 \*\*\*

Individual data on the 73 slices

Slice No.	Width (ft)	Weight (lbs)	Water Force		Force Norm (lbs)	Force Tan (lbs)	Earthquake Force		Surcharge Load (lbs)
			Top (lbs)	Bot (lbs)			Hor (lbs)	Ver (lbs)	
1	3.0	456.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	3.1	1232.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	1.2	654.3	0.0	32.2	0.0	0.0	0.0	0.0	0.0
4	4.9	3146.7	0.0	389.7	0.0	0.0	0.0	0.0	0.0
5	4.3	3642.9	0.0	963.2	0.0	0.0	0.0	0.0	0.0
6	3.6	4296.3	0.0	1920.6	0.0	0.0	0.0	0.0	0.0
7	3.8	6074.3	0.0	2967.0	0.0	0.0	0.0	0.0	0.0
8	3.9	7539.6	0.0	3958.4	0.0	0.0	0.0	0.0	0.0
9	4.0	8988.8	0.0	4159.4	0.0	0.0	0.0	0.0	0.0
10	0.5	1275.5	0.0	598.1	0.0	0.0	0.0	0.0	0.0
11	3.6	9061.0	0.0	5610.7	0.0	0.0	0.0	0.0	0.0
12	1.6	4490.1	0.0	2603.3	0.0	0.0	0.0	0.0	0.0
13	2.3	6889.0	0.0	4035.9	0.0	0.0	0.0	0.0	0.0
14	3.3	10909.8	0.0	7001.8	0.0	0.0	0.0	0.0	0.0
15	0.3	1020.9	0.0	658.9	0.0	0.0	0.0	0.0	0.0
16	4.9	17489.5	0.0	8369.5	0.0	0.0	0.0	0.0	0.0
17	3.6	14047.4	0.0	9077.8	0.0	0.0	0.0	0.0	0.0
18	0.4	1791.5	0.0	910.0	0.0	0.0	0.0	0.0	0.0
19	4.2	17700.4	0.0	9004.5	0.0	0.0	0.0	0.0	0.0
20	1.5	6511.7	0.0	4143.0	0.0	0.0	0.0	0.0	0.0
21	2.2	10351.5	0.0	6594.5	0.0	0.0	0.0	0.0	0.0
22	3.7	18397.2	0.0	11789.5	0.0	0.0	0.0	0.0	0.0
23	2.6	13737.1	0.0	7518.7	0.0	0.0	0.0	0.0	0.0
24	1.7	9487.0	0.0	5195.0	0.0	0.0	0.0	0.0	0.0
25	5.0	27741.6	0.0	13217.5	0.0	0.0	0.0	0.0	0.0
26	14.1	79954.0	0.0	37595.4	0.0	0.0	0.0	0.0	0.0
27	0.1	475.7	0.0	123.9	0.0	0.0	0.0	0.0	0.0
28	0.1	523.7	0.0	229.0	0.0	0.0	0.0	0.0	0.0
29	59.8	344302.5	0.0	*****	0.0	0.0	0.0	0.0	0.0
30	20.0	125540.7	0.0	45694.2	0.0	0.0	0.0	0.0	0.0
31	80.0	557783.4	0.0	*****	0.0	0.0	0.0	0.0	0.0
32	20.0	153351.0	0.0	45553.0	0.0	0.0	0.0	0.0	0.0
33	80.0	669024.8	0.0	*****	0.0	0.0	0.0	0.0	0.0
34	20.0	181161.4	0.0	45411.7	0.0	0.0	0.0	0.0	0.0
35	37.6	352434.8	0.0	85200.4	0.0	0.0	0.0	0.0	0.0
36	0.7	7093.8	0.0	3390.5	0.0	0.0	0.0	0.0	0.0
37	1.7	15758.1	0.0	7262.8	0.0	0.0	0.0	0.0	0.0
38	3.1	27665.4	0.0	9356.5	0.0	0.0	0.0	0.0	0.0
39	0.6	4801.9	0.0	2562.2	0.0	0.0	0.0	0.0	0.0
40	0.6	5470.5	0.0	2815.4	0.0	0.0	0.0	0.0	0.0
41	0.6	5353.4	0.0	2640.1	0.0	0.0	0.0	0.0	0.0
42	3.0	24122.5	0.0	6121.3	0.0	0.0	0.0	0.0	0.0
43	0.3	2477.6	0.0	589.6	0.0	0.0	0.0	0.0	0.0
44	3.2	23962.3	0.0	5524.7	0.0	0.0	0.0	0.0	0.0



