

July 31, 2016

Steven G. Morgan
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Southwest District Office
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Re: First Request for Additional Information (RAI)

Pasco County - Solid Waste

Facility Name: Enterprise Road Class III Recycling and Disposal

Facility Site ID: 87895

DEP Application Nos.: 177982-023-SC/T3 and 177982-024-SO/T3

Dear Mr. Morgan:

Thank you for your review of the above-referenced permit modification for the Enterprise Road Class III Recycling and Disposal Facility. The following information is provided in response to the FDEP's First Request for Additional Information (RAI) email dated May 2, 2016. Information is provided in the order requested in the referenced correspondence. In each case, the Department's request is stated in italics with the response immediately following in **bold**.

COVER LETTER:

Comment 1: This application indicates that it is for substantial modification of existing Construction Permit 177982-019-SC/T3 and Operation Permit 177982-020-SO/T3. The 10 and 20 year permit durations specified in Rule 62-701.320(9)(d), F.A.C., are not applicable to a permit modification application and therefore the expiration date for these permit modification will be the expiration dates for Permits 177982-019-SC/T3 and 177982-020-SO/T3. The 20-year permit duration is limited to facilities with a leachate control system. The application requests a partial exemption from the Class III LF leachate control requirements. Please verify whether the permittee is applying for a permit renewal or permit modification and the duration of permits being requested by

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this application, providing supporting information demonstrating that the facility qualifies for that permit duration in accordance with Rule 62-701.320(9)(d), F.A.C.

RESPONSE 1: The permittee is applying for a permit modification. We understand that the modified permit will expire on July 9, 2018 (the current permit expiration date).

SECTION 1 – INTRODUCTION:

Comment 2: In the event that your response to Comment #1 above is that this application is for renewal of existing Permit 177982-019-SC/T3 and 177982-020-SO/T3, please specifically list and reaffirm information previously provided information that will not be resubmitted with this application in accordance with the provision of Rule 62-701.320(10)(c), F.A.C.

RESPONSE 2: Not applicable. See response to Comment 1.

Comment 3: Since the permittee intends to only submit information specific to the modification that revises, consolidates, and/or updates the current permitting documents, the replacement information needs to following the formatting and numbering of the current permit documentation. Please verify and revise this application, as appropriate.

RESPONSE 3: The application formatting has been revised to follow the formatting and numbering of the current permit documentation.

SECTION 2 - APPLICATION FORM #62-701.900(1), [Rule 62-701.320 (7), F.A.C.]:

Comment 4: Part B.21: Please revise this part to indicate that Pond 3 will be an Industrial Wastewater [IW] pond.

RESPONSE 4: Part B.21 of APPLICATION FORM #62-701.900(1) has been revised to indicate that Pond 3 will be an Industrial Wastewater [IW] pond.

Comment 5: Parts B.23: The pending IW permit application for Pond 3 indicates that the facility leachate is treated by dilution and evaporation. Please verify and revise this part, as appropriate.

RESPONSE 5: The Department is correct; the facility leachate will be treated by dilution and evaporation. Part B.23 of APPLICATION FORM #62-701.900(1) has been revised to indicate that the leachate will be treated by dilution and evaporation.

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Comment 6: Parts B.24: Since a portion of the leachate will gravity drain to IW Pond 3, then a portion of the leachate will be disposed into a percolation pond. Please verify and revise this part as appropriate.

RESPONSE 6: The Department is correct; a portion of the leachate will be disposed into a percolation pond. Part B.24 of APPLICATION FORM #62-701.900(1) has been revised to indicate that the leachate will be disposed into a percolation pond and treated by dilution and evaporation.

Comment 7: D.13.: Based on your response to Comment #1 above, please publish the attached Notice of Application and provide proof of publication to the Department.

RESPONSE 7: Publication of the attached Notice of Application is under way. Proof of publication will be provided to the Department as soon as it is available.

Comment 8: Part H.1.g.: This part is checked N/C. If the response to Comment #1 above, indicates this application represents a renewal of existing Construction Permit 177982-019-SC/T3 and Operation Permit 177982-020-SO/T3, please provide an updated inventory of all public and private wells within a one-mile radius of the site. However, if the response to Comment #1., above, indicates the application represents a modification of existing Construction Permit 177982-019-SC/T3 and Operation Permit 177982-020-SO/T3, please submit revisions to this item of the application form that refer to the information submitted in support of the 2013 permit renewal application (Kelner Engineering, Renewal Application, Part H – Hydrogeological Investigation Requirements, Section H.1.g., and Attachment H-1, received March 20, 2013).

RESPONSE 8: As per the response to Comment #1, Part H.1.g has been revised to refer to the information submitted in support of the 2013 permit renewal application. Figure 5 has been revised to reflect the information provided in the Kelner 2013 permit renewal application. The revised Figure 5 also shows that the well located north of future cell 13 was abandoned in June 2015.

Comment 9: Parts I.1.f.: This part is checked N/C. However a revised sinkhole potential evaluation was included in the Universal Engineering Report including as Attachment 1 of Appendix C of the Engineering Report. Please verify and revise this part, as appropriate.

RESPONSE 9: The Universal Engineering Report is located is Section 2, Part I-1. Part I.1.f of the APPLICATION FORM #62-701.900(1) has been revised to refer to the Universal Engineering Report location.

ENGINEERING REPORT, Rule 62-701.320(7)(d), F.A.C.:

Comment 10: In many cases, the narrative in the engineering report is also utilized in the operation plan. The operation plan narrative should be revised where appropriate to address comments regarding the engineering report.

RESPONSE 10: Comment acknowledged. Revisions to the engineering report are also reflected in the revised operations plan.

Comment 11: §3.2.1: Please provide documentation of well abandonment for the previously identified two north potable wells.

RESPONSE 11: Documentation of well abandonment of the well north of Cell 13 is provided in Appendix 3-D of the revised Engineering Report.

Comment 12: §3.4.1: Figure 9 is not a FEMA flood map as described in this section. Please verify and revise this section and Figure 9 as appropriate.

RESPONSE 12: Figure 9, Flood Zone Map, has been removed. Please refer to the 2013 permit renewal application, which states "Figure S-5, 100-year floodplain, was submitted in the July 2006 Enterprise Recycling and Disposal Class III Landfill Response to 2nd Request for Additional Information, dated July 5, 2006 prepared by Jones Edmunds which is on file with the Department." Section 3.4.1 of the Engineering Report has been revised accordingly.

Comment 13: §3.5: Figure 10 is not a USDA-SCS Soil Survey Map as described in this section. Please verify and revise this section and Figure 10, as appropriate.

RESPONSE 13: Figure 10, Soil Map, has been removed. Please refer to the 2013 permit renewal application, which states "Figure 3-5 Soil Survey Map – Figure 3-5 was submitted as part of the 2005 Enterprise Recycling and Disposal Facility Class III Landfill Permit Renewal Application, Pasco County, dated August 2005, prepared by Tetra-Tech HAI (TTHAI) and is on file with the Department." Section 3.5 of the Engineering Report has been revised accordingly.

Comment 14: §3.7: Please revise this section to specifically describe the specified permeability of the clay layer material [1x10-7 cm/sec] as indicated for the current facility permits.

RESPONSE 14: Section 3.7 of the Engineering Report has been revised to specifically describe the permeability of the clay layer material (1x10-7 cm/sec) as indicated for the current facility permit.

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Comment 15.a: Phase Sequence 1: The description in this section appears to assume that construction of Cell 7 has been completed and certified which is not the current condition of the facility. In addition, the Cell 7 construction details presented on Drawings C-7, C-11, and C-12 of the 2012 Kelner Engineering Plan Set do not appear to be included in the plan set provided with this application. Please verify and revise this section and the plan set, as appropriate.

RESPONSE 15.a: The phasing sequence section of the Engineering Report has been revised. The Plan Set has also been revised to include the Cell 7 construction details presented on Drawings C-7, C-11, and C-12 of the 2012 Kelner Engineering Plan Set.

Comment 15.b: Phase Sequence 1: The currently permitted design for Cells 1-7 and 15 is a maximum 4H:1V slope from elevation 125' to 170' (see Permit Modification Nos. 117982-021-SC/IM & 177982-022-SO/MM). Please revise this section accordingly.

RESPONSE 15.b: The phasing sequence section of the Engineering Report has been revised.

Comment 15.c: The phasing sequence narrative and filling sequence drawings in the Plan Set should describe and show the extent of filling in Cell 7 before proceeding to Cell 16; the extent of filling in Cell 16 before proceeding back to filling Cells 1-7 and 15; and the sequence of filling over Cells 1-7, 15, and 16 to final elevations. Please revise this section and the Plan Set, as appropriate.

RESPONSE 15.c: The phasing sequence narrative and filling sequence drawings in the Plan Set have been revised as requested.

Comment 15.d: Please explain the statement "Use culverts, berms, or best management practices..." in this section and Section 3.8.2.

RESPONSE 15.d: This statement has been removed from this section and Section 3.8.2.

Comment 16: §3.8.1: Please revise this section to clarify that Drawing C2.00 (inclusive of Cell 13-14) is beyond the scope of this application; is provided as a conceptual final buildout closure plan for financial assurance calculations purposes, and that a final closure drawings for Cell 1-7 and 15-16 will be provided in the event that Cells 13 and 14 are not permitted for construction and operation in the future.

RESPONSE 16: Drawing C2.00 has been revised and no longer includes Cells 13 and 14.

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Comment 17: §3.8.2: The statement that filling will start at the 2H:1V slopes appears only applicable to Cell 7. Please verify and as applicable, revise this section also identify where filling will begin in Cell 16.

RESPONSE 17: Section 3.8.2 has been revised to clarify that the 2H:1V slopes are only applicable to the Cell 7 and to identify where filling will begin in Cell 16.

Comment 18: §3.9: Please revise this section to remove the specific references to Drawings C2.00 and C2.10 of the Plan Set (see Comment #16. above).

RESPONSE 18: Section 3.9 has been revised in accordance with the response to Comment 16.

Comment 19: §3.10.1.2: This section refers to Figure 3-14 (provided in Appendix 3-C of the 2012 permit renewal application submitted by Kelner Engineering) for construction details of the proposed landfill gas probes. As the replacement probes are proposed to be located in proximity to the landfill property boundary, the 18-foot length of perforated pipe installed at the bottom of a 20-foot deep gas probe may not be adequate to ensure the bottom of the perforated section of the gas probe extends to the bottom elevation of the adjacent waste disposal cell. Please submit supplemental information that provides proposed elevations of the top and bottom of the perforated section of each proposed gas probe and the estimated land surface of each proposed gas probe as a replacement for Figure 3-14.

RESPONSE 19: Section 3.10.1.2 has been revised to include supplemental information related to the anticipated total depths of the proposed gas monitoring probes.

Comment 20: §3.10.1.5: Please provide the supporting information, calculations, and or assumptions utilized in support of the proposed location of gas vents shown on Drawing C2.00, concentrated at the highest level of the facility, rather located at roughly equidistant locations throughout the entire footprint of the closed facility, as depicted on Sheet C-8 of the 2012 Kelner Engineering Plan Set.

RESPONSE 20: Section 3.10.1.5 and Drawing C2.00 have been revised to reflect the gas vent spacing shown on sheet C8 of the 2012 Kelner Engineering Plan Set.

§3.10.2.:

Comment 21.a: Leachate will also continue to be conveyed to the portion of the existing temporary stormwater located in conceptual future Cell 14. Please verify and revise the narrative in this section accordingly.

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RESPONSE 21.a: The Department is correct. A portion of the leachate will continue to be conveyed to the portion of the existing temporary stormwater pond located in conceptual future Cell 14. Section 3.10.2 has been revised accordingly.

Comment 21.b: Please provide specific design and operation descriptions of how leachate is conveyed from Cells 1-7 and 15 to Pond 3 while Cell 16 is being constructed and how leachate is conveyed to Pond 3 during Cell 16 operation without causing disposal of waste in water.

Prior to starting construction in Cell 16, a berm will be constructed RESPONSE 21.b: immediately north of Cell 15. The berm will extend east to west the full width of Cell 16. A portion of the leachate generated in existing cells 1-7 and 15 will move to the remaining temporary stormwater pond in the future Cell 14 area. The remainder of the leachate generated in existing cells 1-7 and 15 will move to Pond 3 via the berm located immediately north of Cell 15. Once Cell 16 construction is complete, the berm will remain in place while the initial lift of waste is placed across the entire floor of Cell 16. Once Cell 16 is "floored out," the berm will be removed for the remainder of Leachate generated in existing cells 1-7 and 15 will then move to operations. temporary stormwater pond in the future Cell 14 area as it did prior to removal of the berms. The remainder of the leachate generated in cells 1-7, 15 and all leachate generated in Cell 16 will move to Pond 3 via the clay barrier layer beneath Cell 16. Under no circumstances will waste be placed in water. In the event that water is present above the clay barrier layer at the time waste is to be placed, the operator will utilize pumps to remove the water to Pond 3. Section 3.10.2 has been revised accordingly.

Comment 21.c: Please explain how "the controlled method of waste screening" impacts leachate generation and control at the facility.

RESPONSE 21.c: Waste screening does not impact leachate generation. However, screening does positively impact the chemical composition of the leachate through the removal of prohibited materials.

<u>APPENDIX A - 2014 PLAN SET</u> (Rule 62-701.320(7)(f), F.A.C.):

Drawing C0.03:

Comment 22a: Please verify whether gas probes GP-11 and GP-14 will continue to be existing gas probes or will abandoned and replaced as part of Cell 16 construction (per Section 3.10.1.1 of Engineering Report) and revise this drawing as appropriate.

RESPONSE 22.a: Gas probes GP-11 and GP-14 will be abandoned and replaced with GP-11R and GP-14R, respectively. Drawing C0.03 has been revised accordingly.

Comment 22.b: Please verify whether gas probes GP-12R and GP-13R depicted on this drawing are existing or proposed replacement gas probes (per Section 3.10.1.1 of Engineering Report) and revise the drawing, as appropriate.

RESPONSE 22.b: Gas probes GP-12R and GP-13R will continue to be existing gas probes. Section 3.10.1.1 of the Engineering Report has been revised.

Comment 22.c: Please verify whether gas probes GP-1 through GP-5 and GP-16 depicted on this drawing are existing or proposed future gas probes (per Section 3.10.1.1 of Engineering Report) and revise the drawing, as appropriate.

RESPONSE 22.c: Gas probes GP-1 through GP-5 and GP-16 are proposed future gas probes. Drawing C0.03 has been revised to clarify the status of these gas probes.

Comment 22.d: Please provide sections through Cell 16, each of the three sets of monitor wells (MW-4/MW-4B, MW-5AR/MW-5BR, MW-6/MW-6B), and Pond 3 to show the following:

- the lateral distance from the edge of waste in Cell 16 to the monitor well pairs
- the lateral distance from the monitor well pairs to the top of bank of Pond 3

RESPONSE 22.d: Sections are provided through Cell 16. The three sections profile the monitoring well pairs (MW-4/MW-4B, MW-5AR/MW-5BR, MW-6/MW-6B), the edge of waste of Cell 16 and the top of the bank of Pond 3. The sections are presented in Figure 4 of Section 5 of the revised Groundwater Monitoring Plan.

Comment 23: Drawing C0.04: Please revise this drawing to also include the cell floor grading for Cell 7.

RESPONSE 23: Drawing C0.04 has been revised to include the cell floor grading for Cell 7 as presented in the 2013 Kelner Engineering Permit Application.

Comment 24: Drawings C1.00 / C1.10 and C2.00 / C2.10: The operating and closures contours and slope depicted on these sheets above elevation 125' appear inconsistent with both the fill sequence descriptions in Section 3.8 of the Engineering Report and the currently permitted contours and elevations for Cells 1-7 and 15 (see Permit Modification Nos. 117982-021-SC/IM & 177982-022- SO/MM). In addition, transitioning from a 4H:1V side slope in Cells 5 and 15 above elevation 125' to a 3H:1V side slope in Cell 16 appears problematic. Please verify and revise these drawings, as appropriate.

RESPONSE 24: Drawings C1.00 / C1.10 and C2.00 / C2.10 have been revised to reflect the currently permitted contours and elevations for Cells 1-7 and 15.

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Additionally, the drawings have been revised to show 4H:1V side slopes for Cell 16 above elevations 125'.

Comment 25: Drawings C1.00: Please verify that the proposed contouring of the south side slope of the temporary stormwater pond to elevation 89' depicted on this sheet will not prevent leachate from draining from the existing disposal cells to the temporary stormwater pond.

RESPONSE 25: The Plan Set drawings have been revised to leave the current contouring of the temporary pond south side slope unchanged.

Comment 26: Drawing C2.00: <u>Conceptual Closure Berm</u>: The current stormwater management side slope conveyance system design includes closure berms and drop inlet at each side slope bench (i.e. elevations 125' and 150') and not at elevation 170'. Please verify and provide a revised detail, similar to the current detail provided on Drawing C-15 (see Permit Modification Nos. 117982-021-SC/IM & 177982-022-SO/MM)

RESPONSE 26: Drawing C2.00 has been revised to remove the drop inlets previously shown on the top deck as well as updating the referenced detail.

Drawing C3.00:

Comment 27.a: <u>Detail 1</u>: This detail appears inconsistent with Drawings C2.00 and C2.10. Please verify and revise as appropriate.

RESPONSE 27.a: Drawing C3.00 Detail 1 has been revised to be consistent with drawings C2.00 and C2.10.

Comment 27.b: <u>Detail 2</u>: It is unclear where the temporary diversion swale will be constructed for Cell 16 and where the stormwater will be diverted to. Please explain and revise this drawing and/or Drawings C1.00 and C1.10, as appropriate.

RESPONSE 27.b: Please see response to 21b above.

Comment 27.c: <u>Details 5 and 6</u>: There are not north and east clay side slopes proposed for the construction of the Cell 16 bottom liner. Please verify the purpose of these details and/or remove these details, as appropriate.

RESPONSE 27.c: Drawing C3.00 Details 5 and 6 have been modified to refer only to Cell 7.

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<u>APPENDIX B - FIGURES</u> (Rule 62-701.320(7)(f), F.A.C.):

Comment 28: It is unclear which currently permitted and valid figures are being replaced by the figures in Appendix B and which are remaining. Please verify and revise Appendix B, as applicable.

RESPONSE 28: With the exception of Figure 5 (relabeled Figure S-1, Potable Water Wells) located in Section 3, Appendix 3-C, the figures presented in Appendix B of the initial permit modification application have been removed.

Comment 29: Figure 5: Please verify the presence of an off-site potable wells west and southeast of the site, as depicted on Figure S-1 provided with the engineering report for the current facility permits and revise this figure, as applicable.

RESPONSE 29: Potable Well Location Map has been revised and is located in Section 3 Appendix 3-C. The well located north of future cell 13 has been abandoned. The well northwest of future phase 12 has been added to the map, however, this well is currently not used and was presumably used for irrigation historically. The well east of the southeast corner of Cell 2 has been added to the map. The well to the southeast of the southeast corner of the property in Figure S-1 is permitted as "irrigation" by the SWFWMD. Additionally, the two wells identified as "potable wells" in Figure 5 of the 2015 permit modification are also permitted as "irrigation" by the SWFWMD. The Potable Well Location Map (Figure 5) has been revised and is located in Section 3, Appendix 3-C.

APPENDIX C – LINER SYSTEM REQUIREMENTS EVALUATION (62-701.340(2)(b), F.A.C.):

Comment 30: §6.2: ¶2 of this section indicates ground water data was compiled for the semi-annual events conducted between October 2005 and September 2015 to assess the change in water quality over time. Please submit revisions to the graphs and the box-and-whisker plots presented in Attachment 2 to include the results reported through September 2015. It appears that Attachment 2 contains two sets of graphs and box-and-whisker plots; please indicate if the second set of graphs and box-and-whisker plots provide different information and submit revisions to Attachment 2, as appropriate.

RESPONSE 30: Two identical sets of graphs and plots were inadvertently provided in Attachment 2. The superfluous set has been removed. The graphs and plots have been revised to include the September 2015 data. The revised Liner System Requirements Evaluation is provided in Section 2, Part G-1.

§6.2.2: Please note that the following comments regarding sub-sections titled "Dissolved Oxygen," "Total Dissolved Solids," and "Iron" were included in the comments memorandum prepared by John Morris, P.G., dated October 30, 2015 regarding the

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draft Liner System Requirements Study Report dated September 2015. It does not appear that these comments were addressed in the revised Liner System Requirements Study Report dated March 2016. Please address the following regarding ground water quality reported for surficial aquifer monitor wells:

Comment 31.a: The sub-section titled "Dissolved Oxygen" indicated the variation in D.O. values may be attributed to the on-going excavation and cell construction activities at the site – materials excavation may result in re-oxygenation of lower portions of the surficial aquifer and cell construction/waste placement may result in reduction in D.O. values. The "Liner Report" does not demonstrate whether D.O. values recorded during well purging for the semi-annual sampling events is a reflection of ambient conditions or is influenced by purging activities. To provide additional characterization of the variability in D.O. values reported for the surficial aquifer wells, the information presented in Section FS 2212, Item #3.5 of the Department's Standard Operating Procedure #FS 2200 needs to be collected. Specifically, the use of a downhole oxygen probe to collect D.O. readings within the screened interval of the monitor wells prior to the initiation of well purging activities should be completed.

SOP #FS 2200 can be accessed on the Department's web site at the following link: http://www.dep.state.fl.us/water/sas/sop/sops.htm

RESPONSE 31.a: An evaluation of site specific D.O. values was performed by Jones Edmunds in 2006. Table 1 shows the D.O. for various wells during typical sampling and Table 2 shows the downhole D.O. in multiple wells. There are some wells that are in Table 1 that are not in Table 2, and vice versa. There are five wells that are common to both tables: MW-5A, MW-5B, MW-8B, MW-9B, and MW-10B. Below is a comparison of the D.O. results for these five wells as follows:

<u>Well</u>	Sampling DO Range	Downhole DO Range
MW-5A	5.06 - 5.30	2.67 – 6.10
MW-5B	3.25 – 3.35	3.02 – 4.55
MW-8B	0.15 – 0.18	0.13 – 0.29
MW-9B	5.71 – 5.92	0.26 - 0.27
MW-10B	0.78 – 1.82	0.24 – 1.16

Of the five common wells, four of them have essentially the same downhole DO values as sampling DO values. The one outlier is MW-9B, which showed a higher DO during sampling than in the downhole sampling. The data shows a strong correlation between the DO at sampling and downhole DO. It seems reasonable that elevated DO observed in samples collected during routine semiannual monitoring are representative of natural conditions and not deficiencies in sampling procedures. The sub-section titled "Dissolved Oxygen" has been revised to include this information.

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Comment 31.b: The sub-section titled "Total Dissolved Solids" indicated the elevated TDS concentrations reported for well MW-4 are most likely a naturally high mineral content relative to the other wells, however no information was provided to explain why the TDS concentrations are lower at the adjacent surficial aquifer monitor wells. It is also noted that while well MW-4 was installed in 2006, it was first successfully sampled during October 2009. Therefore, no ground water quality data is available to characterize "background" conditions prior to landfilling activities and the operation of the temporary stormwater pond.

RESPONSE 31.b: The TDS values reported for MW-4 typically range from 300 to 450 mg/L. All of these values are below the SDWS of 500 mg/L. TDS values in adjacent well MW-3 typically range from 200 to 270 mg/L, which is comparable to the range observed in MW-4.

Comment 31.c: The sub-section titled "Iron" indicated the change in D.O. and ORP of water directly relates to change in redox conditions and variation in iron concentrations. This sub-section also indicated it was possible that iron exceedances were related to reducing conditions resulting from landfill construction and site earthwork activities and not an actual release from the waste placed in the landfill. This section did not provide plots of iron concentration vs. D.O., or iron concentrations vs. ORP to demonstrate this relationship.

RESPONSE 31.c: Iron concentrations vs. D.O. and Iron vs. ORP plots are provided in Section 2, Part G-1, Attachment 2.

§6.2.3: Please note that the following comments regarding sub-sections titled "Overview," pH," "Dissolved Oxygen," and "Iron" were included in the comments memorandum prepared by John Morris, P.G., dated October 30, 2015 regarding the draft Liner System Requirements Study Report dated September 2015. It does not appear that these comments were addressed in the revised Liner System Requirements Study Report dated March 2016. Please address the following regarding ground water quality reported for Floridan aquifer monitor wells:

Comment 32.a: The sub-section titled "Overview" referenced the installation of new background well BW-1B. It is noted that the Ground Water Quality Plots provided in Appendix C omitted results reported for well BW-1B.

RESPONSE 32.a: The Ground Water Quality Plots have been revised to include data results reported for well BW-1B.

Comment 32.b: The sub-section titled "pH" described the period of time pH values were reported to exceed 8.5 S.U. at well MW-7BR, however the increasing pH values reported

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at well MW-16B (reported at 10.48 S.U. during the September 2015 event) were not discussed.

RESPONSE 32.b: This subsection of the Liner System Requirements Evaluation Report has been revised to include a discussion of pH values reported for MW-16B.

Comment 32.c: The sub-section titled "Dissolved Oxygen" indicated D.O. levels in Floridan aquifer wells ranged from 0.09 to 8.1 mg/L. See Comment #31.a, above, regarding supplemental characterization of D.O. values using a down-hole oxygen probe prior to initiation of well purging activities.

RESPONSE 32.c: This sub-section has been revised accordingly.

Comment 32.d: The sub-section titled "Iron" indicated the lack of oxygenation can result in the dissolution of naturally-occurring iron, resulting in elevated concentrations in ground water. See Comment #31.c. above, regarding submittal of plots of iron concentrations vs. D.O., and iron concentrations vs. ORP to demonstrate this relationship.

RESPONSE 32.d: This sub-section has been revised as requested. See response to Comment 31.c above.

Comment 33: §6.2.4: ¶2 of this section refers to the potable well survey provided in Attachment 3. The figure provided in Attachment 3 (titled "Potable Well Location Map") was compared to the locations depicted on Figure S-1 (titled "Potable Water Wells") presented in Attachment H-1 of the Engineering Report submitted by Kelner Engineering dated march 2013 in support of the permit renewal application. It is understood that the private well located north of conceptual Cell 13 has been abandoned; however the two other wells on Figure S-1 (in the citrus grove west of conceptual Cell 11 and off-site to the southeast of Cell 2) have been omitted. Additionally, the on-site supply well located southwest of Cell 7 is not presented on the figure in Attachment 3. Please review the omitted well locations and submit revisions to Attachment 3 as appropriate.

RESPONSE 33: The figure provided in Attachment 3 has been revised to be consistent with the Potable Well Location Map provided in Section 3, Appendix 3-C. Please see the response to Comment 29.

Attachment 1 – Universal Engineering Report (Rule 62-701.410, F.A.C.):

Comment 34: Appendix A: The figure titled, "Site Aerial Photograph" appears outdated and not reflective of the proposed facility. Please verify and revise as appropriate.

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RESPONSE 34: The Universal Engineering "Site Aerial Photograph" has been updated. The revised Site Aerial Photograph is located in Section 2, Part I-1.

Comment 35: Appendix B: The boring designation on the figure titled, "Boring Location Map" are illegible on both the electronic and paper copies of this figure submitted with this application. Please provide a legible copy of this figure.

RESPONSE 35: The "Boring Location Map" has been revised to ensure boring designation legibility. The revised Boring Location Map is located in Section 2, Part I-1.

Comment 36: Appendix C: §2.3 (Cell 16 Borings and Geologic Cross Sections), subsection "Geologic Summary" described a few borings which show a few one to two foot thick layers of soft sediments. This section concluded: "However, in all borings dense to very dense sediments have surrounded these softer soil layers in a stable setting." It does not appear that this conclusion accurately describes the low blow counts reported at the bottom of boring B-21 (N-value @ 4), boring B-33 (N-value @ 3), and boring DCL01-13 (N-value @ 3). Please revise this section as appropriate.

RESPONSE 36: The "Geologic Summary" has been revised. The revised Geology Summary is located in Section 2, Part I-1.

<u>APPENDIX D - GROUNDWATER MONITORING PLAN</u> (Rule 62-701.510, F.A.C.):

§1.: This section refers to the ground water monitoring network described in Table 1 and Figure 1. Please submit revisions to address the following:

Comment 37.a: Figure 1:

- Please revise the label to refer to existing well MW-6
- Please include a depiction of the lateral extent of the zone of discharge around the disposal footprint (Cells 1through 7, Cell 15 and Cell 16). As indicated in Appendix 3, Para. 2.a., of permit #177982-020-SO/T3, the zone of discharge extends horizontally 100 feet from the limits of the landfill disposal areas or to the property boundary, whichever is less.

RESPONSE 37.a: Figure 1 has been revised per Comment 37.a. The revised Figure 1 is located in Section 5.

Comment 37.b: Table 1:

- Please revise the "Notes" column to indicate existing well MW-15B will be abandoned in conjunction with Cell 7 construction
- Please revise the "Notes" column to indicate existing well MW-16B will be abandoned in conjunction with Cell 7 construction

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- Rule 62-701.510(3)(b), F.A.C., indicates the following: "If site-specific conditions require installation of compliance wells within the zone of discharge, then a confirmed exceedance of a ground water standard above background at such wells will be considered a violation of that standard." Based on the response to Comment #22.d., above, it appears appropriate to designate wells MW-4/MW-4B, MW-5AR/MW-5BR, and MW-6/MW-6B as compliance wells. Please submit revisions to Table 1 to reflect the compliance well designation for these wells.

RESPONSE 37.b: Table 1 has been revised to indicate abandonment of MW-15B and MW-16B in conjunction with Cell 7 construction. Monitoring wells MW-4/MW-4B, MW-5AR/MW-5BR, and MW-6/MW-6B will be detection wells based on Rule 62-701.510(3)(a), F.A.C.: the wells will be within the zone of discharge, hydraulically downgradient from the solid waste disposal unit; located no more than 50 feet from the edge of solid waste disposal unit of Cell 16. The revised Table 1 is located in Section 5.

Comment 38: §1.a.: Please submit revisions to indicate well abandonment shall be performed in accordance with the requirements of Rule 62-532.500(5), F.A.C.

RESPONSE 38: §1.a has been revised as requested.

§1.d.:

Comment 39.a: It appears that existing monitor wells MW-4/MW-4B and wells MB-6/MW-6B will remain in place during construction of Cell 16 and Pond 3. Please describe how these well pairs will be protected during construction activities.

RESPONSE 39.a: Monitor wells MW-4/MW-4B and wells MB-6/MW-6B will be protected during construction of Cell 16 and Pond 3 with the use of bollards or jersey barriers.

Comment 39.b: It is indicated in Table 1 that replacement wells MW-5AR/MW-5BR will be installed within 60 days of permit modification issuance. Please describe how this replacement well pair will be protected during construction of Cell 16 and Pond 3.

RESPONSE 39.b: Table 1 has been revised to indicate that replacement wells MW-5AR/MW-5BR will be installed within 60 days prior to placement of waste in Cell 16.

Comment 39.c: ¶2 of this section refers to construction details for proposed monitor wells presented on Figure 2 (titled "Proposed Surficial Aquifer Monitor Well Detail") and Figure 3 (titled "Proposed Floridan Aquifer Monitor Well Detail"). To ensure the proposed surficial and Floridan aquifer monitor wells are adequately constructed for the targeted interval, please submit revisions to Figures 2 and 3 to specify the elevations of the top of the well screen and the bottom of the well screen at each proposed monitor well

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based on site-specific lithology and water level data. For proposed surficial aquifer wells the elevation of the top of the clay confining unit at the base of the surficial aquifer and the historic range of ground water elevations at adjacent monitor wells or piezometers should be summarized. For proposed Floridan aquifer monitor wells the elevation of the top of limestone sediments and the historic range of ground water elevations at adjacent monitor wells or piezometers should be summarized. Please submit revisions to this section to indicate that the ground surface elevation shall be established at each proposed monitor well location prior to the initiation of well installation.

RESPONSE 39.c: Figures 2 and 3 have been revised to specify the elevations of the top and bottom of the well screens at each proposed monitor well based on site-specific lithology and water level data. ¶2 of section §1.d has been revised to summarize the top of the clay confining unit at the base of the surficial aquifer and the historic range of ground water elevations at adjacent monitor wells or piezometers for the proposed surficial aquifer wells. ¶2 of section §1.d has been revised to summarize the top of limestone sediments and the historic range of ground water elevations at adjacent monitor wells or piezometers for the proposed Floridan aquifer wells.

Comment 40: §1.e.: The Department acknowledges the indication that Ponds 1, 2 and 3 do not have off-site discharge associated with the 100-year flood event and therefore routine surface water monitoring is not required. Please note that it is the Department's intention to retain the current surface water monitoring requirement in the event of a surface water discharge event from the stormwater management system (refer to Appendix 3, Para. 8.a., and Para. 8.b., of Permit #177982-020-SO/T3).

RESPONSE 40: §1.e has been revised per Comment 40.

APPENDIX E – SLOPE STABILITY ANALYSIS (Rule 62-701.410, F.A.C.):

Comment 41: As discussed in Comment #24 above, filling to a 3H:1V side slopes above elevation 125' may be problematic when the permitted side slopes of adjacent disposal cells is 4H:1V. Please verify and revise the assumptions, calculations, and/or conclusions presented in this report, as applicable.

RESPONSE 41: The slope stability analysis has been performed again using the revised 4H:1V side slopes above elevation 125' as discussed in the response to Comment 24.

Comment 42: <u>Reference Documents</u>: In multiple discussions with the permittee and their consultants, the Department has expressed our opinion that the soil borings from the 2000 geotechnical report could not be relied upon as representative of the site subsurface soils layers and conditions. As a result, the January 29, 2016 Universal

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Engineering Geotechnical Exploration Report utilized to evaluate the liner system requirements for Cell 16 and re-evaluated the Cell 16 subsurface, relied primarily on subsurface investigations and reports generated after 2003. Please provide supporting justification why this report relied upon boring logs generated as part of the 2000 geotechnical report to characterize the Cell 16 subsurface and/or revise this report accordingly to utilize more reliable site information.

RESPONSE 42: The slope stability analysis has been revised to utilize and reference the appropriate geotechnical information.

Comment 43: <u>Slope Stability Model Analysis</u>: As indicated by Comment #24 above, the Locklear & Associates Plans that were "... used as the basis for modeling the slope geometry" appear incorrect. Please verify and revise this analysis, as appropriate.

RESPONSE 43: The slope stability model analysis has been updated to utilize the corrected side slope design as discussed in the response to Comment 23.

<u>APPENDIX F - CLOSURE AND RECLAMATION PLAN</u> (Rule 62-701.600, F.A.C.):

Appendix F-1:

Comment 44.a: It appears that the cost estimates provided utilized the cost estimates information, calculations, and/or assumptions from the 2014 approved revised estimates submitted in support of Permits 177982-019/SC/T3 and 177982-020-SO/T3 and prorated quantities based the addition of Cell 16. While the Department does not object to this approach, the final calculated closing and long-term care costs should be inflation-adjusted based on the 2015 and 2016 inflation factors (1.015 & 1.014 respectively). Please revise the cost estimates accordingly

RESPONSE 44.a: The Closing and Long-Term Care costs have been inflation-adjusted per the 2015 and 2016 inflation factors. Please see the revised DEP Form 62-701.900(28) in Section 7, Appendix 7-A.

Comment 44.a: <u>Long-Term Care – Groundwater Monitoring</u>: It appears that the assumed number of monitor wells in this section (21 wells) may be inconsistent with the number of wells proposed in the Groundwater Monitoring Plan provided in Appendix D (16 wells). Please verify and revise the long-term care costs accordingly

RESPONSE 44.b: The number of sampling points will range between 23 and 26 based on the presence of water bearing soils above the clay layer in the locations of monitoring wells MW-18B, -19B and -20B. The 23 to 26 sampling points include two background wells, eight to eleven surficial aquifer detection wells, twelve Floridan aquifer detection wells and one supply well. To be conservative, the maximum number

Mr. Steve Morgan July 31, 2016 Page **18** of **19**

of 26 wells was used in the long term care cost estimates. Section 7, Appendix 7-A (previously Appendix F-1) and Section 5 (previously Appendix D) have been revised to reflect the number of sampling points.

APPENDIX G - OPERATIONS PLAN (Rule 62-701.500(9), F.A.C.):

Comment 45: §5.4: Based on the listing of unpainted and untreated wood as acceptable wastes, painted and treated wood should be added to the list of unacceptable waste materials for disposal at this facility. Please verify and revise this section, as appropriate

RESPONSE 45: The facility also accepts painted wood. The list of acceptable wastes has been revised to reflect this. CCA-treated wood has been added to the list of unacceptable waste materials.

Comment 46: §5.8: The facility is not currently a registered Source-Separated Organics Processing Facility and the Operation Plan does not appear to include procedures for storage and processing of wood waste in accordance with Rule 62-709.320, F.A.C. Please revise this section to reference the facility's Source- Separated Organics Processing Facility registration or to include procedures for storage and processing of wood waste in accordance with Rule 62-709.320, F.A.C.

RESPONSE 46: This section has been revised to reference the facility's SSOP facility registration. A copy is provided in Attachment 7 of the revised Operations Plan.

Comment 47: §5.9: This section does not appear to discuss how the facility operators/spotters will determine that wood received at the facility is CCA treated wood. Please revise this section accordingly.

RESPONSE 47: Section 5.9 has been revised to discuss how the facility operator/spotters will determine that wood received at the facility is CCA treated wood.

Comment 48: §8.0: Please revise this section consistent with revisions made to the Engineering Report in response to this letter.

RESPONSE 48: Section 8.0 has been revised to be consistent with revisions made to the Engineering Report.

Comment 49: Attachment 6: Based on review of the training certificates in Attachment 6, all of individuals training certifications are expired. Please verify and revise this attachment, as appropriate.

Mr. Steve Morgan July 31, 2016 Page 19 of 19

RESPONSE 49: Current training certifications are provided in Attachment 6 of the Operations Plan provided in Section 3, Appendix 3-A.

APPENDIX I - CONTINGENCY PLAN (Rules 62-701.320(7)(e)2. & (16), F.A.C.):

Comment 50: §1.1 &: §1.4: The FDEP Southwest District phone number has recently changed to (813) 470-5700. Please revise these sections, accordingly.

RESPONSE 50: Sections 1.1 and 1.4 of the Contingency Plan provided in Section 3, Appendix 3-B have been revised to reflect the updated phone number.

Please feel free to call me or John Locklear at (352) 672-6867 with any questions regarding this submittal.

Sincerely,

Lisa J. Baker, P.E.

Sisa Baker

Engineering Division Director

cc: John Arnold, Angelo's Aggregate Materials, Ltd.

John Locklear, Locklear & Associates, Inc.

<u>Attachments</u>

Attachment 1:

Revised Permit Modification Application

ATTACHMENT 1

PERMIT MODIFICATION APPLICATION FOR THE ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY

WACS Facility ID: 87895 WACS No.: SWD/29/41084

Construction Permit No.: 177982-019-SC/T3 Operation Permit No.: 177982-020-SO/T3

Prepared for:

ANGELO'S AGGREGATE MATERIALS, LTD.

855 28th Street South St. Petersburg, Florida 33712

Presented to:

FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION SOLID WASTE SECTION

13051 North Telecom Parkway Temple Terrace, Florida 33637-0926

Prepared by:

LOCKLEAR AND ASSOCIATES, INC.

4140 NW 37 Place, Suite A Gainesville, Florida 32606 Certificate of Authorization #30066

Project No.: 02000-144-15

March 2016

Revised July 2016 (RAI 1 Response)

Performed Under the Supervision of No. 74652

No. 74652

Lisa Labrakor, P.E.

Riorida Bei #74653

Contents

NOTE: Contents page is from the 2012 Permit Renewal Application submitted by

Kelner Engineering, Inc. and 2015 Permit Modification Application submitted by Locklear & Associates, Inc. Only items in **BOLD** are provided in the current application package. The remaining items are unchanged.

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FDEP FORM 62-701.900(1) Application to Construct, Operate, Modify or Close a Solid Waste Management Facility

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PART D SOLID WASTE MANAGEMENT FACILITY PERMIT

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HYDROGEOLOGICAL INVESTIGATION

PART H REQUIREMENTS

PART I GEOTECHNICAL INVESTIGATION REQUIREMENTS

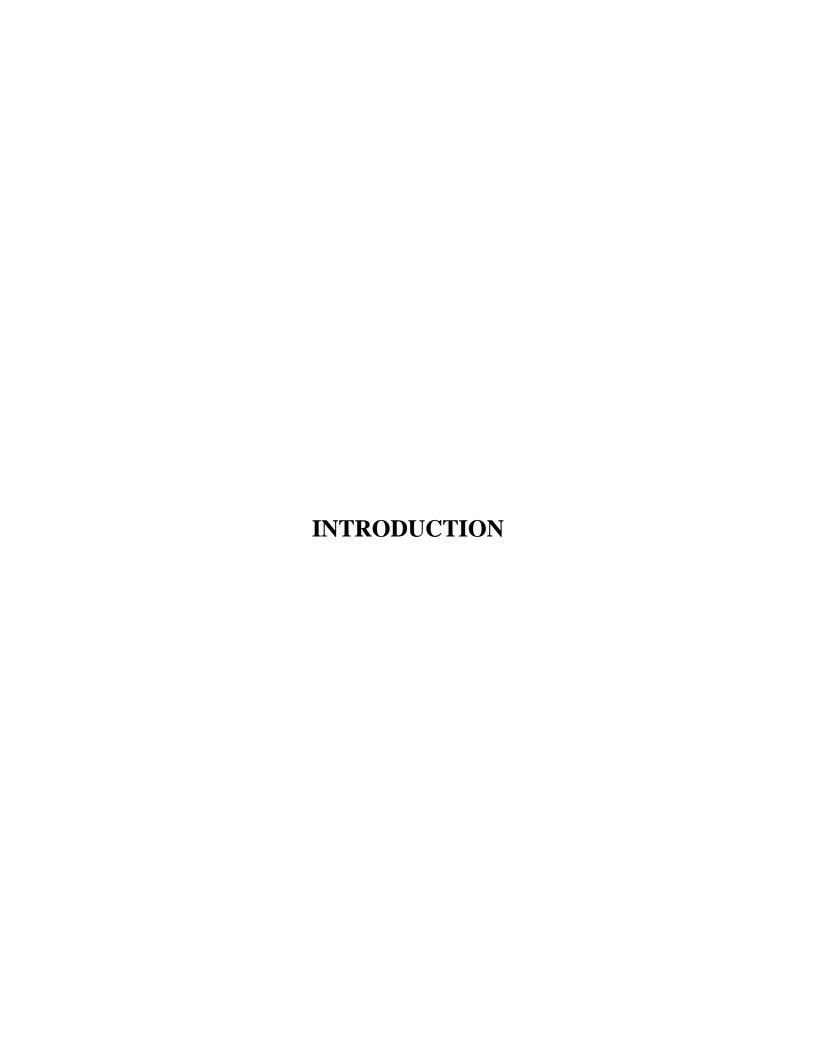
I-1 UNIVERSAL ENGINEERING SCIENCES REPORT

I-2 SLOPE STABILITY ANALYSIS PART J VERTICAL EXPANSION OF LANDFILLS PART K LANDFILL OPERATION REQUIREMENTS WATER QUALITY AND LEACHATE MONITORING PART L **REQUIREMENTS** PART M SPECIAL WASTE HANDLING REQUIREMENTS PART N GAS MANAGEMENT SYSTEM REQUIREMENTS PART O LANDFILL FINAL CLOSURE REQUIREMENTS PART P OTHER CLOSURE PROCEDURES PART Q LONG-TERM CARE PART R FINANCIAL ASSURANCE **SECTION 3 ENGINEERING REPORT APPENDIX** 3-A **OPERATIONS PLAN APPENDIX** 3-B **CONTINGENCY PLAN APPENDIX 3-C FIGURES APPENDIX** 3-D WELL ABANDONMENT DOCUMENTATION **SECTION 4** 2016 PLAN SET (Previous plan set is replaced in its entirety) **SECTION 5** GROUNDWATER MONITORING PLAN WATER QUALITY MONITORING PLAN **SECTION 6 EVALUATION SECTION 7 CLOSURE AND RECLAMATION PLAN APPENDIX**

ALLENDIA

7-A FINANCIAL ASSURANCE COST ESTIMATES

SECTION 8 ENVIRONMENTAL RESOURCE PERMIT



INTRODUCTION

Locklear & Associates, Inc. (L&A) is submitting one (1) copy of the completed Form 62-701.900(1), F.A.C. and all supporting documentation for the modification of Solid Waste Construction Permit 177982-019-SC/T3 and Solid Waste Operations Permit 177982-020-SO/T3 on behalf of Angelo's Aggregate Materials, LTD (Applicant) for the Enterprise Road Class III Recycling and Disposal Facility (Facility) located in Pasco County, Florida. Proof of ownership is provided in Section 2 Part D-1 Attachment 1. L&A has been authorized by the Applicant to act on its behalf in the preparation and submittal of this document. A letter of authorization is provided in Section 1 S-1 Attachment 2.

In accordance with Rule 62-701.320, F.A.C., facility information that was submitted to the Department to support the current permits, and which is still valid, has not been re-submitted for permit modification. As discussed in multiple pre-application meetings with the Department, this permit modification application lists and reaffirms the information that was previously provided to the Department that is still valid. Information related to the specific modification requests has been revised/consolidated/updated and is being resubmitted as discussed herein.

The application generally involves modifying the current permits to allow for the construction and operation of an approximately six-acre lateral expansion referred to as Cell 16. Cell 16 is proposed to be constructed with a 3-foot thick clay layer consistent with the previously constructed cells. As discussed with the Department, a separate application has been submitted concurrently to permit Pond 3 (not yet constructed) as an Industrial Wastewater (IW) pond. Based on discussions with the Department, the applicant may elect to submit a permit application to modify the designation of Pond 3 from an IW pond to a stormwater pond following closure of the landfill.

SECTION 1

APPLICATION FOR PERMIT TO CONSTRUCT, OPERATE, MODIFY, OR CLOSE A SOLID WASTE MANAGEMENT FACILITY

DEP FORM 62-701.900(1)

S-1 Letter of Authorization



Florida Department of Environmental Protection

Bob Martinez Center 2600 Blair Stone Road Tallahassee, Florida 32399-2400 DEP Form #: 62-701.900(1), F.A.C.

Form Title: Application to Construct, Operate, Modify, or Close a Solid Waste Management Facility

Effective Date: February 15, 2015

Incorporated in Rule: 62-701.330(3), F.A.C.

STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION

APPLICATION TO CONSTRUCT, OPERATE, MODIFY, OR CLOSE A SOLID WASTE MANAGEMENT FACILITY

APPLICATION INSTRUCTIONS AND FORMS

INSTRUCTIONS TO APPLY FOR A SOLID WASTE MANAGEMENT FACILITY PERMIT

I. General

Solid Waste Management Facilities shall be permitted pursuant to Section 403.707, Florida Statutes (FS) and in accordance with Florida Administrative Code (FAC) Chapter 62-701. A permit application shall be submitted in accordance with the requirements of Rule 62-701.320(5)(a), F.A.C., to the appropriate Department office having jurisdiction over the facility. The appropriate fee in accordance with Rule 62-701.315, FAC, shall be submitted with the application by check made payable to the Department of Environmental Protection (DEP).

Complete appropriate sections for the type of facility for which application is made. Entries shall be typed or printed in ink. All blanks shall be filled in or marked "Not Applicable" or "No Substantial Change". Information provided in support of the application shall be marked "Submitted" and the location of this information in the application package indicated. The application shall include all information, drawings, and reports necessary to evaluate the facility. Information required to complete the application is listed on the attached pages of this form.

II. Application Parts Required for Construction and Operation Permits

- A. Landfills and Ash Monofills Submit Parts A through S
- B. Asbestos Monofills Submit Parts A, B, C, D, E, F, I, K, M, O through S
- C. Industrial Solid Waste Disposal Facilities Submit Parts A through S

NOTE: Portions of some Parts may not be applicable.

NOTE: For facilities that have been satisfactorily constructed in accordance with their construction permit, the information required for A, B and C type facilities does not have to be resubmitted for an operation permit if the information has not substantially changed during the construction period. The appropriate portion of the form should be marked "no substantial change".

III. Application Parts Required for Closure Permits

- A. Landfills and Ash Monofills Submit Parts A, B, L, N through S
- B. Asbestos Monofills Submit Parts A, B, M, O through S
- C. Industrial Solid Waste Disposal Facilities Submit Parts A, B, L through S

NOTE: Portions of some Parts may not be applicable.

IV. Permit Renewals

The above information shall be submitted at time of permit renewal in support of the new permit. However, facility information that was submitted to the Department to support the expiring permit, and which is still valid, does not need to be re-submitted for permit renewal. Portions of the application not re-submitted shall be marked "no substantial change" on the application form.

V. Application Codes

S - Submitted

LOCATION - Physical location of information in application

N/A - Not Applicable

N/C - No Substantial Change

VI. Listing of Application Parts

PART A: GENERAL INFORMATION

PART B: DISPOSAL FACILITY GENERAL INFORMATION

PART C: PROHIBITIONS

PART D: SOLID WASTE MANAGEMENT FACILITY PERMIT REQUIREMENTS, GENERAL

PART E: LANDFILL PERMIT REQUIREMENTS

PART F: GENERAL CRITERIA FOR LANDFILLS

PART G: LANDFILL CONSTRUCTION REQUIREMENTS

PART H: HYDROGEOLOGICAL INVESTIGATION REQUIREMENTS

PART I: GEOTECHNICAL INVESTIGATION REQUIREMENTS

PART J: VERTICAL EXPANSION OF LANDFILLS

PART K: LANDFILL OPERATION REQUIREMENTS

PART L: WATER QUALITY AND LEACHATE MONITORING REQUIREMENTS

PART M: SPECIAL WASTE HANDLING REQUIREMENTS

PART N: GAS MANAGEMENT SYSTEM REQUIREMENTS

PART O: LANDFILL CLOSURE REQUIREMENTS

PART P: OTHER CLOSURE PROCEDURES

PART Q: LONG-TERM CARE

PART R: FINANCIAL ASSURANCE

PART S: CERTIFICATION BY APPLICANT AND ENGINEER OR PUBLIC OFFICER

STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION APPLICATION FOR A PERMIT TO CONSTRUCT, OPERATE, MODIFY OR CLOSE A SOLID WASTE MANAGEMENT FACILITY

Please Type or Print

PART A	A. GENERAL INFORMATION	
1.	Type of disposal facility (check all that apply): □ Class I Landfill □ Class III Landfill □ Industrial Solid Waste □ Other (describe):	□ Ash Monofill □ Asbestos Monofill
NOTE:	Waste Processing Facilities should apply on Form Yard Trash Disposal Facilities should notify on Compost Facilities should apply on Form 62-70 C D Disposal Facilities should apply on Form	Form 62-701.900(3), FAC; 09.901(1), FAC; and
2.	Type of application: ☐ Construction ☐ Operation ☐ Construction/Operation ☐ Closure ☐ Long-term Care Only	
3.	Classification of application: ☐ New ☐ Renewal	☑ Substantial Modification☐ Intermediate Modification☐ Minor Modification
4.	Facility name: Enterprise Road Class	s III Recycling and Disposal Facility
5.	DEP ID number: SWD/51/87895	County: Pasco
6.	Facility location (main entrance): The main entrance gate is on the	north side of Enterprise Road, 1.5 miles east
	C.R. 35 Alt. The address is 41111 Ente	rprise Road in Dade City, Florida 33525.
7.	Location coordinates: Section: 5 and 8 Townshi Latitude: 28 • 19 53	_{p:} <u>25 S</u> Range: <u>22 E</u> Longitude: <u>82 </u>
	Datum: NGVD 29 Coordinate	State Plane West
	Collected by: Professional Land Surveyo	Company/Affiliation: Picket Surveying and Photogrammetry

8.	Applicant name (operating authority): Angelo's Agg	gregat	e Materials, Li	td.		
	Mailing address: 855 28th St. South	St.	Petersburg	FL	33712	
	Street or P.O. Box		City	State	Zip	
	Contact person: John Arnold, P.E.		Telephone: (813)	477-1	719	
	Title: Director of Engineering Facilities					
		john	.phillip.arnold			
			E-Mail addres	s (if avai	lable)	
9.	Authorized agent/Consultant: Locklear Assoc	ciates,	Inc.			
	Mailing address: 4140 NW 37th Place, Suite			FL	32606	
	Street or P.O. Box		City	State	Zip	
	Contact person: Lisa Baker, P.E.		Telephone: $(\frac{352}{})$	672-6	8867	
	Title: Engineering Division Director					
		lisa	locklearcons	_		
			E-Mail address	(if avail	able)	
10.	Landowner (if different than applicant): Same as A	pplica	nt			
	Mailing address:					
	Street or P.O. Box		City	State	Zip	
	Contact person:		Telephone: ()			
4.4	Otto a town and accept to be accept		E-Mail addres	s (if ava	ilable)	
11.	Cities, towns, and areas to be served: Pasco County and surrounding areas					
	1 does county and surrounding areas					
12.	Population to be served:					
12.	187 588 (Pasco County 2015 Census Est)	Five-Ye		County 2	2020 Projections)	
40		Projection N/A	on		<u> </u>	
13.	Date site will be ready to be inspected for completion:					
14.	Expected life of the facility: 10+ years					
15.	Estimated costs:					
	Total Construction: N/A	_ Closing	Costs:			
16.	Anticipated construction starting and completion dates:					
	From: Ongoing	_To: <u>O</u> I	ngoing			
17.	Expected volume or weight of waste to be received:					
		s/day	gal	llons/day	<i>(</i>	

PART B. DISPOSAL FACILITY GENERAL INFORMATION

for details		III landfill. Please refeates submitted as part Idie" Martinez	of this application.
Facility site s	upervisor: Alfredo "Fred	Idie" Martinez	
			507 7070
		i eleptione. ()	567-7676
			E-Mail address (if available)
Disposal are	a: Total acres: 67.0	Used acres: 50.5	Available acres: 16.5
Weighing sca	ales used: ✓ Yes No		
Security to p	revent unauthorized use: 🗸	Yes No	
Charge for w	raste received: +/- 9.00	/yds³	/ton
Surrounding	land use, zoning:		
□ Resid	ential	□ Industrial	
☑ Agricu	ltural	□ None	
□ Comm	nercial	☐ Other (describe):	
Types of was	ste received:		
☐ House	hold	☑ C D debris	
□ Comm	nercial	☑ Shredded/cut tires	
□ Incine	rator/WTE ash		
□ Treate	ed biomedical	□ Septic tank	
□ Water	treatment sludge	□ Industrial	
□ Air tre	atment sludge	☐ Industrial sludge	
	lt. rol	□ Domestic sludge	
□ Agricu	illural	_ boiliootto sidage	
□ Agricu☑ Asbes			

9.	Salvaging permitted: Yes ✓ No					
10.	0. Attendant: ✓ Yes No Trained operator: ✓ Yes No					
11.	Trained spotters: ✓ Yes No	Number of spotters u	used: 1 - 2			
12.	Site located in: □ Floodplain Orange groves	□ Wetlands	☑ Other (describe):			
13.	Days of operation: Monday through	ı Friday, Saturday				
14.	Hours of operation: 7 am to 6 pm (M-F); 7 am - 2 pm (Sat)					
15.	Days working face covered: Once per	r week				
16.		ft. Datum Used:	NGVD 29			
17.	Number of monitoring wells: 21					
18.	Number of surface monitoring points: 0					
19.	Gas controls used: ✓ Yes No	Type controls: Acti	ive Passive			
	Gas flaring: Yes ✓ No	Gas recovery: Yes	No			
20.	Landfill unit liner type:					
	☐ Natural soils	□ Double geomemb	orane			
	☑ Single clay liner	☐ Geomembrane	composite			
	☐ Single geomembrane	□ Double composite	9			
	☐ Single composite	□ None				
	□ Slurry wall □ Other (describe):					
21.	Leachate collection method:					
	☐ Collection pipes	□ Double geomemble	brane			
	□ Geonets	☐ Gravel layer				
	□ Well points □ Interceptor trench					
	□ Perimeter ditch	□ None				
	☑ Other (describe):					
	Gravity drainage to temporary stormwater pond (Cell 14) and proposed Pond 3.					
		Pond 3 will be an industrial wastewater pond.				
	- Ond O will be all industrial was	Stowator porid.				

Leachate storage method:	
□ Tanks	☐ Surface impoundments
☐ Other (describe):	
None	
Leachate treatment method:	
☐ Oxidation	☐ Chemical treatment
□ Secondary	□ Settling
☐ Advanced	□ None
☑ Other (describe):	
As described in the IW permit appli	ication, the leachate will be treated by dilution and evaporat
Leachate disposal method:	
□ Recirculated	□ Pumped to WWTP
☐ Transported to WWTP	□ Discharged to surface water/wetland
☐ Injection well	☑ Percolation ponds
☐ Evaporation	☐ Spray irrigation
☐ Other (describe):	
A portion of the leachate will I	be disposed in a percolation pond.
For leachate discharged to surface wa	ters:
For leachate discharged to surface wa Name and Class of receiving water:	ters:
-	ters:
Name and Class of receiving water:	ters:
Name and Class of receiving water:	ters:

	Storm Water:				
	Collected: ✓ Yes No				
	Type of treatment: 100 year, 24-hour storm event retained on-site without discharge.				
	Name and Class of receiving water: None				
	Environmental Resources Permit (ERP) number or status: ERP 51-0172489-006				

PART C. PROHIBITIONS (62-701.300, FAC)

	LOCATION			
s 🗹	Section 4	N/A □	N/C □	1. Provide documentation that each of the siting criteria will be satisfied for the facility; (62-701.300(2), FAC)
s□		N/A □	N/C ☑	2. If the facility qualifies for any of the exemptions contained in Rules 62-701.300(12), (13) and (16) through (18), FAC, then document this qualification(s);
s□		N/A □	N/C ☑	3. Provide documentation that the facility will be in compliance with the burning restrictions; (62-701.300(3), FAC)
s□		N/A □	N/C ☑	4. Provide documentation that the facility will be in compliance with the hazardous waste restrictions; (62-701.300(4), FAC)
s□		N/A □	N/C ☑	5. Provide documentation that the facility will be in compliance with the PCB disposal restrictions; (62-701.300(5), FAC)
s□		N/A □	N/C ☑	6. Provide documentation that the facility will be in compliance with the biomedical waste restrictions; (62-701.300(6), FAC)
s□		N/A □	N/C ☑	7. Provide documentation that the facility will be in compliance with the Class I surface water restrictions; (62-701.300(7), FAC)
s□		N/A □	N/C ☑	8. Provide documentation that the facility will be in compliance with the special waste for landfills restrictions; (62-701.300(8), FAC)
s□		N/A □	N/C ☑	9. Provide documentation that the facility will be in compliance with the liquid restrictions; (62-701.300(10), FAC)
s□		N/A □	N/C ☑	10. Provide documentation that the facility will be in compliance with the used oil and oily waste restrictions; (62-701.300(11), FAC)
s□		N/A □	N/C ☑	11. Provide documentation that the facility will be in compliance with the CCA treated wood restrictions; (62-701.300(14), FAC)
s□		N/A □	N/C 🗹	12. Provide documentation that the facility will be in compliance with the dust control restrictions; (62-701.300(15), FAC)

PART D. SOLID WASTE MANAGEMENT FACILITY PERMIT REQUIREMENTS, GENERAL (62-701.320, FAC)

	LOCATION			
s 🗹	Section 1	N/A □	N/C □	1. A minimum of one completed electronic application form, all supporting data and reports; (62-701.320(5)(a), FAC)
s 🗹	Sections 1 3	N/A □	N/C □	2. Engineering and/or professional certification (signature, date, and seal) provided on the applications and all engineering plans, reports, and supporting information for the application; (62-701.320(6), FAC)
s 🗹	Cover Letter	N/A □	N/C □	3. A letter of transmittal to the Department; (62-701.320(7)(a), FAC)
s 🗹	Section 1	N/A □	N/C □	4. A completed application form dated and signed by the applicant; (62-701.320(7)(b), FAC)
s 🗹	Cover Letter	N/A □		5. Permit fee specified in Rule 62-701.315, FAC in check or money order, payable to the Department; (62-701.320(7)(c), FAC)
s 🗹	Section 3	N/A □	N/C □	6. An engineering report addressing the requirements of this rule and with the following format: a cover sheet, text printed on 8 inch by 11 inch consecutively numbered pages, a table of contents or index, the body of the report and all appendices including an operation plan, contingency plan, illustrative charts and graphs, records or logs of tests and investigations, engineering calculations; (62-701.320(7)(d), FAC)
s 🗹	Sec. 3, App 3-A Sec. 7	N/A □	N/C □	7. Operation Plan and Closure Plan; (62-701.320(7)(e)1, FAC)
s 🗹	Section 3, App 3-B	N/A □	N/C □	8. Contingency Plan; (62-701.320(7)(e)2, FAC)
s 🗹	Section 4	N/A □	N/C □	9. Plans or drawings for the solid waste management facilities in appropriate format (including sheet size restrictions, cover sheet, legends, north arrow, horizontal and vertical scales, elevations referenced to NGVD 1929) showing: (62-701.320(7)(f), FAC)
s□		N/A □	N/C ☑	 a. A regional map or plan with the project location in relation to majo roadways and population centers;
s 🗹	Section 4	N/A □	N/C □	b. A vicinity map or aerial photograph no more than one year old showing the facility site and relevant surface features located within 1000 feet of the facility;
s 🗹	Section 4	N/A □	N/C □	c. A site plan showing all property boundaries certified by a Florida
s 🗹	Section 4	N/A □	N/C □	Licensed Professional Surveyor and Mapper; d. Other necessary details to support the engineering report, including referencing elevations to a consistent, nationally recognized datum, and identifying the method used for collecting latitude and longitude data:

LOCATION PART D CONTINUED $S \square$ N/A \square N/C \square 10. Documentation that the applicant either owns the property or has legal authority from the property owner to use the site; (62-701.320(7)(g), FAC) N/A ☑ N/C □ s□ 11. For facilities owned or operated by a county, provide a description of how, if any, the facilities covered in this application will contribute to the county's achievement of the waste reduction and recycling goals contained in Section 403.706, FS; (62-701.320(7)(h), FAC) S \square N/A \square N/C \square 12. Provide a history and description of any enforcement actions taken by the Department against the applicant for violations of applicable statutes, rules. orders, or permit conditions relating to the operation of any solid waste management facility in the state; (62-701.320(7)(i), FAC) Section 2, Part D-2 N/A N/C 13. Proof of publication in a newspaper of general circulation of notice of application for a permit to construct or substantially modify a solid waste management facility; (62-701.320(8), FAC) Section 3, App 3-C N/A □ N/C □ 14. Provide a description of how the requirements for airport safety will be achieved, including proof of required notices if applicable. If exempt, explain how the exemption applies; (62-701.320(13), FAC) $S \square$ N/A \square N/C \square 15. Explain how the operator and spotter training requirements and special criteria will be satisfied for the facility; (62-701.320(15), FAC) LANDFILL PERMIT REQUIREMENTS (62-701.330, FAC) PART E. LOCATION Section 3, App 3-C N/A □ N/C □ s 🗹 1. Regional map or aerial photograph no more than five years old showing all airports that are located within five miles of the proposed landfill; (62-701.330(3)(a), FAC) Section 4 $_{\text{N/A}}$ $_{\text{N/C}}$ 2. Plot plan with a scale not greater than 200 feet to the inch showing: (62-701.330(3)(b), FAC) Section 4 $_{\text{N/A}}$ $_{\text{N/C}}$ $_{\text{N/C}}$ a. Dimensions: Section 5 N/A □ N/C □ b. Locations of proposed and existing water quality monitoring wells; Section 2 Part G-1 s 🗹 · N/A □ N/C □ c. Locations of soil borings; Section 4 _{N/A □ N/C □} d. Proposed plan of trenching or disposal areas; Section 4 N/A N/C N/C e. Cross sections showing original elevations and proposed final contours which shall be included either on the plot plan or on separate sheets;

LOCATION PART E CONTINUED Section 4 $_{\text{N/A}}$ $_{\text{N/C}}$ f. Any previously filled waste disposal areas: Section 4 N/A □ N/C □ g. Fencing or other measures to restrict access; Section 4 N/A N/C N 3. Topographic maps with a scale not greater than 200 feet to the inch with five foot contour intervals showing: (62-701.330(3)(c), FAC) Section 4 N/A N/C N/C a. Proposed fill areas; N/A □ N/C ☑ b. Borrow areas: Section $\underline{\mathbf{4}}_{\text{N/A}} \square \text{N/C} \square$ c. Access roads; Section 4 N/A N/C N d. Grades required for proper drainage; Section 4 N/A N/A N/C e. Cross sections of lifts; N/A ☑ N/C □ f. Special drainage devices if necessary; Section 4 N/A N/A N/C N g. Fencing; S \square ______ N/A \square N/C \square h. Equipment facilities; S \square _____ N/A \square N/C $ot \square$ 4. A report on the landfill describing the following: (62-701.330(3)(d), FAC) S \square N/A \square N/C \square a. The current and projected population and area to be served by the proposed site; S \square _____ N/A \square N/C $ot \square$ b. The anticipated type, annual quantity, and source of solid waste expressed in tons: s \boxtimes Section 4 N/A \square N/C \square c. Planned active life of the facility, the final design height of the facility, and the maximum height of the facility during its operation; S □ _____ N/A □ N/C ☑ d. The source and type of cover material used for the landfill; S \square _____ N/A \square N/C \square 5. Provide evidence that an approved laboratory shall conduct water quality monitoring for the facility in accordance with Chapter 62-160, FAC; (62-701.330(3)(g), FAC S □ _____ N/A □ N/C ☑ 6. Provide a statement of how the applicant will demonstrate financial responsibility for the closing and long-term care of the landfill; (62-

701.330(3)(h), FAC)

PART F. GENERAL CRITERIA FOR LANDFILLS (62-701.340, FAC)

	LOCATION				
s 🗹	Section 3, App 3-C			available) how the 100 year flo reduce the tem	In the landfill or solid waste disposal unit shall not be located in the landfill or solid waste disposal unit shall not be located in bodplain where it will restrict the flow of the 100 year flood, porary water storage capacity of the floodplain unless storage is provided, or result in a washout of solid waste; (62-FAC)
s 🗹	Section 4	N/A □	N/C □	in the landfill ar	w the minimum horizontal separation between waste deposits nd the landfill property boundary shall be 100 feet, measured the proposed final cover slope; (62-701.340(3)(c), FAC)
PART	G. LAND	FILL CO	NSTRUCTIO	N REQUIREME	ENTS (62-701.400, FAC)
s 🗹	LOCATION Section 3	N/A □	N/C □	units will be cor design period of factor of safety	w the landfill shall be designed so the solid waste disposal instructed and closed at planned intervals throughout the of the landfill, and shall be designed to achieve a minimum of 1.5 using peak strength values to prevent failures of side ep-seated failures; (62-701.400(2), FAC)
s 🗹	Section 2, part G-1	N/A □	N/C □	·	requirements; (62-701.400(3), FAC)
s□		N/A ☑	N/C □	a. Gen	eral construction requirements; (62-701.400(3)(a), FAC)
s□		N/A ☑	N/C □	(1)	Provide test information and documentation to ensure the liner will be constructed of materials that have appropriate physical, chemical, and mechanical properties to prevent failure;
s□		N/A ☑	N/C □	(2)	Document foundation is adequate to prevent liner failure;
s□		N/A ☑	N/C □	(3)	Constructed so bottom liner will not be adversely impacted by fluctuations of the ground water;
s□		N/A ☑	N/C □	(4)	Designed to resist hydrostatic uplift if bottom liner located below seasonal high ground water table;
s□		N/A ☑	N/C □	(5)	Installed to cover all surrounding earth which could come into contact with the waste or leachate:

LOCATION PART G CONTINUED

s 🗆	N/A ☑ N/C □	b. Co	mposite liners; (62-701.400(3)(b), FAC)
s 🗆	N/A ☑ N/C □	(1)	Upper geomembrane thickness and properties;
s□	N/A ☑ N/C □	(2)	Design leachate head for primary leachate collection and removal system (LCRS) including leachate recirculation if appropriate;
s 🗆	N/A 🗹 N/C 🗆	(3)	Design thickness in accordance with Table A and number of lifts planned for lower soil component;
s 🗆	N/A ☑ N/C □	c. Do	uble liners; (62-701.400(3)(c), FAC)
s 🗆	N/A ☑ N/C □	(1)	Upper and lower geomembrane thickness and properties;
s 🗆	N/A ☑ N/C □	(2)	Design leachate head for primary LCRS to limit the head to one foot above the liner;
s 🗆	N/A ☑ N/C □	(3)	Lower geomembrane sub-base design;
s 🗆	N/A ☑ N/C □	(4)	Leak detection and secondary leachate collection system minimum design criteria (k ≥ 10 cm/sec, head on lower liner ≤ 1 inch, head not to exceed thickness of drainage layer);
s 🗆	N/A ☑ N/C □	d. Sta	andards for geosynthetic components; (62-701.400(3)(d), FAC)
s 🗆	N/A ☑ N/C □	(1)	Factory and field seam test methods to ensure all geomembrane seams achieve the minimum specifications;
s 🗆	N/A ☑ N/C □	(2)	Geomembranes to be used shall pass a continuous spark test by the manufacturer;
s 🗆	N/A 🗹 N/C 🗆	(3)	Design of 24-inch-thick protective layer above upper geomembrane liner;
s 🗆	N/A ☑ N/C □	(4)	Describe operational plans to protect the liner and leachate collection system when placing the first layer of waste above a 24-inch-thick protective layer;
s□	N/A ☑ N/C □	(5)	HDPE geomembranes, if used, meet the specifications in GRI GM13, and LLDPE geomembranes, if used, meet the specifications in GRI GM17;
s 🗆	N/A ☑ N/C □	(6)	PVC geomembranes, if used, meet the specifications in PGI 1104;

LOCATION **PART G CONTINUED** S □ N/A ☑ N/C □ Interface shear strength testing results of the actual (7) components which will be used in the liner system; S \square _____ N/A \square N/C \square (8) Transmissivity testing results of geonets if they are used in the liner system; S \square _____ N/A $\overline{\square}$ N/C \square (9)Hydraulic conductivity testing results of geosynthetic clay liners if they are used in the liner system; S \square _____ N/A \overline{Z} N/C \square e. Geosynthetic specification requirements; (62-701.400(3)(e), FAC) S \square _____ N/A \square N/C \square Definition and qualifications of the designer, manufacturer, (1) installer, QA consultant and laboratory, and QA program; S \square _____ N/A \overline{Z} N/C \square Material specifications for geomembranes, geocomposites, (2) geotextiles, geogrids, and geonets; S \square _____ N/A \square N/C \square (3) Manufacturing and fabrication specifications including geomembrane raw material and roll QA, fabrication personnel qualifications, seaming equipment and procedures, overlaps, trial seams, destructive and nondestructive seam testing, seam testing location, frequency, procedure, sample size, and geomembrane repairs; S □ _____ N/A ☑ N/C □ (4) Geomembrane installation specifications including earthwork, conformance testing, geomembrane placement, installation personnel qualifications, field seaming and testing, overlapping and repairs, materials in contact with geomembranes, and procedures for lining system acceptance; (5) Geotextile and geogrids specifications including handling and placement, conformance testing, seams and overlaps, repair, and placement of soil materials and any overlying materials: S \square _____ N/A $\overline{\mathbb{Z}}$ N/C \square Geonet and geocomposites specifications including handling (6) and placement, conformance testing, stacking and joining, repair, and placement of soil materials and any overlying materials: S □ N/A ☑ N/C □ (7) Geosynthetic clay liner specifications including handling and

materials:

placement, conformance testing, seams and overlaps, repair, and placement of soil materials and any overlying

LOCATION **PART G CONTINUED** S \square _____ N/A $\overline{\mathbb{Z}}$ N/C \square f. Standards for soil liner components; (62-701.400(3)(f), FAC) (1) Description of construction procedures including overexcavation and backfilling to preclude structural inconsistencies and procedures for placing and compacting soil components in layers: S \square _____ N/A \overline{Z} N/C \square Demonstration of compatibility of the soil component with (2) actual or simulated leachate in accordance with EPA Test Method 9100, or an equivalent test method; S \square N/A \overline{Z} N/C \square (3) Procedures for testing in situ soils to demonstrate they meet the specifications for soil liners; S \square _____ N/A \square N/C \square (4) Specifications for soil component of liner including at a minimum: S \square N/A \overline{Z} N/C \square (a) Allowable particle size distribution, and Atterberg limits including shrinkage limit; S \square _____ N/A \square N/C \square (b) Placement moisture and dry density criteria; Maximum laboratory-determined saturated hydraulic (c) conductivity using simulated leachate; (d) Minimum thickness of soil liner; S \square _____ N/A \square N/C \square Lift thickness; (e) (f) Surface preparation (scarification); Type and percentage of clay mineral within the soil (g) component: S \square N/A \overline{Z} N/C \square (5) Procedures for constructing and using a field test section to document the desired saturated hydraulic conductivity and thickness can be achieved in the field; S □ _____ N/A ☑ N/C □ g. If a Class III landfill is to be constructed with a bottom liner system,

will be achieved:

provide a description of how the minimum requirements for the liner

LOCATION PART G CONTINUED S \square N/A \square N/C \square 3. Leachate collection and removal system (LCRS); (62-701.400(4), FAC) S \square N/A \overline{Z} N/C \square a. The primary and secondary LCRS requirements; (62-701.400(4)(a), FAC) (1) Constructed of materials chemically resistant to the waste and leachate: S \square N/A \overline{Z} N/C \square (2) Have sufficient mechanical properties to prevent collapse under pressure; S \square N/A \overline{Z} N/C \square (3) Have granular material or synthetic geotextile to prevent clogging; S \square _____ N/A \square N/C \square (4) Have a method for testing and cleaning clogged pipes or contingent designs for reducing leachate around failed areas: S \square _____ N/A \square N/C \square b. Other LCRS requirements; (62-701.400(4)(b), (c) and (d), FAC S \square _____ N/A \square N/C \square (1) Bottom 12 inches having hydraulic conductivity ≥ 1 x 10 ° cm/sec: S \square _____ N/A \square N/C \square Total thickness of 24 inches of material chemically resistant (2) to the waste and leachate: S □ _____ N/A ☑ N/C □ (3) Bottom slope design to accommodate for predicted settlement and still meet minimum slope requirements; S \square N/A \overline{Z} N/C \square (4) Demonstration that synthetic drainage material, if used, is equivalent or better than granular material in chemical compatibility, flow under load, and protection of geomembranes liner; (5) Schedule provided for routine maintenance of LCRS. S \square _____ N/A \square N/C \square 4. Leachate recirculation; (62-701.400(5), FAC) a. Describe general procedures for recirculating leachate; b. Describe procedures for controlling leachate runoff and minimizing mixing of leachate runoff with storm water;

gas buildup;

S \square _____ N/A \overline{Z} N/C \square

c. Describe procedures for preventing perched water conditions and

LOCATION PART G CONTINUED S \square N/A \overline{Z} N/C \square d. Describe alternate methods for leachate management when it cannot be recirculated due to weather or runoff conditions, surface seeps, wind-blown spray, or elevated levels of leachate head on the e. Describe methods of gas management in accordance with Rule 62-701.530, FAC; S \square N/A \square N/C \square f. If leachate irrigation is proposed, describe treatment methods and standards for leachate treatment prior to irrigation over final cover. and provide documentation that irrigation does not contribute significantly to leachate generation; S \square _____ N/A ot Z N/C \square 5. Leachate storage tanks and leachate surface impoundments; (62-701.400(6), FAC) a. Surface impoundment requirements; (62-701.400(6)(b), FAC) S \square N/A \overline{Z} N/C \square (1) Documentation that the design of the bottom liner will not be adversely impacted by fluctuations of the ground water: S \square ______ N/A \square N/C \square (2) Designed in segments to allow for inspection and repair, as needed, without interruption of service; S \square _____ N/A \overline{Z} N/C \square (3) General design requirements; S \square _____ N/A \square N/C \square (a) Double liner system consisting of an upper and lower 60-mil minimum thickness geomembrane; S \square _____ N/A \square N/C \square (b) Leak detection and collection system with hydraulic conductivity ≥ 1 cm/sec; S \square _____ N/A \square N/C \square (c) Lower geomembrane place on subbase ≥ 6 inches thick with $k \le 1 \times 10^{-5}$ cm/sec or on an approved geosynthetic clay liner with $k \le 1 \times 10^{-7}$ cm/sec; S □ _____ N/A ☑ N/C □ (d) Design calculation to predict potential leakage through the upper liner; S \square _____ N/A \overline{Z} N/C \square (e) Daily inspection requirements, and notification and corrective action requirements if leakage rates exceed that predicted by design calculations; S \square N/A \overline{Z} N/C \square (4) Description of procedures to prevent uplift, if applicable;

LOCATION **PART G CONTINUED** S □ N/A ☑ N/C □ (5) Design calculations to demonstrate minimum two feet of freeboard will be maintained; S □ N/A ☑ N/C □ (6) Procedures for controlling vectors and off-site odors; S □ N/A ☑ N/C □ b. Above-ground leachate storage tanks; (62-701.400(6)(c), FAC) S \square _____ N/A \overline{Z} N/C \square (1) Describe tank materials of construction and ensure foundation is sufficient to support tank; (2) Describe procedures for cathodic protection for the tank, if needed: S □ _____ N/A ☑ N/C □ (3) Describe exterior painting and interior lining of the tank to protect it from the weather and the leachate stored; S □ N/A ☑ N/C □ (4) Describe secondary containment design to ensure adequate capacity will be provided and compatibility of materials of construction; S \square N/A \overline{Z} N/C \square (5) Describe design to remove and dispose of stormwater from the secondary containment system; S □ N/A ☑ N/C □ (6) Describe an overfill prevention system, such as level sensors, gauges, alarms, and shutoff controls to prevent overfilling; S \square _____ N/A \square N/C \square (7) Inspections, corrective action, and reporting requirements; (a) Weekly inspection of overfill prevention system; Weekly inspection of exposed tank exteriors; (b) S \square _____ N/A $\overline{\square}$ N/C \square (c) Inspection of tank interiors when tank is drained, or at least every three years; Procedures for immediate corrective action if failures (d) detected:

(e)

S \square _____ N/A \square N/C \square

S \square N/A \square N/C \square

Inspection reports available for Department review;

c. Underground leachate storage tanks; (62-701.400(6)(d), FAC)

PART G CONTINUED LOCATION S \square _____ N/A $\overline{\mathbb{Z}}$ N/C \square (1) Describe materials of construction; A double-walled tank design system to be used with the (2) following requirements: S □ N/A ☑ N/C □ (a) Interstitial space monitoring at least weekly; S \square _____ N/A \overline{Z} N/C \square (b) Corrosion protection provided for primary tank interior and external surface of outer shell: (c) Interior tank coatings compatible with stored leachate: S □ _____ N/A ☑ N/C □ Cathodic protection inspected weekly and repaired (d) as needed: S □ N/A ☑ N/C □ (3)Describe an overfill prevention system, such as level sensors, gauges, alarms, and shutoff controls to prevent overfilling, and provide for weekly inspections; S □ _____ N/A ☑ N/C □ (4) Inspection reports available for Department review; 6. Liner systems construction quality assurance (CQA); (62-701.400(7), FAC) S \square _____ N/A \square N/C \square a. Provide CQA Plan including: S \square _____ N/A \square N/C \square Specifications and construction requirements for liner (1) system; S \square N/A \overline{Z} N/C \square (2) Detailed description of quality control testing procedures and frequencies: S \square N/A \overline{Z} N/C \square Identification of supervising professional engineer; (3) S □ _____ N/A ☑ N/C □ (4) Identify responsibility and authority of all appropriate organizations and key personnel involved in the construction project;

(5)

support personnel;

State qualifications of CQA professional engineer and

LOCATION PART G CONTINUED S □ N/A ☑ N/C □ (6) Description of CQA reporting forms and documents; S □ N/A ☑ N/C □ b. An independent laboratory experienced in the testing of geosynthetics to perform required testing; S □ N/A ☑ N/C □ 7. Soil liner CQA; (62-701.400(8), FAC) S \square _____ N/A \overline{Z} N/C \square a. Documentation that an adequate borrow source has been located with test results, or description of the field exploration and laboratory testing program to define a suitable borrow source; b. Description of field test section construction and test methods to be implemented prior to liner installation; S \square N/A \square N/C \square c. Description of field test methods, including rejection criteria and corrective measures to insure proper liner installation; S \square N/A \overline{Z} N/C \square 8. For surface water management systems at aboveground disposal units, provide documentation showing the design of any features intended to convey stormwater to a permitted or exempted treatment system; (62-701.400(9), FAC) S \square _____ N/A \overline{Z} N/C \square 9. Gas control systems; (62-701.400(10), FAC) S \square N/A \square N/C \square a. Provide documentation that if the landfill is receiving degradable wastes, it will have a gas control system complying with the requirements of Rule 62-701.530, FAC; S \square N/A \square N/C \square 10. For landfills designed in ground water, provide documentation that the landfill will provide a degree of protection equivalent to landfills designed with bottom liners not in contact with ground water; (62-701.400(11), FAC) HYDROGEOLOGICAL INVESTIGATION REQUIREMENTS (62-701.410(2), FAC) PART H. LOCATION Section 2 Part G-1 N/A N/C 1. Submit a hydrogeological investigation and site report including at least the following information: Section 2 Part G-1 _____ N/A 🗌 N/C 🗌 s 🗹 a. Regional and site specific geology and hydrology; Section 2 Part G-1 N/A N/C s 🗸 b. Direction and rate of ground water and surface water flow including seasonal variations;

LOCATION PART H CONTINUED Section 2 Part G-1 s 🗸 N/A □ N/C □ c. Background quality of ground water and surface water; Section 2 Part G-1 _____ N/A 🗌 N/C 🗌 s 🗸 d. Any on-site hydraulic connections between aquifers; Section 2 Part G-1 _____ N/A 🗆 N/C 🗆 s 🗹 e. Site stratigraphy and aquifer characteristics for confining layers, semi-confining layers, and all aguifers below the site that may be affected by the disposal facility; Section 2 Part G-1 _____ N/A □ N/C □ f. Description of topography, soil types, and surface water drainage systems; Section 3 Appendix 3-C _____ N/A 🗆 N/C 🗆 g. Inventory of all public and private water wells within a one mile radius of the site including, where available, well top of casing and bottom elevations, name of owner, age and usage of each well, stratigraphic unit screened, well construction technique, and static water level: S \square N/A \square N/C $\overline{\square}$ h. Identify and locate any existing contaminated areas on the site: Section 3, App 3-C N/A N/C s 🔽 i. Include a map showing the locations of all potable wells within 500 feet of the waste storage and disposal areas; Section 2 Part G-1 _____ N/A \square N/C \square 2. Report signed, sealed, and dated by P.E. and/or P.G. PART I. GEOTECHNICAL INVESTIGATION REQUIREMENTS (62-701.410(3) and (4), FAC) **LOCATION** Section 2 Part I-1 N/A N/C 1. Submit a geotechnical site investigation report defining the engineering properties of the site including at least the following: Section 2 Part I-1 _____ N/A 🗌 N/C 🗌 s 🗹 a. Description of subsurface conditions including soil stratigraphy and ground water table conditions: Section 2 Part I-1 N/A N/C b. Investigate for the presence of muck, previously filled areas, soft ground, and lineaments; Section 2 Part I-1 _____ N/A 🗌 N/C 🗆 c. Estimates of average and maximum high water table across the site: Section 2 Part I-1 _____ N/A 🗌 N/C 🗌 s 🗹 d. Evaluation of potential for fault areas and seismic impact zones; Section 2 Part I-2 _____ N/A □ N/C □ s 🗹 e. Foundation analysis including:

LOCATION PART I CONTINUED Section 2 Part I-2 N/A □ N/C □ s 🗸 (1) Foundation bearing capacity analysis; Section 2 Part I-2 N/A N/C s 🗸 (2) Total and differential subgrade settlement analysis; Section 2 Part I-2 _____ N/A 🗆 N/C 🗆 Slope stability analysis; (3) Section 2 Part I-1 N/A N/C s 🗹 f. Evaluation of potential for sinkholes and sinkhole activity at the site that is based upon the investigations required in Rule 62-701.410(3)(f), F.A.C.; S \square ______ N/A \square N/C \square g. A geotechnical report providing a description of methods used in the investigation, and includes soil boring logs, laboratory results, analytical calculations, cross sections, interpretations, conclusions, and a description of any engineering measures proposed for the site: Sec. 2 Part G-1 I-2 N/A N/C 2. Report signed, sealed, and dated by P.E. and/or P.G. PART J. **VERTICAL EXPANSION OF LANDFILLS** (62-701.430, FAC) **LOCATION** S \square N/A \square N/C \square 1. Describe how the vertical expansion shall not cause or contribute to any violations of water quality standards or criteria, shall not cause objectionable odors, or adversely affect the closure design of the existing landfill; S \square _____ N/A \overline{Z} N/C \square 2. Describe how the vertical expansion over unlined landfills will meet the requirements of Rule 62-701.400, FAC with the exceptions of Rule 62-701.430(1)(c), FAC; S \square _____ N/A ot Z N/C \square 3. Provide foundation and settlement analysis for the vertical expansion; S \square _____ N/A \overline{Z} N/C \square 4. Provide total settlement calculations demonstrating that the final elevations of the lining system, gravity drainage, and no other component of the design will be adversely affected; S \square N/A \overline{Z} N/C \square 5. Minimum stability factor of safety of 1.5 for the lining system component interface stability and for deep stability; 6. Provide documentation to show the surface water management system will not be adversely affected by the vertical expansion; S \square N/A \overline{Z} N/C \square 7. Provide gas control designs to prevent accumulation of gas under the new liner for the vertical expansion;

PART K. LANDFILL OPERATION REQUIREMENTS (62-701.500, FAC)

	LOCATION			
s□		N/A □	N/C ☑	1. Provide documentation that the landfill will have at least one trained operator during operation and at least one trained spotter at each working face; (62-701.500(1), FAC)
s 🗹	Section 3, App 3-A	N/A □	N/C □	2. Provide a landfill operation plan including procedures for: (62-701.500(2), FAC)
s□		N/A □	N/C ☑	a. Designating responsible operating and maintenance personnel;
s□		N/A □	N/C ☑	b. Emergency preparedness and response, as required in subsection 62-701.320(16), FAC;
s□		N/A □	N/C ☑	c. Controlling types of waste received at the landfill;
s□		N/A □	N/C ☑	d. Weighing incoming waste;
s□		N/A □	N/C ☑	e. Vehicle traffic control and unloading;
s 🗹	Section 3, App 3-A	N/A □	N/C □	f. Method and sequence of filling waste;
s□		N/A □	N/C ☑	g. Waste compaction and application of cover;
s 🗹	Section 3, App 3-A			h. Operations of gas, leachate, and stormwater controls;
s 🗹	Section 5	N/A □	N/C □	i. Water quality monitoring;
s□		N/A ☑	N/C □	j. Maintaining and cleaning the leachate collection system;
s□		N/A □	N/C ☑	3. Provide a description of the landfill operation record to be used at the landfill, details as to location of where various operational records will be kep (i.e. DEP permit, engineering drawings, water quality records, etc.); (62-701.500(3), FAC)
s□		N/A □	N/C ☑	4. Describe the waste records that will be compiled monthly and provided to the Department annually; (62-701.500(4), FAC)
s□		N/A □	N/C ☑	5. Describe methods of access control; (62-701.500(5), FAC)
s□		N/A □	N/C ☑	6. Describe load checking program to be implemented at the landfill to discourage disposal of unauthorized waste at the landfill; (62-701.500(6), FAC)

LOCATION PART K CONTINUED S \square N/A \square N/C \square 7. Describe procedures for spreading and compacting waste at the landfill that include: (62-701.500(7), FAC) S \square N/A \square N/C \square a. Waste layer thickness and compaction frequencies; S □ N/A ☑ N/C □ b. Special considerations for first layer of waste placed above the liner and leachate collection system; c. Slopes of cell working face and side grades above land surface, and planned lift depths during operation; d. Maximum width of working face; e. Description of type of initial cover to be used at the facility that controls: S \square _____ N/A \square N/C $ot
\square$ (1) Vector breeding/animal attraction: S \square N/A \square N/C \square (2) Fires: S \square _____ N/A \square N/C \square (3) Odors: S \square _____ N/A \square N/C \square (4) Blowing litter; (5) Moisture infiltration; S \square N/A \square N/C $\overline{\square}$ f. Procedures for applying initial cover, including minimum cover frequencies; S \square _____ N/A \square N/C \square g. Procedures for applying intermediate cover; h. Time frames for applying final cover; i. Procedures for controlling scavenging and salvaging; S \square _____ N/A \square N/C \square j. Description of litter policing methods;

k. Erosion control procedures;

S \square _____ N/A \square N/C \square

LOCATION PART K CONTINUED S \square N/A \square N/C \square 8. Describe operational procedures for leachate management including: (62-701.500(8), FAC) S \square N/A \square N/C \square a. Leachate level monitoring; S □ N/A ☑ N/C □ b. Operation and maintenance of leachate collection and removal system, and treatment as required; S \square N/A \overline{Z} N/C \square c. Procedures for managing leachate if it becomes regulated as a hazardous waste: d. Identification of treatment or disposal facilities that may be used for off-site discharge and treatment of leachate; S \square N/A \overline{Z} N/C \square e. Contingency plan for managing leachate during emergencies or equipment problems; S \square N/A \overline{Z} N/C \square f. Procedures for recording quantities of leachate generated in gal/day and including this in the operating record; S \square N/A \overline{Z} N/C \square g. Procedures for comparing precipitation experienced at the landfill with leachate generation rates and including this information in the operating record; S \square N/A \square N/C \square h. Procedures for water pressure cleaning or video inspecting leachate collection systems: S □ N/A ☑ N/C □ 9. Describe how the landfill receiving degradable wastes shall implement a gas management system meeting the requirements of Rule 62-701.530, FAC; (62-701.500(9), FAC) Section 3, App 3-A N/A N/C 10. Describe procedures for operating and maintaining the landfill stormwater management system to comply with the requirements of Rule 62-701.400(9), FAC; (62-701.500(10), FAC) 11. Equipment and operation feature requirements; (62-701.500(11), FAC) S \square _____ N/A \square N/C $ot
\square$ a. Sufficient equipment for excavating, spreading, compacting, and covering waste;

b. Reserve equipment or arrangements to obtain additional

equipment within 24 hours of breakdown;

c. Communications equipment;

S \square _____ N/A \square N/C $ot
\square$

PART K CONTINUED LOCATION S \square N/A \square N/C ot Zd. Dust control methods; S \square N/A \square N/C $\not\square$ e. Fire protection capabilities and procedures for notifying local fire department authorities in emergencies; S \square N/A \square N/C \square f. Litter control devices; S \square _____ N/A \square N/C $ot
\square$ g. Signs indicating operating authority, traffic flow, hours of operation, and disposal restrictions; 12. Provide a description of all-weather access road, inside perimeter road, and other on-site roads necessary for access at the landfill; (62-701.500(12), FAC) S \square N/A \square N/C \square 13. Additional record keeping and reporting requirements; (62-701.500(13), FAC) S \square N/A \square N/C $\overline{\square}$ a. Records used for developing permit applications and supplemental information maintained for the design period of the landfill; S \square N/A \square N/C \square b. Monitoring information, calibration and maintenance records, and copies of reports required by permit maintained for at least 10 years; S \square N/A \square N/C \square c. Maintain annual estimates of the remaining life of constructed landfills, and of other permitted areas not yet constructed, and submit this estimate annually to the Department; S \square N/A \square N/C \square d. Procedures for archiving and retrieving records which are more than five years old; PART L. WATER QUALITY MONITORING REQUIREMENTS (62-701.510, FAC) LOCATION s \square Section 5 N/A \square N/C \square 1. A water quality monitoring plan shall be submitted describing the proposed ground water and surface water monitoring systems, and shall meet at least the following requirements: s \square Section 5 N/A \square N/C \square a. Based on the information obtained in the hydrogeological investigation and signed, dated, and sealed by the P.G. or P.E. who prepared it; (62-701.510(2)(a), FAC)