				result.out					
45	0.3	2548.7	0.0	811.0	0.0	0.0	0.0	0.0	0.0
46	1.7	12148.6	0.0	3398.3	0.0	0.0	0.0	0.0	0.0
47	0.7	5005.8	0.0	936.5	0.0	0.0	0.0	0.0	0.0
48	1.8	12293.9	0.0	1893.4	0.0	0.0	0.0	0.0	0.0
49	3.5	21905.1	0.0	1598.1	0.0	0.0	0.0	0.0	0.0
50	0.5	3158.4	0.0	138.8	0.0	0.0	0.0	0.0	0.0
51	2.8	16710.0	0.0	346.4	0.0	0.0	0.0	0.0	0.0
52	0.2	1275.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
53	2.0	11107.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54	2.8	14917.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
55	3.2	16041.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
56	1.9	8924.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
57	3.3	14901.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
58	3.5	14891.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
59	3.5	14085.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60	3.5	13219.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
61	1.9	6695.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
62	1.6	5061.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
63	2.0	5705.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
64	3.2	8164.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
65	2.4	5337.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
66	1.7	3331.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
67	2.4	3853.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
68	3.5	4710.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
69	3.4	3748.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70	2.5	2022.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71	2.8	1457.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
72	3.4	875.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0
73	1.6	106.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Failure Surface Specified By 52 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	413.98	137.85
2	415.62	136.80
3	419.70	133.92
4	423.85	131.13
5	427.48	127.68
6	431.02	124.16
7	434.60	120.66
8	439.10	118.48
9	443.63	116.37
10	448.00	113.94
11	451.64	110.51
12	456.58	109.75
13	460.59	106.77
14	464.46	103.60
15	468.04	100.11
16	471.80	96.82
17	475.42	93.37
18	479.38	90.32
19	482.96	86.83
20	816.83	81.98
21	818.52	86.68
22	821.76	90.49
23	825.20	94.12
24	826.99	98.79
25	829.42	103.16
26	832.49	107.11
27	832.97	112.08

		result.out
28	836.43	115.69
29	837.64	120.54
30	839.31	125.26
31	841.19	129.89
32	844.53	133.61
33	848.05	137.16
34	851.31	140.95
35	853.16	145.59
36	856.68	149.15
37	859.95	152.93
38	863.45	156.51
39	866.02	160.79
40	867.40	165.60
41	868.95	170.35
42	872.41	173.96
43	875.74	177.69
44	879.27	181.23
45	880.36	186.11
46	883.83	189.71
47	886.25	194.09
48	889.47	197.91
49	892.54	201.86
50	893.02	206.84
51	896.34	210.58
52	896.73	211.13

\*\*\* 1.731 \*\*\*

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Failure Surface Specified By 50 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	405.44	137.64
2	407.82	137.10
3	411.80	134.07
4	415.84	131.12
5	420.26	128.78
6	424.19	125.69
7	428.28	122.81
8	432.21	119.72
9	436.82	117.79
10	441.76	117.00
11	446.03	114.40
12	450.02	111.39
13	454.81	109.98
14	458.45	106.54
15	462.14	103.18
16	465.68	99.65
17	469.32	96.21
18	472.86	92.68
19	477.02	89.91
20	803.13	83.71
21	806.24	87.62
22	807.69	92.41
23	811.06	96.10
24	814.57	99.67

		result.out
25	817.44	103.76
26	820.98	107.30
27	824.51	110.83
28	827.96	114.45
29	830.81	118.56
30	831.05	123.55
31	831.85	128.49
32	834.45	132.76
33	835.83	137.56
34	837.47	142.29
35	838.98	147.05
36	840.27	151.88
37	843.67	155.55
38	846.36	159.76
39	849.19	163.89
40	852.39	167.72
41	854.74	172.14
42	858.07	175.87
43	858.47	180.86
44	859.71	185.70
45	862.94	189.52
46	863.62	194.47
47	866.00	198.87
48	869.53	202.41
49	871.13	207.15
50	874.44	210.69

\*\*\* 1.767 \*\*\*

Failure surface specified by 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

\*\*\* 0.000 \*\*\*

1

Failure surface specified by 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

\*\*\* 0.000 \*\*\*

Failure surface specified by 0 Coordinate Points

result.out

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

***	0.000	***
-----	-------	-----

1

Failure Surface Specified By 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

***	0.000	***
-----	-------	-----

Failure Surface Specified By 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

***	0.000	***
-----	-------	-----

1

Failure Surface Specified By 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

***	0.000	***
-----	-------	-----

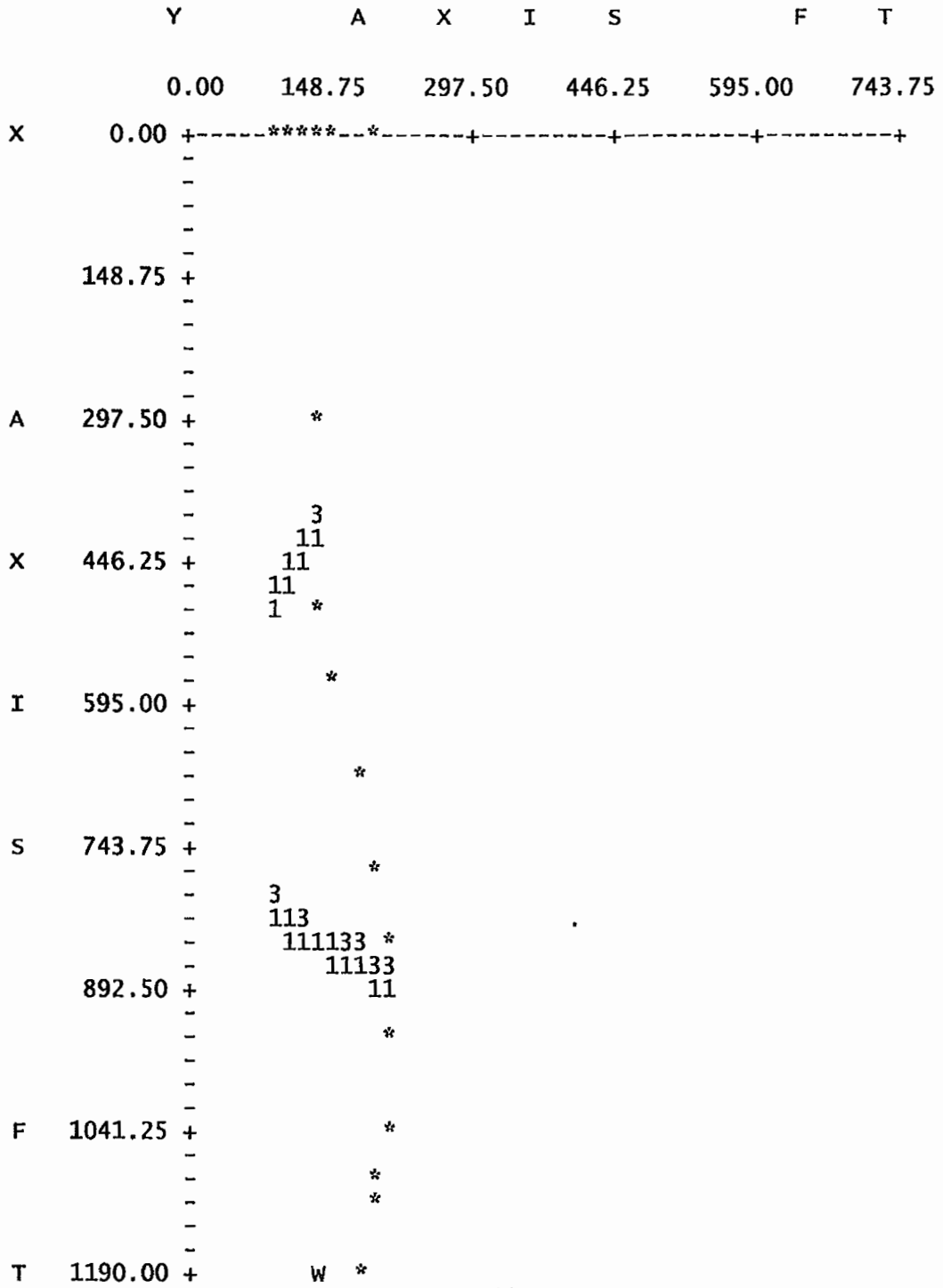
Failure Surface Specified By 0 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
-----------	-------------	-------------