	LOCATION				PART L CONTINUED
s 🗹	Section 5	N/A □	N/C □		ampling and analysis performed in accordance with Chapter FAC; (62-701.510(2)(b), FAC)
s 🗹	Section 5	N/A □	N/C □	c. Grou	nd water monitoring requirements; (62-701.510(3), FAC)
s 🗹	Section 5	N/A □	N/C □	(1)	Detection wells located downgradient from and within 50 feet of disposal units;
s 🗹	Section 5	N/A □	N/C □	(2)	Downgradient compliance wells as required;
s 🗹	Section 5	N/A □	N/C □	(3)	Background wells screened in all aquifers below the landfill that may be affected by the landfill;
s 🗹	Section 5	N/A □	N/C □	(4)	Location information for each monitoring well;
s 🗹	Section 5	N/A □	N/C □	(5)	Well spacing no greater than 500 feet apart for downgradient wells and no greater than 1500 feet apart for upgradient wells, unless site specific conditions justify alternate well spacings;
s 🗹	Section 5	N/A □	N/C □	(6)	Properly selected well screen locations;
s 🗹	Section 5			(7)	Monitoring wells constructed to provide representative ground water samples;
s□		N/A □	N/C ☑	(8)	Procedures for properly abandoning monitoring wells;
s□		N/A □	N/C ☑	(9)	Detailed description of detection sensors, if proposed;
s□		N/A □	N/C ☑	d. Surfa	ace water monitoring requirements; (62-701.510(4), FAC)
s□		N/A □	N/C ☑	(1)	Location of and justification for all proposed surface water monitoring points;
s□				(2)	Each monitoring location to be marked and its position determined by a registered Florida land surveyor;
s 🗹	Section 5	N/A □	N/C □		and routine sampling frequency and requirements; (62-0(5), FAC)
s□		N/A □	N/C ☑	(1)	Initial background ground water and surface water sampling and analysis requirements;

	LOCATION					PART L CONTINUED
s 🗹	Section 5	N/A □	N/C □		(2)	Routine monitoring well sampling and analysis requirements
s□					(3)	Routine surface water sampling and analysis requirements;
s 🗹	Section 5				prevent	ribe procedures for implementing evaluation monitoring, ion measures, and corrective action as required; (62-0(6), FAC)
s 🗹	Section 5				g. Wate FAC)	er quality monitoring report requirements; (62-701.510(8),
s 🗹	Section 5				(1)	Semi-annual report requirements; (see paragraphs 62-701.510(5)(c) and (d), FAC for sampling frequencies)
s 🗹	Section 5				(2)	Documentation that the water quality data shall be provided to the Department in an electronic format consistent with requirements for importing into Department databases, unless an alternate form of submittal is specified in the permit;
s 🗹	Section 5	N/A □	N/C □		(3)	Two and one-half year, or annual, report requirements, or every five years if in long-term care, signed dated, and sealed by P.G. or P.E.;
PART	M. SPECI	AL WAS	TE HANDLI	NG REC	QUIREM	ENTS (62-701.520, FAC)
	LOCATION					
s□		N/A ☑	N/C □	1. Desc	cribe prod	cedures for managing motor vehicles; (62-701.520(1), FAC)
s□		N/A ☑	N/C □	2. Desc	cribe prod	cedures for landfilling shredded waste; (62-701.520(2), FAC)
s□		N/A □	N/C ☑	3. Desc	cribe prod	cedures for asbestos waste disposal; (62-701.520(3), FAC)
s□		N/A ☑	N/C □		cribe prod 1.520(4),	cedures for disposal or management of contaminated soil; FAC)
s□		N/A ☑	N/C □	5. Desc FAC)	cribe prod	cedures for disposal of biological wastes; (62-701.520(5),

PART N. GAS MANAGEMENT SYSTEM REQUIREMENTS (62-701.530, FAC)

	<u>LOCATION</u>			
s 🗹	Section 3	N/A □	N/C □	1. Provide documentation for a gas management system that will: (62-701.530(1), FAC)
s□		N/A □	N/C ☑	 a. Be designed to prevent concentrations of combustible gases from exceeding 25% the LEL in structures and 100% the LEL at the property boundary;
s□		N/A □	N/C ☑	b. Be designed for site specific conditions;
s□		N/A □	N/C ☑	c. Be designed to reduce gas pressure in the interior of the landfill;
s□				d. Be designed to not interfere with the liner, leachate control system, or final cover;
s 🗹	Section 3	N/A □	N/C □	2. Provide documentation that will describe locations, construction details, and procedures for monitoring gas at ambient monitoring points and with soil monitoring probes; (62-701.530(2), FAC)
s□		N/A □	N/C ☑	3. Provide documentation describing how the gas remediation plan and odor remediation plan will be implemented; (62-701.530(3), FAC)
s□		N/A ☑	N/C □	4. Landfill gas recovery facilities; (62-701.530(5), FAC)
s□		N/A 🗹	N/C □	a. Provide information required in Rules 62-701.320(7) and 62-701.330(3), FAC;
s□		N/A ☑	N/C □	b. Provide information required in Rule 62-701.600(4), FAC, where relevant and practical;
s□		N/A 🗹	N/C □	c. Provide estimates of current and expected gas generation rates and description of condensate disposal methods;
s□		N/A 🗹	N/C □	d. Provide description of procedures for condensate sampling, analyzing, and data reporting;
s□		N/A ☑	N/C □	e. Provide closure plan describing methods to control gas after recovery facility ceases operation, and any other requirements contained in Rule 62-701.400(10), FAC;

PART O. LANDFILL FINAL CLOSURE REQUIREMENTS (62-701.600, FAC)

	LOCATION					
s 🗹	Section 7	N/A □	N/C □	1. Closi	ure perm	nit requirements; (62-701.600(2), FAC)
s 🗹	Section 7	N/A □	N/C □			cation submitted to the Department at least 90 days prior to ceipt of wastes;
s 🗹	Section 7	N/A □	N/C □		b. Closu	ure plan shall include the following:
s 🗹	Section 7	N/A □	N/C □		(1)	Closure design plan;
s 🗹	Section 7	N/A □	N/C □		(2)	Closure operation plan;
s 🗹	Section 7	N/A □	N/C □		(3)	Plan for long-term care;
s 🗹	Section 7, App. 7-A	N/A □	N/C □		(4)	A demonstration that proof of financial assurance for long- term care will be provided;
s 🗹	Section 4	N/A □	N/C □	2. Closi FAC)	ure desiç	gn plan including the following requirements: (62-701.600(3),
s 🗹	Section 4	N/A □	N/C □		a. Plan	sheet showing phases of site closing;
s 🗹	Section 4	N/A □	N/C □		b. Draw	rings showing existing topography and proposed final grades;
s 🗹	Section 4	N/A □	N/C □		c. Provi	sions to close units when they reach approved design ions;
s 🗹	Section 4	N/A □	N/C □		d. Final	elevations before settlement;
s 🗹	Section 4	N/A □	N/C □		drainag	slope design including benches, terraces, down slope e ways, energy dissipaters, and description of expected ation effects;
s□		N/A □	N/C ☑			cover installation plans including:
s□		N/A □	N/C ☑		(1)	CQA plan for installing and testing final cover;
s□		N/A □	N/C ☑		(2)	Schedule for installing final cover after final receipt of waste;
s□		N/A □	N/C ☑		(3)	Description of drought resistant species to be used in the vegetative cover:

PART O CONTINUED LOCATION Section 4 $_{\text{N/A}}$ $_{\text{N/C}}$ (4) Top gradient design to maximize runoff and minimize erosion: S \square N/A \square N/C \square Provisions for cover material to be used for final cover (5) maintenance: Section 4 $_{_{\rm N/A}\;\square}$ $_{_{\rm N/C}\;\square}$ g. Final cover design requirements; Section $\underline{\mathbf{4}}_{\text{N/A}\ \square}$ N/C \square (1) Protective soil layer design; Section 4 N/A \square N/C \square Barrier soil layer design; (2)Section 4 N/A N/C N/C (3) Erosion control vegetation; _____ N/A 🗹 N/C 🗆 (4) Geomembrane barrier layer design; Geosynthetic clay liner design, if used; (5) S 🗹 Section 2 Part I-2 N/A 🗆 N/C 🗆 (6) Stability analysis of the cover system and the disposed waste: Section 3, App 3-A N/A N/C h. Proposed method of stormwater control; S \square _____ N/A \square N/C $ot
\square$ i. Proposed method of access control; S \square _____ N/A \square N/C $ot
\square$ j. Description of the proposed or existing gas management system which complies with Rule 62-701.530, FAC; S \square _____ N/A \square N/C \square 3. Closure operation plan shall include: (62-701.600(4), FAC) S \square _____ N/A \square N/C $ot
\square$ a. Detailed description of actions which will be taken to close the landfill: S \square _____ N/A \square N/C $ot
\square$ b. Time schedule for completion of closing and long-term care; c. Describe proposed method for demonstrating financial assurance for long-term care; S \square _____ N/A \square N/C \square d. Operation of the water quality monitoring plan required in Rule 62-701.510, FAC; e. Development and implementation of gas management system

required in Rule 62-701.530, FAC;

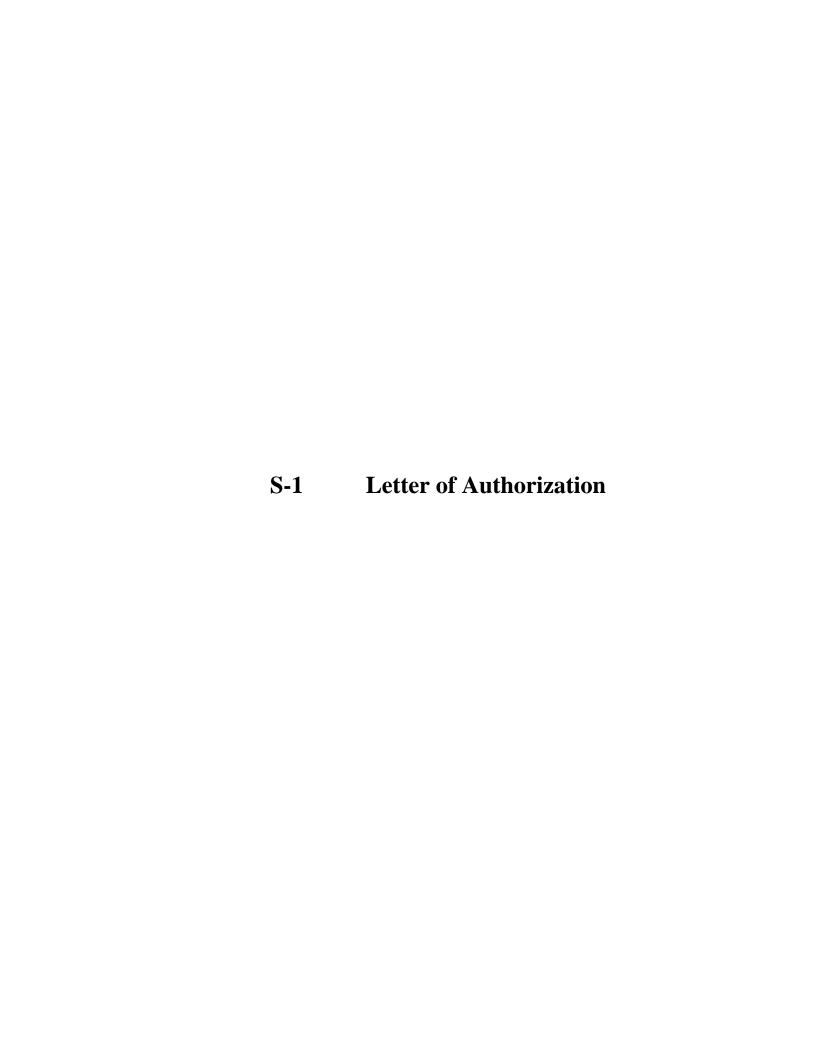
PART O CONTINUED LOCATION S \square N/A \square N/C \square 4. Certification of closure construction completion and final reports including: (62-701.600(6), FAC) S \square _____ N/A \square N/C $ot
\square$ a. Survey monuments; (62-701.600(6)(a), FAC) b. Final survey report; (62-701.600(6)(b), FAC) S \square _____ N/A \square N/C $ot
\square$ c. Closure construction quality assurance report; (62-701.400(7), FAC) S □ _____ N/A □ N/C ☑ 5. Declaration to the public; (62-701.600(7), FAC) 6. Official date of closing; (62-701.600(8), FAC) 7. Justification for and detailed description of procedures to be followed for temporary closure of the landfill, if desired; (62-701.600(9), FAC) PART P. OTHER CLOSURE PROCEDURES (62-701.610, FAC) **LOCATION** 1. Describe how the requirements for use of closed solid waste disposal areas will be achieved; (62-701.610(1), FAC) S \square N/A \square N/C \square 2. Describe how the requirements for relocation of wastes will be achieved; (62-701.610(2), FAC) PART Q. **LONG-TERM CARE** (62-701.620, FAC) LOCATION S \square _____ N/A \square N/C $ot
\square$ 1. Maintaining the gas collection and monitoring system; (62-701.620(5), FAC) S \square _____ N/A \square N/C $ot
\square$ 2. Stabilization report requirements; (62-701.620(6), FAC) S \square _____ N/A \square N/C $ot
\square$ 3. Right of access; (62-701.620(7), FAC) S \square N/A \square N/C \square 4. Requirements for replacement of monitoring devices; (62-701.620(8), FAC) S \square _____ N/A \square N/C \square 5. Completion of long-term care signed and sealed by professional engineer; (62-701.620(9), FAC)

PART R. FINANCIAL ASSURANCE (62-701.630, FAC)

	LOCATION		
s 🗹	Section 7, App 7-A	N/A □ N/C □	1. Provide cost estimates for closing, long-term care, and corrective action costs estimated by a P.E. for a third party performing the work, on a per unit basis, with the source of estimates indicated; (62-701.630(3) (7), FAC)
s□		N/A □ N/C ☑	2. Describe procedures for providing annual cost adjustments to the Department based on inflation and changes in the closing, long-term care, and corrective action plans; (62-701.630(4) (8), FAC)
s□		N/A □ N/C ☑	3. Describe funding mechanisms for providing proof of financial assurance and include appropriate financial assurance forms. (62-701.630(5), (6), (9) FAC)

PART S. CERTIFICATION BY APPLICANT AND ENGINEER OR PUBLIC OFFICER

	ative of Angelos Aggregate Materials, LTI
	nat statements made in this form and attached inform
Protection, and certifies that the information in this a his/her knowledge and belief. Further, the undersig Florida Statutes, and all rules and regulations of the	permit from the Florida Department of Environme application is true, correct, and complete to the best of ned agrees to comply with the provisions of Chapter Department. It is understood that the Permit is not for to the sale or legal transfer of the permitted facility 855 28th Street South
Signature of Applicant or Agent	Mailing Address
John Arnold, P.E., Director of Engineering Facilities	St. Petersburg, FL 33712
Name and Title (please type)	City, State, Zip Code
John.Phillip.Arnold gmail.com	(813) 477-1719
E-Mail Address (if available)	Telephone Number
	Date:
Troiscolorial Engineer regional art terraa (e a.z.	ic Officer if authorized under Sections 403.707 and
403.7075, Florida Statutes):	ic Officer if authorized under Sections 403.707 and
403.7075, Florida Statutes): This is to certify that the engineering features of this designed/examined by me and found to conform to professional judgment, this facility, when properly me	s solid waste management facility have been engineering principles applicable to such facilities. In taintained and operated, will comply with all applicabe artment. It is agreed that the undersigned will providuance and operation of the facility.
This is to certify that the engineering features of this designed/examined by me and found to conform to professional judgment, this facility, when properly m statutes of the State of Florida and rules of the Department with a set of instructions of proper mainter	s solid waste management facility have been engineering principles applicable to such facilities. In taintained and operated, will comply with all applicabe artment. It is agreed that the undersigned will provid
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June 19, 2013

Dominic Iafrate, Vice President Angelo's Aggregate Materials, LLC 855 28th Street South St. Petersburg, FL 33712

RE:

Angelo's Aggregate Materials, LLC (d/b/a Angelo's Recycled Materials)
Agent Authorization

To Whom It May Concern,

Mr. John Arnold, P.E. is authorized by Angelo's Aggregate Materials, LLC to act on its behalf for all matters related to our existing and contemplated facilities in the state of Florida. Such authorization includes permitting, construction, operations, closure activities, and dealings as may be necessary in the pursuit of Angelo's Aggregate Materials, LLC interests. This authorization shall remain in effect until rescinded in writing by an authorized agent of Angelo's Aggregate Materials, LLC.

Sincerely,

Dominic Infrate, Vice President Angelo's Aggregate Materials, LLC

Witness Signature:

Witness Name (printed): NEIRO DE RUBEIS

Date: 6/20/2013

July 25, 2014

Angelo's Aggregate Materials, LLC John Arnold, P.E. 41111 Enterprise Road Dade City, FL 33525

RE: Engineer of Record Authorization

To Whom It May Concern,

Locklear and Associates, Inc. is authorized to act as the engineer of record on behalf of Angelo's Aggregate Materials, LLC for solid waste facilities located at 41111 Enterprise Road, Dade City, FL 33525. This authorization shall remain in effect until rescinded in writing by an authorized agent of Angelo's Aggregate Materials, LLC.

Sincerely,

John Arnold, P.E.

Manager

Angelo's Aggregate Materials, LLC

Witness Signature:

Witness Name (printed): 31

Date: 7/25/14

SECTION 2

CHECKLIST SUPPORT

PART D D-2 Proof of Publication

PART G G-1 Liner System Requirements

Evaluation

PART I I-1 Universal Engineering Sciences

Report

I-2 Slope Stability Analysis

PART D D-2 Proof of Publication

TO BE PUBLISHED IN A LOCAL NEWSPAPER OF GENERAL CIRCULATION UPON RECEIPT OF NOTIFICATION FROM THE DEPARTMENT TO PUBLISH NOTIFICATION.

PART G G-1 Liner System Requirements Evaluation

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY LINER SYSTEM REQUIREMENTS STUDY REPORT

Prepared for:

ANGELO'S AGGREGATE MATERIALS, LTD.

855 28th Street South St. Petersburg, Florida 33712

Presented to:

FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION SOUTHWEST DISTRICT – SOLID WASTE DIVISION

13051 N. Telecom Parkway Temple Terrace, Florida 33637

Prepared by:

LOCKLEAR AND ASSOCIATES, INC.

4140 NW 37th Place, Suite A Gainesville, Florida 32606 Certificate of Authorization #30066

Project No.: 02000-144-15

March 2016
Revised July 2016 (RAI 1 Response)

John D. Locklear, P.G. Florida License Number 2467

7/31/16

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1.0 INTRODUCTION

Angelo's Aggregate Materials, Ltd. (Applicant) operates the Enterprise Road Class III Landfill in accordance with Florida Department of Environmental Protection (FDEP) operation permit 177982-022-SO and construction permit 177982-021-SC. The Applicant desires to expand the disposal footprint laterally to the north of the existing disposal cells and is seeking a determination from FDEP regarding specific construction requirements. The initial lateral expansion will be limited to Cell 16 as shown in Figure 1.

Rule 62-701.400(3)(g) of the Florida Administrative Code (F.A.C.) reads as follows:

A Class III landfill shall be constructed with a bottom liner consisting of a single 60-mil minimum average thickness HDPE geomembrane. In the sumps located inside the landfill footprint and in the leachate collection trenches, the geomembrane shall be placed on a GCL with a hydraulic conductivity of less than or equal to 1×10^{-7} cm/sec, or on a compacted clay liner which is a minimum six inches thick with a saturated hydraulic conductivity of less than or equal to 1×10^{-7} cm/sec. The liner shall be placed on a prepared subgrade that will not damage the geomembrane liner or the GCL. A primary leachate collection and removal system and a drainage layer shall be installed above the geomembrane liner. Except in sumps and leachate collection trenches, the system shall be designed to limit leachate head above the liner during routine landfill operation after placement of initial cover to no greater than 12 inches. An applicant may request exemption from the requirements of this paragraph in accordance with paragraph 62-701.340(2)(b), F.A.C.

Rule 62-701.340(2)(b), F.A.C. reads as follows:

Class III landfills are those which receive only Class III waste. The Department shall exempt Class III landfills from some or all of the requirements for liners, leachate controls, and water quality monitoring in subsections 62-701.400(3) and (4), and Rule 62-701.510, F.A.C., if the applicant demonstrates that no significant threat to the environment will result from the exemption based upon the types of waste received, methods for controlling types of waste disposed of, and the results of the hydrogeological and geotechnical investigations required in Rule 62-701.410, F.A.C. Such a demonstration must include a CCA treated wood management plan as described in subsection 62-701.730(20), F.A.C., if the landfill will not have a constructed liner system.

The applicant is seeking a partial exemption from the bottom liner and leachate collection requirements of Rule 62-701.400(3)(g), F.A.C. as allowed by Rule 62-701.340(2)(b), F.A.C. for the proposed lateral expansion referred to as Cell 16 (the applicant understands that additional geotechnical data will be required to evaluate the applicability of the exemption for future cells 13 and 14). Specifically, in lieu of the single HDPE geomembrane and leachate collection system, the applicant proposes to construct a compacted clay layer with a minimum thickness of three feet and a saturated hydraulic conductivity of less than or equal to 1×10^{-7} cm/sec (note that this is the average value of the existing clay layer which ranges from 1×10^{-6} cm/sec to 1×10^{-8} cm/sec). Leachate that reaches the clay layer will be conveyed to Pond 3 (not constructed yet), which will be an industrial wastewater pond permitted with the FDEP.

The requested partial exemption is consistent with the existing approved and constructed system at the facility. Therefore, it is contingent upon the applicant to demonstrate the in-place infrastructure and operating procedures have not resulted in

environmental impacts and, as such, extending the same infrastructure and operating procedures to the proposed Cell 16 expansion would not be expected to be a significant threat to the environment.

The information provided herein will demonstrate that no significant threat to the environment will result from the partial exemption based on: the types of waste received; methods for controlling types of waste disposed; the results of hydrogeological and geotechnical investigations.

2.0 CELL 16 DESIGN CONCEPT

The conceptual closure design for Cell 16 is shown in Appendix A of the March 2016 Major Permit Modification Application. The cell will be constructed with a compacted clay layer with a minimum thickness of three feet and a saturated hydraulic conductivity of less than or equal to 1×10^{-7} cm/sec, consistent with the existing cells. The clay layer will tie into the existing clay layer on the northern boundary of Cell 15 and slope to the north and northwest towards Pond 3.

3.0 TYPES OF WASTE RECEIVED

Class III waste is defined by Section 62-701.200 (14), F.A.C. as "yard trash, construction and demolition debris, processed tires, asbestos, carpet, cardboard, paper, glass, plastic, furniture other than appliances, or other materials approved by the Department, that are not expected to produce leachate that poses a threat to public health or the environment."

4.0 METHODS FOR CONTROLLING TYPES OF WASTE DISPOSED

The facility is operated in accordance with the Operations Plan which is incorporated by reference in operations permit 177982-022-SO. The following items summarize the key components of the operations plan which directly address controlling the types of waste disposed at the facility:

- The site is protected from unauthorized disposal by a fence and a locked gate during nonoperating hours; A trained operator is on site and trained spotters are at the working face whenever waste is being accepted;
- All waste is inspected prior to placement for final disposal;
- All customers must enter through the scalehouse and are questioned about the type of waste to be disposed;
- Any customer having unauthorized waste is refused entry to the facility;
- Signs are posted notifying customers that hazardous and household wastes are not accepted at the facility;
- Unauthorized waste detected by a spotter is removed from the waste stream and placed in a separate container for transport to an authorized facility;
- No other loads are tipped in the vicinity of detected non-Class III waste until the

- authorized waste has been removed:
- CCA-treated wood is not accepted for disposal and is removed from the waste stream and stored in a container until it can be transported to a lined disposal facility.

5.0 GEOTECHNICAL INVESTIGATION

A geotechnical site investigation as required by Section 62-701.410(3), F.A.C. was performed for the entire facility by Universal Engineering Sciences, Inc. (UES) in 1999 and 2000 (report dated May 5, 2000). An update to the site geotechnical investigation was performed by UES in 2005 (report dated January 25, 2006. Substantial geotechnical data has been collected across the site including in the proposed Cell 16 lateral expansion area. UES has prepared a second update to the original geotechnical investigation report which focuses on the proposed Cell 16 footprint. A copy of the UES report is provided in Attachment 1.

6.0 HYDROGEOLOGIC EVALUATION

6.1 Groundwater Flow

Groundwater flow characteristics were provided in the March 2013 Water Quality Monitoring Plan Evaluation Report prepared by L&A. Conclusions from the March 2013 report are excerpted below.

- Historically, the site hydrogeologic regime was interpreted to include a surficial aquifer and the semi-confined Floridan aquifer. As a result, the site monitoring network includes groundwater monitoring well clusters with shallow wells screened within unconsolidated sands and clays and deeper wells screened within the limestone of the upper Floridan aquifer.
- Prior to 2007, contour interpretations of the surficial aquifer varied in both directions and the aerial extent of the water bearing unit itself. Contour maps prepared in 2001 through 2005 show a surficial aquifer of limited extent primarily on the eastern portion of the site. This interpretation is consistent with the limited lateral continuity of the fine sand unit discussed in Section 2.2.
- Water levels show a seasonal fluctuation with highs observed during the second semiannual events.
- Water is consistently observed in the monitoring wells in the northeastern portion of the site (e.g. MW-4, MW-5, MW-6 and MW-7A). However, wells located in the east-central and southeastern portions of the site (e.g., MW-8, MW-9 and MW-10) consistently lacked water (or contained water within the well sump only). This data appears to contradict the presence of a laterally continuous surficial aquifer even in the eastern portion of the site
- Regional Floridan aquifer potentiometric contour maps prepared by the Southwest Florida Water Management District show that the site is located in an area of relatively low hydraulic gradient. The flow direction indicated by the SWFWMD maps is to the north-northwest.
- Floridan aquifer water levels show a seasonal fluctuation with highs observed during the second semiannual events.

- Floridan aquifer flow beneath the site during is consistently to the west-northwest, with the highest elevations located in the southeastern corner of the site. A northnortheasterly flow component is also consistently observed in the northeastern corner of the site.
- Groundwater flow velocities calculated for the Floridan aquifer vary from a minimum of 0.4 to a maximum of 18 feet per year.
- Vertical hydraulic gradients and groundwater velocities were calculated by Jones Edmunds in the Response to Comment 6.f in the July 5, 2006 Response to 2nd Request for Additional Information and Section 5.2.3 of the revised Hydrogeologic Investigation. The maximum vertical groundwater velocity was calculated to be 1.06 feet per year with a median of 0.007 feet per year (both with positive values indicating a downward flow direction). The median vertical groundwater velocity (0.007 ft/year) was compared to the median horizontal groundwater velocity (3.7 ft/year) which indicated that leakage through the confining unit was unlikely. At the median vertical groundwater velocity it would take any leakage over 700 years to penetrate 5 feet of the confining unit.
- Groundwater elevations for paired surficial and Floridan aquifer wells were reviewed to provide an evaluation of the continuity of the confining layer overlying the Floridan aquifer beneath the site. The differential in water levels between paired wells is much more significant in the MW-4, 5 and 7 well clusters than in the MW-11 and 12 well clusters. The vertical gradient was consistently downward in well clusters MW-4, 5 and 11. The vertical gradient was consistently upward in well cluster MW-7 and variable in well cluster MW-12. The very minor differential in water levels in the MW-11 and 12 well clusters and the fluctuating direction of the vertical gradient in the MW-12 well cluster appears to indicate that the continuity of the confining layer is limited in the southeastern portion of the site. However, the consistent and more substantial differential in well clusters MW-4, 5 and 7 appears to indicate that continuity of the confining layer is consistent in the west-northwestern portion of the site.

6.2 Groundwater Quality

Groundwater quality at the site is monitored by a network of wells screened in the Floridan aquifer system and in the water bearing units above the Floridan, historically referred to as the surficial aquifer system. It should be noted that several monitoring wells historically categorized as surficial aquifer wells are more likely screened within perched zones above the surficial aquifer. These include MW-3A, MW-4, and MW-5A. For the purposes of this evaluation, these wells are grouped with the surficial aquifer wells. The site monitoring network is summarized in Table 1 and shown in Figure 2.

TABLE 1

TABLE 1 Well ID Mell Time Assisting or Notes					
Well ID	Well Type	<u>Aquifer</u>	<u>Future</u>	<u>Notes</u>	
<u>BW-1A</u>	<u>Background</u>	<u>Surficial</u>	<u>Existing</u>	-	
<u>BW-1B</u>	<u>Background</u>	<u>Floridan</u>	<u>Existing</u>	Ξ.	
MW-1A	Water Level	<u>Surficial</u>	<u>Existing</u>	<u>:</u>	
MW-1B	Water Level	<u>Floridan</u>	Existing	<u>:</u>	
<u>MW-3</u>	Detection	Surficial	Existing	_	
MW-3B	<u>Detection</u>	<u>Floridan</u>	Existing	_	
MW-4	Detection	Surficial	Existing	_	
MW-4B	<u>Detection</u>	<u>Floridan</u>	<u>Existing</u>	-	
MW-5A	Detection	Surficial	Existing	To be abandoned 60 days prior to placement of waste in Cell 16	
MW-5AR	Detection	Surficial	<u>Future</u>	To be installed 60 days prior to placement of waste in Cell 16	
MW-5B	<u>Detection</u>	<u>Floridan</u>	Existing	To be abandoned 60 days prior to placement of waste in Cell 16	
MW-5BR	Detection	Floridan	<u>Future</u>	To be installed 60 days prior to placement of waste in Cell 16	
<u>MW-6</u>	<u>Detection</u>	Surficial	Existing	_	
MW-6B	<u>Detection</u>	<u>Floridan</u>	Existing		
MW-7A	Detection	Surficial	Existing		
MW-7BR	Detection	Floridan	Existing	_	
MW-8	Detection	Surficial	Existing		
MW-8B	Detection	Floridan	Existing		
MW-9	Detection	Surficial	Existing	<u> </u>	
MW-9B	Detection	Floridan	Existing	<u>-</u>	
MW-10	Detection	Surficial	Existing	-	
MW-10B	Detection	Floridan	Existing	-	
MW-11	Water Level	Surficial	Existing	-	
MW-11B	Water Level	Floridan	Existing	-	
MW-12A	Water Level	Surficial	Existing	-	
MW-12B	Water Level	Floridan	Existing	-	
MW-15B	Detection	Floridan	Existing	To be abandoned in conjunction with Cell 7 construction	
MW-16B	Detection	Floridan	Existing	To be abandoned in conjunction with Cell 7 construction	
MW-17B	Detection	Floridan	Existing		
Water Supply	Supply	Floridan	Existing	-	
MW- 18A*	<u>Detection</u>	Surficial	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
MW-18B	Detection	<u>Floridan</u>	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
MW- 19A*	<u>Detection</u>	Surficial	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
MW-19B	Detection	<u>Floridan</u>	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
MW- 20A*	<u>Detection</u>	Surficial	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
MW-20B	Detection	Floridan	<u>Future</u>	To be installed in conjunction with Cell 7 construction	
<u>P-4</u>	<u>Piezometer</u>	Surficial	Existing	To be abandoned within 60 days of permit modification issuance	
<u>P-6</u>	<u>Piezometer</u>	Surficial	Existing		
P-8	Piezometer	Floridan	Existing	-	
P-10	Piezometer	Floridan	Existing	-	
P-11	Piezometer	Surficial	Existing	-	

Well	Top of Casing Elevation (ft, NGVD)	Total Well- Depth (ft- below top of casing)*	Sump Length (ft)**	Screen Length (ft)***	Bottom of Screen Interval Elevation (ft, NGVD)****	Top of Screen- Interval Elevation (ft, NGVD)*****	Aquifer- Monitored
BW-1A	122.50	74.50	1	20	48	68	Surficial
BW-1B	122.82	104.82	1	10	18	38	Floridan
MW-3	85.39	14.47	3	20	73.92	93.92	Surficial
MW-3B	84.80	43.90	3	10	43.90	53.90	Floridan
MW-4	100.59	26.40	3	20	77.19	97.19	Surficial
MW-4B	100.87	59.52	3	10	44.35	54.35	Floridan
MW-5A	86.74	30.50	3	20	59.24	79.24	Surficial
MW-5B	85.70	47.58	3	10	41.12	51.12	Floridan
MW-6	88.65	30.00	3	20	61.65	81.65	Surficial
MW-7A	101.16	45.85	3	20	57.87	77.87	Surficial
MW-7BR	103.27	61.20	3	10	4 5.07	55.07	Floridan
MW-8	100.10	35.90	3	20	67.20	87.20	Surficial
MW-8B	108.52	57.55	3	15	53.97	68.97	Floridan
MW-9	108.00	29.75	3	15	81.25	96.25	Surficial
MW-9B	109.75	48.80	3	15	63.95	78.95	Floridan
MW-10	111.62	37.66	3	15	76.96	91.96	Surficial
MW-10B	110.00	61.80	3	15	51.20	66.20	Floridan
MW-11*	104.45	42.50	3	20	64.95	84.95	Surficial
MW-11B*	106.11	84.90	3	15	24.21	39.21	Floridan
MW-15B	147.87	103.4	1	20	45.47	65.47	Floridan
MW-16B	138.01	103.2	1	20	35.81	55.81	Floridan
MW-17B	87.21	81.1	1	20	7.11	27.11	Floridan

^{* =} MW-11 and MW-11B not included in the current permit

Groundwater data for the site were compiled from the semi-annual groundwater monitoring reports submitted to the Department between October 2005 and September 2015 to assess the change in water quality over time with respect to different chemical parameters monitored for the site. The parameter concentrations were compared to the respective GCTL. The GCTLs are tabulated in Rule 62-777, FAC, and were established to identify individual chemical concentration limits above which aesthetics or human health may be negatively impacted.

6.2.1 Background Water Quality Comparisons

Florida solid waste rules require groundwater monitoring systems to consist of background and detection wells so that site-specific comparisons in groundwater quality can be made for the aquifers monitored. Despite several years of groundwater monitoring data at the site, rigorous comparisons between background groundwater concentrations and concentrations in detection wells in the surficial aquifer is not feasible. The original background surficial aquifer well (MW-1) was abandoned in 2008 and replaced by MW-1A. MW-1A was recently replaced by a new shallow background well, BW-1A. Both replacement background wells have been dry since installation. Therefore, evaluating changes in parameter concentrations in downgradient wells over time becomes the best indicator of potential impacts from landfilling activities.

6.2.2 Groundwater Quality of Surficial Aquifer Wells

Overview

Box-and-whisker plots were developed for various parameters of surficial and Floridan aquifers and other monitoring locations to compare measured concentrations to the corresponding GCTL for each aquifer monitored. These plots provide a visual portrayal of the statistical distribution of the data, and presented in Attachment 2. The temporal plots are also presented in Attachment 2. Figure 3 presents a definition sketch of the box-and-whisker plot. The line inside the box represents the median. The top of the box represents the 75th percentile and the bottom of the box represents the 25th percentile. The lines that extend upward and downward (whiskers) from the box represent the 90th and 10th percentiles, respectively. The outliers (data points that lie outside the 90th and 10th percentiles) are presented individually outside the whiskers-note that outliers are only visible when a minimum of 9 data points are used to construct the box and whisker plot. For the sample constituents that were detected below the respective detection limit, the detection limit was used as the concentration for plotting the box-and-whisker plots.

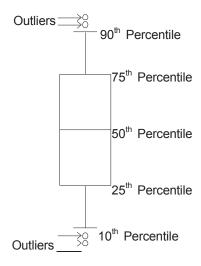


Figure 3. Box-and-whisker plot definition sketch

Note: The results of the August 2013 sampling event at BW-1A are considered to be unreliable. Historically, pH values in surficial aquifer waters do not trend toward basic results (> 7.0~S.U.). Based on the unusually high pH (10.44 S.U.), high Turbidity (796 NTU) and the fact that subsequent attempts to sample BW-1A failed due to insufficient water volume, we believe this sample reflected remnant waters as a result of the well installation.

pН

The pH is a measure of strength of acid or base in a solution, and its value ranges between 0 and 14. A solution with pH of 7 is neutral solution. A solution with pH below 7 is considered as acidic solution, and solutions with pH greater than 7 are considered basic. pH reflects the potential for acid-base reactions in water. As such, it is often treated as a variable that determines the reactions in the aquifer system, rather than as the product of those reactions.

The pH values in the surficial aquifer wells were found below the lower GCTL limit of 6.5 standard units (SU).

The temporal plots of pH for each surficial aquifer monitoring well were analyzed to identify trends in pH variation. In general, pH values remained constant or varied within a limited range for each well from the start of monitoring at the site. No increasing or decreasing trends were apparent in the data.

Conductivity

Conductivity is a measurement of the ability of water to pass electrical current and is affected by the presence of dissolved solids such as anions and cations in the water. Conductivity was observed to be less than 200 μ S/cm for each well except for BW-1A (335 μ S/cm during the 13S2 event) and MW-4 (557 to 1,007 μ S/cm).

The temporal plots of conductivity for each surficial aquifer monitoring well were analyzed to identify trends in conductivity variation. No increasing or decreasing trends were evident from measured data with conductivity values generally remaining constant or varied within a limited range for each well from the start of monitoring.

Turbidity

Turbidity is a measure of the dispersing effect that suspended solids and colloidal matter have on the transmission of light through water. The presence of clay, silt, organic and inorganic matter, and microbes among other substances impacts the measured turbidity for a given water sample. High turbidity can result in an increase of water temperature and subsequently can lead to reduced dissolved oxygen (DO) levels in water.

The temporal plots of turbidity for each surficial aquifer monitoring well were analyzed to identify trends in turbidity variation. Turbidity generally remained constant or varied within a limited range for each well from the start of monitoring and no increasing or decreasing trends were apparent in the data.

Dissolved Oxygen

The temporal plots of DO for each monitoring well of the surficial aquifer were analyzed to identify trends in DO variation. The trend in measured DO was variable. MW-7A showed a generally decreasing trend, while MW-4 and MW-5A were variable, and MW-6 was slightly increasing.

The variation in DO values may be attributed to the on-going excavation and cell construction activities at the site. A combination of materials excavation (which could result in a temporary re-oxygenation of lower portions of the surficial aquifer) and cell construction and waste placement activities (which involves the placement of compacted clay prior to waste placement) would ultimately be expected to cut off the ability for atmospheric oxygen to reach the surficial aquifer compared to the pre-construction case.

An evaluation of site specific D.O. values was performed by Jones Edmunds in 2006. Table 1 shows the D.O. for various wells during typical sampling and Table 2 shows the downhole D.O. in multiple wells.

There are some wells that are in Table 1 that are not in Table 2, and vice versa. There are five wells that are common to both tables: MW-5A, MW-5B, MW-8B, MW-9B, and MW-10B. Below is a comparison of the D.O. results for these five wells as follows:

Well	Sampling DO Range	Downhole DO Range
MW-5A	<u>5.06 – 5.30</u>	2.67 - 6.10
MW-5B	<u>3.25 – 3.35</u>	3.02 - 4.55
MW-8B	0.15 - 0.18	0.13 - 0.29
MW-9B	<u>5.71 – 5.92</u>	0.26 - 0.27
MW-10B	0.78 - 1.82	0.24 - 1.16

Of the five common wells, four of them have essentially the same downhole DO values as sampling DO values. The one outlier is MW-9B, which showed a higher DO during sampling than in the downhole sampling. The data shows a strong correlation between the DO at sampling and downhole DO. It seems reasonable that elevated DO observed in samples collected during routine semiannual monitoring are representative of natural conditions and not deficiencies in sampling procedures.

Oxidation Reduction Potential

In oxidation reduction chemistry, certain chemical reactions result in the loss of electrons (reduction reactions) while others result in the acquisition of electrons (oxidation reactions). ORP is a measure of the relative strength of oxidizing and reducing agents in relation to their respective concentrations and is measured in terms of voltage. A positive voltage reading indicates an oxidizing solution (attracting electrons) while a negative voltage reading indicates a reducing solution (losing electrons). ORP can also be indicative of bacterial activity in a body of water (Suslow, 2004).

The temporal plots of ORP for each surficial aquifer monitoring well were analyzed to identify trends in ORP variation. Several wells had sporadic data points with no real trends. However, overall ORP values were consistently positive. Similar to the trend seen for DO, the variation in ORP values is likely attributed to the on-going excavation and cell construction activities at the site.

Total Dissolved Solids

TDS in groundwater mainly consists of carbonates, bicarbonates, chlorides, sulfates, phosphates, nitrates, calcium, magnesium, sodium, potassium, iron, manganese, and a few others. The box- and-whisker plots and temporal plots of TDS concentrations in the surficial aquifer monitoring wells show that the concentrations were below the GCTL (500 mg/L) in each well except in monitoring well MW-4. The TDS values reported for MW-4 typically range from 300 to 450 mg/L. All of these values are below the SDWS of 500 mg/L. TDS values in adjacent well MW-3 typically range from 200 to 270 mg/L, which is comparable to the range observed in MW-4.

TDS was measured to be 530 mg/L during the October 2009 sampling event. TDS levels have been historically high in MW-4 which have led to historically high conductivities, as well (conductivity is directly related to TDS as dissolved solids aid the passage of electrical current). The well MW-4 has exhibited low levels in other TDS and conductivity related parameters such as chloride and sodium. Surficial aquifer well MW-4 was installed in 2006; however, in most of the sampling events since that time, the well was found to be dry or had insufficient water to be sampled. It is likely, therefore, that the water in the well simply has a naturally high mineral content relative to other wells. The monitoring events conducted after October 2009 showed no exceedances of the GCTL for TDS.

The temporal plots of TDS for each surficial aquifer monitoring well were analyzed to identify trends in TDS variation. The results generally show that TDS remained relatively constant or remained within a limited range.

1,2-Dibromoethane

Among all the measurements conducted in the samples collected from the surficial aquifer monitoring wells, 1,2-Dibromoethane was detected in 2 of 71 (3%) samples and among all the detections, the concentration of 1,2-Dibromoethane exceeded the GCTL (0.02 μ g/L) once in

MW-7A. The temporal impact plot of 1,2-Dibromoethane for MW-7A shows that 1,2-Dibromoethane concentrations were generally below the laboratory method detection limit $(0.02~\mu g/L)$ except in one sample collected in the monitoring event of October 2009 $(0.024~\mu g/L)$. Results from equipment and trip blanks from the sampling event were analyzed to assess potential cross- contamination; however, the data from the blanks do not indicate any contamination. The concentrations of 1,2-Dibromoethane were found below the detection limit in all subsequent sampling events. The single exceedance of the 1,2-dibromoethane concentration in MW-7A can be considered an isolated event and does not reflect any significant change in water quality in well MW-7A.

Ammonia

Ammonia is a standard indicator of leachate impacts to groundwater. Ammonia concentrations were consistent over time.

Nitrate as N

Nitrate as N is another common indicator of leachate impacts to groundwater. All Nitrate concentrations were significantly below the GCTL. Concentrations of Nitrate were consistent over time.

Nitrite as N

Nitrite as N is another common indicator of leachate impacts to groundwater. Temporal plots for Nitrite in the surficial aquifer monitoring wells were not possible. All Nitrite concentrations were below the laboratory method detection limit (0.007 mg/L) for the surficial aquifer wells. Evaluating trends is not possible as Nitrite was only analyzed in samples collected during the first semiannual monitoring event of 2006.

Chloride is another common indicator of leachate impacts to groundwater. All Chloride concentrations were significantly below the GCTL. Concentrations of Chloride were consistent over time.

Sodium

Sodium is another common indicator of leachate impacts to groundwater. All Sodium concentrations were significantly below the GCTL. Concentrations of Sodium were consistent over time, with the exception of values in MW-4 which show a slightly decreasing trend over time.

Chromium

The GCTL of Chromium (100 μ g/L) was exceeded once in MW-7A. The temporal impact plot of Chromium for MW-7A shows that the Chromium concentration exceeded its GCTL in the November 2008 sampling event with a measured level of 120 μ g/L. Results from equipment and trip blanks were assessed to evaluate potential cross-contamination; however, data from the blanks do not indicate any cross-contamination. The concentrations of Chromium ranged from below the laboratory method detection limit to 6.12 μ g/L in all subsequent sampling events. The single exceedance of the Chromium concentration in MW-7A can be considered an isolated event and does not reflect any significant change in water quality in well MW-7A.

<u>Iron</u>

The box-and-whisker plots and temporal plots of Iron concentrations of surficial aquifer monitoring wells show that Iron concentrations exceeded the GCTL (300 μ g/L) in six monitoring wells at least once (BW-1A, MW-4, MW-5A, MW-6, MW-7A, and MW-10). The BW-1A exceedance is considered to be unreliable as previously stated. Iron is a naturally-occurring mineral in most Florida soils, and the state of Iron is greatly affected by reduction/oxidation (redox) conditions within the aquifer. In the presence of oxygen (oxidizing condition), naturally-occurring Iron remains in the precipitate form, while the absence of oxygen (reducing conditions) can cause the solid-phase Iron to become soluble. The presence of Iron at the concentrations measured at the site may be attributable to normal background concentrations or potentially due to an alteration in the redox conditions beneath the landfill in the surficial aquifer as a result of landfill construction activities. The site has implemented a cell construction sequence that includes excavation of existing soil and placement and compaction of clay prior to waste placement.

The construction of a landfill (either a lined or and unlined landfill) can disturb the natural redox conditions beneath the landfill footprint by limiting the natural transport of atmospheric oxygen into the surficial aquifer. The limited availability of oxygen can cause the aquifer to transition into reducing conditions, thus causing the Iron to enter into the dissolved phase – this process is typically referred to as *reductive dissolution*. This phenomenon has been observed at several other landfills (lined and unlined) throughout the US and Florida, including two lined facilities in the FDEP's Southwest District.

The change in DO and ORP of water directly relates to the change in redox conditions, hence, the variation in Iron concentrations can be explained by its relationship with DO and ORP. Smaller DO values correspond to stronger reducing conditions, which can lead to reductive

dissolution of Iron. A smaller ORP represents stronger reducing conditions. The relationships of DO and ORP with Iron concentrations show that the Iron exceedances in monitoring wells MW-4, MW-5A, MW-6, MW-7A, and MW-10 were possibly because of the development of reducing conditions as a result of landfill construction and site earthwork activities and not an actual release from the waste placed in the landfill itself.

Linear regression plots of DO vs. iron and ORP vs iron are provided in Attachment 2. The linear regression plots support the relationship between both DO and ORP and iron. The highest iron concentrations are absorbed at the lowest DO values (less than 1 mg/L). Similarly, the highest iron concentrations are observed at the lowest ORP values (less than 0). Therefore, the date appears to indicate that reducing concentrations are influencing iron concentrations reported in samples collected from site groundwater monitoring wells.

<u>Irrespective</u> of the mechanism causing the observed iron concentrations, it should be noted that the <u>surficial aquifer</u> is not used for potable purposes. There are no potential receptors within the immediate vicinity of the site.

Mercury

The temporal impact plot of Mercury for MW-7A shows that the Mercury concentration exceeded its GCTL (2 μ g/L) in the November 2008 (7.0 μ g/L) and the October 2009 (2.35 μ g/L) sampling events. Equipment and trip blanks were evaluated to assess potential influences from contaminated laboratory equipment; however, data from blanks do not indicate any cross contamination. Turbidity levels were evaluated for each of these exceedances; however, the measured turbidity was within FDEP SOP requirements (FDEP, 2008). All samples collected after the October 2009 monitoring event did not show any exceedance of the GCTL for Mercury. The exceedances of the Mercury concentration in MW-7A can be considered isolated events and do not reflect any significant change in water quality in well MW-7A.

Nickel

All concentration of Nickel were below the GCTL (100 $\mu g/L$). Concentrations of Nickel in the surficial aquifer wells predominantly were recorded below the laboratory detection limit, however the Nickel was reported as high as 70 $\mu g/L$ in the November 2008 sample from MW-7A. Subsequent samples collected from MW-7A reported Nickel concentrations below 6.5 $\mu g/L$. The November 2008 Nickel concentration in MW-7A can be considered an isolated event and does not reflect any significant change in water quality in well MW-7A.

Vanadium

The box-and-whisker plots and temporal plots of Vanadium concentrations in surficial aquifer monitoring wells show that the Vanadium concentrations exceeded its GCTL (49 μ g/L) in four monitoring wells BW-1A, MW-5A, MW-6, and MW-7A. The BW-1A exceedance is considered to be unreliable as previously stated. Each Vanadium exceedance in the remaining wells occurred in the May 2006 sampling event. In the July 2006 Semi-Annual Groundwater Monitoring Report, ENCO laboratories confirmed that a sample carryover had been the origin of the elevated Vanadium levels. Samples were later re-analyzed, and all of the samples had detections below the MCL for Vanadium. No other exceedances were observed for Vanadium.

The temporal plots of Vanadium for each monitoring well of the surficial aquifer were analyzed to identify trends in Vanadium variation. In general, vanadium remained constant or varied within a limited range for each well. The temporal plots of MW-5A, MW-6, and MW- 7A show the single exceedance of May 2006 sampling event, however, as previously explained, upon reanalysis these samples had Vanadium concentrations below the detection limit.

Zinc

All concentrations of Zinc were substantially below the GCTL in all samples. Concentrations were consistent over time.

Additional Constituents

The following constituents were sporadically encountered at one or few surficial aquifer monitoring wells significantly below their established GCTL: Acetone, Antimony, Arsenic, Barium, Beryllium, Cadmium, Carbon Disulfide, Cobalt, Copper, Lead, Selenium, Silver and Toluene.

6.2.3 Groundwater Quality of Floridan Aquifer Wells

Overview

This section evaluates the water quality measured in the Floridan aquifer at the site. The Floridan aquifer original site background well was MW-1B. A re-interpretation of groundwater flow direction beneath the site resulted in the installation of BW-1B as a replacement background well. In addition to comparing site monitoring data to background data, trend analyses were performed to further evaluate changes in water quality over time which could be reasonably attributable to Class III landfilling activities.

<u>pH</u>

Floridan aquifer monitoring wells showed pH ranging from 5.9 to 11.66 S.U. with approximately 85% of measurements falling within the GCTL range of 6.5 to 8.5 S.U. Monitoring wells MW-7BR and MW-16B exhibited the highest pH levels ranging as high as 11.66 S.U. and monitoring wells MW-10B exhibited the lowest pH of 5.9 S.U. The pH of the Floridan aquifer

at the site ranged from 7.6 to 9.6 S.U. in 2003 which is before waste placement activity began at the site. The Floridan aquifer is composed of carbonate rock and expected to have relatively higher pH as the carbonate acts as a pH buffer which counteracts acids (pH<7) as they enter the body of water.

The temporal variation of pH in monitoring wells MW-7BR show that the pH of this well was trended from a high of 11.66 S.U. to a neutral value in recent sampling events. This is due This has historically been attributed to the residual grout in the well.

Values of pH in monitoring well MW-16B were slightly less than the upper limit during the initial sampling event. The pH values increased to just above 8.5 s.u. after the initial sampling event and remained fairly consistent until the second semiannual 2015 sampling event. In the 15S2 event, pH was reported above 10 s.u. This may be attributed to residual grout, similar to that observed in monitoring well MW-7BR.

The temporal plots of pH for each Floridan aquifer monitoring well were analyzed to identify trends in pH variation. In general, pH values remained constant or varied within a limited range for each well from the start of monitoring with the exception of MW-7BR which shows a decreasing trend over time.

Conductivity

Higher conductivity values of monitoring well MW-8B (226 to 898 μ S/cm) were observed compared to the other Floridan aquifer monitoring wells.

The temporal plots of conductivity for each monitoring well installed in the Floridan aquifer were analyzed to identify trends in conductivity variation. Conductivity values generally were within a limited range for each well since the start of monitoring with the exception of wells MW-9B and MW-10B, which showed a slight increasing trend.

Turbidity

The Turbidity of each well was below 20 NTU throughout the monitoring period. The temporal plots of Turbidity for each Floridan aquifer well were analyzed to identify trends in turbidity measurements. In general, turbidity values remained constant or varied within a limited range (0 to 19.9 NTU) for each well since the start of monitoring. As a whole, decreasing trends of Turbidity are expressed in the temporal plots.

Dissolved Oxygen

The temporal plots of DO for each Floridan aquifer monitoring well were analyzed to identify trends in DO levels. DO values exhibited either a variable or slightly decreasing trend in the Floridan aquifer wells ranging from 0.09 to 8.1 mg/L. Refer to DO portion of Surficial aquifer section for further analysis.

Oxidation Reduction Potential

The temporal plots of ORP for each Floridan aquifer monitoring well were analyzed to identify trends in ORP levels. ORP values were variable or slightly increasing over time during the monitoring period analyzed ranging from -301 to 537.6 mV.

Ammonia-N

Ammonia-N (NH₃-N) is the most reduced form of nitrogen and is highly soluble in water. Values in MW-8B increased slightly in 2009, but have been decreasing in monitoring events conducted since 2009.

Chloride

All Chloride concentrations were significantly below the GCTL. Concentrations of Chloride were consistent over time.

Nitrate-N

Nitrate-N (NO₃-N) forms due to oxidation of ammonia-N present in water. The box-and-whisker plots and temporal plots of nitrate-N concentration for each Floridan aquifer monitoring wells show that the nitrate-N concentrations did not exceeded its GCTL (10 mg/L) in the Floridan aquifer wells.

Nitrite-N

All Nitrite concentrations were below the laboratory method detection limits (0.007 and 0.002 mg/L) for the Floridan aquifer wells, with the exception of MW-7BR (0.21 mg/L). Evaluating trends is not possible as Nitrite was only analyzed in samples collected during the first semiannual monitoring event of 2006.

Chromium

All Chromium concentrations were significantly below the GCTL ($100 \mu g/L$). Concentrations of Chromium were consistent over time. Chromium levels spiked in December 2007 in MW-9B to 55.5 $\mu g/L$. Based on subsequent Chromium results in MW-9B, this result is considered to be erroneous and not representative.

Vanadium

The box-and-whisker plots and temporal plots of Vanadium concentration for each Floridan aquifer monitoring well show that the Vanadium concentrations exceeded the GCTL of 49 μ g/L in two monitoring wells (MW-5B and MW-7B). Each of these exceedances occurred in the May 2006 sampling event. As discussed previously, in the July 2006 Semi-Annual Groundwater Monitoring Report, ENCO laboratories confirmed that a sample carryover had been the origin of the elevated Vanadium levels in MW-5B and MW-7B, in addition to several other surficial aquifer monitoring wells. Samples were later re-analyzed, and all of the samples had detections below the GCTL for Vanadium. No other exceedances were observed for Vanadium.

Iron

The box-and-whisker plots and temporal plots of Iron concentrations in the Floridan aquifer monitoring wells show that Iron concentrations exceeded the GCTL (300 $\mu g/L$) in four monitoring wells MW-5B, MW-9B and MW-10B in at least one monitoring event.

The temporal plots for Iron in monitoring wells MW-5B and MW-9B show single instances where the GCTL was exceeded ranging from 365 μ g/L to 540 μ g/L. The temporal plot of Iron concentrations for monitoring well MW-10B showed two exceedances of the GCTL (350 μ g/L in October 2005 and 480 μ g/L in December 2009). The Iron exceedances in these wells dropped below the GCTL in the subsequent monitoring event. Hence, these exceedances of Iron concentrations relative to its GCTL in MW-5B, MW-9B and MW-10B can be considered as sporadic events, and they do not reflect any significant impact on water quality of the Floridan aquifer.

The temporal plot of the Iron concentration in monitoring well MW-8B showed multiple exceedances of the GCTL since December 2007 ranging from 1,920 μ g/L to 5,450 μ g/L. The concentrations measured in this well may be the result of reducing conditions present in this area – for example, the measured DO concentrations have been consistently low (<1.0 mg/L) since late 2006. As described earlier, lack of oxygenation in the aquifer can result in the dissolution of

naturally-occurring Iron, resulting in elevated concentrations in groundwater. The construction of the landfill may have had an impact on the DO levels, resulting in elevated Iron, which is a phenomenon that has been observed at several landfills throughout Florida. The increase in Iron concentration over time is not unexpected as it would be a function of the amount of solid-phase Iron present in this area. Regardless of the origin of the elevated Iron concentrations in MW-8B, the impact is very localized and there are no downgradient receptors in the immediate vicinity of the site. Therefore, the Iron values are not considered to be a significant impact; particularly considering that Iron is a Secondary Drinking Water Standard.

Mercury

Mercury was reported in groundwater samples collected from piezometer well MW-11B beginning with the second semiannual sampling event of 2010. Mercury values showed an increasing trend between 2010 and 2014 reaching a maximum concentration of 3.2 μ g/L. However, MW-11B was resampled following the second semiannual 2014 sampling event and mercury concentrations were found to be below the PDWS. A downward trend was confirmed by the first semiannual sampling event of 2015 which reported mercury at a concentration of 0.2 μ g/L.

Additional Constituents

The following constituents were sporadically encountered at one or few Floridan aquifer monitoring wells significantly below their established GCTL: Acetone, Antimony, Arsenic, Barium, Beryllium, Carbon Disulfide, Chloroform, Cobalt, Copper, Lead, Methylene Chloride, Nickel, Selenium, Silver, Toluene, Trichlorofluoromethane, Vanadium and Zinc.

6.2.4 Summary of Groundwater Quality

Groundwater quality in the site monitoring wells has remained very consistent over time. Concentrations of leachate indicator parameters, such as sodium, chloride and ammonia, are not elevated and have remained relatively constant since the initial sampling event. The consistency of the parameter concentrations over time combined with the absence of elevated leachate indicator parameters demonstrates that the landfilling activities had little to no impact on groundwater quality beneath the site.

Several parameters, including iron, have shown concentrations above their applicable Secondary Drinking Water Standard. These concentrations have been isolated to single wells (for example Iron in MW-8B) or have been sporadic in nature. These concentrations are not considered to represent a significant environmental impact nor are they considered to be a potential threat to human health and safety. The potable well survey provided in Attachment 3 shows that there are no potential downgradient receptors within ½ mile of the facility. The elevated secondary parameters, which may be attributable to natural variations in the local geology between wells, do not represent a significant environmental impact.

7.0 CONCLUSIONS AND RECOMMENDATIONS

Conclusions

We offer the following conclusions based upon our review of the information as discussed herein:

- The types of waste received, as defined by the Department, are not expected to produce leachate that poses a threat to public health or the environment.
- The applicant has implemented methods as required by Chapter 62-701, F.A.C. to control the types of waste disposed at the facility.
- Collectively, the SPT borings show dense to very dense sediments and indicate no significant signs of active sinkholes, such as raveling soils, voids and large areas of soft soils.
- The small subsidence feature observed in 2004 was successfully remediated with grouting. The feature has remained stable for 12 years despite continued hydraulic loading.
- No other subsidence features have been observed at the facility despite the removal of substantial clay overburden as part of mining operations.
- Groundwater quality for samples collected from the site monitoring network between July 2003 and September 2015 has shown only minor exceedances of secondary drinking water standards, with the exception of low levels of Mercury in a single well which have decreased well below the primary drinking water standard.
- There are no potential downgradient receptors within ½ mile of the facility based on potable well surveys. The elevated secondary parameters do not represent a significant environmental impact.
- The groundwater quality data, including a lack of elevated leachate indicator parameters, demonstrates that the current clay layer and facility operational procedures have resulted in minimal groundwater impacts in 15 years.
- The proposed clay layer combined with the existing subgrade geology provide reasonable assurances that the system will not result in a significant threat to the environment.

Recommendations

Based on the data reviewed herein, we offer the following recommendations regarding Cell 16:

- Cell 16 should be designed with a compacted clay layer with a minimum thickness of three feet and a saturated hydraulic conductivity of less than or equal to 1×10^{-7} cm/sec.
- The clay layer should tie into the existing clay layer beneath Cell 15 and slope to the north and northwest towards Pond 3.

ATTACHMENT 1 UNIVERSAL ENGINEERING REPORT



UNIVERSAL ENGINEERING SCIENCES

GEOTECHNICAL EXPLORATION

Enterprise Class III Landfill Dade City, Florida

UES Project No. 0830.1500202

PREPARED FOR:

Angelo's Materials c/o Lockler & Associates 4140 NW 37th Place, Suite A Gainesville, FL 32606

PREPARED BY:

Universal Engineering Sciences 9802 Palm River Road Tampa, Florida 33619 (813) 740-8506

> January 29, 2016 (Revised May 31, 2016)



Consultants In: Geotechnical Engineering • Environmental Sciences Geophysical Services • Construction Materials Testing • Threshold Inspection Building Inspection • Plan Review • Building Code Administration

(Revised May 31, 2016)

January 29, 2016

Orlando (Headquarters) Palm Coast

Daytona Beach Fort Myers Fort Pierce Gainesville Jacksonville

- Miami Ocala
- Panama City
- Pensacola

LOCATIONS: Atlanta

- Rockledge
- Sarasota
- St. Petersburg
- Tampa Tifton
- West Palm Beach

Angelo's Materials c/o Lockler & Associates 4140 NW 37th Place, Suite A Gainesville, FL 32606

Attention:

John Locklear, P.E.

Reference:

Geotechnical Services/Documentation Review

Dade City Landfill, Cell 16

NWC of Ente rprise Rd. and Auton Rd. Dade City, Pasco County, Florida UES Project No. 0830.1500202 UES Report No. 1306524

Dear Mr. Locklear:

As requested Universal Engineering Sciences, Inc. (UES) has completed the review of documentation and field conditions related to the Permit Renewal Applications being prepared by Locklear & Associates, Inc. (L&A).

This report contains the results of our study, an engineering interpretation of the subsurface data obtained with respect to the project characteristics described to us, geotechnical design recommendations, and general construction and site preparation considerations.

We appreciate the opportunity to have worked with you on this project and look forward to a continued association with Angelo's Materials. Please do not hesitate to contact us if you should have any questions, or if we may further assist you as your plans proceed.

Respectfully submitted,

UNIVERSAL ENGINEERING SCIENCES, INC.

Certificate of Authorization No. 549

Dušan Jovanović

Senior Project Manager

Mark KEHardy

Regional Manager

Professional Engineer No

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1.0 INTRODUCTION

Universal Engineering Sciences, Inc. (UES) has completed the review of documentation and field conditions related to the permit modification application being prepared by Locklear & Associates, Inc. (L&A). We understand the permit modification involves the construction of a lateral expansion of the landfill north of existing Cell 15 into the area referred to as Cell 16. Furthermore, we understand the Department has requested a re-evaluation of the geotechnical conditions present in the area of Cell 16.

A general location map of the project area appears in Appendix A: Site Location Map. Also included in Appendix A for your reference are a Site Aerial Photographs, USGS Site Topographic Map and SCS Soil Survey Map.

2.0 DOCUMENT REVIEW

2.1 GENERAL

The following documents, provided to us by the applicant and L&A, were reviewed for this reevaluation report:

- January 19, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- February 11, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- February 18, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- March 30, 2004 (Revised July 15, 2004) Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E. Grouting Completion Report
- Site Map, prepared by L&A with cell boundaries (existing and future) superimposed on it.
- January 6, 2011 letter from John Arnold, P.E. to Ms. Susan Pelz, P.E., subject: Enterprise Class III Landfill and Recycling Facility, Permit No.: 177982-007-SOfT3 & 177982-008-SCfT3, Response to January 5, 2011 email.
- October 2011 Enterprise Recycling and Disposal Facility Cell 6 Construction Completion Certification Report, prepared by John P. Arnold, P.E.
- December 7, 2011 letter from Steven Morgan to Mr. John Arnold, subject: Certification of Construction – Cell 6 Construction Enterprise Recycling and Disposal Facility, Permit No.: 177982-008-SCfT3, Pasco County, WACS No.: SWD/51/87895.



- March 2, 2012 letter from John Arnold, P.E. to Mr. Steve Morgan, subject: Enterprise Recycling and Disposal Facility, Cell 6 Construction Completion Report
 – RAI No. 1 Response, Angelo's Aggregate Materials, Ltd., FDEP Permit Nos. 177982-008-SCfT3 and 177982-007-SOfT3, WACS No.: 87895, Pasco County, Florida.
- March 26, 2012 letter from John Locklear, P.G. to John Morris, P.G., subject: Cell 6 Monitoring Well Installation, Enterprise Class III Landfill and Recycling Facility, Permit No. 177982-007-SOfT3, WACS No. 87895.
- April 24, 2012 letter from Steve Morgan to Mr. John Arnold subject: Certification of Construction – Cell 6 Construction Enterprise Recycling and Disposal Facility, Permit No.: 177982-008-SC/T3, Pasco County, WACS No.: SWD/51/87895.
- May 11, 2012 letter from John Arnold, P.E. to Mr. Steve Morgan subject: Enterprise Recycling and Disposal Facility Cell 6 Construction Completion Report – Response to RAI#2.
- June 2015 plan set from L&A compiling previous geotechnical boring data for the Cell 16 area.
- June 2015 plan set from L&A of geologic cross sections for the Cell 16 area.

In addition we revisited the following reports previously prepared by UES:

- Geotechnical Exploration, Proposed Dade City Class 111 Landfill, prepared for Hartman & Associates, Inc. (UES Project No. 80010-002-01), dated May 5, 2000.
- Geotechnical Exploration Update, Dade City Class III Landfill (UES Project No. 80010-002-01), prepared for Hartman & Associates, Inc. dated January 26, 2006.

2.2 GENERAL GEOLOGY

2.2.1 GEOLOGY

According to the Geologic Map of the State of Florida, 2001, the surficial deposits underlying the site and the general vicinity are classified as the Hawthorn Group (Th) of Miocene geologic age. The Hawthorn Group sediments are light olive gray and blue gray, poorly to moderately consolidated, clayey sands to silty clays.

The Oligocene Suwannee Limestone (Ts) generally lies below the Hawthorn Group sediments in the region. The Suwannee Limestone generally consists of a white to cream, poorly to well indurated, fossiliferous limestone. The upper portion of the limestone is highly variable due to paleo-weathering it is not uncommon for limestone to be found at relatively shallow depths (< 50 feet) or at depths greater than 100 feet below the land surface.



2.2.2 HYDROGEOLOGY

The Floridan aquifer is semi-confined in this area of Pasco County. The Floridan aquifer system consists of the Upper and Lower Floridan aquifers separated by the middle confining unit. The middle confining unit and the Lower Floridan aquifer in west-central Florida generally contain highly mineralized water. The water-bearing units containing fresh water are herein referred to as the Upper Floridan aquifer. The Upper Floridan aquifer is the principal source of water in the Southwest Florida Water Management District (SWFWMD) and is used for major public supply, domestic use, irrigation, and brackish water desalination in coastal communities (SWFWMD, 2000).

According to the Potentiometric Surface of the Upper Floridan Aquifer, West Central Florida, September 2008, groundwater flow is generally towards the west and depth to water is approximately 5 feet NGVD 1929

2.3 CELL 16 BORINGS AND GEOLOGIC CROSS SECTIONS

All geotechnical data collected within and immediately adjacent to the proposed Cell 16 lateral expansion area was compiled and reviewed. Sources of information included the following: (1) mining exploration borings performed prior to 2000; (2) borings performed during initial 1999/2000 geotechnical investigation; (3) borings performed as part of the 2004 subsidence remediation; (4) borings performed in conjunction with groundwater monitoring well installations. Because many of these borings were performed prior to mining and landfilling activities, the site land surface has changed significantly. As a result, the original borings include lithology which is no longer present. In order to update this information and provide a more accurate representation of what actually exists in the area, each boring log was reviewed relative to the current topographic elevation. In locations where natural material has been removed (either from mining or landfilling activities), the log has been revised to remove the portions of the column which no longer exist. Copies of the revised boring logs are provided in Appendix B. Also, geologic cross sections were generated with the boring log data and are provided in Appendix B. The cross sections also include the existing and proposed clay liner and cell boundaries to assist in visualizing the proposed expansion concept.

A total of 51 borings have been performed in the Cell 16 area and vicinity. The majority of the borings were performed as Standard Penetration Test Borings and include the required blow count and N values. N values are shown on the boring logs provided in Appendix B. It should be noted that the boring logs were prepared by different people and the lithologic descriptions are variable.

Geologic Cross Section A-A'

Cross section A-A' extends north to south through the approximate center of the Cell 16 area. The northern extent (A) begins with boring SSA-29 approximately 50 feet south of the northern cell boundary. The section ends with boring DCL01-12 located in the southern portion of Cell 15. Boring SSA-29 was completed to a depth of 55 feet, NGVD. The geology encountered consisted of silty sands and silty clays. Progressing south along the section the next boring is



B-32, which was completed to a depth of 35 feet, NGVD. The geology encountered consisted of alternating layers of silty sands to sandy clays until limestone was observed at an elevation of 36 feet, NGVD. The next two borings, B-26 and B-22, show deeper silty sands underlain by silty to sandy clays. Limestone was not encountered in either of the borings which terminated at elevations of 15 and 30 feet, NGVD, respectively. The two southernmost borings, DCL01-13 and DCL01-12, were completed within the existing Cell 15 footprint. Sandy clays were observed in both borings, with limestone encountered at an elevation of 65 feet, NGVD in DCL01-13.

N-values for the borings comprising cross section A-A' are provided in Appendix B. Of the six borings, all but SSA-29 included SPT data. N-values for B-22 ranged from 7 to 58. N-values for B-26 and B-32 ranged from 3 to 12 and 10 to 23, respectively. N-values for DCL01-12 and DCL01-13 ranged from 2 to 18 and 2 to 9, respectively. Note that discussions of N-values include values for those intervals that still remain in place. Therefore, the range discussed herein may be different than the full range displayed on the original boring logs.

Geologic Cross Section B-B'

Cross section B-B' extends from the southwest corner to the northeast corner of the Cell 16 area. The southwestern extent of the section begins with boring L-14 located within the Cell 1 footprint. The section ends in the northeastern corner of the proposed Cell 16 footprint with boring B-21. Borings L-14 and SSA-25 were both completed to depths of 65 feet, NGVD. The lithology described for both borings consists of sandy clays. As we move north in the proposed Cell 16 footprint, boring B-23 shows interbedded clayey sand, sandy clays and clays to a depth of 55 feet, NGVD. Borings B-33 and B-31 were completed to depths of 43 and 40 feet, NGVD, respectively. Both columns show similar interbedded clayey sands, sandy clays and clays. Boring B-33 shows a limestone marl underlain by limestone beginning at an elevation of 47 feet, NGVD. The limestone marl is seen at the same elevation in B-31 but is underlain by clayey sand rather than limestone. The section terminates with boring B-21 which was completed to a depth of 55 feet, NGVD. This column shows interbedded clayey sands and silty clays with a thin limestone marl layer from 64 to 61 feet, NGVD.

N-values for the borings comprising cross section B-B' are provided in Appendix B. Of the six borings, B-21, B-23, B-31 and B-33 included SPT data. N-values for B-21 ranged from 4 to 9. N-values for B-23 ranged from 5 to 19. N-values for B-31 ranged from 8 to 18. N-values for B-33 ranged from 3 (at the limestone contact) to 33. It is very common to observe lower blow counts and N-values at the contact between two differing lithologic units.

Geologic Cross Section C-C'

Cross section C-C' extends from the northwest corner to the southeast corner of the Cell 16 area. The section begins with boring B-34 in the northwest corner of the proposed Cell 16 footprint and extends to MW-6 just outside of the southeastern corner of Cell 16. Boring B-34 was completed to a depth of 50 feet, NGVD and consists of silty sand overlying interbedded clayey sand, silty clay and sandy clay. Boring SSA-26 was completed to a depth of 55 feet, NGVD. It consists of silty to clayey sands overlying silty clay. The upper portion of boring B-32 shows similar lithology to SSA-26 which is then underlain by more sandy clay and clayey sands



and ultimately limestone at a depth of 36 feet, NGVD. Boring B-31 shows a very similar column to that of B-32, though a thin limestone marl layer is encountered at approximately 47 feet, NGVD. SSA-30 is the last boring located within the Cell 16 footprint. SSA-30 was completed to a depth of 55 feet, NGVD. The column consists of silty clay underlain by a thin clayey sand layer and then silty clay with limestone fragments. Limestone was encountered at an elevation of 56 feet, NGVD. The boring performed during construction of monitoring well MW-6B represents the southern extent of the section. The boring was completed to a depth of 30 feet, NGVD. The column consists of sandy clay to clay underlain by limestone starting at an elevation of 55 feet, NGVD.

N-values for the borings comprising cross section C-C' are provided in Appendix B. Of the six borings, B-21, B-23, B-31 and B-33 included SPT data. N-values for B-21 ranged from 4 to 9. N-values for B-23 ranged from 5 to 19. N-values for B-31 ranged from 8 to 18. N-values for B-33 ranged from 3 (at the limestone contact) to 33. It is very common to observe lower blow counts and N-values at the contact between two differing lithologic units.

Geologic Cross Section D-D'

A geologic cross section (D-D') running north to south through the southeastern corner of Cell 16 is provided in Appendix B. The northern extent of the section is represented by boring B-42 and the southern extent by boring B-39. Boring B-42 was completed to a depth of 55 feet, NGVD. The column consists of sandy clay underlain by clay to clayey sand limestone marl at an elevation of 60 feet, NGVD. Boring B-41 shows sandy clay overlying limestone marl, followed by limestone at an elevation of 57 feet, NGVD. Borings B-40, B-36 and B-35 show a similar sequence though B-35 was completed deeper than the other borings (40 versus 57 feet, NGVD). Boring B-39 shows a slightly thinner layer of sandy clay underlain by limestone at an elevation of 70 feet, NGVD.

N-values for the borings comprising cross section D-D' are provided in Appendix B. All six borings included SPT data. N-values for B-42 ranged from 9 to 23. N-values for B-41 ranged from 7 to 36. N-values for B-40 ranged from 3 to refusal. N-values for B-36 ranged from 8 to refusal. N-values for B-35 ranged from 1 (at the limestone contact which is common) to 21. Boring B-39 N-values ranged from 9 to 36.

Geologic Summary

Collectively, the SPT borings show dense to very dense sediments and indicate no significant signs of active sinkholes, such as raveling soils, voids and large areas of soft soils. There is evidence of the typical loss of circulation at the soil-limestone interface at depth, and a few one to two foot thick layers of soft sediments (one to three blow counts). However, in all borings dense to very dense sediments have surrounded these softer soil layers in a stable setting.

The low blow count and even weight-of-rod/hammer strength material near the top of the limestone is a normal occurrence associated with the ancient weathering or erosional features of the epikarst. Epikarst is the zone of weathering at the upper surface of a limestone stratum. Weathering of limestone results in development of rubble, fine-grained carbonate-rich silt and clay, karren (including pinnacles and valleys in the limestone rock surface), and other features.



Epikarst is frequently associated with losses of drilling fluid circulation, low blow counts, weight of rod or hammer events, and recovery of gravel-sized particles of rock. The epikarst can occur at the land surface or be buried under later sediments. Raveling of soil or sediments into the voids within the epikarst formation can lead to sinkhole activity, but in most cases there is no evidence of on-going or contemporaneous raveling and the epikarst is not synonymous with sinkhole activity.

2.4 EVALUATION OF 2004 SUBSIDENCE FEATURE

In 2004, a small (12 feet in diameter) subsidence feature was observed by Hartman & Associates, Inc. (HAI) in the southeastern portion of the Cell 16 area. The area was investigated through the advancement of additional SPT borings.

The feature was subsequently remediated through grouting. The purpose of the grouting program was to seal the upper limestone zones and compact, fill and improve loose soil conditions encountered at this location. The grouting operation was conducted using present industry standards.

The remediation included 26 grout injection points. The casing depths of the injection points generally ranged from 25 to 45 feet below land surface (bls), with the exception of injection point 26 which extended to 60 feet, bls. The higher quantities of grout were generally injected in the points with deeper casing depths. The largest quantity of grout was injected in point 26. The initial grout take within the lower portion of this grout injection point, at depths between 60 and 42 feet, was relatively large per foot of depth. The grout take was significantly less per linear foot within the upper portion of this grout injection point with much higher line pressures. Based on the above observation we believe the upper limestone zone was sealed and the cavity was filled with low slump grout.

For the remaining grout injection points the njection pressures were generally higher at shallow depths.

A copy of Grouting Completion Report as presented to Department of Environmental Protection by Hartman & Associates in 2004 is attached.

Since completion of the grouting remediation, the entire area around the feature has been hydraulically loaded by the temporary stormwater pond. The feature has been stable for more than 10 years under conditions which are considered conducive to the formation of subsidence features.

3.0 CONCLUSIONS

As a result of our review process we concluded the following:

 Both reports issued by UES conform to the requirements of the Florida Administrative Code including the assessment of potential for sinkhole occurrence presented in our May 5, 2000 report.



- O UES report Geotechnical Exploration Update, dated January 25, 2006 was a result of the proposed change in the landfill geometry (fill thickness and change in slopes) and questions raised by FDEP. The report provided analysis and conclusions related to the soil bearing capacity and total settlement of foundation soils, slope stability analysis and potential for sinkhole occurrence related to loss of circulation (LOC) events at the time of our geotechnical exploration.
- No additional information presented in the documentation provided to us warranted any changes, revisions or additions to analysis and/or conclusions and recommendations presented in our reports.

Generally our conclusions can be summarized as:

- This report confirms the conclusion drawn in previous geotechnical site investigations and that the site meets geotechnical requirements of Rule 62-701.410 F.A.C.
- Sinkhole risk in the proposed disposal footprint is low. This conclusion is particularly applicable to the temporary retention pond area (Cell 15 and Cell 16) based on ten years of monitoring under conditions which are considered conducive to the formation of subsidence features.
- Placement of three feet of clay layer in the proposed fill areas including Cell #16 is adequate to meet the geotechnical requirements for the site.

We also performed a site visit on June 10, 2014 accompanied by Mr. John Arnold. The area of the former subsidence received a clay liner and was used as a temporary stormwater pond. Based on the site reconnaissance and information provided by Mr. Arnold no ground subsidence or indications of surficial expressions of sinkhole activity were observed within the temporary stormwater pond (future Cell 14 and 16) or anywhere at the site.

4.0 LIMITATIONS

During the early stages of most construction projects, geotechnical issues not addressed in this report may arise. Because of the natural limitations inherent in working with the subsurface, it is not possible for a geotechnical engineer to predict and address all possible subsurface variations. An Association of Engineering Firms Practicing in the Geosciences (ASFE) publication, "Important Information About Your Geotechnical Engineering Report" appears in Appendix C, and will help explain the nature of geotechnical issues. Further, we present documents in Appendix C: Constraints and Restrictions, to bring to your attention the potential concerns and the basic limitations of a typical geotechnical report.

Do not apply any of this report's conclusions or recommendations if the nature, design, or location of the facilities is changed. If changes are contemplated, UES must review them to



Angelo's Materials UES Project No. 0830.1500202. January 29, 2016, (Revised May 31, 2016) Page 8

assess their impact on this report's applicability. Also, note that UES is not responsible for any claims, damages, or liability associated with any other party's interpretation of this report's subsurface data or reuse of this report's subsurface data or engineering analyses without the express written authorization of UES.

* * * * * * * * *



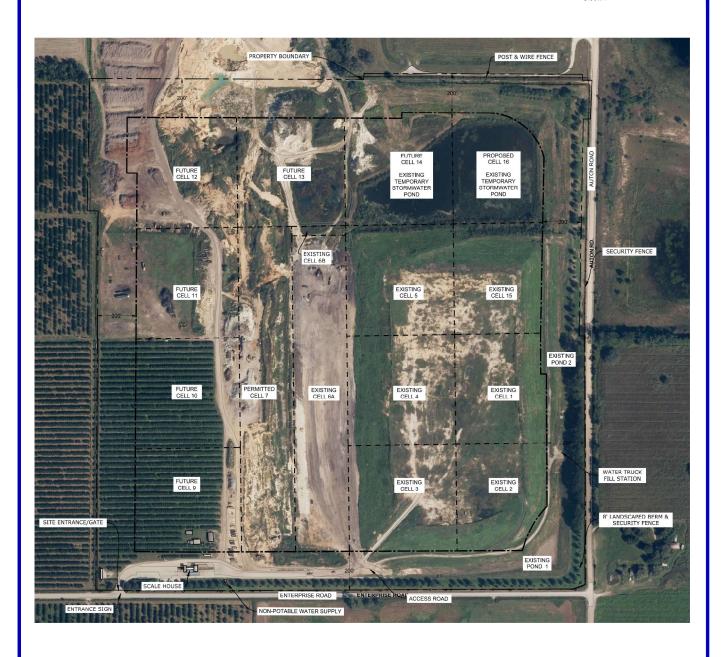
APPENDIX A

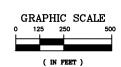




SITE LOCATION MAP							
CLIENT: ANGELO'S MATERIALS	DRAWN BY: SB DATE: AUG 10, 2015	j					
SCALE: NOT TO SCALE PROJECT NO: 0830.1500202	REVIEWED BY: SS APPENDIX: A						



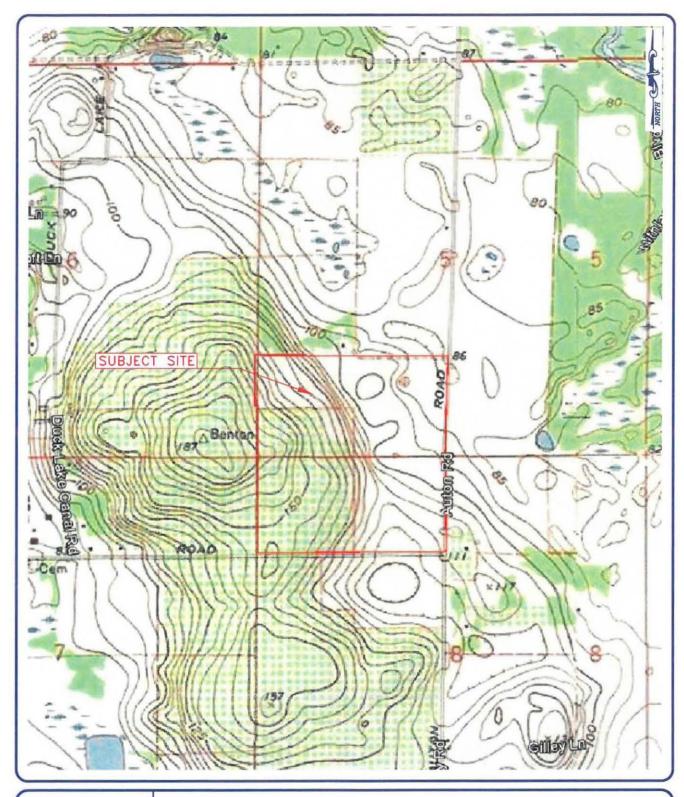






SITE AERIAL PHOTOGRAPH

CLIENT: ANGELO'S MATERIA	ALS	DRAWN BY: SB	DATE: MAY 6, 2016
SCALE: 1" = 500'	PROJECT NO: 0830.1500202	REVIEWED BY: SS	APPENDIX: A





SITE TOPOGRAPHIC MAP								
CLIENT: ANGELO'S MATER	ALS	DRAWN BY: SB	DATE: AUG 10, 2015					
SCALE: NOT TO SCALE	PROJECT NO: 0830.1500202	REVIEWED BY: SS	APPENDIX: A					

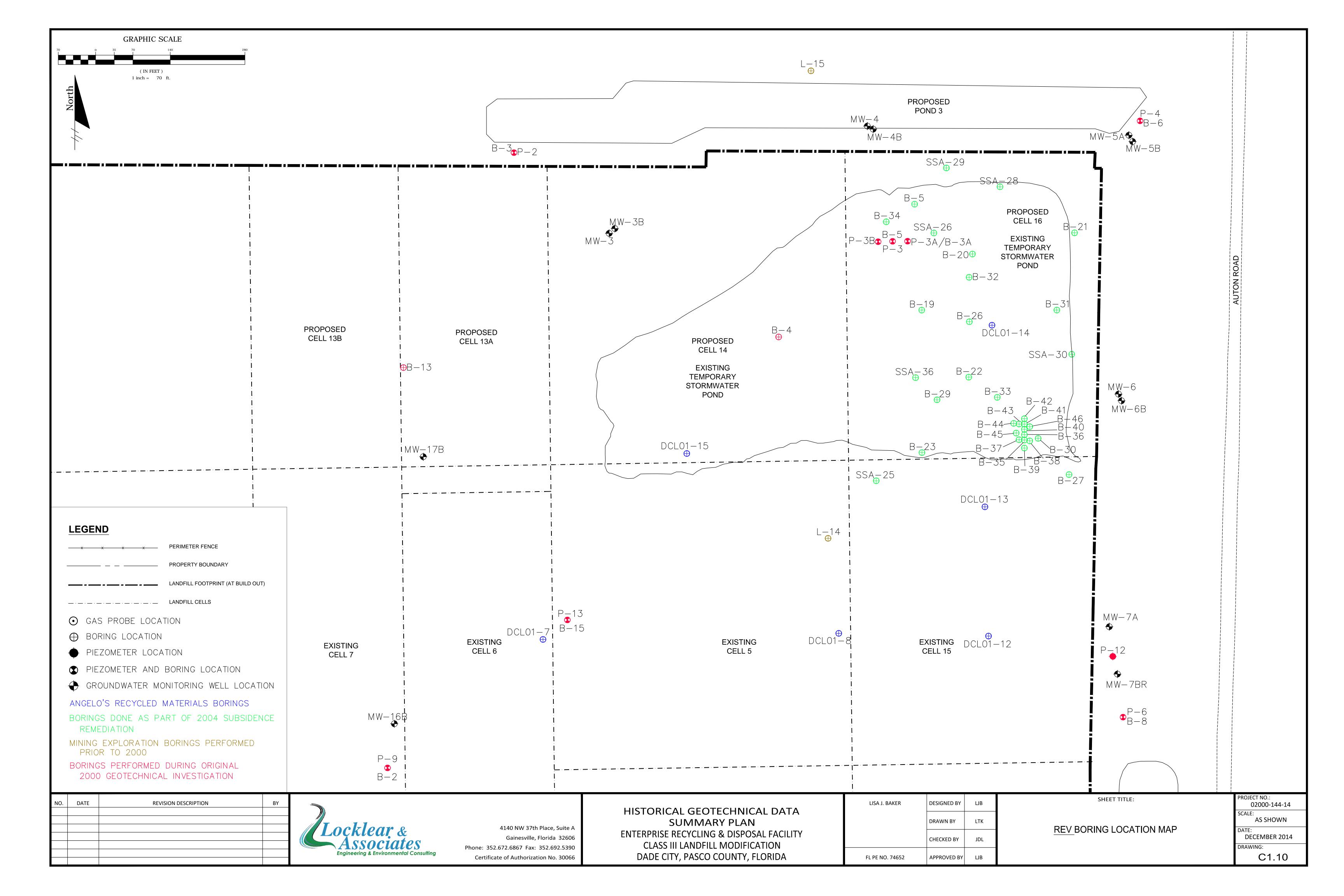


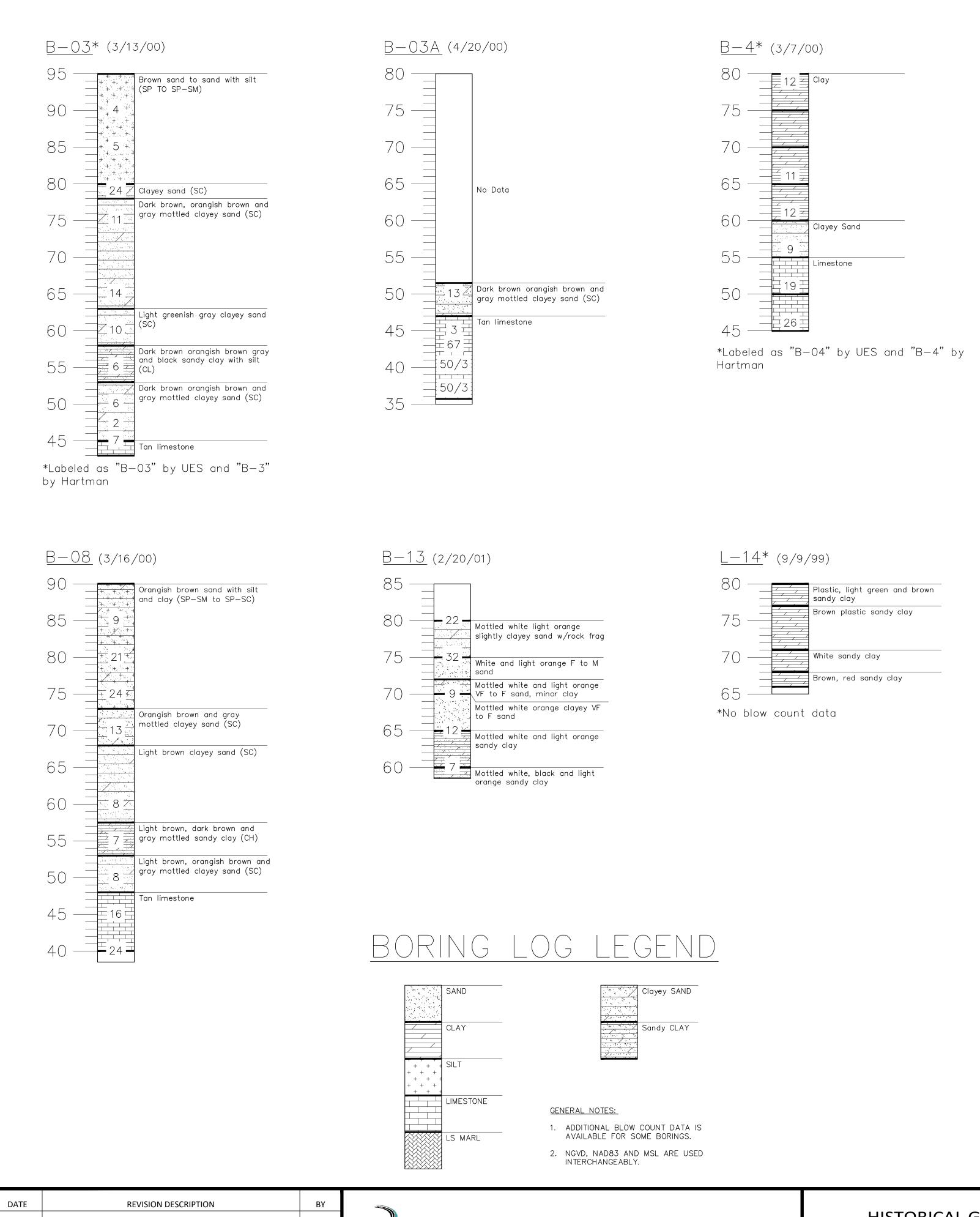


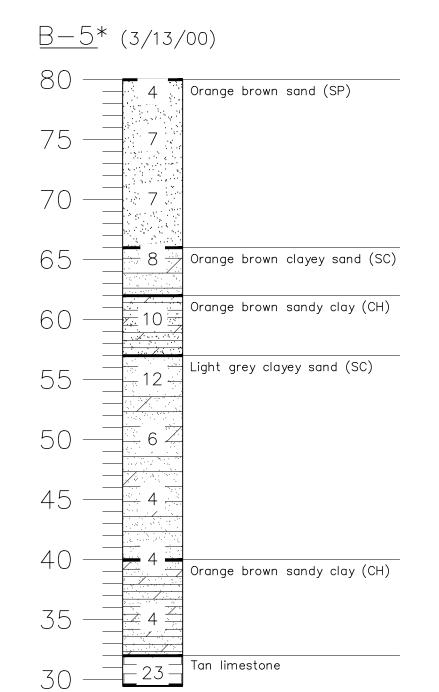
SCS SOIL SURVEY MAP

CLIENT: ANGELO'S MATERIALS			DRAWN BY: SB		DATE: AUG 10, 2015			
SCALE:	NOT TO SCALE	PROJECT NO:	0830.1500202	REVIEWED BY:	ss	APPENDIX:	Α	

APPENDIX B







by Hartman **Ground elevation listed as 77' MSL on

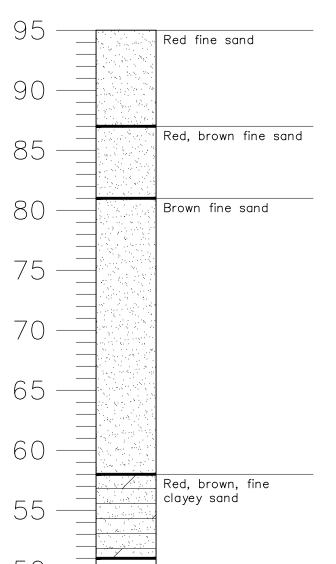
*Labeled as "B-05" by UES and "B-5"

boring log, however based on elevations of surrounding borings performed during the same time frame an elevation of 95' MSL was used.