result.out

\*\*\* 0.000 \*\*\*

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**ATTACHMENT C**  
**SETTLEMENT ANALYSIS RESULTS**

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole B-1 Elev 37 ft-NGVD

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 105 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 68 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft<sup>2</sup>  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft<sup>2</sup>  
 Thickness above GWL 5 ft  
 Thickness below GWL 23.5 ft

Medium Dense Silty Sand, Unit wt below GWL 120 pcf Es 720,000 lb/ft<sup>2</sup>  
 Thickness 15 ft

Very Stiff Silty Clay, Unit wt below GWL 115 pcf w 62 % eo 1.67 Cc 0.300 Cr 0.060  
 Very Stiff Clay, OCR 3.5  
 Thickness 5 ft

Stiff Clay, Unit weight below GWL 110 pcf w 46 % eo 1.23 Cc 0.200 Cr 0.040  
 Stiff Clay, OCR 3  
 Thickness 13.5 ft

Hard Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Clay, OCR 4  
 Thickness 18 ft

Excavation to bottom of landfill 0  
 Landfill Load 7480  
 Net Loading (delta sigma) 7480

Settlement of Loose/Med. Dense Sand		Settlement of Med. Dense Silty Sand		Settlement of Silty Clay Layer			Settlement of Stiff Clay layer			Settlement of Hard Clay layer		
Elastic Settlement		Elastic Settlement		Primary			Primary			Primary		
Thickness	Settlement	Thickness	Settlement	Thickness	Eff Stress	Settlement	Thickness	Eff Stress	Settlement	Thickness	Eff Stress	Settlement
(ft)	(ft)	(ft)	(ft)	(ft)	(psf)	(ft)	(ft)	(psf)	(ft)	(ft)	(psf)	(ft)
28.5	0.49	15	0.16	5	2049.1	0.06	13.5	3555.7	0.12	18	4592.5	0.07

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.49 ft  
 Elastic (Immediate) Settlement of Medium Dense Silty Sand 0.16 ft  
 Primary Consolidation Settlement of Very Stiff Silty Clay 0.06 ft  
 Primary Consolidation Settlement of Stiff Clay 0.12 ft  
 Primary Consolidation Settlement of Hard Clay 0.07 ft  
**Total 0.90 ft**

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-2** Elev 34 ft-NGVD

**Assumptions:**

Landfill:	Max. Height of Landfill @ Elevation	130 ft-NGVD
	Unit Weight of Landfill Material	110 pcf
	Separation of Landfill Bottom from GWL	5 ft
	Assumed HGWL Elevation =	32 ft
	Thickness	96 ft

Soils:	Loose/Med. Dense Sand, Unit wt above GWL	110 pcf	Es	432,000 lb/ft2
	Loose/Med. Dense Sand, Unit wt below GWL	115 pcf	Es	432,000 lb/ft2
	Thickness above GWL	5 ft		
	Thickness below GWL	13.5 ft		

	Medium Dense Silty Sand, Unit wt below GWL	115 pcf	Es	720,000 lb/ft2
	Thickness	5 ft		

	Very Soft Sandy Clay, Unit wt below GWL	95 pcf	w	30 %	eo	0.80	Cc	0.500	Cr	0.100	Cv	0.3	Ca	0.02
	Very Soft Sandy Clay, OCR	1.2												
	Thickness	6.5 ft												

	Very Stiff Clay, Unit weight below GWL	115 pcf	w	62 %	eo	1.66	Cc	0.200	Cr	0.040
	Very Stiff Clay, OCR	3.5								
	Thickness	18.5 ft								

	Hard Silty Clay to Clay, Unit weight below GWL	120 pcf	w	80 %	eo	2.14	Cc	0.100	Cr	0.020
	Hard Silty Clay to Clay, OCR	4								
	Thickness	31.5 ft								

Excavation to bottom of landfill	0
Landfill Load	10560
Net Loading (delta sigma)	10560