B - 06 (3/15/00)

_		Light brown sand (SP)
80 -	6	
		Light brown dork brown and
¬ _	+ - +	Light brown, dark brown and gray mottled sand with silt
75 -	+ / +	(SP-SM)
	+ + + + + + + + + + + + + + + + + + + +	
70 -	14	
7 0	, , , , , , , , , , , , , , , , , , ,	Light brown, dark brown and gray mottled sandy clay (CH)
		Light brown, dark brown and
65 -		gray mottled clayey sand (SC)
	16	Gray and dark brown mottled
\sim		sandy clay (CH)
60 -		
55 -	8 =	
00		
		Light brown, dark brown and
50 -	5	gray mottled clayey sand (SC)
	#. N# 18 F.M.	Gray sand with silt (SP—SM)
15	+ 16	ordy sand with sire (Si Sin)
45 -	+ + + +	
	, , , , , , , , , , , , , , , , , , ,	Brown, yellowish brown and gray
40 -	27	mottled sandy clay (CL)
. •		
7		Light brown orangish brown and white sandy clay (CH)
35 -	13	, , ,
	50 /0	
30 -	50/2	
\mathcal{O}		

<u>L-15</u> (9/9/99)



B-15 (2/21/01)

(01)
1
Orange V fine sand, minor black mottled slightly silty
Orange brown F-VF sand
Orange light brown sand with
rock fragment
O
Orange brown F sand
Orange to brownish VF-F sand with black fragments
Orange to light brown VF-M
sand with minor clay rock fragments
Orange to light brown VF—F
sand
Light brown to rusty F sand
Light brown to rusty i saila
Orange to dark brown F sand, slightly silty
Singility Sinty
Orange F—VF sand with minor
clay materials
Orango to light harms VE V
Orange to light brown VF-V sand, slightly silty
Orange to light brown V sand, slightly silty
gr y v - y
Orange F—VF sand slightly silty and minor clay
Dark brown VF sand slightly
silty, minor clay
Brownish to light VF sand,
slightly silty
Slightly silty, VF—F sand, black
pigment of minor clay
Light to gray VF to M sand with black pigment of rock
fragments

Gray to white F-VF sand well

Light brown VF to F sand, well

Gray to light brown VF to F sand, well rounded, sorted

Gray sandy clay, slightly silty,

sorted, slightly silty

Gray to white sandy clay,

slightly silty

Dark gray clay

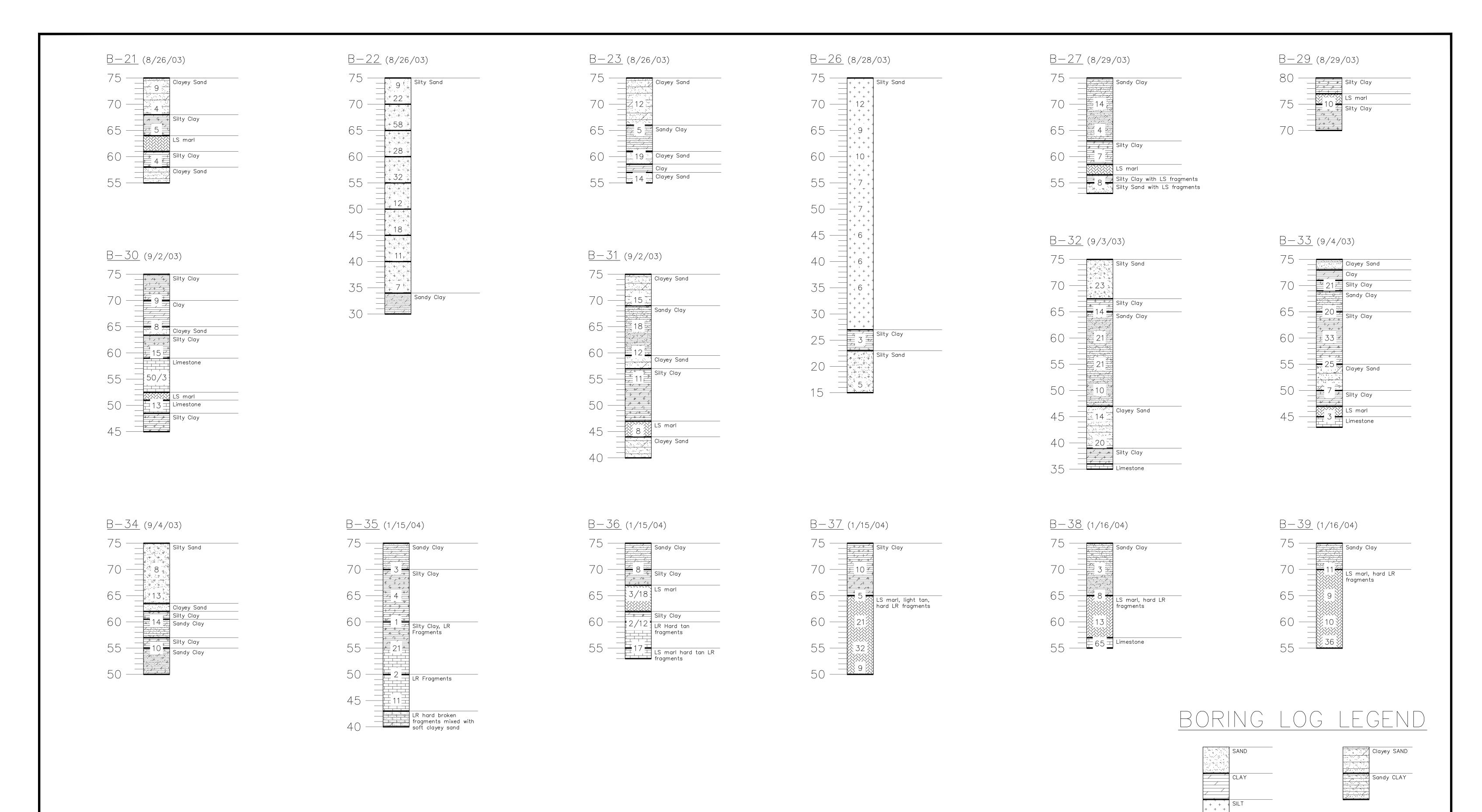
Locklear & Associates
ASSOCIATES Engineering & Environmental Consulting

4140 NW 37th Place, Suite A Gainesville, Florida 32606 Phone: 352.672.6867 Fax: 352.692.5390 Certificate of Authorization No. 30066

HISTORICAL GEOTECHNICAL DATA SUMMARY PLAN ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LTK
	CHECKED BY	JDL
FL PE NO. 74652	APPROVED BY	LJB

SHEET TITLE: 02000-144-14 **AS SHOWN BORING LOGS** DECEMBER 2014 DRAWING: C1.11



NO.	DATE	REVISION DESCRIPTION	ВҮ



4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

HISTORICAL GEOTECHNICAL DATA SUMMARY PLAN ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LTK
	CHECKED BY	JDL
FL PE NO. 74652	APPROVED BY	LJB

BORING LOGS

GENERAL NOTES:

 ADDITIONAL BLOW COUNT DATA IS AVAILABLE FOR SOME BORINGS.

2. NGVD, NAD83 AND MSL ARE USED INTERCHANGEABLY.

LIMESTONE

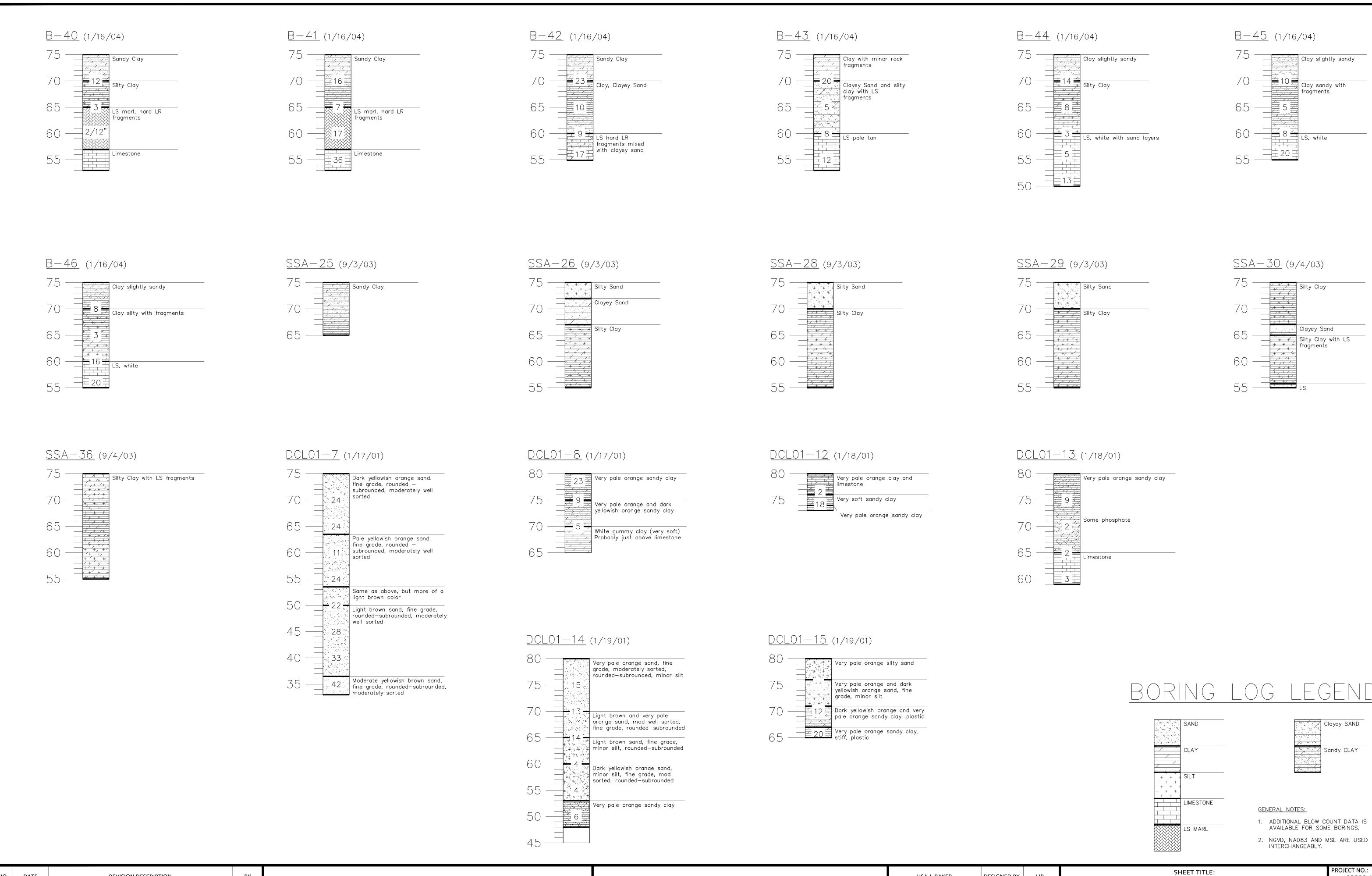
LS MARL

PROJECT NO.:
02000-144-14

SCALE:
AS SHOWN

DATE:
DECEMBER 2014

DRAWING:
C1.12



NO.	DATE	REVISION DESCRIPTION	BY	



4140 NW 37th Place, Suite A Gainesville, Florida 32606 Phone: 352.672.6867 Fax: 352.692.5390 Certificate of Authorization No. 30066

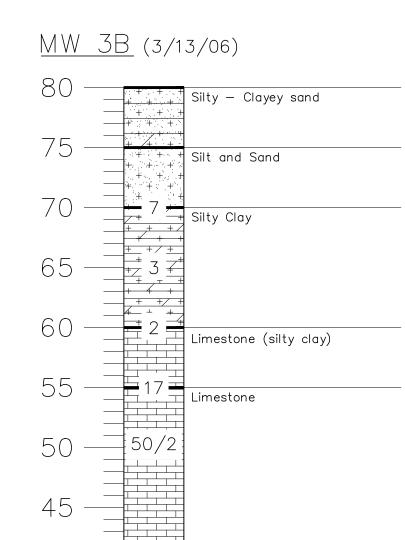
HISTORICAL GEOTECHNICAL DATA SUMMARY PLAN ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

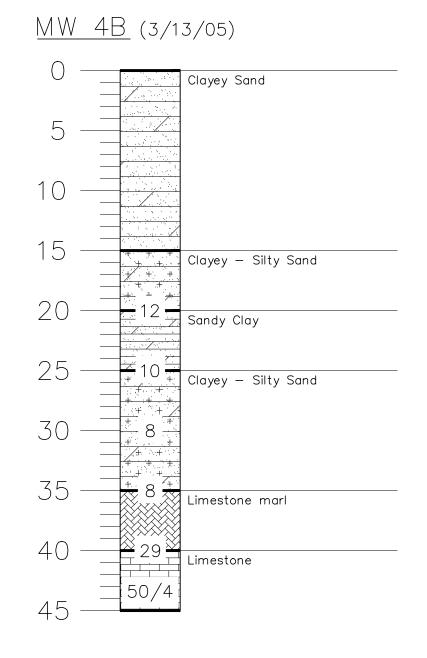
LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LTK
	CHECKED BY	JDL
FL PE NO. 74652	APPROVED BY	LJB

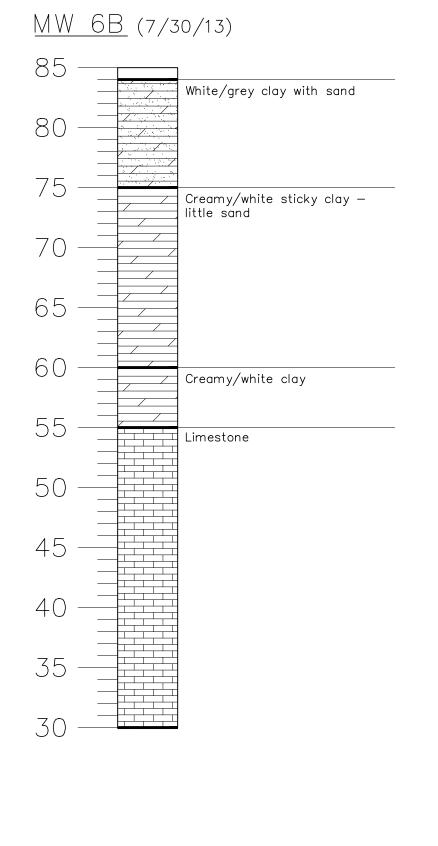
BORING LOGS

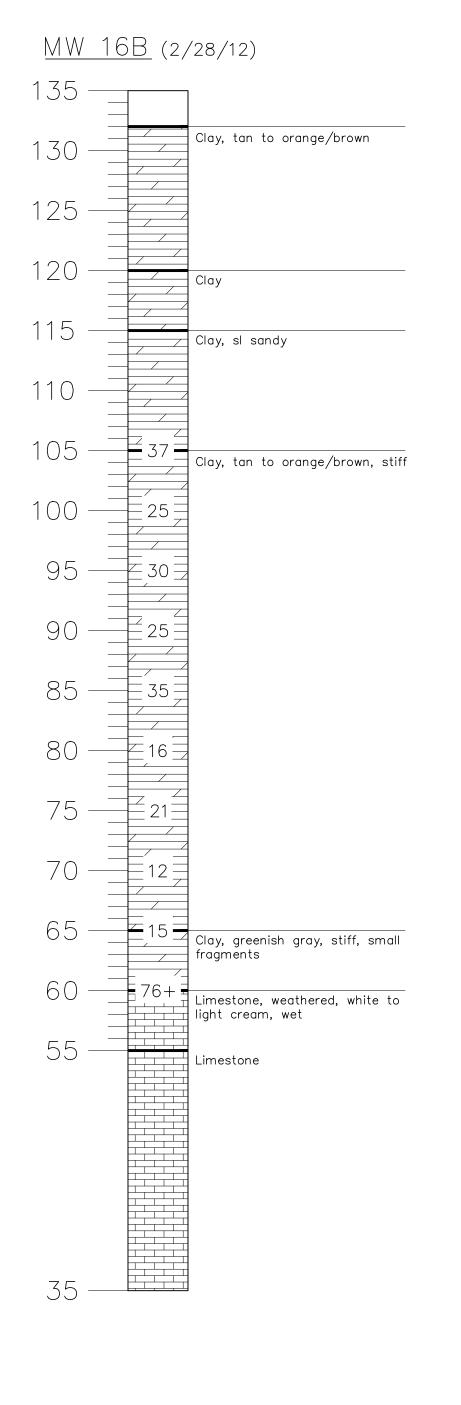
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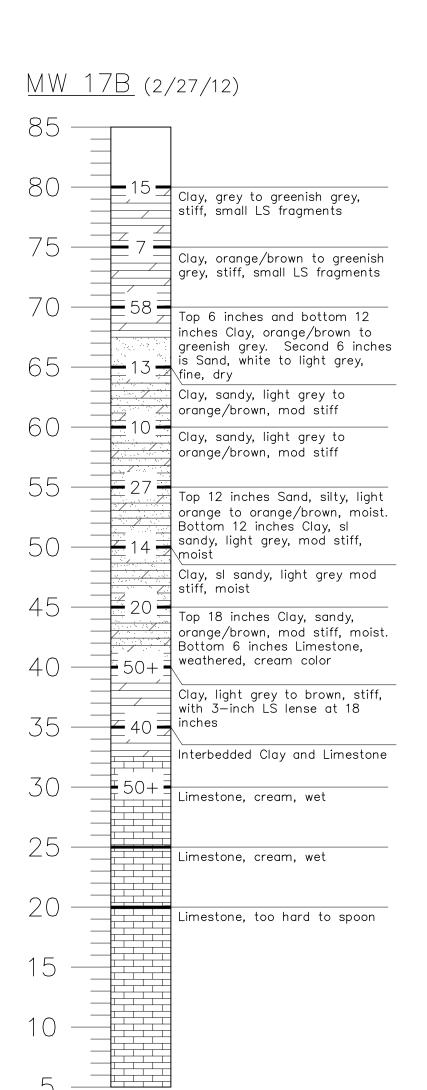
Sandy CLAY

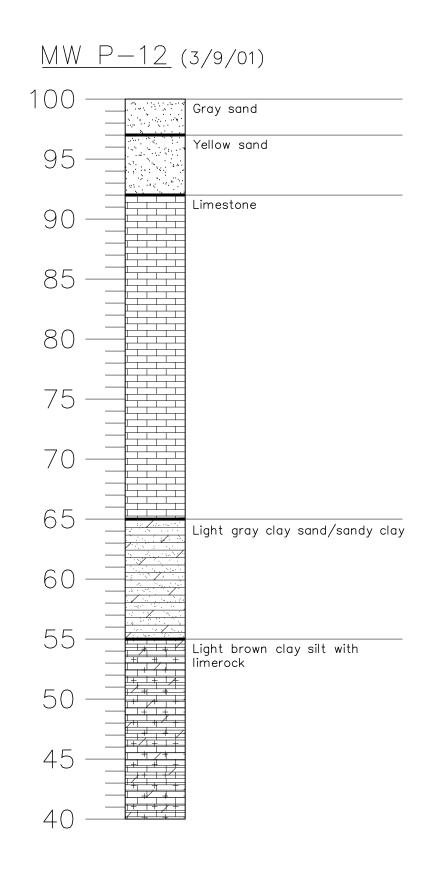




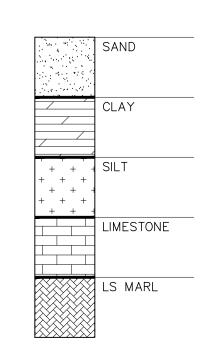








BORING LOG LEGEND



Clayey SAND
Sandy CLAY

GENERAL NOTES:

- 1. ADDITIONAL BLOW COUNT DATA IS AVAILABLE FOR SOME BORINGS.
- 2. NGVD, NAD83 AND MSL ARE USED INTERCHANGEABLY.

NO.	DATE	REVISION DESCRIPTION	ВҮ



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Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

HISTORICAL GEOTECHNICAL DATA
SUMMARY PLAN
ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

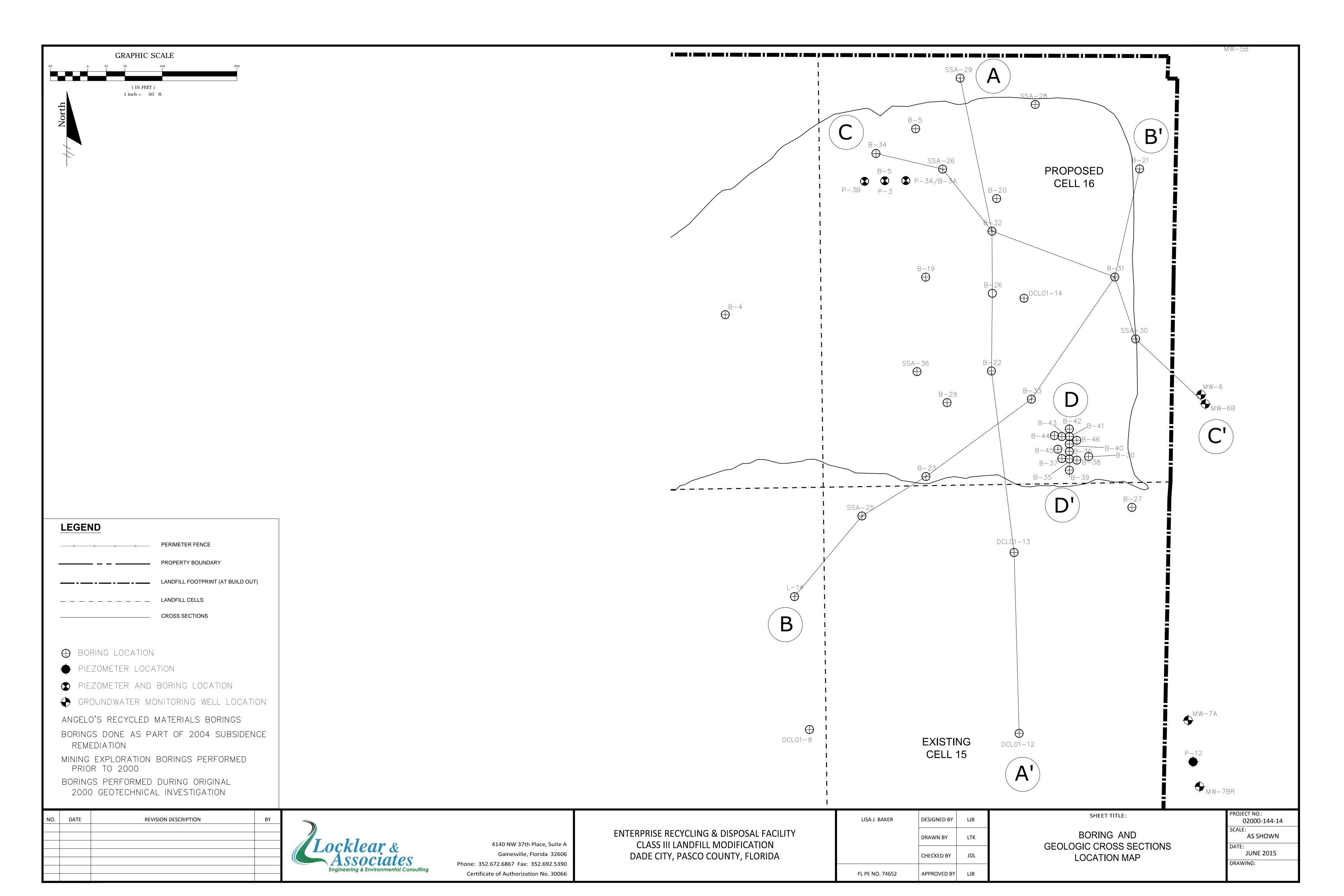
LISA J. BAKER	DESIGNED BY	IJВ	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

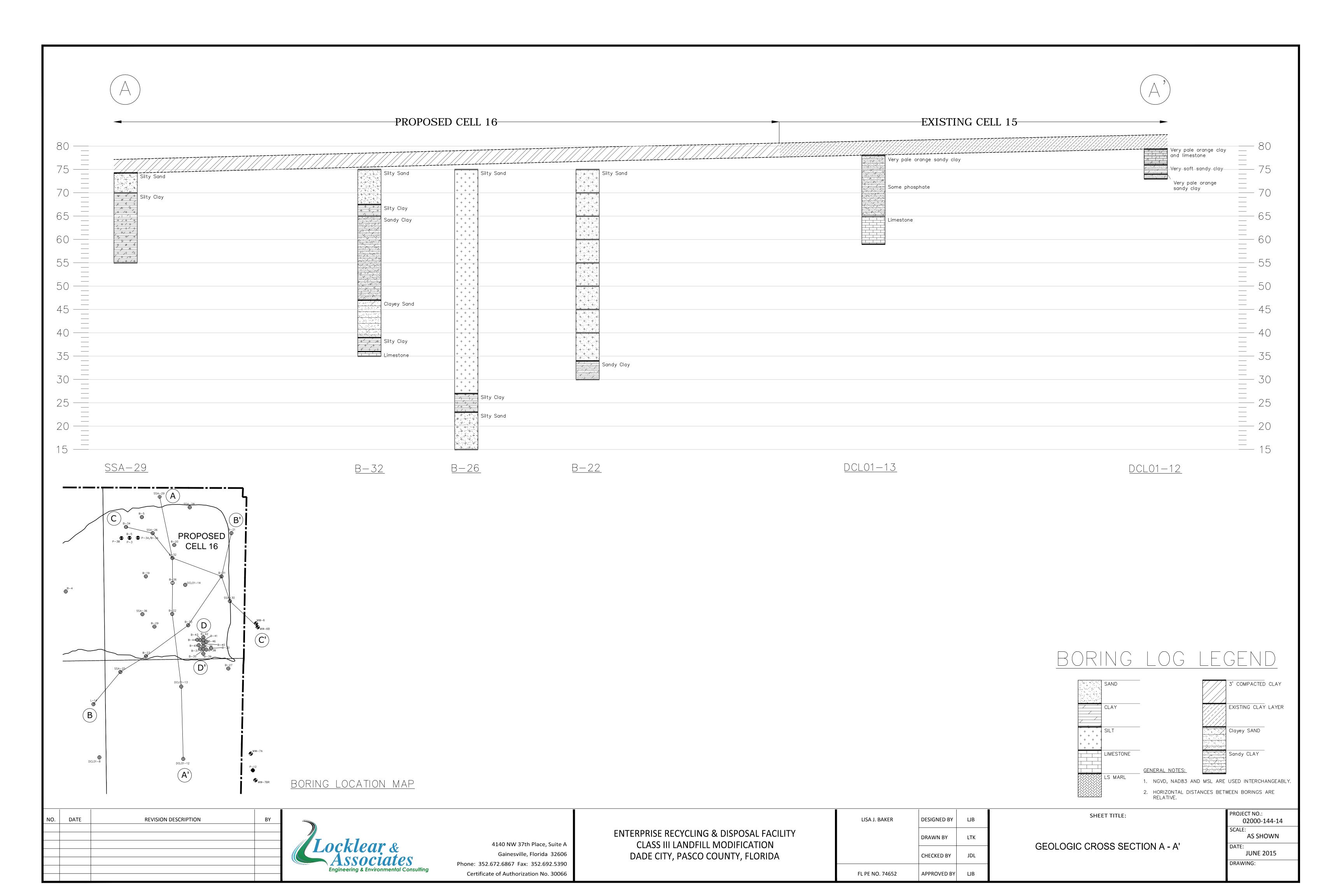
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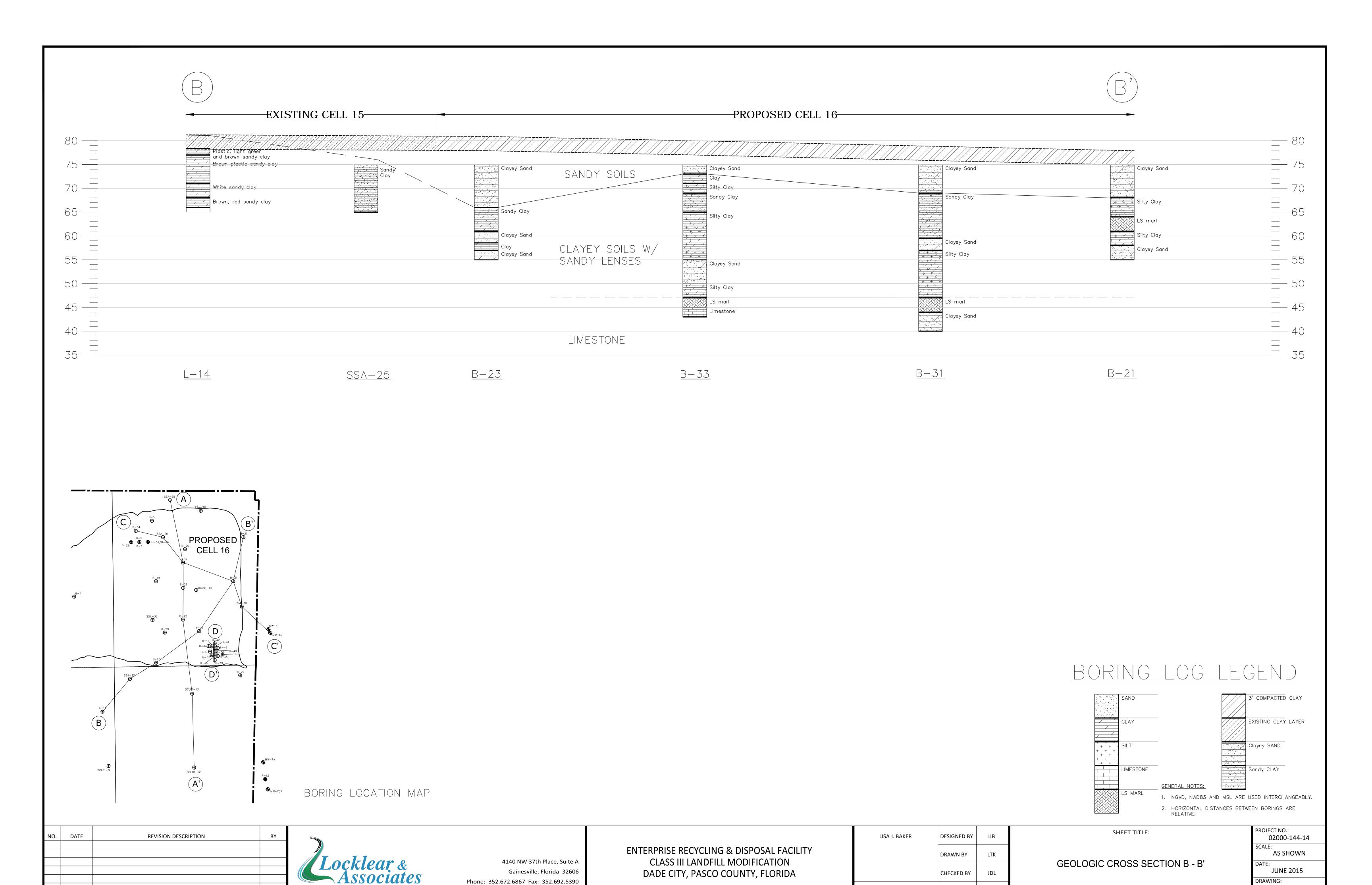
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DECEMBER 2014

C1.14



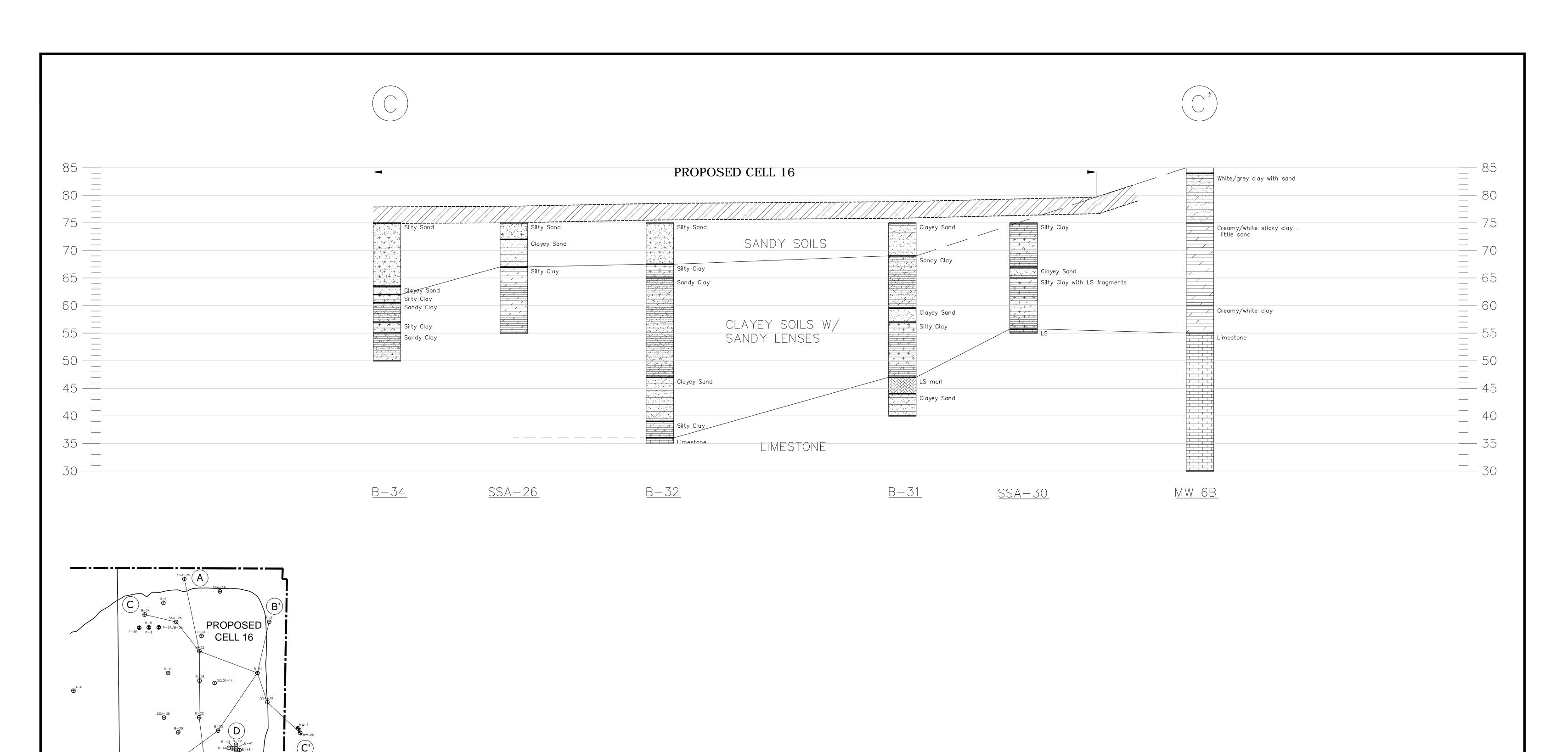




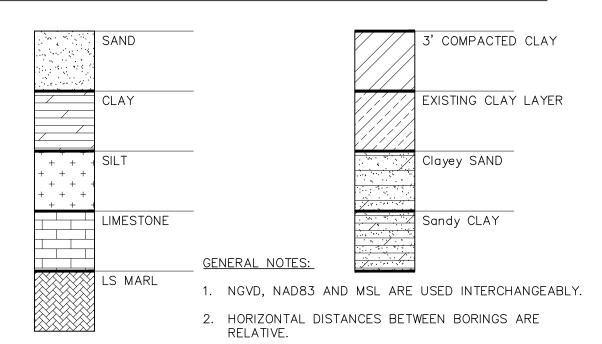
FL PE NO. 74652

APPROVED BY LJB

Certificate of Authorization No. 30066







NO.	DATE	REVISION DESCRIPTION	BY	
				Locklear Associa
				Associa
				Engineering & Environme

Locklear &

Gainesville, Florida 32606

Associates

Engineering & Environmental Consulting

4140 NW 37th Place, Suite A

Gainesville, Florida 32606

Phone: 352.672.6867 Fax: 352.692.5390

Certificate of Authorization No. 30066

BORING LOCATION MAP

ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

GEOLOGIC CROSS SECTION C - C'

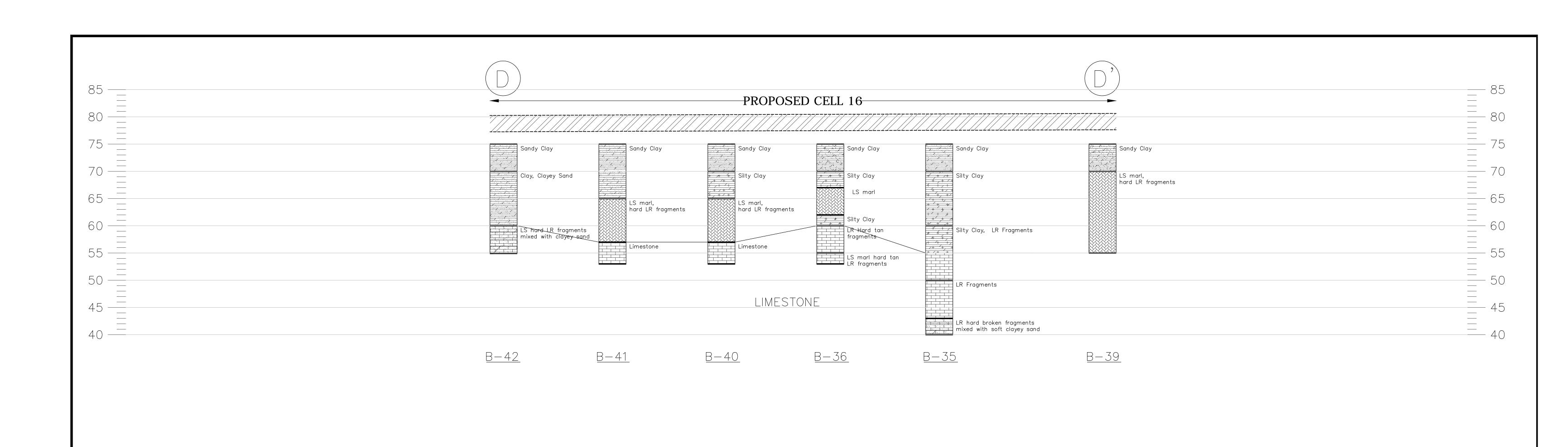
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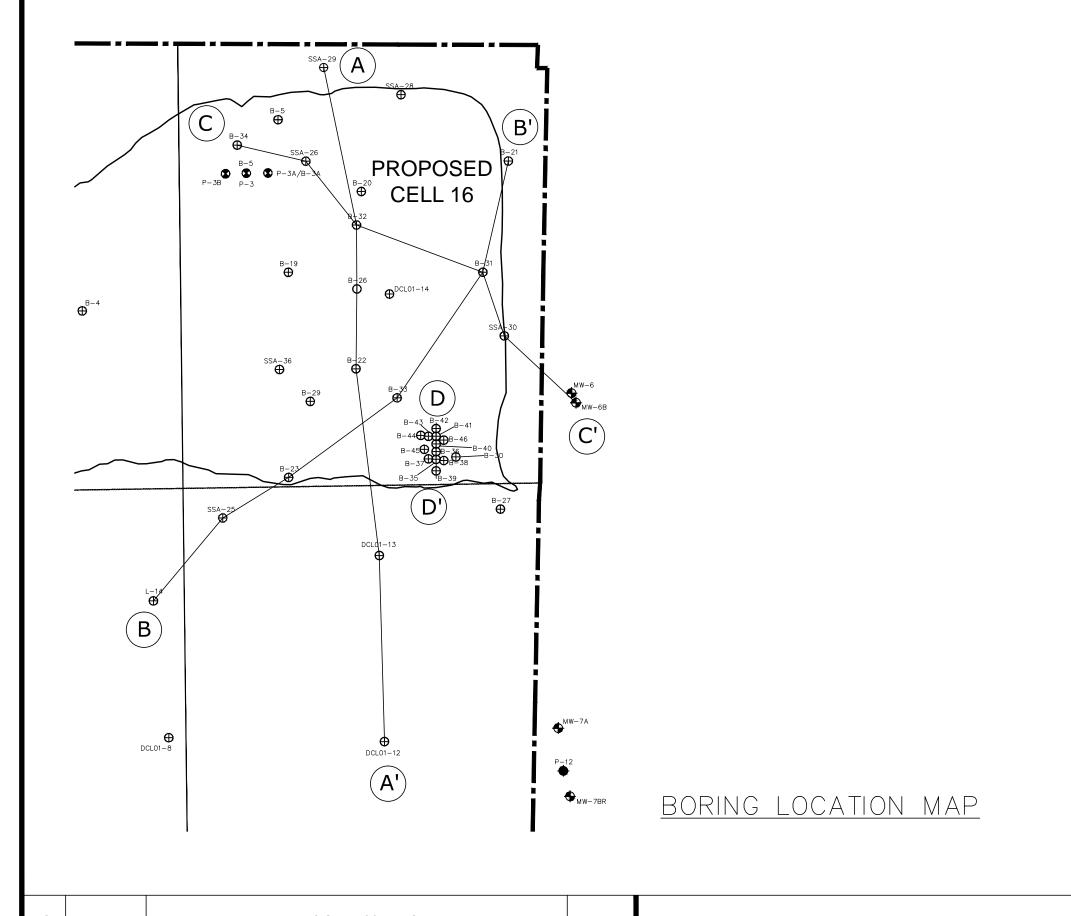
PROJECT NO.:
02000-144-14

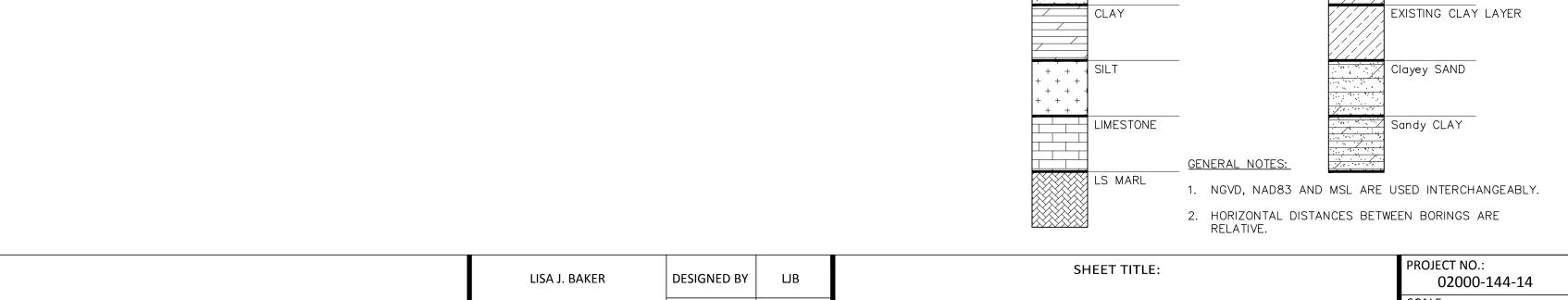
SCALE:
AS SHOWN

DATE:
JUNE 2015

DRAWING:







NO. DATE REVISION DESCRIPTION

BY

Locklear & Associates

Engineering & Environmental Consulting

4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LTK
	CHECKED BY	JDL
FL PE NO. 74652	APPROVED BY	LJB

GEOLOGIC CROSS SECTION D - D'

BORING LOG LEGEND

O2000-144-14

SCALE:
AS SHOWN

DATE:
JUNE 2015

DRAWING:

3' COMPACTED CLAY



UNIVERSAL ENGINEERING SCIENCES 9802 Palm River Road Tampa, Florida 33619

(813) 740-8506

SOIL CLASSIFICATION CHART

TERMS DESCRIBING CONSISTENCY OR CONDITION

COARSE-GRAINED SOILS (major portions retained on No. 200 sieve); includes (1) clean gravel and sands and (2) silty or clayey gravels and sands. Condition is rated according to relative density as determined by laboratory tests or standard penetration resistance tests.

Descriptive Terms	Relative Density	SPT Blow Co
Very loose	0 to 15 %	< 4
Loose	15 to 35 %	4 to 10
Medium dense	35 to 65 %	10 to 30
Dense	65 to 85 %	30 to 50
Very dense	85 to 100 %	> 50

FINE-GRAINED SOILS (major portions passing on No. 200 sieve): includes (1) inorganic and organic silts and clays, (2) gravelly, sandy, or silty clays, and (3) clayey silts. Consistency is rated according to shearing strength, as indicated by penetrometer readings, SPT blow count, or unconfined compression tests.

Unconfined Compressive

Strength kPa	SPT Blow Count				
< 25	< 2				
25 to 50	2 to 4				
50 to 100	4 to 8				
100 to 200	8 to 15				
200 to 400	15 to 30				
> 400	> 30				
	< 25 25 to 50 50 to 100 100 to 200 200 to 400				

GENERAL NOTES

- 1. Classifications are based on the United Soil Classification System and include consistency, moisture, and color. Field descriptions have been modified to reflect results of laboratory tests where deemed appropriate.
- 2. Surface elevations are based on topographic maps and estimated
- Descriptions on these boring logs apply only at the specific boring locations and at the time the borings were made. They are not guaranteed to be representative of subsurface conditions at other locations or times.

SOIL SYMBOLS

FIL	ES ES Y ES TOPSOIL	ASPHALT	CONCRETE	SANO	SAND W	SAND W	SILTY SANO	CLAYEY SAND
E ES PEAT	Sut LOW 2 4510	SLT HIGH B ASTC	ORGANIC SILT	GLAV LOW	GLAY HIGH BLASTIF	LIMESTONE HIGHLY	LINESTONE	DOLOWITE

ОТ	HER SYMBOLS		
<u></u>	Measured Water	$\bar{\nabla}$	Estimated Seasonal

Ma	jor Divi	isions	Group Symbols	Typical Names			Laboratory Classification	Criteria							
	raction size)	gravel no fines)	GW	Well-graded gravels, gravel-sand mixtures, little or no fines			$C_u = \frac{D_{60}}{D_{10}}$ greater than 4; $C_c =$	$\frac{\left(\ D_{30}\right)^2}{D_{10} \ x \ D_{60}} \text{between 1 and 3}$		Sieve sizes	< #200	#200 to #40	#40 to #10	N# 01 01#	
(exe size)	vels if coarse fr o 4 sieve	Clean g (Little or r	GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines	curve,	ols*	Not meeting all gradation require	rements for GW	0)	Sieve	* >	#500	#40 1	*	
No. 200 s	Gravels (More than half of coarse fraction is larger than No. 4 sieve size)	Gravel with fines (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures	ain size curthan No.	dual symb	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are border-	Particle Size		1			_	
arger than	(More is larg	Gravel w (Appre amount	GC	Clayey gravels, gravel-sand-silt mixtures	vel from gr on smaller 1 as follow: N, SP SM, SC	requiring	Atterberg limits above "A" line or P.I. greater than 7	line cases requiring use of dual symbols	Part			45	0	a	
naterial is	irse fraction sieve size)	sands no fines)	sw	Weil-graded sands, gravelly sands, little or no fines	sar of o	nd and gravel from fines (fraction sma e classified as follow, W. GP. SW. SP. GM. GC. SM. SC.	d and grav nes (fraction s classified W, GP, SV SM, GC, S ine cases	$C_U = \frac{D_{80}}{D_{10}}$ greater than 6, $C_C =$	$\frac{\left(\ D_{30}\right)^2}{\ D_{10}\ x\ D_{60}}\ \ \text{between 1 and 3}$		mm	< 0.074	0.074 to 0.42	0.42 to 2.00	2 L 04 00 C
n half the r	nnds of coarse for Clean (Little or Clean	SP	Poorly-graded sands, gravelly sands, little or no fines	ages of sar entage of t ed soils ar cent G	Less than 5 percent More than 12 percent 5 to 12 percent Borde	Not meeting all gradation requir	rements for SW								
(More than		SM	Silty sands, sand-silt mixtures	e percentang on 12 perce	2 percent	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are border-	10,0	Material	Silt or clay		En	-		
	sms sms w spre		sc	Clayey sands, sand-clay mixtures	Determin Dependir sieve) co Less t	Atterberg limits above "A" line cases requiring use of dual symbols						Fine	Medium	Control	
size)	s,	0	ML	Inorganic silts and very fine sands, rock floor, silty or clayey fine sands or clayey silts with slight plasticity	80 FOR	R CLA	RIFICATION OF FINE-GRAINED SOIL AND	1.4.			-	_ ⊑	ū	ci ci	
200 sieve	Silts and Clays	ss than 50	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	70 - FINE	E-GRA	AINED FRACTION OF COARSE-GRAINED SOIL	"The	9	Sieve	21 A 10 C C 1 A 14	3/4 in to 3 in.	3 in. to 12 in.	40 to 10 to	
r than No.	S	- je	OL	Organic silts and organic silty clays of low plasticity	NDEX (PI)		100	100	Particle Size	\perp					
sterial is smaller th	s,	20)	МН	Inorganic silts, micaceous or disto- maceous fine sandy or silty soils, organic silts	PLASTICITY INDEX (PI)				Par	mm	1 76 to 10 1	19.1 to 76.2	76.2 to 304.8	X X 10 0 10 0 10 0	
the materia	Silts and Clays	ater than	СН	Inorganic clays of high plasticity, fat clays	20 -	/	100	MH OR OH		F	37.4	19.1	76.2 tc	304 8	
(More than half the material is smaller than No. 200 sieve size)	IS.	gre	ОН	Organic clays of medium to high plasticity, organic silts		10	ML = OL 1620 30 40 50 60 LIQUID LIMIT (LL)	70 80 90 100 110		a la	76	se	ole	940	
(More	Highly	Soils	Pt	Peat and other highly organic soils			Plasticity Cha	art	Mato	Maleria	Gravel	Coarse	Cobble	Boulders	

When the percent passing a No. 200 sieve is between 5% and 12%, a dual symbol is used to denote the soil. For example; SP-SC, poorly-graded sand with clay content between 5% and 12%.