Settlement of Loose/Med. Dense Sand			Settlement of Med. Dense Silty Sand			Settlement of Very Soft Sandy Clay				Settlement of Very Stiff Clay			Settlement of Hard Clay layer		
Elastic Settlement			Elastic Settlement			Primary				Primary			Primary		
Thickness (ft)	Settlement (ft)		Thickness (ft)	Settlement (ft)		Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	
18.5	0.45		5	0.07		6.5	1472	0.16	18.5	2445.1	0.16	31.5	4522.5	0.12	
						Secondary for 50 years									
						Thickness (ft)	Drainage (ft)	tp (years)	Settlement (ft)						
						6.5	3.25	0.11	0.19						

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand	0.45 ft
Elastic (Immediate) Settlement of Medium Dense Silty Sand	0.07 ft
Primary Consolidation Settlement of Very Stiff Silty Clay	0.16 ft
Primary Consolidation Settlement of Stiff Clay	0.16 ft
Primary Consolidation Settlement of Hard Clay	0.12 ft
Secondary Consolidation Settlement of Soft Clay	0.19 ft
<b>Total</b>	<b>1.15 ft</b>



# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-3** Elev 34 ft-NGVD

## Assumptions:

Landfill: Max. Height of Landfill @ Elevation 95 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 61 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft2  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft2  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Medium Stiff Silty Clay, Unit wt below GWL 105 pcf w 62 % eo 1.67 Cc 0.300 Cr 0.060  
 Very Stiff Silty Clay, OCR 3  
 Thickness 15 ft

Stiff Clay, Unit weight below GWL 110 pcf w 46 % eo 1.23 Cc 0.250 Cr 0.050  
 Stiff Clay, OCR 3.5  
 Thickness 10 ft

Hard Silty Clay to Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Silty Clay to Clay, OCR 4  
 Thickness 36.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 6710  
 Net Loading (delta sigma) 6710

## Settlement of Loose/Med. Dense Sand

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft)  
 18.5 0.29

## Settlement of Medium Stiff Silty Clay

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 15 1899.1 0.17

## Settlement of Stiff Clay

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 10 2375.1 0.12

## Settlement of Hard Clay layer

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 36.5 4477.5 0.13

## Total Settlements

Elastic (Immediate) Settlement of Loose and Med Sand 0.29 ft  
 Primary Consolidation Settlement of Medium Stiff Silty Clay 0.17 ft  
 Primary Consolidation Settlement of Stiff Clay 0.12 ft  
 Primary Consolidation Settlement of Hard Clay 0.13 ft  
**Total 0.72 ft**

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-4** Elev **34 ft-NGVD**

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 115 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 81 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 576,000 lb/ft<sup>2</sup>  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 576,000 lb/ft<sup>2</sup>  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Medium Stiff Silty Clay, Unit wt below GWL 105 pcf w 62 % eo 1.67 Cc 0.300 Cr 0.060  
 Very Stiff Silty Clay, OCR 3  
 Thickness 10 ft

Hard Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Clay, OCR 4  
 Thickness 20 ft

Very Stiff Clay, Unit weight below GWL 115 pcf w 46 % eo 1.23 Cc 0.200 Cr 0.040  
 Very Stiff Clay, OCR 3  
 Thickness 5 ft

Hard Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Clay, OCR 4  
 Thickness 46.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 8910  
 Net Loading (delta sigma) 8910

Settlement of Loose/Med. Dense Sand			Settlement of Med Stiff Clay Layer			Settlement of Hard Clay Layer			Settlement of Very Stiff Clay layer			Settlement of Hard Clay layer		
Elastic Settlement			Primary			Primary			Primary			Primary		
Thickness (ft)	Settlement (ft)		Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)
18.5	0.29		10	1686.1	0.12	20	2838.1	0.08	13.5	2802.9	0.12	18	5481.3	0.07

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.29 ft  
 Primary Consolidation Settlement of Medium Stiff Silty Clay 0.12 ft  
 Primary Consolidation Settlement of Hard Clay 0.08 ft  
 Primary Consolidation Settlement of Very Stiff Clay 0.12 ft  
 Primary Consolidation Settlement of Hard Clay 0.07 ft  
**Total 0.67 ft**

**Lena Road Stage II Landfill - Manatee County, FL**

Bore Hole **B-5** Elev 34 ft-NGVD

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 105 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 71 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 576,000 lb/ft2  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 576,000 lb/ft2  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Very Soft Silty Clay, Unit wt below GWL 95 pcf w 26 % eo 0.70 Cc 0.500 Cr 0.100 Cv 0.3 Ca 0.02  
 Very Soft Silty Clay, OCR 1.2  
 Thickness 5 ft

Very Stiff Clay, Unit weight below GWL 115 pcf w 62 % eo 1.66 Cc 0.200 Cr 0.040  
 Very Stiff Clay, OCR 3.5  
 Thickness 5 ft

Hard Silty Clay to Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Silty Clay to Clay, OCR 4  
 Thickness 51.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 7810  
 Net Loading (delta sigma) 7810

**Settlement of Loose/Med. Dense Sand**

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft)  
 18.5 0.25

**Settlement of Very Soft Silty Clay**

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 5 1423.1 0.10

**Settlement of Very Stiff Clay**

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 5 1686.1 0.04  
 Secondary for 50 years  
 Thickness Drainage tp Settlement  
 (ft) (years) (ft)  
 5 2.5 0.06 0.17

**Settlement of Hard Clay layer**

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft)  
 51.5 4652.5 0.19

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.25 ft  
 Elastic (Immediate) Settlement of Medium Dense Silty Sand 0.00 ft  
 Primary Consolidation Settlement of Very Stiff Silty Clay 0.10 ft  
 Primary Consolidation Settlement of Stiff Clay 0.04 ft  
 Primary Consolidation Settlement of Hard Clay 0.19 ft  
 Secondary Consolidation Settlement of Soft Clay 0.17 ft  
**Total 0.75 ft**

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-6** Elev 35 ft-NGVD

## Assumptions:

Landfill: Max. Height of Landfill @ Elevation 110 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 75 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 115 pcf Es 576,000 lb/ft<sup>2</sup>  
 Loose/Med. Dense Sand, Unit wt below GWL 120 pcf Es 576,000 lb/ft<sup>2</sup>  
 Thickness above GWL 5 ft  
 Thickness below GWL 18.5 ft

Stiff Sandy Clay, Unit wt below GWL 110 pcf w 41 % eo 1.11 Cc 0.300 Cr 0.060  
 Stiff Sandy Clay, OCR 3  
 Thickness 5 ft

Hard Sandy Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Sandy Clay, OCR 4  
 Thickness 15 ft

Stiff Clay, Unit weight below GWL 110 pcf w 46 % eo 1.23 Cc 0.300 Cr 0.060  
 Stiff Clay, OCR 3  
 Thickness 14 ft

Hard Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Clay, OCR 4  
 Thickness 22.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 8250  
 Net Loading (delta sigma) 8250

Settlement of Loose/Med. Dense Sand			Settlement of Stiff Sandy Clay Layer			Settlement of Hard Sandy Clay Layer			Settlement of Stiff Clay layer			Settlement of Hard Clay layer		
Elastic Settlement			Primary			Primary			Primary			Primary		
Thickness (ft)	Settlement (ft)		Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)
23.5	0.34		5	1878.6	0.07	15	2742.6	0.06	14	3313.8	0.19	22.5	4609.8	0.08

## Total Settlements

Elastic (Immediate) Settlement of Loose and Med Sand 0.34 ft  
 Primary Consolidation Settlement of Stiff Clay 0.07 ft  
 Primary Consolidation Settlement of Hard Silty Clay 0.06 ft  
 Primary Consolidation Settlement of Stiff Clay 0.19 ft  
 Primary Consolidation Settlement of Hard Clay 0.08 ft  
**Total 0.74 ft**

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-7** Elev 34 ft-NGVD

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 75 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 41 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft<sup>2</sup>  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft<sup>2</sup>  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Hard Sandy Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Sandy Clay, OCR 4  
 Thickness 20 ft

Very Stiff Clay, Unit weight below GWL 115 pcf w 99 % eo 2.65 Cc 0.200 Cr 0.040  
 Very Stiff Clay, OCR 3.5  
 Thickness 21.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 4510  
 Net Loading (delta sigma) 4510