HARTMAN & ASSOCIATES, INC.

OFFICERS

Gerald C. Hartman, P.E., DEF Harold F. Schmidt, Jr., P.E., DEF James E. Christopher, P.E. Charles W. Drake, P.G. Mark A. Rynning, P.E., M.B.A. William D. Musser, P.E., P.H. Michael B. Bomar, P.E. Lawrence, E. Jenkims, P.S. M.

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> March 30, 2004 (Resubmitted July 15, 2004)

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W Bruce Liferna, PG
Alexis K Stewart, PE
Ada R Terrero

HAI #99.0331.007

We Brace Lairenz, Palexis K Stewart, I Alexis K

Via UPS Ground

Ms. Susan Pelz, P.E. Florida Department of Environmental Protection Southwest District 3804 Coconut Palm Drive Tampa, Florida 33619

Subject:

Grouting Completion Report

Enterprise Recycling & Disposal Facility Angelo's Aggregate Materials, Ltd.

FDEP Permit Nos. 177982-001-SC, 177982-002-SO

Pasco County, Florida

Dear Ms. Pelz:

On behalf of Angelo's Aggregate Materials, Inc. (AAM), Hartman & Associates, Inc. (HAI) is submitting for your review the grouting completion report for the remediation of the subsidence area in cell 16, at the subject site in Dade City, Florida.

The subsidence area was discovered during an HAI site visit on January 12, 2004. The Department was notified about the existing site conditions within 24-hours, as required by the approved Construction Permit. AAM was advised by one of its consultants to fill in the subsidence area with clay immediately to prevent any additional slumping and to create areas stable enough to accommodate a drill rig. The approximate location of the subsidence area prior to being filled and the top of the excavated slope was marked and surveyed by Foresight Surveyors, Inc. A map showing the surveyed location of the subsidence area is included as Figure 1. HAI was onsite from January 15 through 17, 2004 with UES drillers to complete SPT borings in an effort to delineate the lateral and vertical extent of the subsidence area.

Using the lithologic description and blow count data from the SPT borings, engineers from UES calculated the approximate volume of grout required to remediate the subsidence area. LRE Ground Services, Inc. was onsite from March 2 through 9, 2004 to complete the grouting operation. A total of 357 cubic yards of grout was injected into a total of twenty-seven (27) grout injection points, within and adjacent to the original subsidence area.

Universal Engineering Sciences, Inc. (UES) observed the remedial grouting operation at the site, performed by LRE Ground Services, Inc. A grouting completion report, signed and sealed by a UES engineer has been included in Attachment A. Field notes completed by the onsite UES technician during the remedial grouting are included in Attachment B.



Ms. Susan Pelz, P.E. March 30, 2004 Page 2

We trust that we have provided the adequate information required for the submittal of the grouting completion report for the subject site in Dade City, Florida. Please feel free to contact us if you require additional information or have any questions.

Very truly yours,

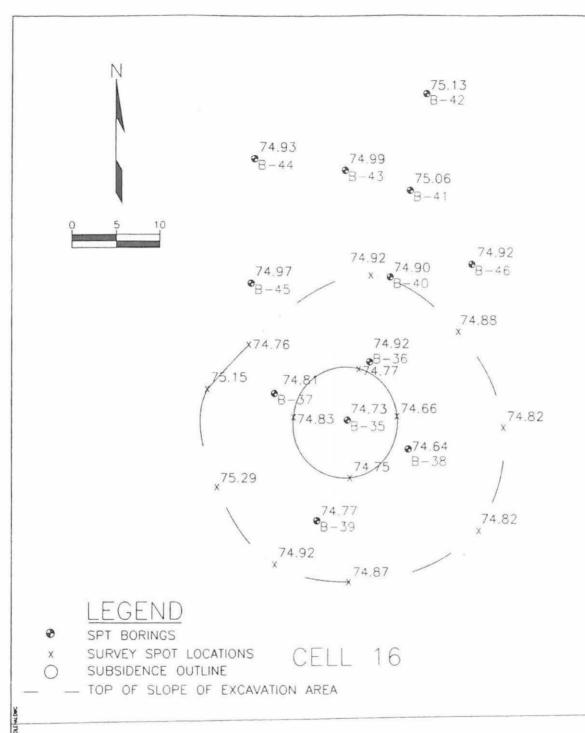
Hartman & Associates, Inc.

Miguel A. Garcia Project Hydrogeologist Bruce W. Lafrenz Project Hydrogeologist/Associate

MAG/cr/99.0331.007/corresp/grouting completion.doc

CC'

Dominic Iafrate, Angelo's Recycled Materials, Inc., Warren, MI Craig Bryan, Angelo's Aggregate Materials, Inc., Largo, FL



CELL 15



HARTMAN & ASSOCIATES, INC. engineers, hydrogeologists, surveyors & management consultants

201 EAST PINE STREET - SUITE 1000 - ORLANDO, FL 32801 TELEPHONE (407) 839-3955 - FAX (407) 839-3790

SUBSIDENCE AREA ENTERPRISE LANDFILL & DISPOSAL FACILITY PASCO, FLORIDA

FIGURE 1



ATTACHMENT A





March 10, 2004

Mr. Dominic lafrate Angelo's Recycled Materials, Inc. 1755 20th Avenue SE Largo, FL 34641

Reference:

Grouting Completion Report

Dade City Class III Landfill NEC Enterprise Rd. and Auton Rd.

Dade City, Florida

UES Project No. 80626-002-02

Dear Mr. lafrate:

As authorized, Universal Engineering Sciences, Inc. (UES) observed remedial grouting operation at the proposed retention area at Dade City landfill, performed by LRE Ground Services, Inc. The purpose of the grouting operation was to remediate suspected sinkhole conditions below the portion of the retention area by filling of any subsurface voids encountered in the general vicinity of the soil subsidence that occurred recently at this location.

UES developed the grouting program based on geotechnical subsurface exploration at the subject site directed by Hartman and Associates. The assessment regarding the remedial scope of work was made based upon the subsurface information provided by the SPT borings performed within the general vicinity of the soil subsidence.

A total of twenty seven (27) grout injection points were used during the grouting program. The approximate location, depth of installed casing, and actual pumped grout quantity for each grout injection point location are presented on the attached Grout Injection Point Location Plan. The installed length of the grout injection points generally varied from 10 to 46 feet, reflecting the variable subsurface conditions encountered during the geotechnical exploration. Grout injection point #26 however, was installed within a major void or partially filled void within limestone, believed to have contributed to the recent sinkhole related subsidence. A total of 68.6 yards of grout (nearly 20% of the grout total) was injected through this grout injection point alone. Total of 886 feet of casing was used to inject 357 cubic feet of grout. Approximately 8 cubic yards of grout was returned after completion of the grouting program.

The completion date, installed length of each grout injection point and the amount of grout pumped is presented in the following table. The grout injection points are listed in numerical order.

Angelo's Recycled Materials, Inc. UES Project No. 80626-002-02 March 10, 2004

GIP#	DATE COMPLETED	CASING LENGTH (FT)	TOTAL GROUT PUMPED (YDS ³			
1	March 3, 2004	45	27.2			
2	March 2, 2004	45	27.0			
3	March 2, 2004	38	19.9			
4	March 2, 2004	34	7.1			
5	March 3, 2004	26	3.0			
6	March 8, 2004	30	26.0			
7	March 8, 2004	46	32.5			
8	March 5, 2004	32	9.4			
9	March 5, 2004	34	14.5			
10	March 3, 2004	26	17.2			
11	March 9, 2004	22	1.8			
12	March 9, 2004	27	1.2			
13	March 5, 2004	31	7.0			
14	March 5, 2004	32	17.9			
15	March 9, 2004	35	4.1			
16	March 9, 2004	35	3.8			
17	March 5, 2004	29	0.2			
18	March 4, 2004	33	10.2			
19	March 8, 2004	34	0.2			
20	March 8, 2004	35	6.8			
21	March 8, 2004	36	1.4			
22	March 9, 2004	10	0.1			
23	March 5, 2004	38	19.0			
24	March 8, 2004	30	16.5			
25	March 8, 2004	43	14 4			
26	March 5, 2004	60	68.6			
	TOTAL	886	357.0			

Based on the grout take and depth of grout injection points, it appears that one major cavity and several zones of very loose soil conditions indicating possible sinkhole activity may have existed in the immediate vicinity and to the north of the occurred subsidence

Angelo'S Recycled Materials, Inc. UES Project No. 80626-002-02 March 10, 2004

Based on our observation of the grouting program performed within the proposed retention area, and our subsequent analysis of data gathered during the grouting, we feel that the intent of the remedial program was met. In our opinion, the subsurface grouting met the goals of the remedial program, by improving the overall subsurface conditions within the treated area and reducing the risk of future soil subsidences. We note that measures such as subsurface grouting are intended to treat, in a practical and cost-effective manner, potentially detrimental subsurface conditions which could affect the ground surface. However, evaluation of the effectiveness of treatment is subject to inference and interpretation of the end result and cannot be predicted with certainty.

It has been a pleasure assisting you with this phase of your program. If you have any questions regarding this report or when we can be of further assistance please contact the undersigned at (813) 740-8506.

Respectfully submitted,

UNIVERSAL ENGINEERING SCIENCES, INC.

Certificate of Authorization No. 549

Dusan Jovanovic

Senior Project Manager

Mark Hardy, P.E.

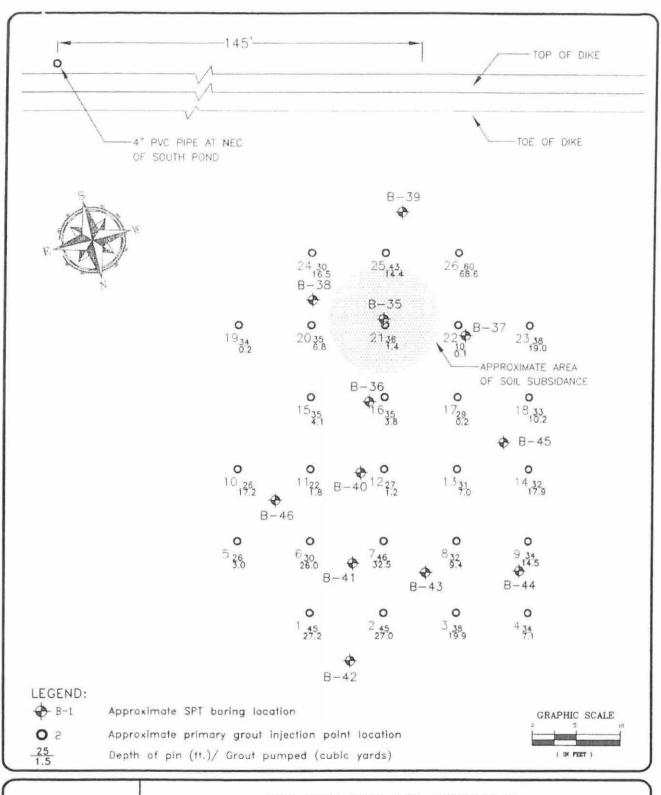
Tampa Regional Manager

Professional Engineer No. 57233

Date_ 3-10-04

Attachment: Grout Injection Point Location Plan

cc: Client (3)





RETENTION POND SOIL SUBSIDENCE DADE CITY CLASS III LANDFILL DADE CITY, FLORIDA

FINAL GROUT INJECTION POINT LOCATION PLAN

DRAWN BY: C.C.	DATE: MAR.	10, 2004	CHECKED BY: D.J.	DATE: MAR. 10, 2004
SCALE: 1" = 10'	PROJECT NO:	80626-002	-02 REPORT NO:	APPENDIX:



9802 Palm River Road
Tampa, Florida 33619-4438
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Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.ues@com
Tampa, Florida 33619-4438 Universal Engineering Sciences, Inc.

onent.						Injection Point							
roject:		DADE CI	TY LANDFI		Injection Point:								
Csng. Depth	Grou	ut Time	Max. Pressure	Pump	R	Reason to stop pumping							
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks				
45	← TOTAL C	ASING DEPTH	1	8					Soit much				
1/5	10:11	1037	200	496					End Time Comes	(9.0			
				601.55					New Truck				
42	1129		5004	5					00057				
38			256/40	86					00007				
38		1:56	220	192					End Truck Piece 16	(90			
				3-7	ş Î				NEW Truck BRES				
32	1210	1237	200	490			/		End Truck BRE 5	90			
				7-5									
27	1036		JUD+	2					00017				
25			17	1/					R6017				
22	1315	13/1	300+	9				X	completed	(.2			
2 1500									Go To 10				
										The state of the s			
		GH - Groun	d Heave;	GP - Grout	out				Communication				
Supervisor: Company: LRE					Total (Cu. Yd.):								
0.00	Date (Cu. Y		40- p										



Universal Engineering Sciences, Inc. 9802 Palm River Road

Tampa, Florida 33619-4438

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Client: Project:	ANG	LL				1	Injection Point: 2	-		
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F	Reasor	n to ste	op		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks	
45	← TOTAL C	ASING DEPTH						Continue Truck		
115	1401	1126	160	1168					End Truck BEET	9.0
				5.4%					Now Truck	
42	14 33	1433	4014	5	X				0015	-
110			400+	1.	X				10057 10055	-
38	1434	1458	140	427					End Trycle 11th 10	90
				C.					NEW Tirck	
32	1531	15 58	216	523					Earl Truck BPK5	(9,0
27							X	1	Ret 5	_
22		16 18						X	Flusti	_
									Comple Ted	1
									EDD DAY	
										_
										_
HP - Higi	h Pressure;	GH - Groun	d Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication	
Supervis	sor:				_		Insp	ecto	r: JOHN MOTKO	_
Compan	y:	LRE			Total (Cu. Yd.): 27.0					
Total To	Date (Cu. Y	d.):			-					



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GROUT MONITORING LOG

DAYONE

Client:	ANG	ELO'S RECY	CLING					[Date: . 3-2-04	
Project:	-	DADE CIT	TY LANDEL	<u> </u>					Injection Point: 3	
Csng.	Grou	ıt Time	Max	Pump	F	Reason		op qu		ĺ
(ft.)	Start	Finish	Pressure (psi)	Strokes	H	G H	G P	C M	Remarks	
38	← TOTAL C	ASING DEPTH		进事					STORT Tivek	
37	1028	1050	180	446					End Truck BRY 5	9.0
32	1131	1156	200	1/94					X/ Tul Terek End Truck Part	9.0
				3.7					New Time	
27	125/	1251	400+	3	X				P.p. 2147 3 FT	
22			400+	8	χ				REKIO	
17	1301	12 (1)	200	53	ſ				Water put Ground IP 8	
13	1705	1307	200	110	X	X			South Side of I.P.	
									completed	(1.9
									Co To 4	
		GH - Groun	d Heave;	GP - Grout	tout				Communication	
Supervis	-	LRE			-	Total			r: JOHN MOTKO):	
Total To	Data (Cir V	d).								



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Client: Project:						: ANGELO'S RECYCLING Date: 3 2 0 4 :t: DADE CITY LANDFILL Injection Point: 4								Injection Point:
Csng. Depth	Grou	ut Time	Max. Pressure	Pump	F	leasor purr	n to ste	ор						
(ft.)	Start	Finish	(psi)	Strokes 3-9	H			C M	Remarks					
34	← TOTAL C	ASING DEPTH	1	110					Continue Twee					
32	1321		200	1.5					WATER OUT GOILS AT IP					
32		1341	220	511					End Truck BAKT (7					
27							X		End Truck BAKT (7					
22							X		BEKS					
17														
				雙中					New Truck					
17	1351	1351	100	2				X						
									compleTell					
									Go TO 2					
HP - High	n Pressure;	GH - Grour	nd Heave;	GP - Grout	out	of Pi	ipe;	CM -	Communication					
Supervis	or:						Insp	ecto	r: JOHN MOTKO					
Company	y:	LRE			Total (Cu. Yd.): 7.									
Total To	Date (Cu. Y	d.):			i.									



Universal Engineering Sciences, Inc. 9802 Palm River Road

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Client:	ANG											
Project:	DADE CITY LANDFILL			<u> </u>					Injection Point: 5			
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to ste	ор				
(ft.)	Start	Finish	(psi)	Strokes 5-9	H	G H	G P	C M	Remarks -			
26	← TOTAL C	ASING DEPTH		459					Continue True			
26	1501		160	465					Food Truck Out Groved IP			
		1503	160	492					End Truck			
			(5) (F. 7)					NEW Truck				
26	1517	1517 1504 210 125							Bet 5			
22							X		cer 5			
17	15.7.1	15.32 180 /32				X			Deet			
12							X		completed 6			
									Go To 26			
		-15-75-75-75-75-75-75-75-75-75-75-75-75-75										
HP - High	P - High Pressure; GH - Ground Heave; GP - Grou						ipe;	CM -	- Communication			
Supervis	upervisor:						Insp	ecto	or: JOHN MOTKO			
Company	Company: LRE					Tota	(Cu	Yd.	.):			
Total To	al To Date (Cu. Yd.):											



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Client:	ANG	ANGELO'S RECYCLING DADE CITY LANDFILL							Date: 3-8-04	
Project:	\ <u></u>	Grout Time Max.							Injection Point:	
Csng. Depth	Grou	ut Time	Pressure	Pump	F	Reason	n to st	ор		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks	
30	← TOTAL C	ASING DEPTH	1	460					CLAT TOUCK (7.	<u> </u>
	1130	1502	200	647						
30	15//2	15/6 1547 15/210 630							NAW TRUCK port 10.	7
27	1214	12 (1	1-77	450			X			_
		Ktys &					-		Plant Stap sender Trucks	
			KEYS						Continue Truck from	
27	24		435		χ			I.P. 21		
22							X	-	BRICT	_
12	1458	1700	300	456				X	End Tivil	2
HP - Hig	P - High Pressure; GH - Ground Heave; GP - Grou				tout	of P	ipe;	CM -	Communication	
Supervis	upervisor:				-		Insp	ecto	or: JOHN MOTKO	
Compan	mpany: LRE				-	Tota	l (Cu	. Yd.):26.0	
Total To	To Date (Cu. Yd.):									



Tampa, Florida 33619-4438 Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client: Project:	ANG	DADE CIT	CLING Y LANDFIL					[Date: 3-8-04 Injection Point: 7	
i rojedi.		DADE OII	TEARDIN						injection (vint.	
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to sto	pp		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks	
46	← TOTAL CA	ASING DEPTH	CCMEY	100					STAIT TIVILE	
42	10114	1116	160/	672					End Truck nows 10	
37	1159	15.11	Cemix.						That Truck BRKS 10	
3/	1159	1231							Altw Truck BRIES 10.	
32	13 63	1327	180 god	462	V				BEIT	
27	1326	1348	160	668					End Truck BAY (10	
									Alin Trock	
22	1412	1405	JOD 300	451	X	X		-	- BW 5	
17		7 . 2					У		BRY	
12	1439	1444	201/	160		X			(bm ple fel 2.	
		(at mail							(D) TO (D	
HP U:al	Procesure	GH Groun	d Hoover	GD Gra	1.0114	of P	ine: /	- BA	Communication	
Supervis		3r - G10u	i out	UI P			r: JOHN MOTKO			
Çompan	y:		Total (Cu. Yd.): 32.5							



Universal Engineering Sciences, Inc. 9802 Palm River Road

Tampa, Florida 33619-4438

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Client:	ANG	ELO'S RECY	CLING					I	Date: 3-5-04					
Project:	DADE CITY LANDFILL								Injection Point: 8					
Csng. Depth	Grou	t Time	Max. Pressure (psi)	Pump	F	Reason to stop pumping Remarks								
(ft.)	Start	Strokes	H P	G H	G P	C M	Remarks							
32	← TOTAL C	ASING DEPTH		30		12			Commune Testes					
32	1725	1738	180/200	198		X			nert					
27		1					X		CPE					
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17	175#	493												
12					X		End Tives per							
									END MAY					
									60 70 7					
								_						
								_						
HP - High Pressure; GH - Ground Heave; GP - Grou						of P	ipe;	CM -	Communication					
Supervis	upervisor:						Insp	ecto	r: JOHN MOTKO					
Compan	mpany: LRE				Total (Cu. Yd.): 9.4									
Total To	Date (Cu. Y		-											



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Client: Project:	ANG	ELO'S RECY DADE CI	CLING	ш					Date: 3-5-29 Injection Point: 9
Csng. Depth	Grou	it Time	Max. Pressure	Pump	F		n to st	ор	
(ft.)	Start	Finish	(psi) BeTin	Strokes	H P	G H	G P	C M	Remarks
34	← TOTAL C	ASING DEPTH		群物					STORT TOURS
34	12.12	1229	190/100		X				BRY 3
32					,		X		OFF
27	1234	1236	180/100	39/	X		/		RPET
22	1210	1249	150	624					End opull
		1319 13-0 139/80 25					-		How Truck
22	1319	13-6	150/80			X			DEE -
17		12-482-contract					X		Dev -
/2									
									60 70 14
		-	-			-			60 10 17
		 	 			-			
			-						
						-	7-11-1		
			-						
			1			_			
						-			
P - High	n Pressure; GH - Ground Heave; GP - Gro				out	of P	ipe;	CM -	Communication
upervis	or:				_		Insp	ecto	r: JOHN MOTKO
ompan	: LRE					Tota	l (Cu	. Yd.)):14,5
atal To	Date (Cu. Y	'd):							



Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client: Project:	ANG	ELO'S RECY					ı	Date: 3-3-04 Injection Point: /0		
Csng. Depth	oth Pressure Pump	Pump Strokes		Strokes	F	Reason	n to st	ор		
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks	
33	← TOTAL CASING DEPTH 9								Continue Truck	
	1378 1401 160 481								End Twee BRES	8,8
									How Truck	
27	11113	11/35 200/40 371/							WATER OUT Grand I.P. 6	
27									DAT 5	
22	14 43	1443 1419 200 459				X			BAKT	
17							X		BPKT	
12	2						X		campleteel	
	12							/	8.4	
									Go To 5	9
						_				
								_		
	L	L	1			<u></u>				
HP - High	P - High Pressure; GH - Ground Heave; GP - Grou				t out	of P	ipe;	CM -	Communication	
Supervis	upervisor:				_		Insp	ecto	r: JOHN MOTKO	
Compan	y:	LRE				Tota	(Cu	. Yd.):17.2	
Total To	o Date (Cu. Yd.):									



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Client:	ANG	ELO'S RECY					ι	Date: 3-9-04		
Project:		DADE CITY LANDFILL							Injection Point: //	
Csng.	(psi) Strot				F	leason	to sto	op		
Depth (ft.)	Start	Finish	Pressure	Pump Strokes	Н	g G	g G P	С	Remarks	
22	← TOTAL C	ASING DEPTH		249	P	Н	P	М	Continue Timbe	
22	956	1001	170	35/		X			BRKT	
17							X		BERT	
12	1006	1006	170	359				X	Campleted (1)	8
							-			1
									60 TO 12	
				-						
		-								
							_	-		
							-			
HP - Higl	n Pressure;	GH - Groun	d Heave; (GP - Grout	tout	of Pi	pe; (CM -	Communication	
Supervis	or:				_		Insp	ecto	r: JOHN MOTKO	
Compan	y:	LRE				Γotal	(Cu.	. Yd.)):	
Total To	To Date (Cu. Yd.):									



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Client: Project:	ANG					[Date: 3-9-04 Injection Point: 12					
Csng.	Grow	(psi) Stroke						on.				
Depth (ft.)	Groun	rime	Pressure	Pump Strokes		leason pum	ping	ф	Remarks			
1007	Start	Finish	(551)	1-10	H P	G H	G P	C M	7.07.07.10			
27	← TOTAL CA	← TOTAL CASING DEPTH 359							Continue Truck			
27	10 18		210	1/26		X			CONTINUE TRUCK			
22							Y					
17	1027 1028 210 43/					χ		X	completed	1.2		
							GO TO 16					
							_					
HP - High Pressure; GH - Ground Heave; GP - Grou						of Pi	ipe; (CM -	Communication			
Supervis	upervisor:						Insp	ecto	r: JOHN MOTKO			
Compan	mpany: LRE					Total (Cu. Yd.): 1.2						
Total To	al To Date (Cu. Yd.):											



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Client: Project:	ANG	ELO'S RECY	CLING TY LANDFII					ı	Date: 3- 5-0 / Injection Point: 13	
Csng Depth	Grou	t Time	Max. Pressure	Pump	F	Reasor	n to sto	op		
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks	
3/	← TOTAL CA	ASING DEPTH		200					Continu Truck	
3/	1639	1456	180 180	557					Continu Truck	4
			B-mix	语 强度					Mrw Truck	
31	1701	176	500+	2	Y				Pipe DIST	
29		1702 300+ 5 1708 1709 160 30							Par 11/9 REV 10	
22	1708	1708 1709 160 30						X	completed .	6
									60 10 8	
			W							
				10						
HP - High	n Pressure;	GH - Groun	d Heave;	GP - Grout	out	of Pi	ipe;	CM -	Communication	
Supervis	or:		HI	***	-		Insp	ecto	r: JOHN MOTKO	
Compan	Company: LRE							. Yd.): 7.0	119
Total To	Date (Cu. Y	d.):								1



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GROUT MONITORING LOG

Client:	ANG	ELO'S RECY		Date: 3- 5.04							
Project:		DADE CI	TY LANDFII						Injection Point:		
Csng. Depth	Grou	it Time	Max. Pressure	Pump	F	Reasor pum	n to sta	op	Domestic .		
(ft.)	Start Finish		Strokes	H	G H	G P	C M	Remarks			
32	← TOTAL C	ASING DEPTH	1	255					C. Teuck		
	1340	1355	150/20	572					C. Teuck Eny Truck		
			KIYS	skiden.					Mry Truk		
32	1408	1438	160/160	630					End Twik Bots (
			B-MIX	\$45-10A					Min Tivile		
27	1558	11,04	130/400	126	X				BECT		
25				1.0			X		DRE =		
17	16 10	16 13	160/180	189		X			Crti		
12							X		completed 3		
									Co TO 17		
						_					
UD Uint	Draceure	CU C	d Usawa i	CD Crow		- 6 P	ina	CM	Communication		
	- High Pressure; GH - Ground Heave; GP - Groupervisor:			out	Or P			r: JOHN MOTKO			
Company	pmpany: LRE			-	Total			and the second s			
	tal To Date (Cu. Yd.):						191				

H:\djovanovic\GroutIng\Grout Monitoring 7 oaks.wpd



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Client:	ANG	ELO'S RECY	CLING					ı	Date: 3-9-04				
Project:									Injection Point:				
Csng. Depth	Grout	t Time	Pressure	Pump	F	Reasor	to sto	эр	Remarks				
(ft.)	Start	Finish	(psi)	Strokes GMZY	H P	G H	G P	C M	Remarks				
35	← TOTAL CA	ASING DEPTH		THE PARTY					STURT TINK				
35									TIGHT PIPE BEKT				
32									TIGHT PIPE BRYT				
27	930 939 100 187					X			PART 5				
22	9 44 9 19 160 24						X			-			
17	944 949 160 24							X	completed	4.1.			
							60 TO 11						
							,						
	×												
HP - High Supervis		GH - Grour	d Heave;	GP - Grout	out				r: JOHN MOTKO				
Company						Total (Cu. Yd.): 4.1							
Total To	Date (Cu. Y												



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Client:	ANG	ELO'S RECY	CLING					ı	Date: 3-9-04			
Project:	-	DADE CI	TY LANDFII	<u></u>					Injection Point: / 6			
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to sto	op q	Remarks			
(ft.)	Start	Finish	(psi)	Strokes 1-10	H P	G H	G P	C M	Remarks			
35	← TOTAL CA	ASING DEPTH		43/					Continue Touck			
	1036	1	500+	466	X							
			if	1447	У							
		1037	11	441	У				DPY5			
32	10341	1041	500+	169	X				DOUT			
31	1059	10:63	210/	540		X			BRK 5			
27	10 30	1027	210	605		1			End Touch	2.9		
		1	1							1		
			Pros	2-9					Mrw Trull.			
27	111/2	11.1	200	36		1						
2/	1150	1151	277/	40		X			orde T Brut			
17	11.00	11111	277	10		1	X		3811	.9		
17							<u></u>		Chon letal			
10									(1)277 14 141			
									Co To 22			
HP - High	Pressure;	GH - Groun	d Heave; (GP - Grou	tout	of P	ipe; (CM -	Communication			
Supervis	or:						Insp	ecto	r: JOHN MOTKO			
Company	/:		4		Total	(Cu.	Yd.	3, 8				
Total To	Date (Cu. Y	d.):			_							



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Client:	ANG	ELO'S RECY	CLING					ľ	Date:	3.	-5-09	
Project:	200	DADE CIT	TY LANDFIL						Injection	Point:	17	-
Csng. Depth	Grou	t Time	Max. Pressure	Pump	R	leasor pum	to sto	op				
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M		Remarks	3	
29	← TOTAL C	ASING DEPTH		189					Continue	Truck		
29	1425	1626	260	195					Continue Pipe o	117	BATT	
27							X				BAKT	
25	1631	163/	200	198				Ĺ,	Pope ?	17		
20	1433	1637	200	200				X	com	n le Teci	/	\Box (,2
							_		Go To		, ,	_
							_					_
												4
								-				
					_							
HP - High Supervis		GH - Groun	d Heave; (GP - Grout	out				Communication:			_
					7		100		-	0.2		_
Compan	y:	LRE			-	Total	(Cu	. Yd.):	*		
Total To	Date (Cu. Y	d.):		A	-							



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Client:	ANGELO'S RECYCLING DADE CITY LANDFILL						1	Date: 3.4-04				
Project:		DADE CIT	TY LANDFI	LL					Injection Point: 18			
Csng. Depth	Grou	1 Time	Max. Pressure	Pump	F	Reasor pun	n to sta	ор				
(ft.)	Start Finish (psi) Strokes		H	G H	G P	C M	Remarks					
33				0				Π	NEW TINCK			
33	1420	1446	240	468					End Truck BRES 90			
				4.3					1/1W Tisck			
27	15.16	1549	300	77		X		星				
22	15 49	1551	300	43				X	DENT completed 1.2			
17									completed "			
									Go TO 23			
HP - High		d Heave;	GP - Grout	out	of P			Communication or: JOHN MOTKO				
Compan					Total (Cu. Yd.): 10. 2							
Total To	otal To Date (Cu. Yd.):											



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Client: Project:	ANG					,	Date: 3-8-04 Injection Point: 19		
i rojeci.	9-6-	DADE O	TY LANDFII						injection i diffe
Csng Depth	Grou	ut Time	Max. Pressure Pump (psi) Strokes		R		to sto	эр	
(ft.)	Start	Finish	Strokes	H	G H	G P	C M	Remarks	
31/	← TOTAL C	ASING DEPTH	l	37					Continue Truste
34									Dest
32	1415		300 F	39	X				noon
50			500 T	45	4				BRY
27			5001	47	X				BERT
22			5001	49	X				Brr
17			2001	70	Y				BRIET
12.		1450	5001	71	Y				1 umpleted
				_					
									Gn 70 20
		<u></u>	1						
HP - High	h Pressure;	GH - Groun	nd Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication
Supervis	or:						Insp	ecto	r: JOHN MOTKO
Compan	any: LRE				_ :	Total	(Cu	. Yd.): 0.2
Total To	Date (Cu. Y	(d.):					14		



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Client:	ANG					į	Date: 3	-8-7004			
Project:	-	DADE CI	TY LANDFII	<u></u>					Injection Point:	20	
Csng Depth	Grou	t Time	Max. Pressure	Pump	F	Reason pun	n to sta	op			
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Rema	rks	
35	← TOTAL CA	ASING DEPTH		7/					Cont Treck		
32	1956	1956		72	X					13665	
78				73	X					artt	
27	1459		300+	78	X					DUST	
25		1509	400+	285	1				/	DVC	
112	15/4	1521	180/	422		X				DEKS	
17							X			Delex	1
12							y		Complet.	4	6:
							1			*	
									GO TO	2/	
lP - High	Pressure;	GP - Grou	t out	of P	ipe;	CM -	Communication				
Supervis	visor:						Insp	ecto	г: ЈОНИ МОТКО		
Company	any: LRE					Total	(Cu	. Yd.	6.8		
otal To	Date (Cu. Yo	d.):			_						



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Client: Project:	ANG					ľ	Injection Point: 2/						
Cono	Grow	I Time	I May		T	Reasor	, to ek						
Csng. Depth (ft.)	Grou	i rime	Max. Pressure (psi)	Pump Strokes			nping	J.D.	Remarks				
	Start Finish 1/- 9				H P	G H	G P	C M					
36	36 ← TOTAL CASING DEPTH 43								Centime Trucke				
	1536	1540	150	480					End Truck news	(.9			
32							X						
			KEYS	347					STUT TIVEK				
27	1600	1600	180	2		V			nelet				
25	1608	1609	180	24		7			DEKT DEKT				
17	1600	1607	150	27		H	X		BRKS	1.5			
12									Die C				
12													
									GO TO 6				
									50 10 0				
								-					
						-							
							-	_					
						_							
						_							
					_								
HP - High	IP - High Pressure; GH - Ground Heave; GP - Gro							CM -	Communication				
Supervis	upervisor:							ecto	r: JOHN MOTKO				
Compan	npany: LRE						Total (Cu. Yd.):						
Total To	Date (Cu. Y	d.):											



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,11,0

Client:	ANG	ELO'S RECY	CLING					ı	Date: 3-9-04		
Project:		DADE CI	TY LANDFII	LANDFILL					Injection Point: 22		
Csng	Grou	ut Time	Max.		F	Reason		op			
Depth (ft.)	Start	Finish	Pressure (psi)	Pump Strokes	H	G H	G P	СМ	Remarks		
10	← TOTAL C	ASING DEPTH		40		H		Ī	Can Trase Tench		
1159	1159	1139	200	116				X	Completed		
									Job Completed		
		-									
									SFAT BACK 804		
-											
HP - High	n Pressure;	GH - Groun	d Heave;	GP - Grou	t out	of P	ipe; (CM -	Communication		
Supervis	or:						Insp	ecto	or: JOHN MOTKO		
Company	ny: LRE				Total (Cu. Yd.):						
Total To	Date (Cu. Y	'd.):			_						



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Client:	ANG	ELO'S RECY	CLING					j	Date: 3-1/-01/ Injection Point: 23
Project:		DADE CIT	TY LANDFII						Injection Point:
Csng. Depth	Grou	t Time	Max. Pressure	Pump Strokes	F	Reasor	n to sta	op	
(ft.)	Start	Finish	(psi)	11-9	H	G H	G P	C M	Remarks
38	← TOTAL CA	ASING DEPTH	6-	Q209					CIATIANA TRICE
38	1609	/631	140	491					End Trulle But 5 (
HP - High Supervis	d Heave; (3P - Grout	t out				r: JOHN MOTKO		
Company: LRE					- -	Total			2 4
Total To	Date (Cu. Yo	d.):			_				



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Client:	ANG	ANGELO'S RECYCLING DADE CITY LANDFILL							Date: 3.5.04
Project:		DADE C	ITY LANDEI	LL			1	1171	net Injection Point: 23
									from 3 4-05
Csng. Depth	Grou	ıt Time	Max. Pressure	Pump	F	Reasor	n to st	ор	
(ft.)	Start	Finish	(psi)	(psi) Strokes H		G H	G P	C M	Remarks
	← TOTAL C	ASING DEPTH	f	学科学样别					STAIT TNIK
22	1217	124/	160						End Truck DRE-
			KEYS	阿艾尔					X/rw Truck
27	1247	1249	140/110	4/	X				DR165
22	1255	1255	1100 +	1/3	X			X	Mrw Truck OK16 & Completed
17									/
									60 BACK TO 26
									я.
dP - Higi	h Pressure;	GH - Groun	nd Heave;	GP - Grout	out	of P	ipe;	CM -	Communication
Supervis	or:						Insp	ecto	от: ЈОНИ МОТКО
Compan	y:			Tota	I (Cu	. Yd.)	1: 7.8 + 11.2 = 19.0		
fotal To	I To Date (Cu. Yd.):								



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Client:	ANG	ELO'S RECY	CLING						Date: 3-8.04	
Project:		DADE CIT	TY LANDFIL						Injection Point:	
Csng.	Grout	Time	Max.	Pump	R		to sto	op.		
(ft.)	Start	Finish Pressure Pump Strokes			H P	G H	G P	C M	Remarks	
30	← TOTAL CA	SING DEPTH	1	135					Continue Truck	
30	1225	12110	140/	459					End Truck Driet	6.4
									Ktw Teach	
27	1205	1327	180	441					End Tirel DRICT	9.0
			K879	Marie					1/7W Trick	
22	1355	13 = +	160	21				1	WATER AND GENERA IP 20	
17		12-6	160/	5/			¥	X	CompleTeel	(1.1
		- Aurio							,	
									Co To 19	
HP - High	n Pressure;	GH - Groun	d Heave;	GP - Grout	out	of P	ipe;	CM -	Communication	
Supervis	or:				_		Insp	ecto	г: ЈОНИ МОТКО	
Compan	y:	LRE			1	Total	(Cu	. Yd.): 16.5	
Total To	Date (Cu. Yo	d.):								



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Client: Project:		ANGELO'S RECYCLING DADE CITY LANDFILL						ſ	Date: 3-504 Injection Point: 25	
Csng. Depth	Grou	ut Time	Max. Pressure	Pump	F	Reasor	n to sto	ор		
(ft.)	Start	Finish	(psi)	Strokes	H	GH	G P	C M	Remarks	
43	← TOTAL C	ASING DEPTH		325	T				Cin Tauch	
47			I						TIGHT POR DEES	
42									""	_
37	1756	1802	180/	469					FACT TIME 2	,8
32									Constance Tight par press II I' I' End Truck Flush BRK 0	
.32						-			End Dist	
									,	
HP - Higl	h Pressure;	GH - Grour	nd Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication	
Supervis	ior:				-		Insp	ecto	r: JOHN MOTKO	
Compan	y:	LRE			-	Total	l (Cu	. Yd.)	2.8 +	
Total To	Date (Cu. Y	(d.):	Chapter Carlo		_					



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Client:	ANG	ELO'S RECY	CLING				_	1	Date: 3-804	
Project:	-	DADE CIT	TY LANDE!				(0)	7111	from 3-5-04	
Csng. Depth (ft.)	Grou	ut Time	Max Pressure	Pump Strokes	F		n to st	op	Remarks	
(11.)	ft.) Start Finish (psi) Strokes				H P	G H	G P	C M	Remarks	
	← TOTAL C	ASING DEPTH	R8-15	阿兴等					STEPT TIVE	
32										0
27	1026	1048	200	461					End Truck Ext	90
			KEYS	my Sayes					NEW TIVE	
22	1150	1156	200/	126		X			AT I.P. BREST	
17							X		124-	6
12	1205	1205	200	135		X			Completed	2.1
									Go TO 24	
HP - High	n Pressure;	GH - Groun	d Heave; (GP - Grout	out	of P	ipe;	CM -	Communication	
Supervis	or:						Insp	ecto	r: JOHN MOTKO	
Compan	y:	LRE				Total	(Cu	. Yd.)	: 2.8 + 11.6 = 144	
Total To	Date (Cu. Y	'd.):								



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Client:	ANG	ELO'S RECY	CLING					[Date: 3.3.04
Project:	·	DADE CIT	TY LANDFIL	<u> </u>					Injection Point: 26
Csng. Depth	Grou	t Time	Max. Pressure	Pump	R	Reason pum	to sto	ф	
(ft.)	Start	Finish	(psi)	Strokes	НР	G H	G P	C M	Remarks
60	← TOTAL CA	ASING DEPTH		132					Con Tinue Time
60	1551	1610	150	4/3					pump out of fuel
		1622	150	487					pump out of such End Track
									Flush nex
60									
									ENLLY
HP - Higl	h Pressure;	GH - Groun	d Heave; (GP - Grou	t out	of P	ipe; (CM -	- Communication
Supervis	or:				-,		Insp	ecto	or: JOHN MOTKO
Compan	y:	LRE				Total	(Cu	Yd.	.):6.6+
Total To	Date (Cu. Y	d.):			-				



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Client:	ANGELO'S RECYCLING								Date: 3-4-04		
Project:	7	DADE CIT	Y LANDFI	L					Continue from 2-3 a4		
Csng. Depth (ft.)	Grout Time		Max. Pressure (psi)	Pump Strokes	Reason to stop pumping				Remarks		
(8.7	Start	Finish	V-1	7.57	H P	G H	G P	C M	I/Gildina		
	← TOTAL C	ASING DEPTH							576.7 Tive 4		
60	1206	1232	140	485					End Truck BAG 9.		
									Now Truck		
57	1332	/353	140	458				-	End Truck 9.0		
									Go To Pain 7 18		
									00 10 1011 10		

HP - High	n Pressure;	GH - Ground	d Heave; (GP - Grout	out	of Pi	pe; (CM -	Communication		
Supervis	or:						Insp	ecto	r: JOHN MOTKO		
Company: LRE					. 1	Total	(Cu.	Yd.	: 6.6+18		
Total To	Date (Cu. Y	d.):			•:						



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Client:	ANGELO'S RECYCLING						Date: 3-50/						
Project:		LL		10- Ting Injection Point: 26 110- 34-04									
Csng. Depth (ft.)	Grout Time		Max. Pressure (psi)	Pump Strokes 2-9	Reason to stop pumping								
	Start Finish				H	G H	G P	C M	Remarks				
	← TOTAL C	ASING DEPTH		43					CENTIANE TIME				
57	1303	1324	110/	462					End Truck Der 5 7.				
			-	3-10					Nay Truck				
52	1234	1400	200	572					End Truck NAME 10.				
			C-1921X	145-105					NEW Truck				
47	1154	1517	-	-					End Truck Box = 100				
				3-10					New Toric				
1/2	16 18	16 23	200/40-	110	X				DFF+				
37	14,23	113)	1100	113	X	_			BRET				
32	14 33	1652	189/	554					End Truck BIEK! (10.				
			-	(4.44)		_			NEW Tivet				
27	1659	17 14	200/200		7	X			AT IP BEKE				
22	1721	1724	300/gu		1	_			Det 6.2				
17	1726	1726	4007	325	X	-			(2m)				
		100							GOT 25				
HP - Hig	h Pressure;	GH - Groun	d Heave;	GP - Grout	out	of P	ipe; (CM -	Communication				
Supervis	юг:						Insp	ecto	г: ЈОНИ МОТКО				
Company: LRE						Total (Cu. Yd.): $6.5 + 18 + 44 = 66.6$							
Total To	Date (Cu. Y	(d.):											

APPENDIX C

Important Information about Your

Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared solely for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. And no one — not even you — should apply the report for any purpose or project except the one originally contemplated.

Read the Full Report

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

A Geotechnical Engineering Report Is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- · not prepared for your project,
- · not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

 the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership.

As a general rule, always inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

subsurface conditions revealed during construction. The geolechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.

A Geotechnical Engineering Report Is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineering report. Reduce that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should never be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, but recognize that separating logs from the report can elevate risk.

Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. Be sure contractors have sufficient time to perform additional study. Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform a *geoenviron-mental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else*.

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

Rely, on Your ASFE-Member Geotechncial Engineer for Additional Assistance

Membership in ASFE/THE BEST PEOPLE ON EARTH exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your ASFE-member geotechnical engineer for more information.



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CONSTRAINTS AND RESTRICTIONS

WARRANTY

Universal Engineering Sciences has prepared this report for our client for his exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

UNANTICIPATED SOIL CONDITIONS

The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on the Boring Location Plan. This report does not reflect any variations which may occur between these borings.

The nature and extent of variations between borings may not become known until construction begins. If variations appear, we may have to re-evaluate our recommendations after performing on-site observations and noting the characteristics of any variations.

CHANGED CONDITIONS

We recommend that the specifications for the project require that the contractor immediately notify Universal Engineering Sciences, as well as the owner, when subsurface conditions are encountered that are different from those present in this report.

No claim by the contractor for any conditions differing from those anticipated in the plans, specifications, and those found in this report, should be allowed unless the contractor notifies the owner and Universal Engineering Sciences of such changed conditions. Further, we recommend that all foundation work and site improvements be observed by a representative of Universal Engineering Sciences to monitor field conditions and changes, to verify design assumptions and to evaluate and recommend any appropriate modifications to this report.

MISINTERPRETATION OF SOIL ENGINEERING REPORT

Universal Engineering Sciences is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If the conclusions or recommendations based upon the data presented are made by others, those conclusions or recommendations are not the responsibility of Universal Engineering Sciences.

CHANGED STRUCTURE OR LOCATION

This report was prepared in order to aid in the evaluation of this project and to assist the architect or engineer in the design of this project. If any changes in the design or location of the structure as outlined in this report are planned, or if any structures are included or added that are not discussed in the report, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and the conclusions modified or approved by Universal Engineering Sciences.