Settlement of Loose/Med. Dense Sand			Settlement of Hard Sandy Clay Layer			Settlement of Very Stiff Clay Layer		
Elastic Settlement			Primary			Primary		
Thickness (ft)	Settlement (ft)		Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)
18.5	0.19		20	2412.1	0.08	21.5	3543	0.12

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.19 ft  
 Primary Consolidation Settlement of Hard Sandy Clay 0.08 ft  
 Primary Consolidation Settlement of Very Stiff Clay 0.12 ft  
**Total 0.39 ft**

**Lena Road Stage II Landfill - Manatee County, FL**

Bore Hole B-8 Elev 34 ft-NGVD

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 95 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 61 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft2  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft2  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Soft Silty Sand, Unit wt below GWL 100 pcf Es 100,800 lb/ft2  
 Thickness 5 ft

Very Stiff Sandy Clay, Unit weight below GWL 115 pcf w 62 % eo 1.66 Cc 0.200 Cr 0.040 0.3 Ca 0.008  
 Very Stiff Sandy Clay, OCR 3.5  
 Thickness 10 ft

Very Stiff Clay, Unit weight below GWL 115 pcf w 110 % eo 2.95 Cc 0.200 Cr 0.040  
 Very Stiff Clay, OCR 3.5  
 Thickness 20 ft

Hard Silty Clay to Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Silty Clay to Clay, OCR 4  
 Thickness 46.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 6710  
 Net Loading (delta sigma) 6710

Settlement of Loose/Med. Dense Sand			Settlement of Soft Silty Sand		Settlement of Very Stiff Sandy Clay			Settlement of Very Stiff Clay			Settlement of Hard Clay layer		
Elastic Settlement			Elastic Settlement		Primary			Primary			Primary		
Thickness (ft)	Settlement (ft)		Thickness (ft)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)	Thickness (ft)	Eff Stress (psf)	Settlement (ft)
18.5	0.29		5	0.33	10	1974.1	0.08	20	3026.1	0.11	46.5	5704.5	0.16

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.29 ft  
 Elastic (Immediate) Settlement of Soft Silty Sand 0.33 ft  
 Primary Consolidation Settlement of Very Stiff Sandy Clay 0.08 ft  
 Primary Consolidation Settlement of Very Stiff Clay 0.11 ft  
 Primary Consolidation Settlement of Hard Clay 0.16 ft  
**Total 0.98 ft**

## Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **B-9** Elev 33 ft-NGVD

### Assumptions:

Landfill: Max. Height of Landfill @ Elevation 60 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 27 ft

Soils:	Loose/Med. Dense Sand, Unit wt above GWL	110 pcf	Es	576,000 lb/ft <sup>2</sup>						
	Loose/Med. Dense Sand, Unit wt below GWL	115 pcf	Es	576,000 lb/ft <sup>2</sup>						
	Thickness above GWL	5 ft								
	Thickness below GWL	18.5 ft								
	Hard Sandy Clay, Unit weight below GWL	120 pcf	w	31 %	eo	0.82	Cc	0.100	Cr	0.020
	Hard Sandy Clay, OCR	4								
	Thickness	15 ft								
	Very Stiff Clay, Unit weight below GWL	115 pcf	w	88 %	eo	2.35	Cc	0.200	Cr	0.040
	Very Stiff Clay, OCR	3								
	Thickness	10 ft								
	Hard Clay, Unit weight below GWL	120 pcf	w	80 %	eo	2.14	Cc	0.100	Cr	0.020
	Hard Clay, OCR	4								
	Thickness	11.5 ft								

Excavation to bottom of landfill 0  
 Landfill Load 2970  
 Net Loading (delta sigma) 2970

### Settlement of Loose/Med. Dense Sand

Elastic Settlement	
Thickness	Settlement
(ft)	(ft)
23.5	0.12

### Settlement of Hard Sandy Clay Layer

Primary		
Thickness	Eff Stress	Settlement
(ft)	(psf)	(ft)
15	2387.1	0.10

### Settlement of Very Stiff Clay layer

Primary		
Thickness	Eff Stress	Settlement
(ft)	(psf)	(ft)
13.5	2913.1	0.07

### Settlement of Hard Clay layer

Primary		
Thickness	Eff Stress	Settlement
(ft)	(psf)	(ft)
18	3575.5	0.07

### Total Settlements

Elastic (Immediate) Settlement of Loose and Med Sand	0.12 ft
Primary Consolidation Settlement of Hard Clay	0.10 ft
Primary Consolidation Settlement of Very Stiff Clay	0.07 ft
Primary Consolidation Settlement of Hard Clay	0.07 ft
<b>Total</b>	<b>0.36 ft</b>