USE OF REPORT BY BIDDERS

Bidders who are examining the report prior to submission of a bid are cautioned that this report was prepared as an aid to the designers of the project and it may affect actual construction operations.

Bidders are urged to make their own soil borings, test pits, test caissons or other explorations to determine those conditions that may affect construction operations. Universal Engineering Sciences cannot be responsible for any interpretations made from this report or the attached boring logs with regard to their adequacy in reflecting subsurface conditions which will affect construction operations.

STRATA CHANGES

Strata changes are indicated by a definite line on the boring logs which accompany this report. However, the actual change in the ground may be more gradual. Where changes occur between soil samples, the location of the change must necessarily be estimated using all available information and may not be shown at the exact depth.

OBSERVATIONS DURING DRILLING

Attempts are made to detect and/or identify occurrences during drilling and sampling, such as: water level, boulders, zones of lost circulation, relative ease or resistance to drilling progress, unusual sample recovery, variation of driving resistance, obstructions, etc.; however, lack of mention does not preclude their presence.

WATER LEVELS

Water level readings have been made in the drill holes during drilling and they indicate normally occurring conditions. Water levels may not have been stabilized at the last reading. This data has been reviewed and interpretations made in this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, tides, and other factors not evident at the time measurements were made and reported. Since the probability of such variations is anticipated, design drawings and specifications should accommodate such possibilities and construction planning should be based upon such assumptions of variations.

LOCATION OF BURIED OBJECTS

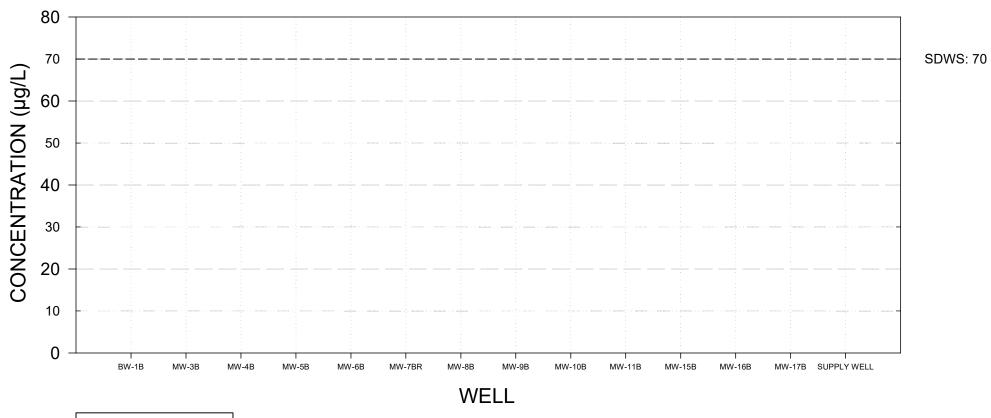
All users of this report are cautioned that there was no requirement for Universal Engineering Sciences to attempt to locate any man-made buried objects during the course of this exploration and that no attempt was made by Universal Engineering Sciences to locate any such buried objects. Universal Engineering Sciences cannot be responsible for any buried man-made objects which are subsequently encountered during construction that are not discussed within the text of this report.

TIME

This report reflects the soil conditions at the time of exploration. If the report is not used in a reasonable amount of time, significant changes to the site may occur and additional reviews may be required.

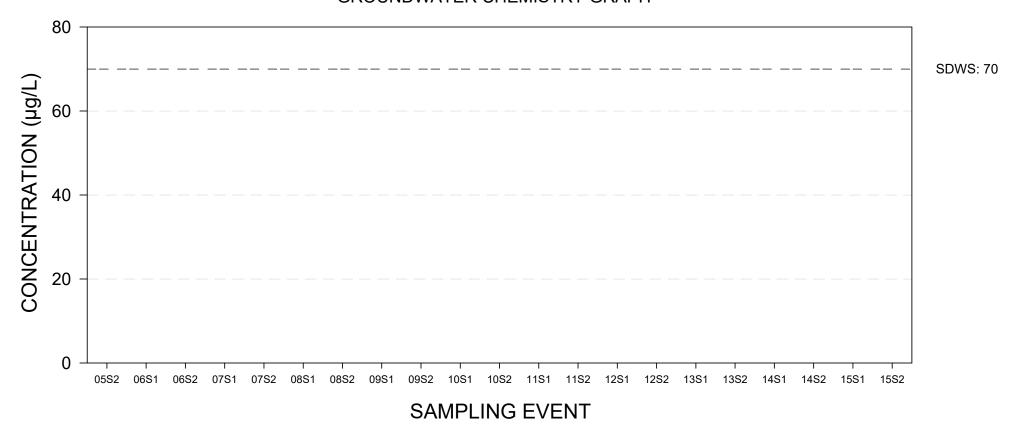
ATTACHMENT 2 GROUNDWATER DATA

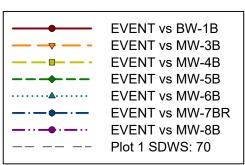
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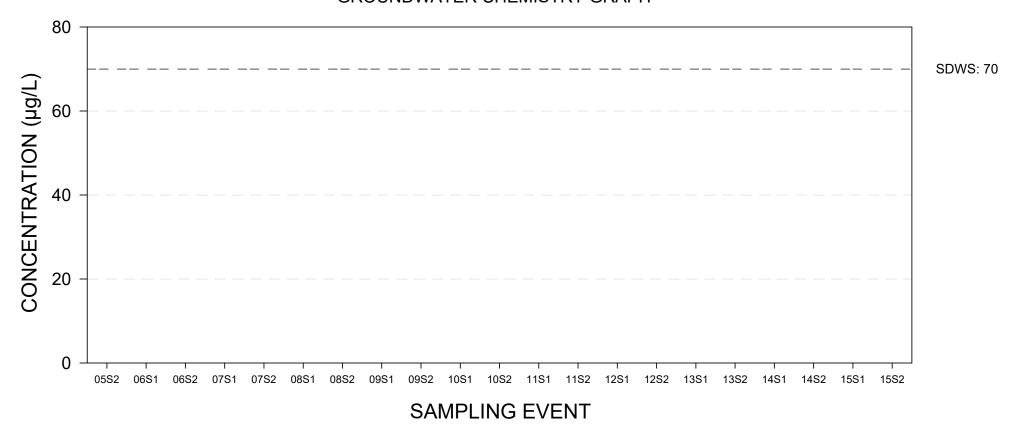
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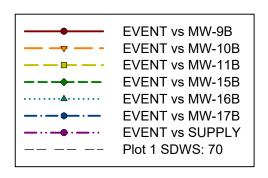
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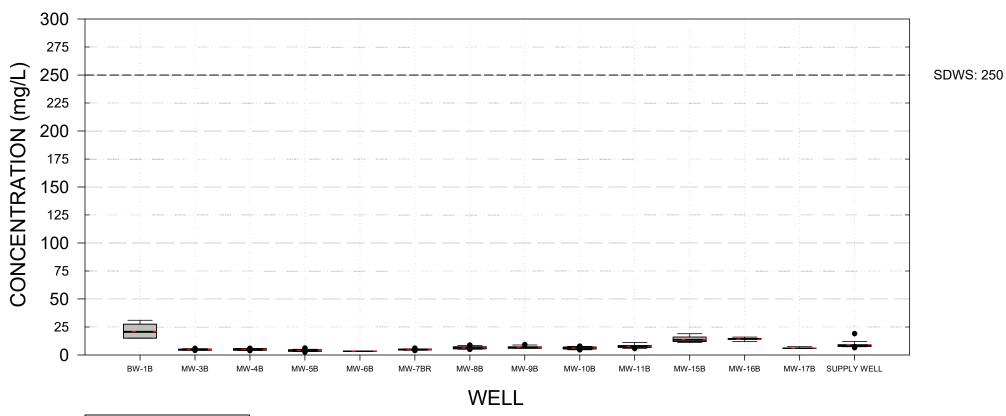
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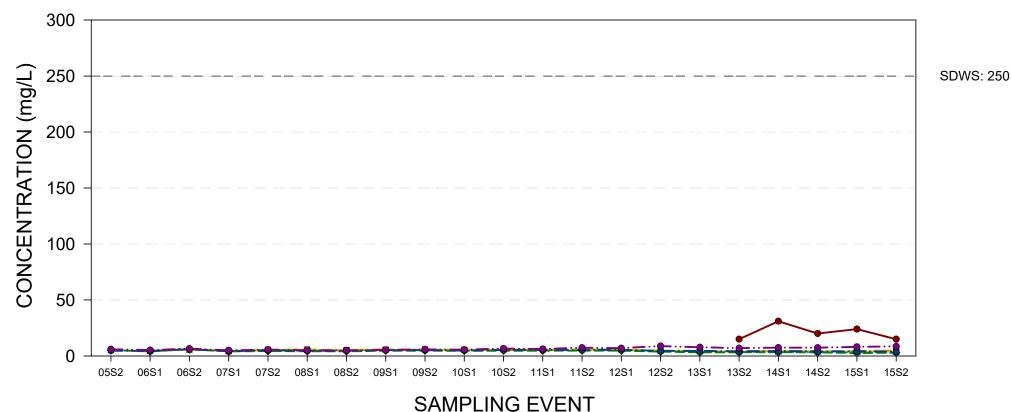
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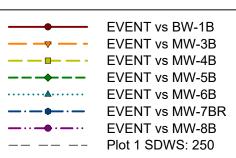
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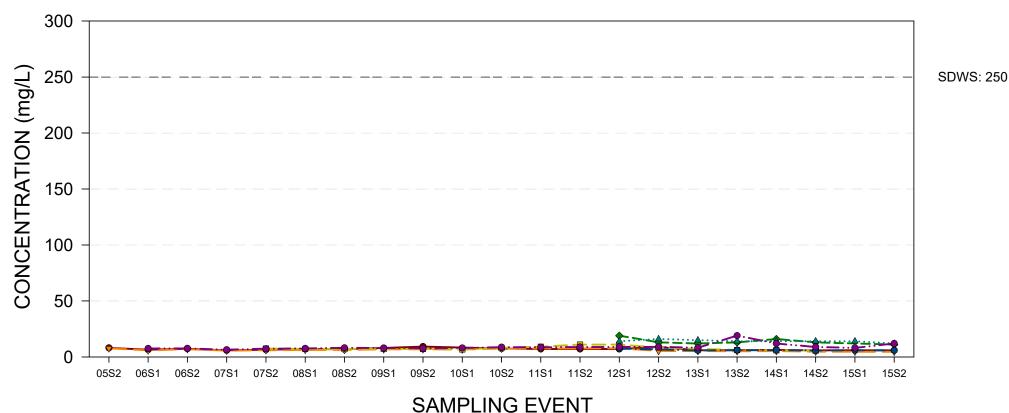
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--- Plot 2 SDWS: 250

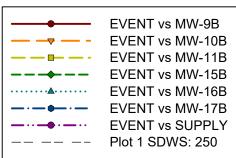
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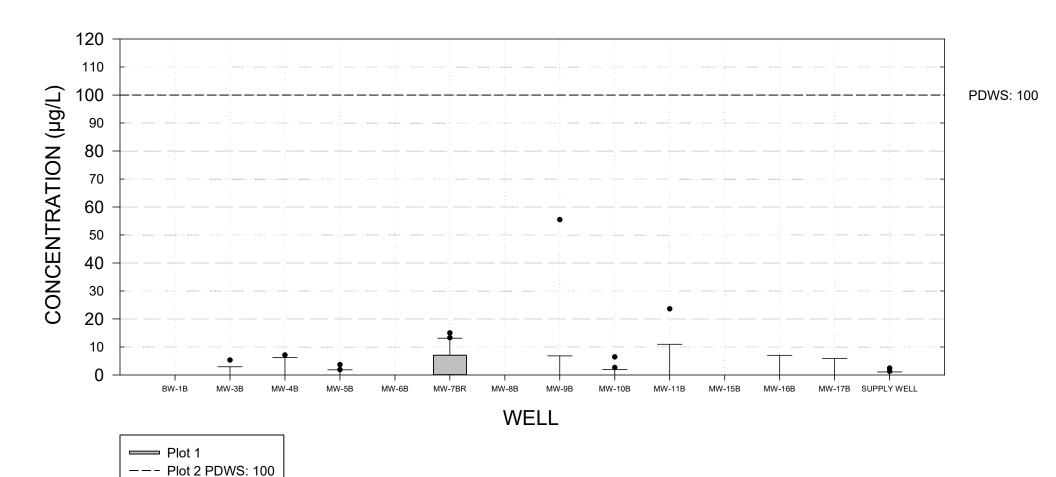


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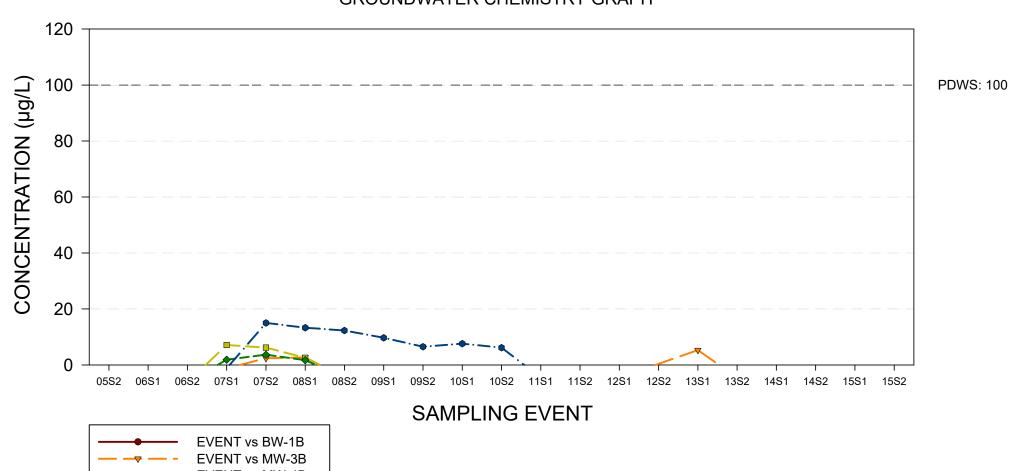




CHROMIUM



CHROMIUM



EVENT vs BW-1B

EVENT vs MW-3B

EVENT vs MW-4B

EVENT vs MW-5B

EVENT vs MW-6B

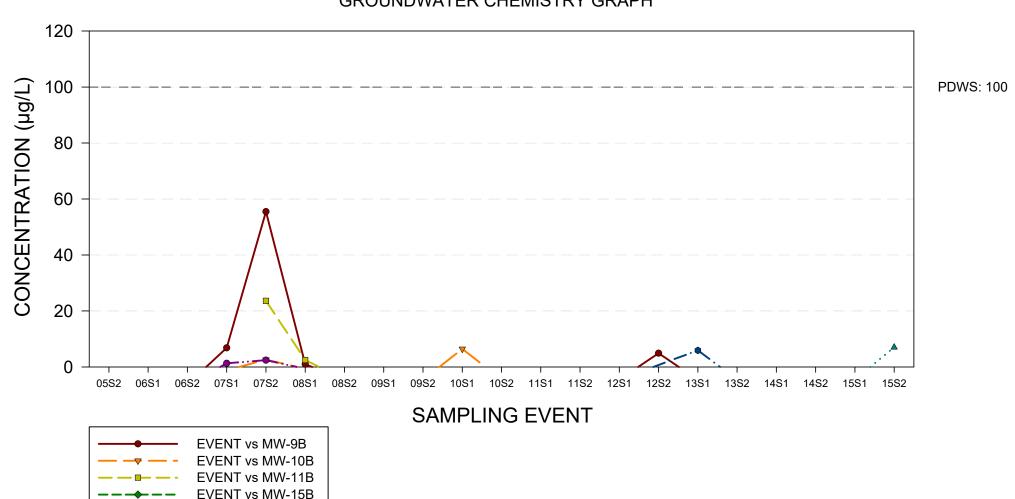
EVENT vs MW-7BR

EVENT vs MW-8B

Plot 1 PDWS: 100

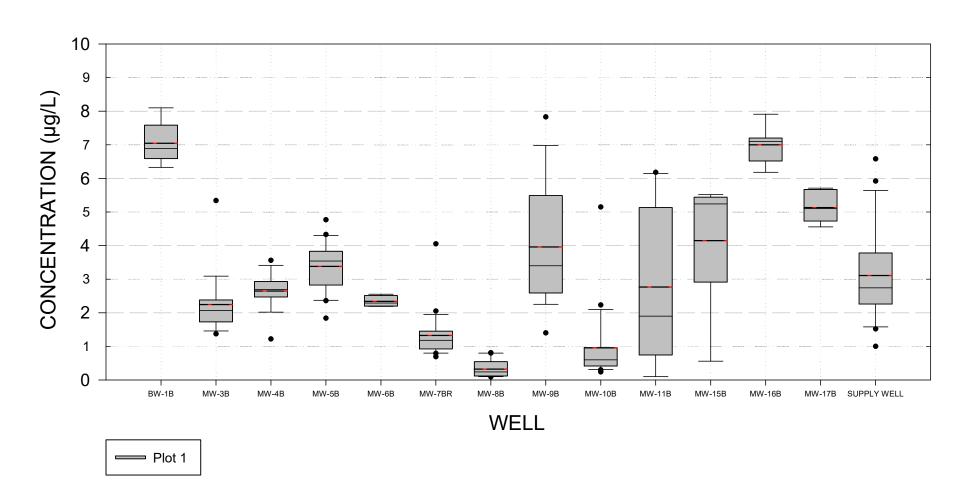
CHROMIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH

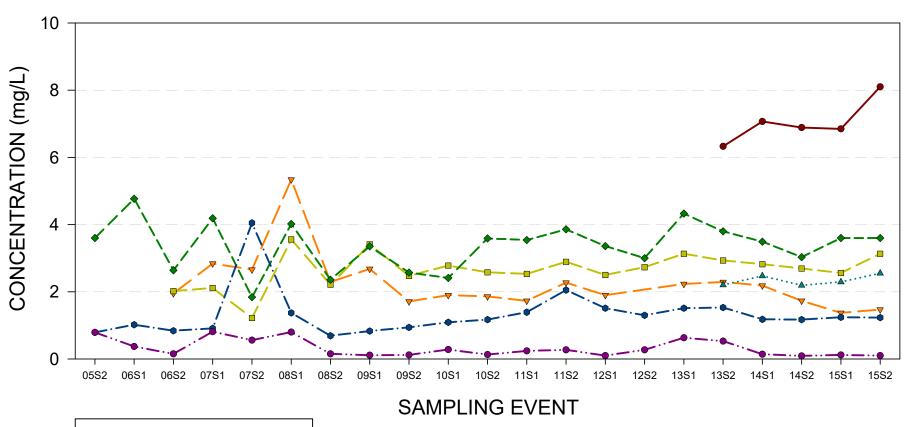


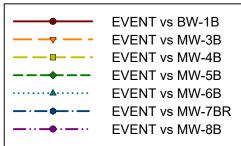
EVENT vs MW-16B EVENT vs MW-17B EVENT vs SUPPLY Plot 1 PDWS: 100

DISSOLVED OXYGEN

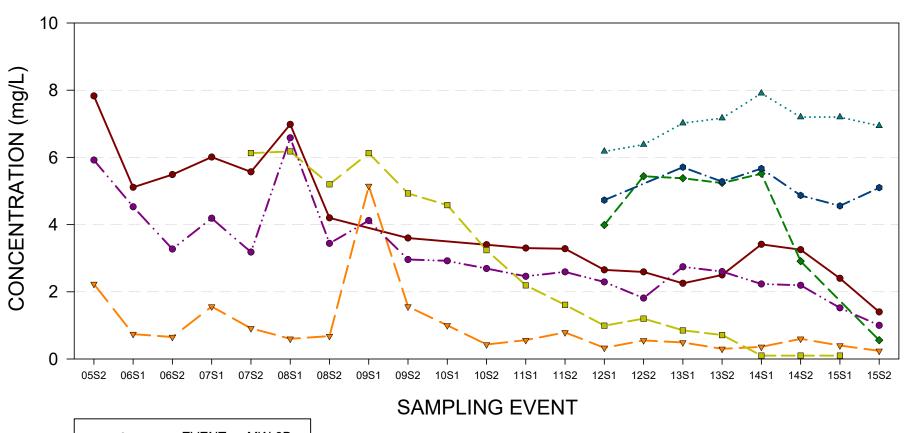


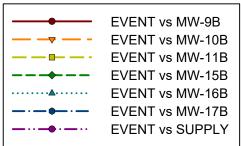
DISSOLVED OXYGEN



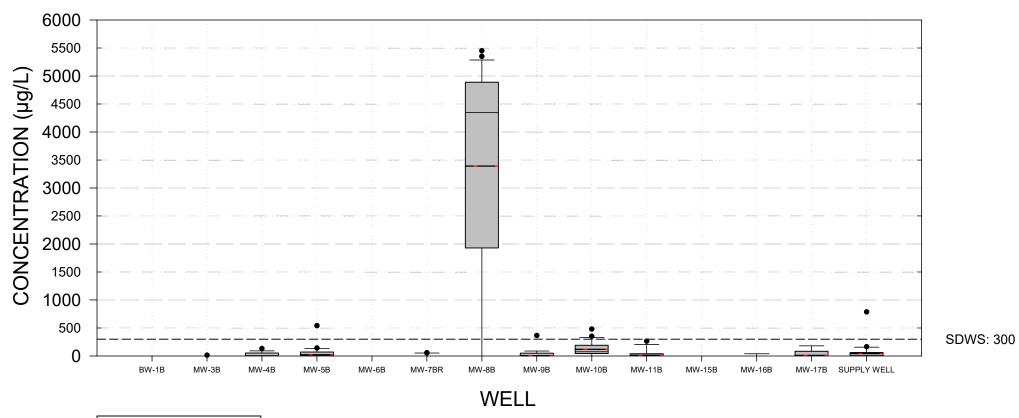


DISSOLVED OXYGEN



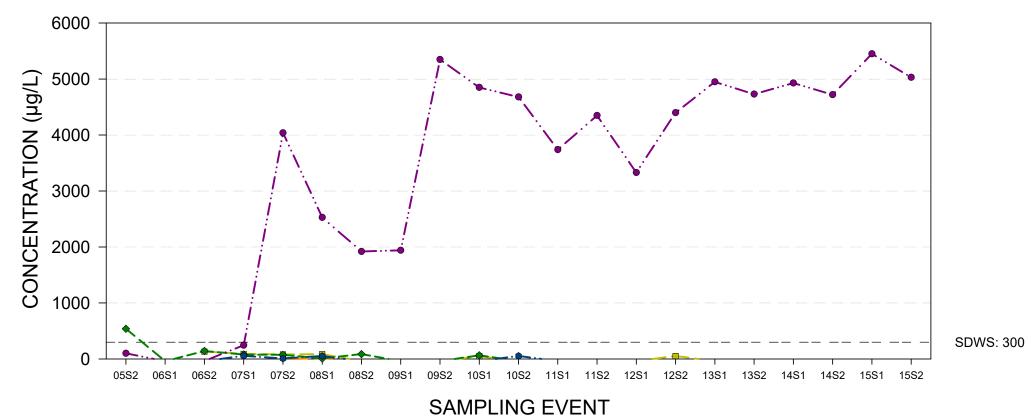


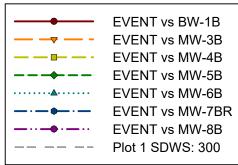
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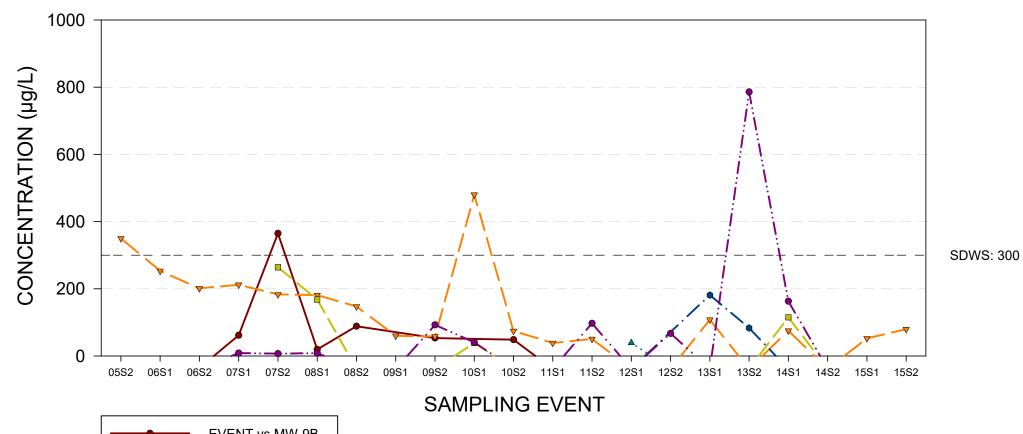
Plot 1
--- Plot 2 SDWS: 300

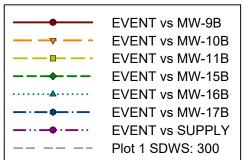
IRON





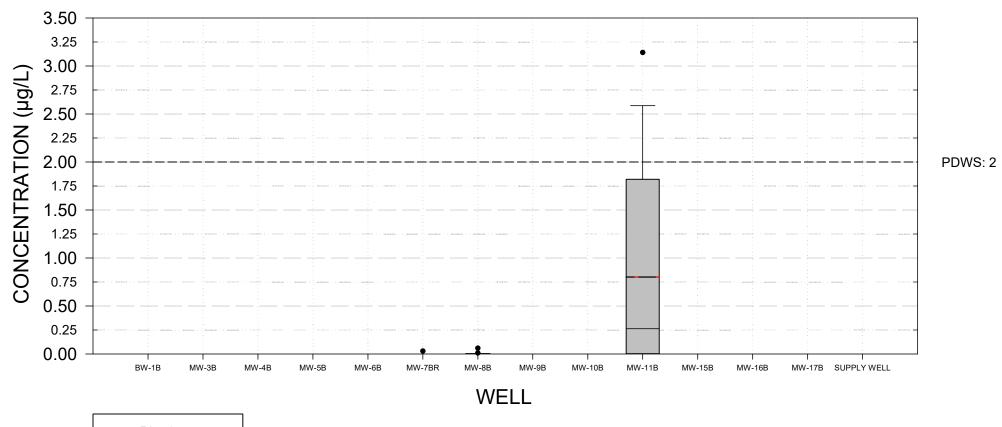
IRON





MERCURY

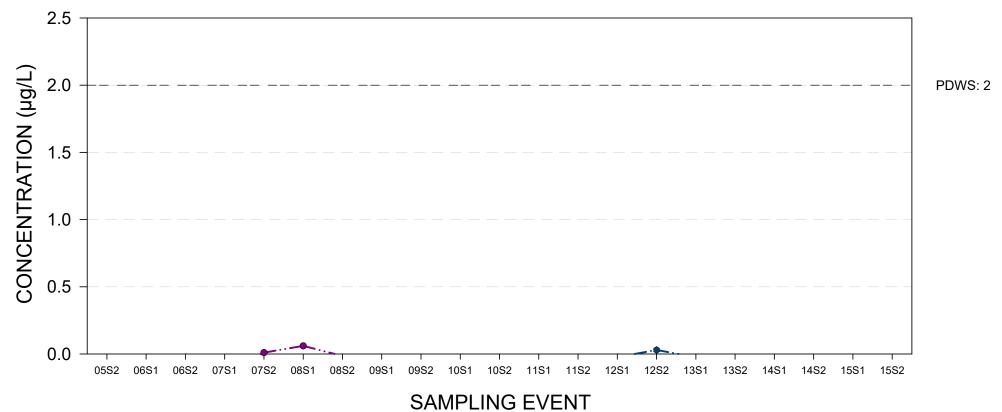
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Plot 1
--- Plot 2 PDWS: 2

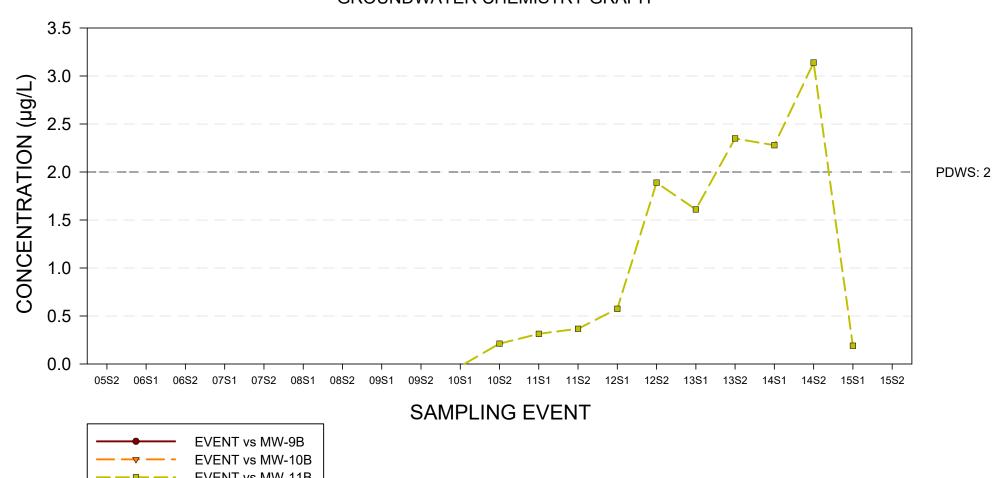
MERCURY

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1B EVENT vs MW-3B EVENT vs MW-4B EVENT vs MW-5B EVENT vs MW-6B EVENT vs MW-7BR EVENT vs MW-7BR EVENT vs MW-7BR Plot 1 PDWS: 2

MERCURY



EVENT vs MW-9B

EVENT vs MW-10B

EVENT vs MW-11B

EVENT vs MW-15B

EVENT vs MW-16B

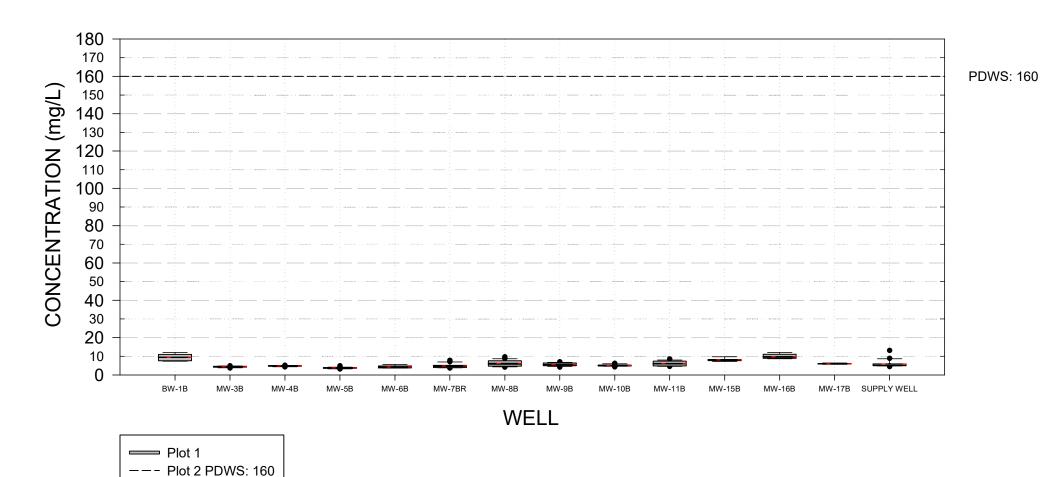
EVENT vs MW-17B

EVENT vs MW-17B

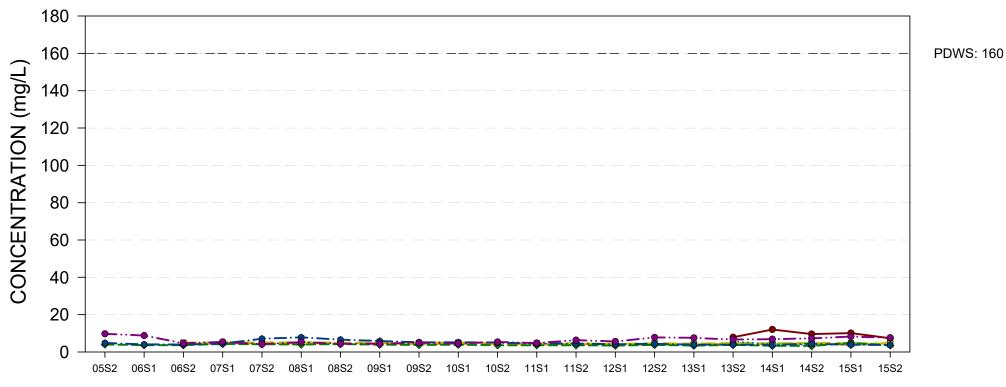
EVENT vs SUPPLY

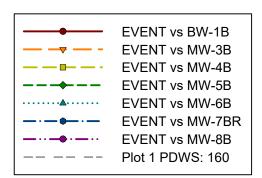
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SODIUM



SODIUM

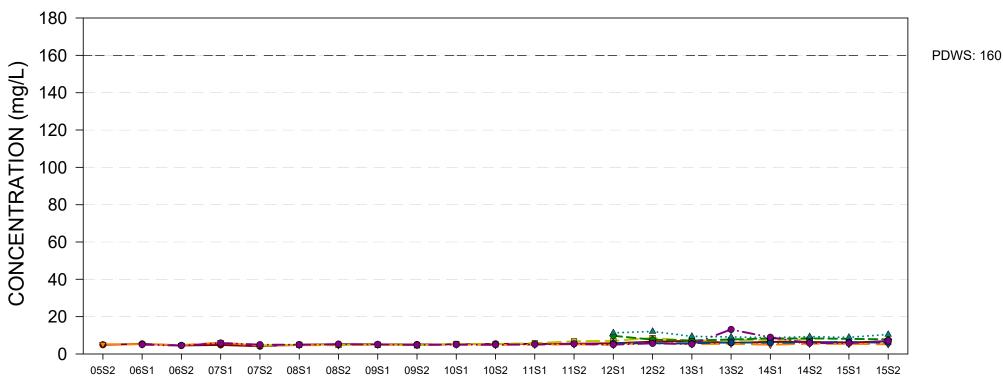




SAMPLING EVENT

SODIUM

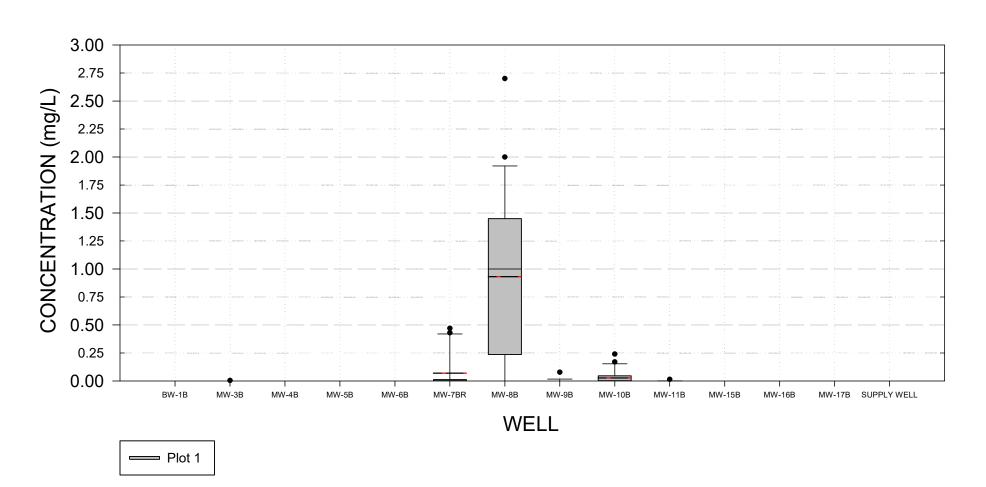
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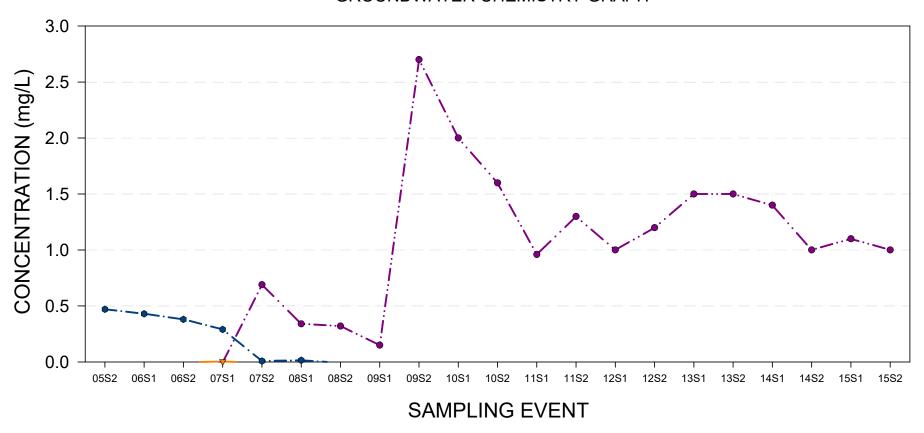
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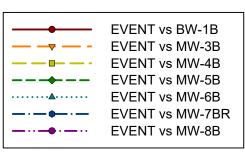
EVENT vs MW-9B
EVENT vs MW-10B
EVENT vs MW-11B
EVENT vs MW-15B
EVENT vs MW-16B
EVENT vs MW-17B
EVENT vs MW-17B
EVENT vs SUPPLY
Plot 1 PDWS: 160

AMMONIA AS NITROGEN

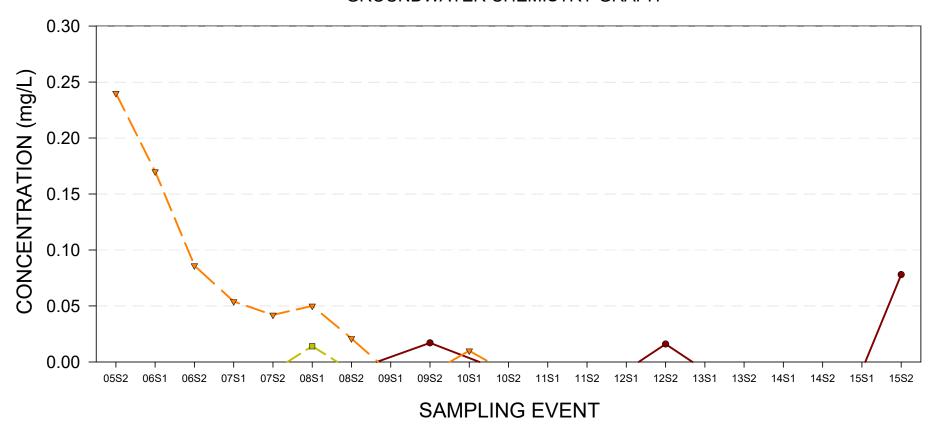


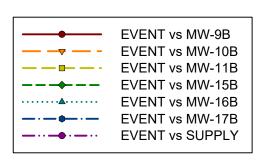
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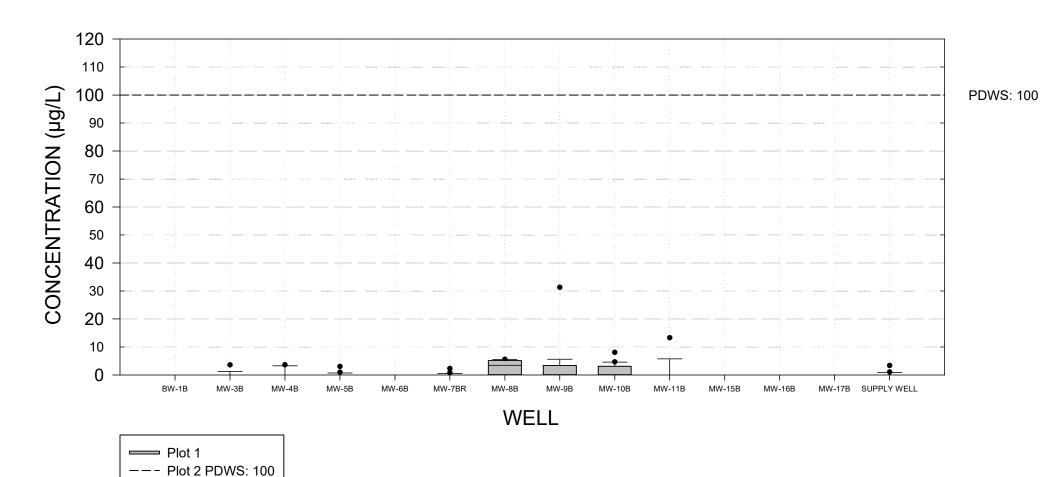


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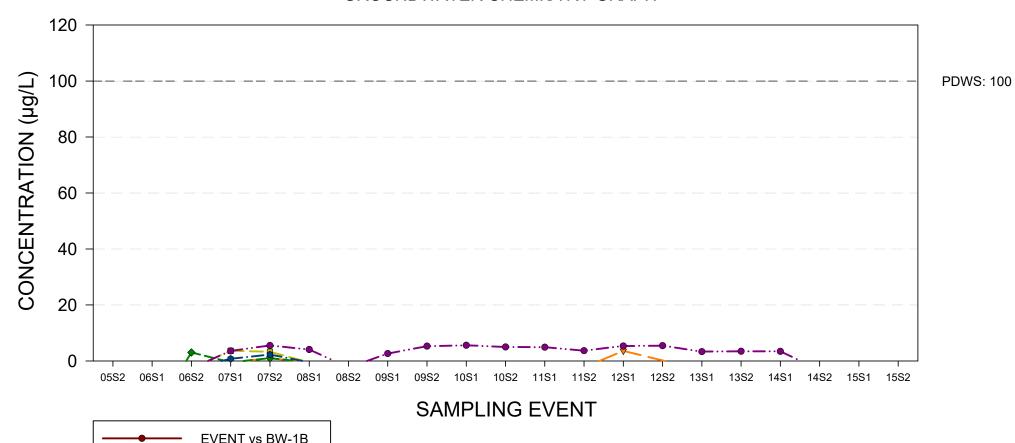




NICKEL



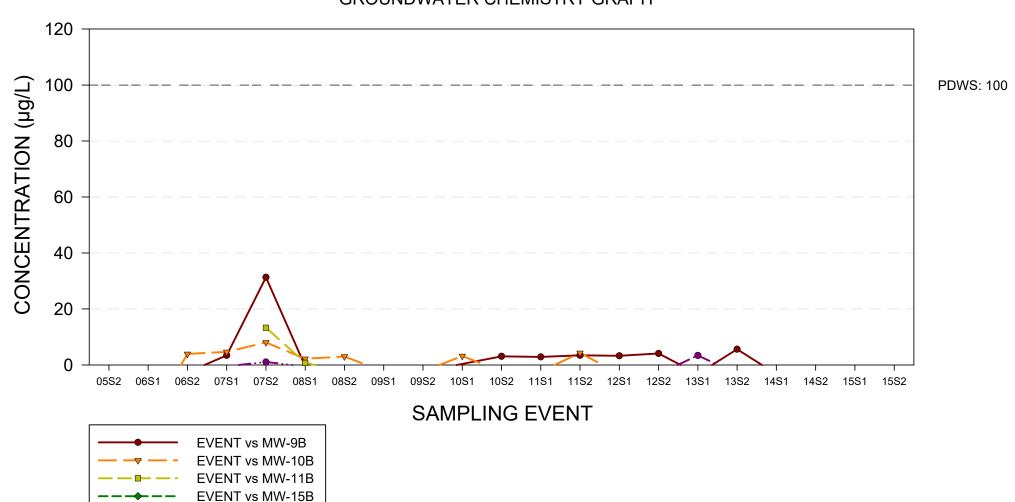
NICKEL



EVENT vs BW-1B
EVENT vs MW-3B
EVENT vs MW-4B
EVENT vs MW-5B
EVENT vs MW-6B
EVENT vs MW-7BR
EVENT vs MW-7BR
FVENT vs MW-8B
Plot 1 PDWS: 100

NICKEL

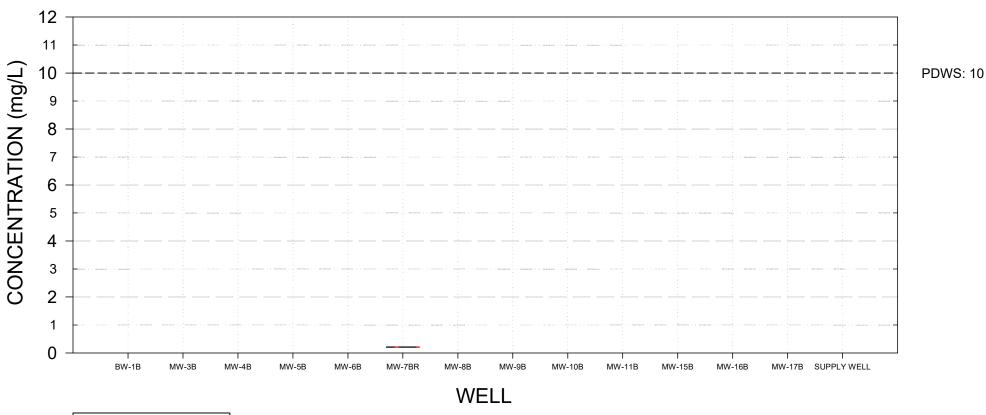
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs MW-16B EVENT vs MW-17B EVENT vs SUPPLY Plot 1 PDWS: 100

NITRITE AS NITROGEN

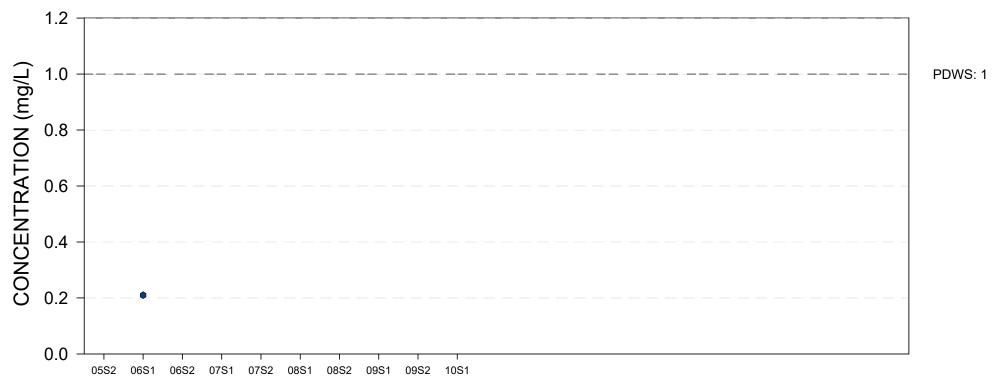
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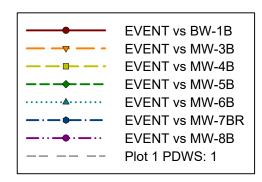
Plot 1
--- Plot 2 PDWS: 10