# Lena Road Stage II Landfill - Manatee County, FL

Bore Hole **TH-16** Elev 33 ft-NGVD

**Assumptions:**

Landfill: Max. Height of Landfill @ Elevation 118 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 85 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft2  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft2  
 Thickness above GWL 5 ft  
 Thickness below GWL 13.5 ft

Medlum Dense Silty Sand, Unit wt below GWL 120 pcf Es 576,000 lb/ft2  
 Thickness 17.5 ft

Medium Stiff Silty Clay, Unit wt below GWL 115 pcf w 80 % eo 2.16 Cc 0.400 Cr 0.080  
 Medium Stiff Silty Clay, OCR 3  
 Thickness 2.5 ft

Hard Silty Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Silty Clay, OCR 4  
 Thickness 21.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 9350  
 Net Loading (delta sigma) 9350

**Settlement of Loose/Med. Dense Sand**

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft) 0.40  
 18.5

**Settlement of Med. Dense Silty Sand**

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft) 0.28  
 17.5

**Settlement of Medium Stiff Silty Clay Layer**

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft) 0.03  
 2.5 1391.6

**Settlement of Hard Silty Clay layer**

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft) 0.08  
 21.5 3638

**Total Settlements**

Elastic (Immediate) Settlement of Loose and Med Sand 0.40 ft  
 Elastic (Immediate) Settlement of Medium Dense Silty Sand 0.28 ft  
 Primary Consolidation Settlement of Medium Stiff Silty Clay 0.03 ft  
 Primary Consolidation Settlement of Hard Silty Clay 0.08 ft  
**Total 0.80 ft**



## Lena Road Stage II Landfill - Manatee County, FL

Bore Hole TH-17 Elev 33 ft-NGVD

### Assumptions:

Landfill: Max. Height of Landfill @ Elevation 118 ft-NGVD  
 Unit Weight of Landfill Material 110 pcf  
 Separation of Landfill Bottom from GWL 5 ft  
 Assumed HGWL Elevation = 32 ft  
 Thickness 85 ft

Soils: Loose/Med. Dense Sand, Unit wt above GWL 110 pcf Es 432,000 lb/ft<sup>2</sup>  
 Loose/Med. Dense Sand, Unit wt below GWL 115 pcf Es 432,000 lb/ft<sup>2</sup>  
 Thickness above GWL 5 ft  
 Thickness below GWL 18.5 ft

Medium Dense Silty Sand, Unit wt below GWL 120 pcf Es 576,000 lb/ft<sup>2</sup>  
 Thickness 10 ft

Hard Sandy Clay, Unit wt below GWL 120 pcf w 80 % eo 2.16 Cc 0.100 Cr 0.020  
 Hard Sandy Clay, OCR 4  
 Thickness 5 ft

Hard Silty Clay, Unit weight below GWL 120 pcf w 80 % eo 2.14 Cc 0.100 Cr 0.020  
 Hard Silty Clay, OCR 4  
 Thickness 21.5 ft

Excavation to bottom of landfill 0  
 Landfill Load 9350  
 Net Loading (delta sigma) 9350

### Settlement of Loose/Med. Dense Sand

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft) 0.51  
 23.5

### Settlement of Med. Dense Silty Sand

Elastic Settlement  
 Thickness Settlement  
 (ft) (ft) 0.16  
 10

### Settlement of Medium Stiff Silty Clay Layer

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft) 0.02  
 5 1811.1

### Settlement of Hard Clay layer

Primary  
 Thickness Eff Stress Settlement  
 (ft) (psf) (ft) 0.08  
 21.5 3625.5

### Total Settlements

Elastic (Immediate) Settlement of Loose and Med Sand 0.51 ft  
 Elastic (Immediate) Settlement of Medium Dense Silty Sand 0.16 ft  
 Primary Consolidation Settlement of Medium Stiff Silty Clay 0.02 ft  
 Primary Consolidation Settlement of Hard Clay 0.08 ft  
**Total 0.77 ft**