NITRITE AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH

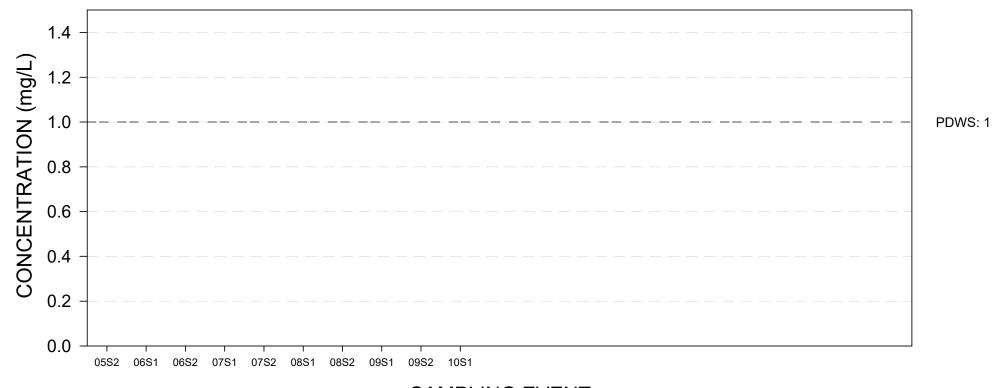


SAMPLING EVENT

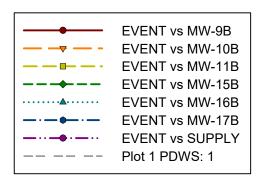


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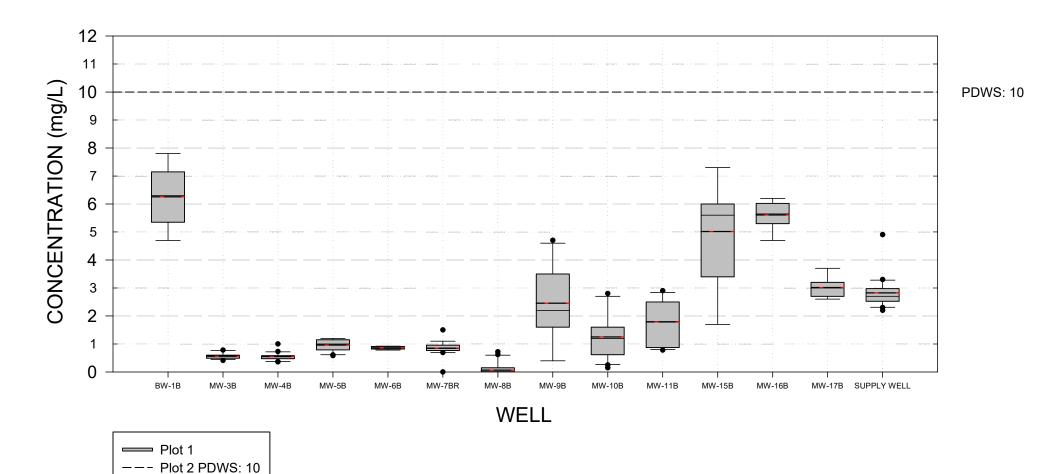
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SAMPLING EVENT

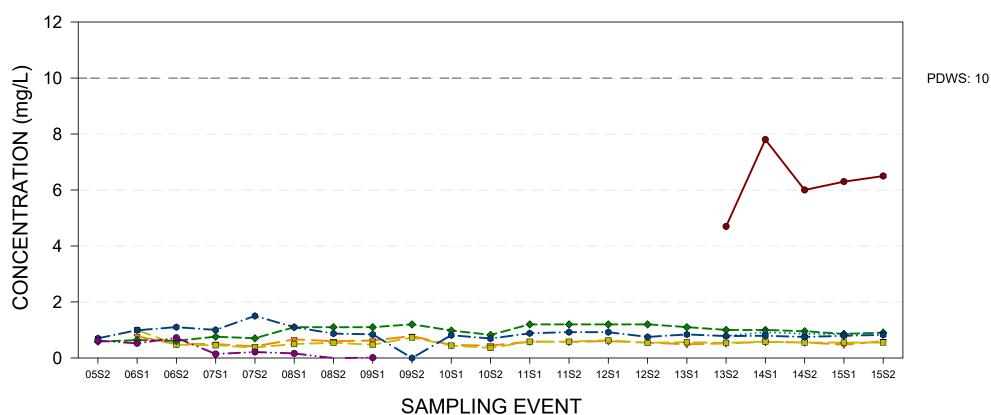


NITRATE AS NITROGEN



NITRATE AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1B

EVENT vs MW-3B

EVENT vs MW-4B

EVENT vs MW-5B

EVENT vs MW-6B

EVENT vs MW-7BR

EVENT vs MW-7BR

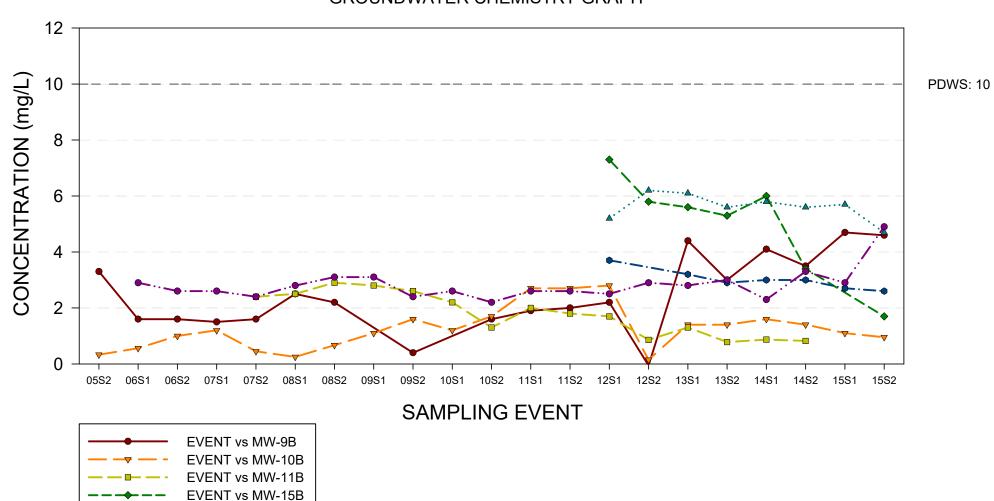
EVENT vs MW-7BR

EVENT vs MW-8B

Plot 1 PDWS: 10

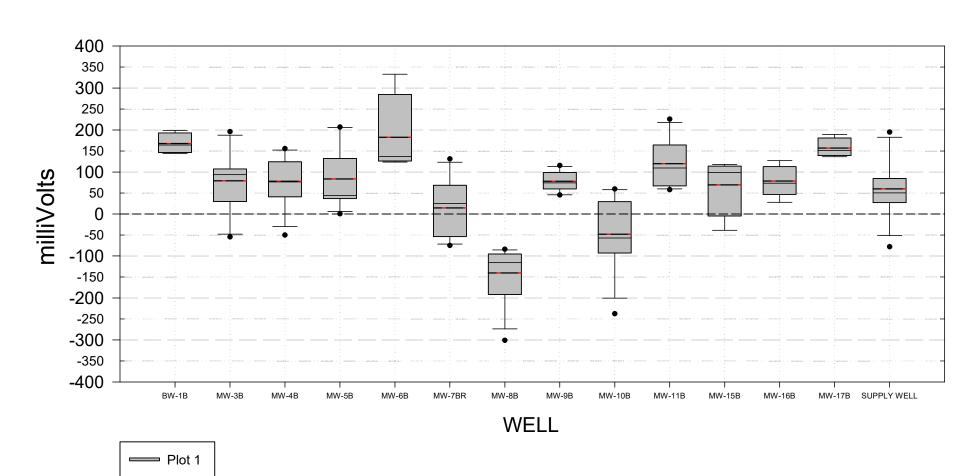
NITRATE AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH

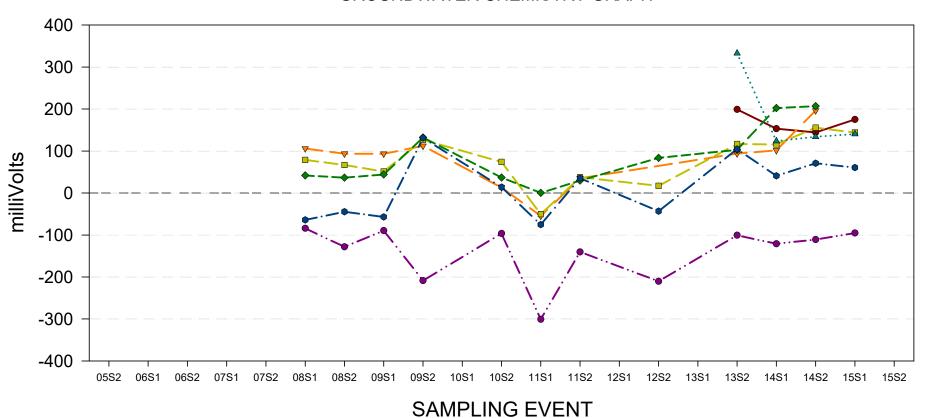


EVENT vs MW-16B EVENT vs MW-17B EVENT vs SUPPLY Plot 1 PDWS: 10

OXIDATION / REDUCTION POTENTIAL

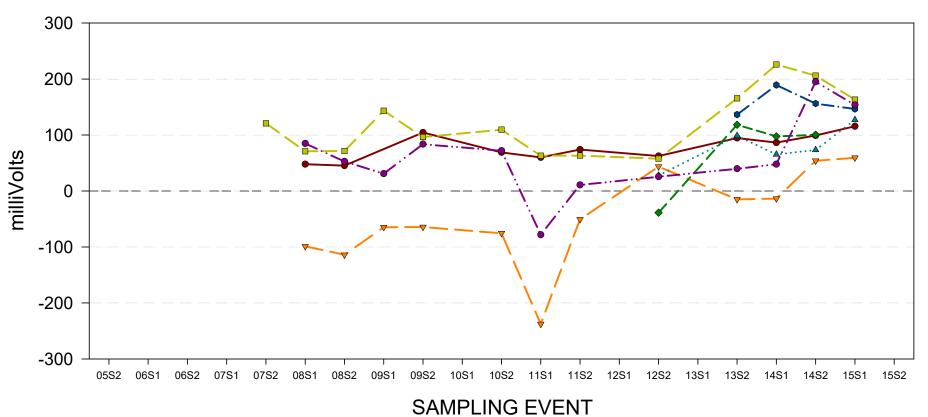


OXIDATION / REDUCTION POTENTIAL



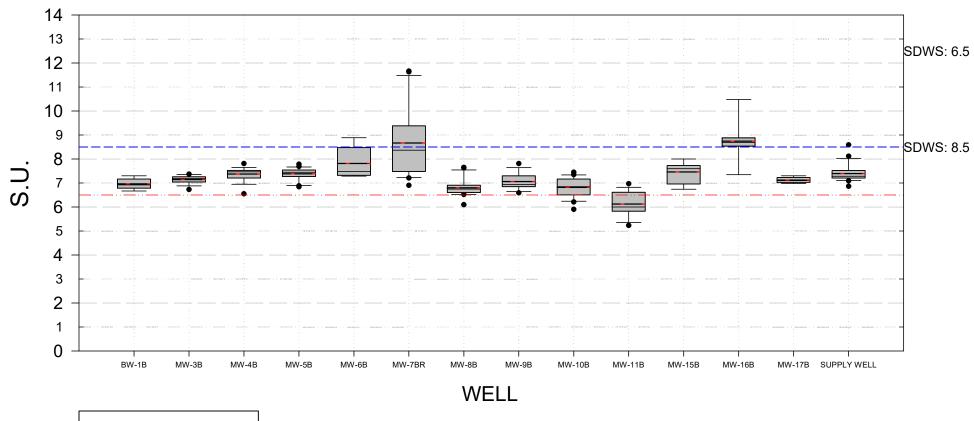
EVENT vs BW-1B
EVENT vs MW-3B
EVENT vs MW-4B
EVENT vs MW-5B
EVENT vs MW-6B
EVENT vs MW-7BR
EVENT vs MW-7BR
EVENT vs MW-8B

OXIDATION / REDUCTION POTENTIAL



EVENT vs MW-9B
EVENT vs MW-10B
EVENT vs MW-11B
EVENT vs MW-15B
EVENT vs MW-16B
EVENT vs MW-17B
EVENT vs MW-17B
EVENT vs SUPPLY

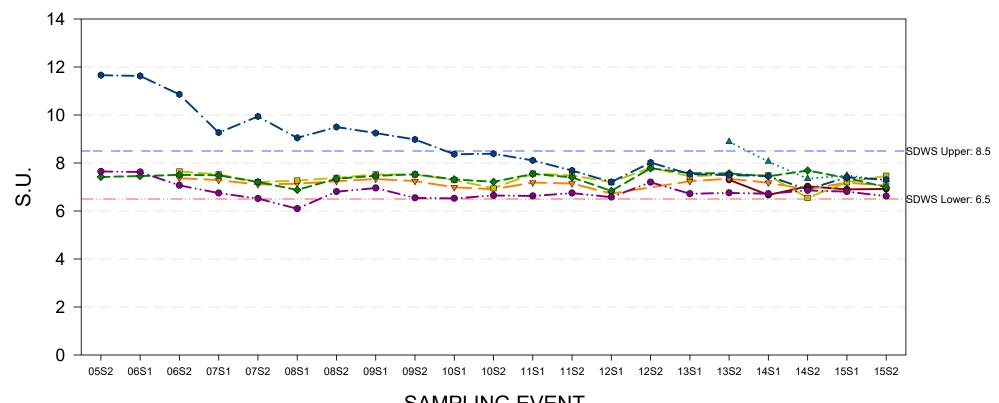
PH
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING
FACILITY FLORIDAN AQUIFER
GROUNDWATER CHEMISTRY GRAPH



Plot 1
Plot 2 SDWS: 8.5
Plot 2 SDWS: 6.5

PH

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING **FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH**

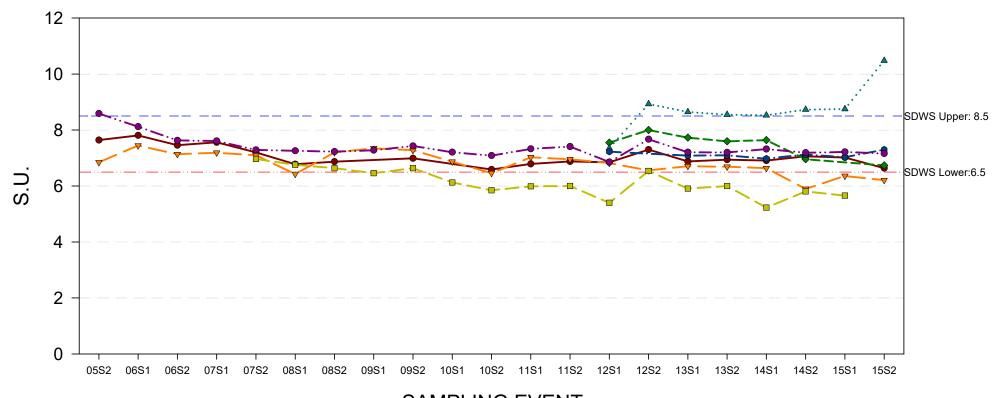


EVENT vs BW-1B EVENT vs MW-3B EVENT vs MW-4B EVENT vs MW-5B EVENT vs MW-6B EVENT vs MW-7BR EVENT vs MW-8B Plot 1 SDWS Upper: 8.5 Plot 1 SDWS Lower: 6.5

SAMPLING EVENT

PH

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH

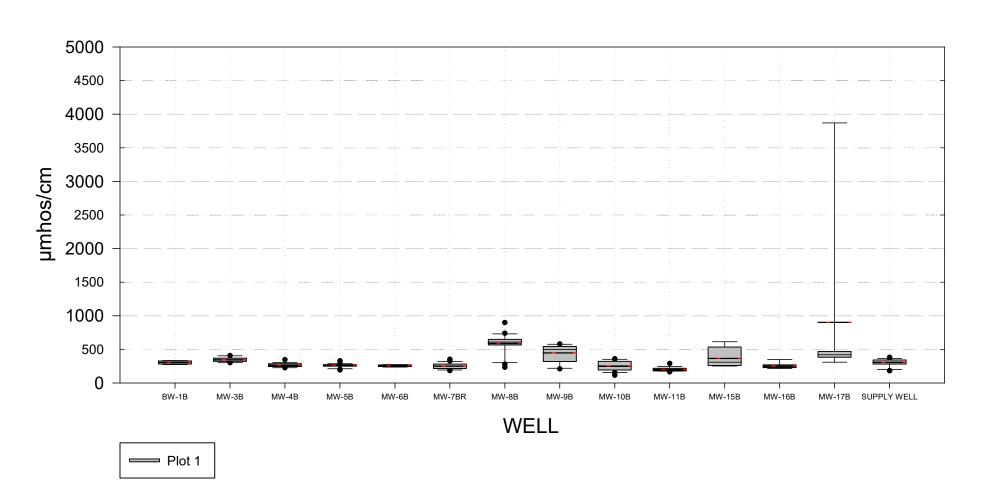


EVENT vs MW-9B EVENT vs MW-10B EVENT vs MW-11B EVENT vs MW-15B EVENT vs MW-16B EVENT vs MW-17B EVENT vs MW-17B EVENT vs MW-17B EVENT vs SUPPLY Plot 1 SDWS Upper: 8.5

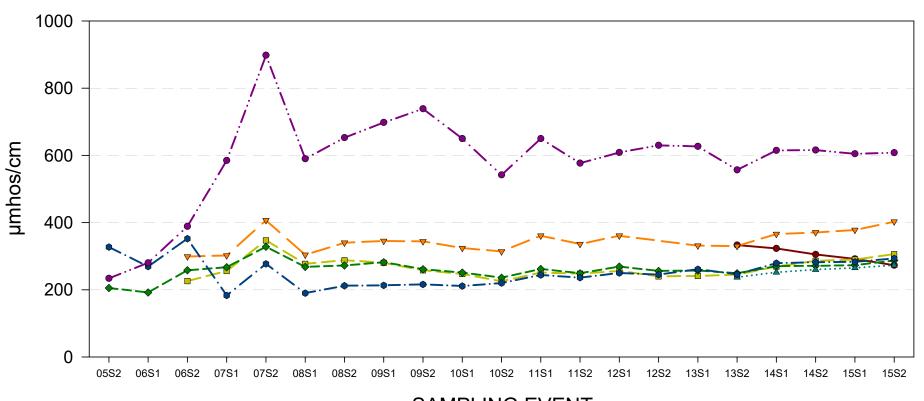
Plot 1 SDWS Lower:6.5

SAMPLING EVENT

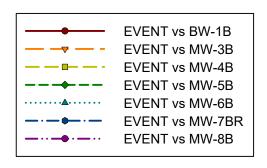
SPECIFIC CONDUCTANCE



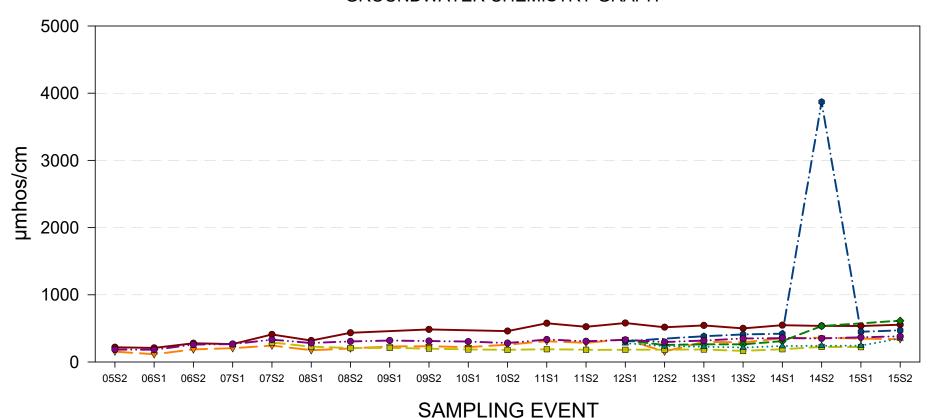
SPECIFIC CONDUCTANCE

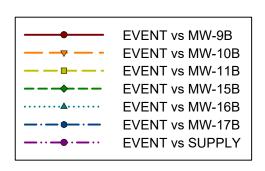


SAMPLING EVENT

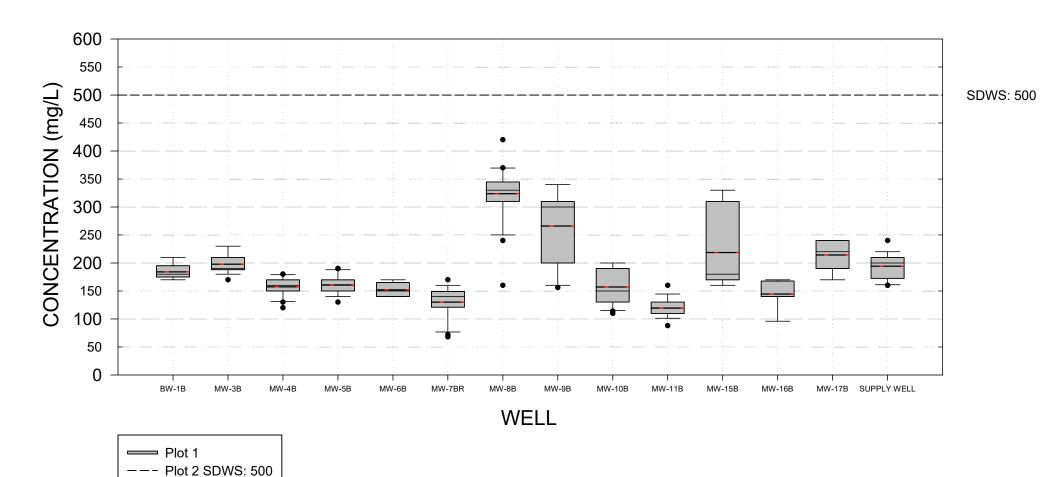


SPECIFIC CONDUCTANCE



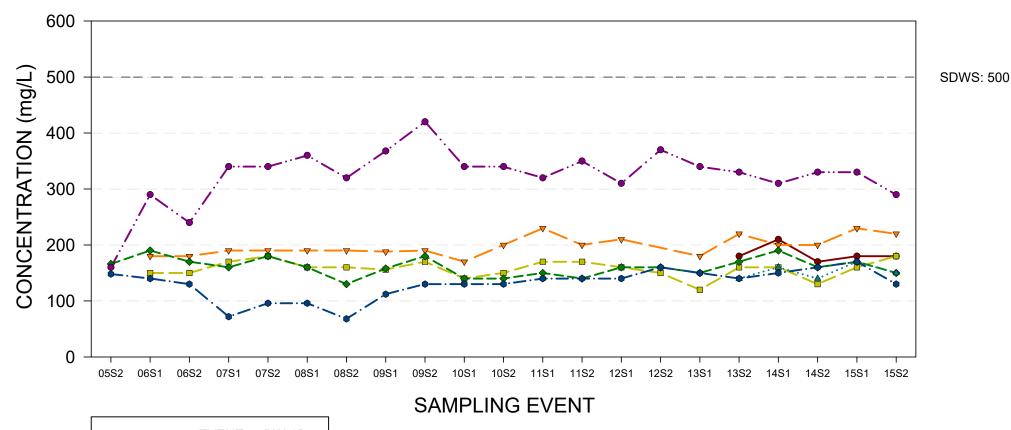


TOTAL DISSOLVED SOLIDS



TOTAL DISSOLVED SOLIDS

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1B

EVENT vs MW-3B

EVENT vs MW-4B

EVENT vs MW-5B

EVENT vs MW-6B

EVENT vs MW-7BR

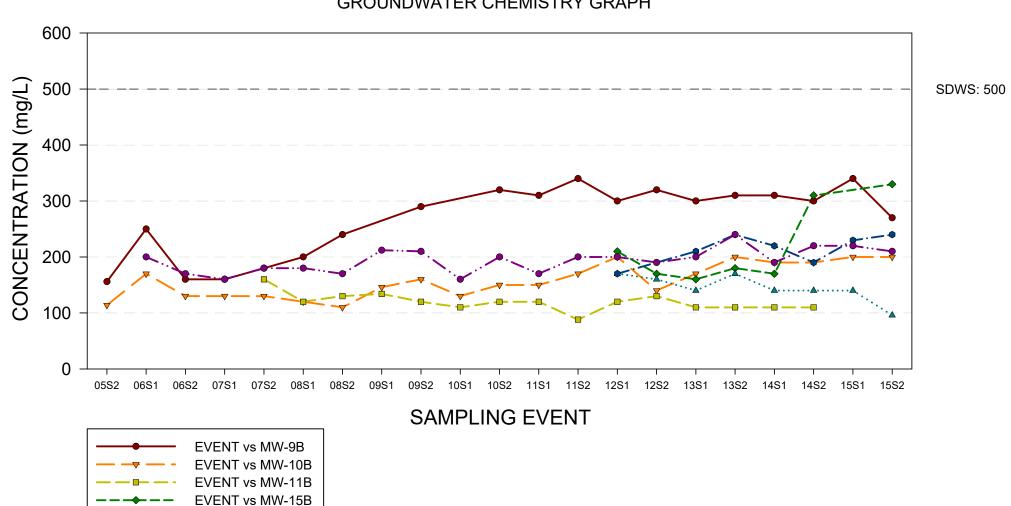
EVENT vs MW-7BR

EVENT vs MW-8B

Plot 1 SDWS: 500

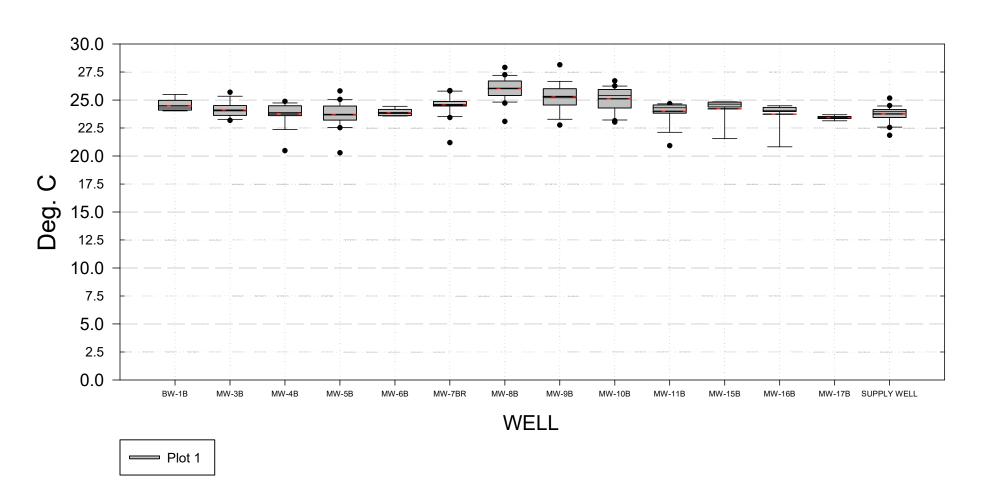
TOTAL DISSOLVED SOLIDS

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



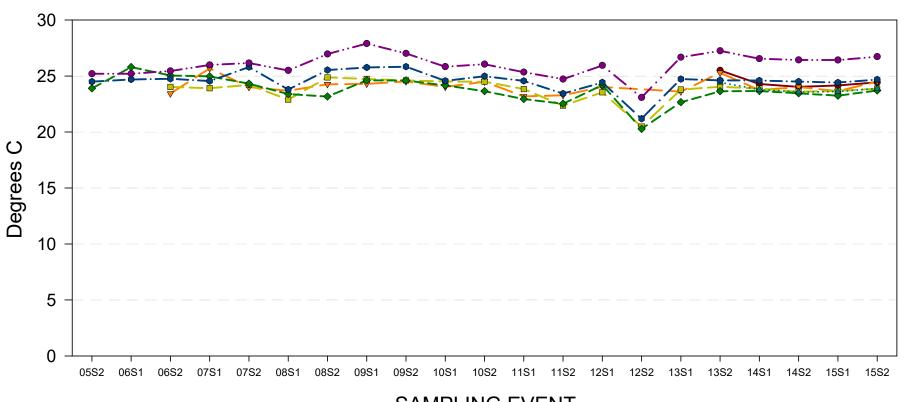
EVENT vs MW-16B EVENT vs MW-17B EVENT vs SUPPLY Plot 1 SDWS: 500

TEMPERATURE

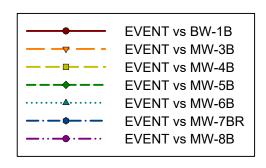


TEMPERATURE

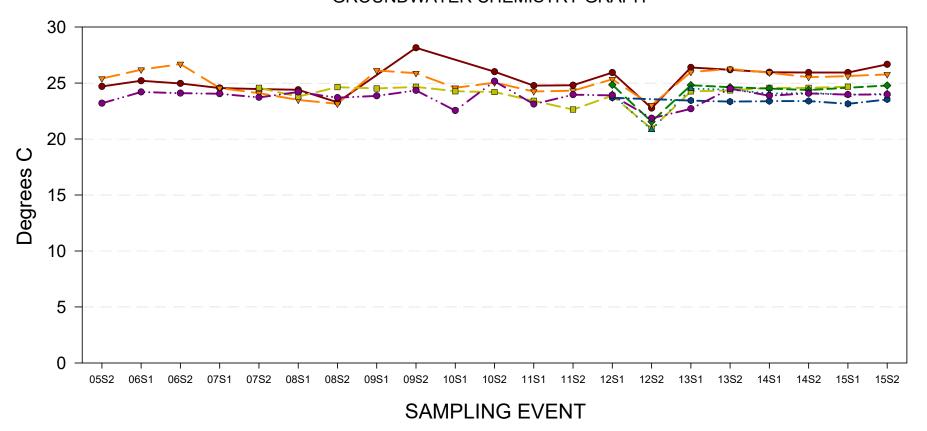
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



SAMPLING EVENT



TEMPERATURE



EVENT vs MW-9B

EVENT vs MW-10B

EVENT vs MW-11B

EVENT vs MW-15B

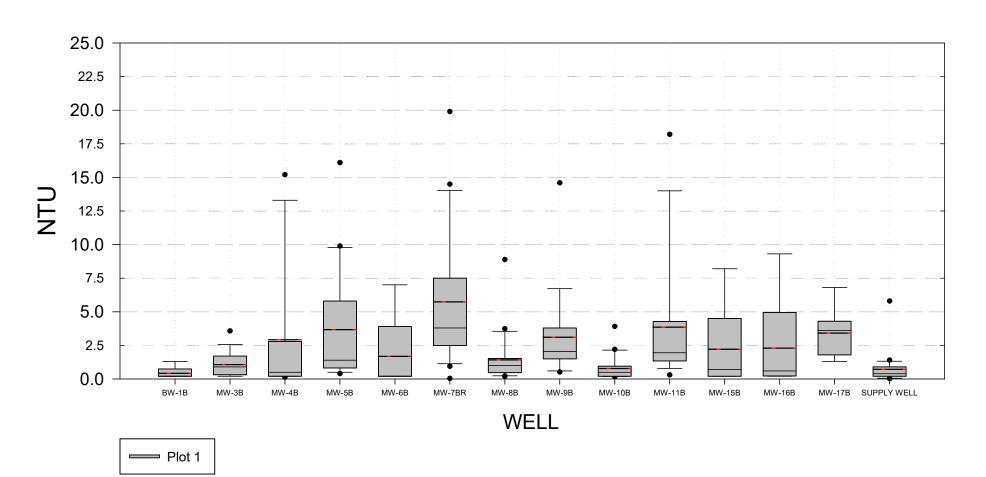
EVENT vs MW-16B

EVENT vs MW-17B

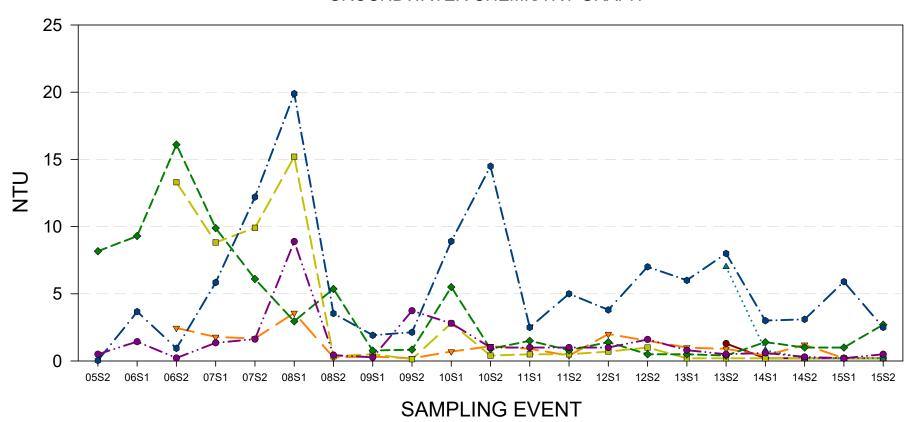
EVENT vs MW-17B

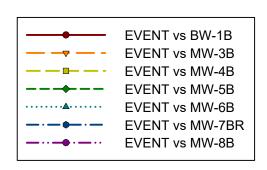
EVENT vs SUPPLY

TURBIDITY

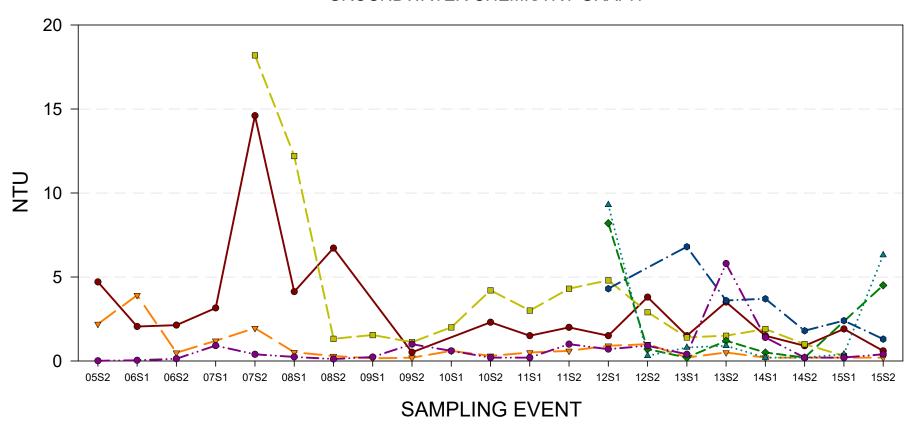


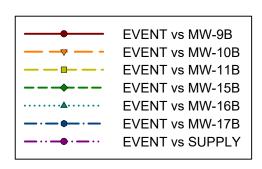
TURBIDITY



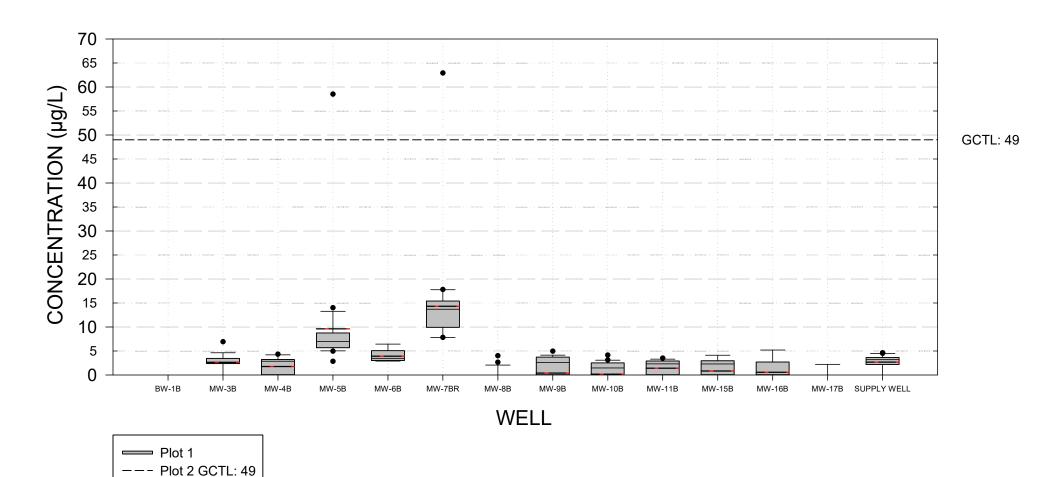


TURBIDITY



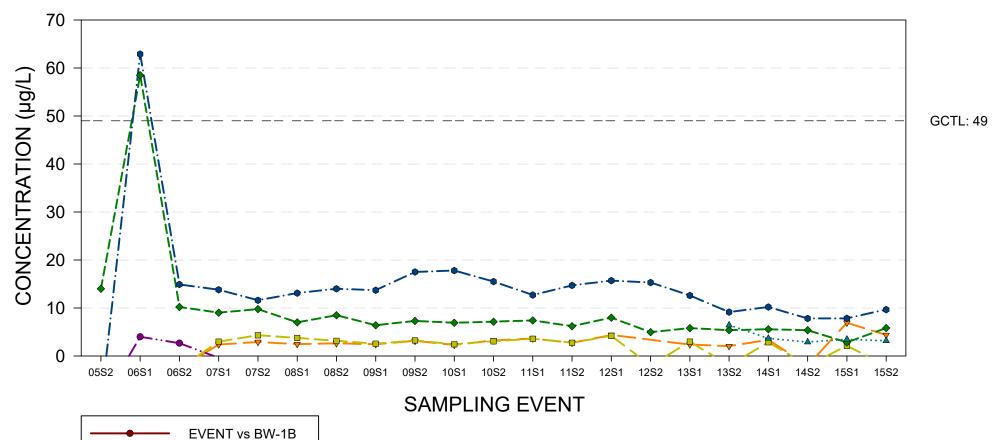


VANADIUM



VANADIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1B

EVENT vs MW-3B

EVENT vs MW-4B

EVENT vs MW-5B

EVENT vs MW-6B

EVENT vs MW-7BR

EVENT vs MW-8B

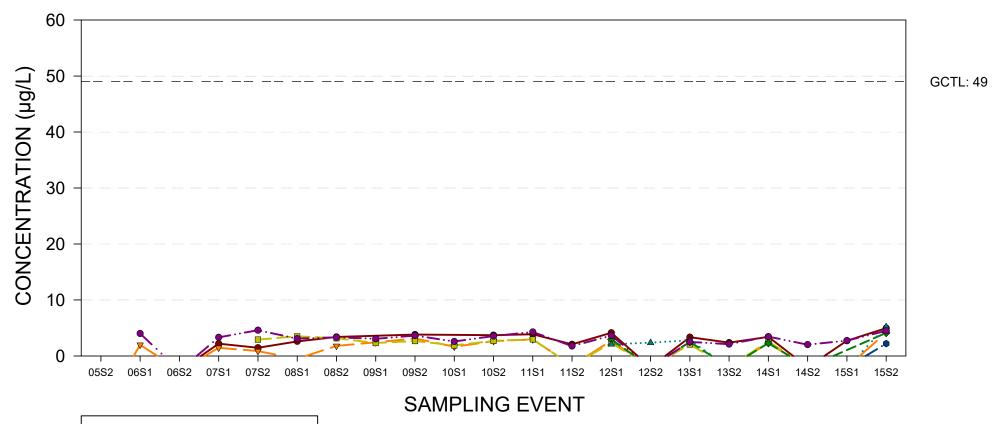
FUENT vs MW-8B

FUENT vs MW-8B

FUENT vs MW-8B

VANADIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs MW-9B

EVENT vs MW-10B

EVENT vs MW-11B

EVENT vs MW-15B

EVENT vs MW-16B

EVENT vs MW-16B

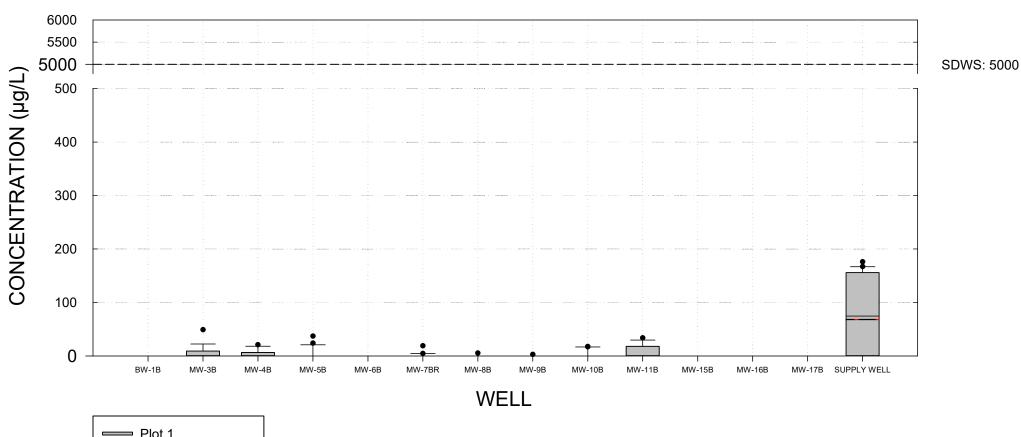
EVENT vs MW-17B

EVENT vs MW-17B

EVENT vs SUPPLY

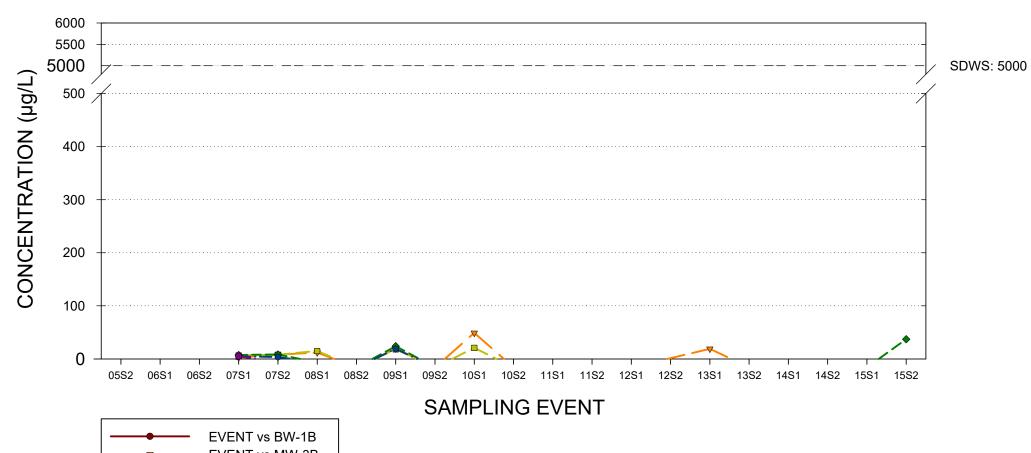
Plot 1 GCTL: 49

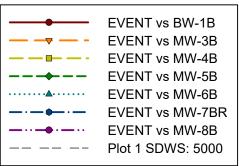
ZINC ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY FLORIDAN AQUIFER GROUNDWATER CHEMISTRY GRAPH



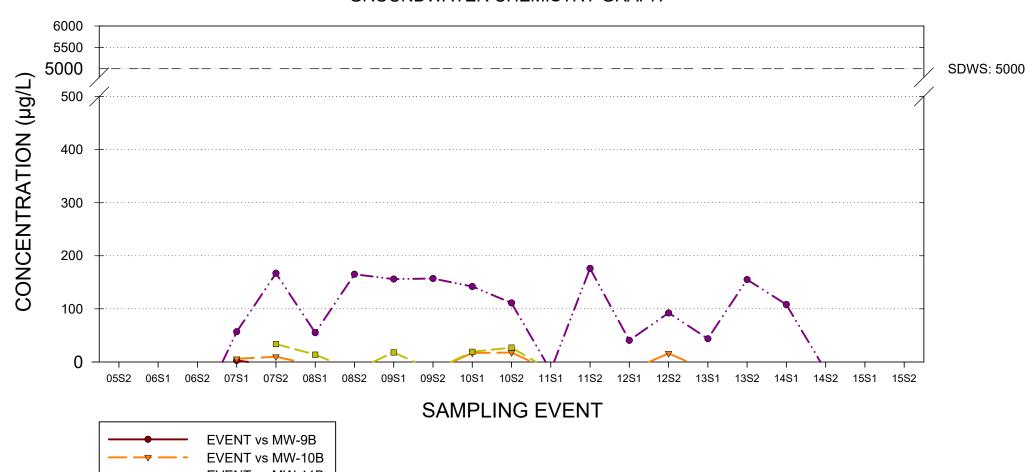
Plot 1
--- Plot 2 SDWS: 5000

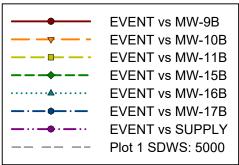
ZINC

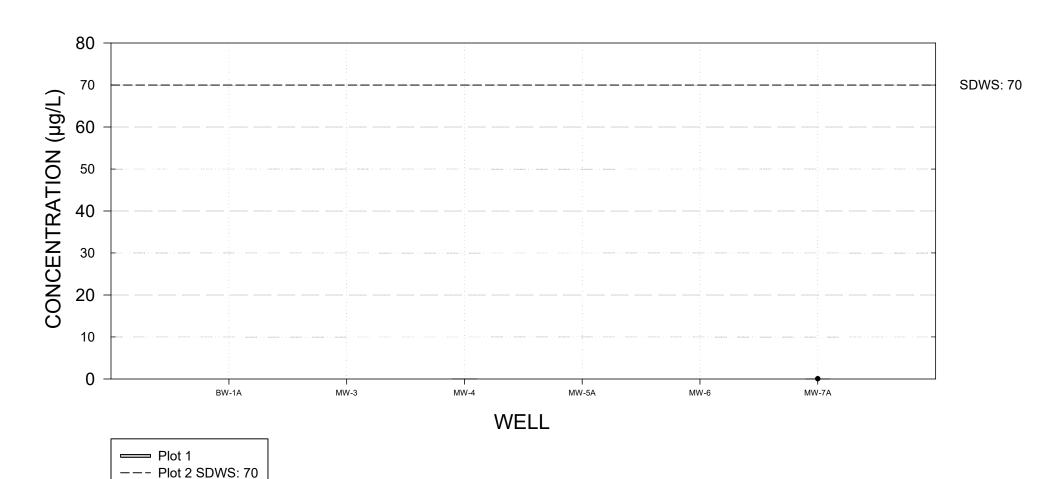




ZINC

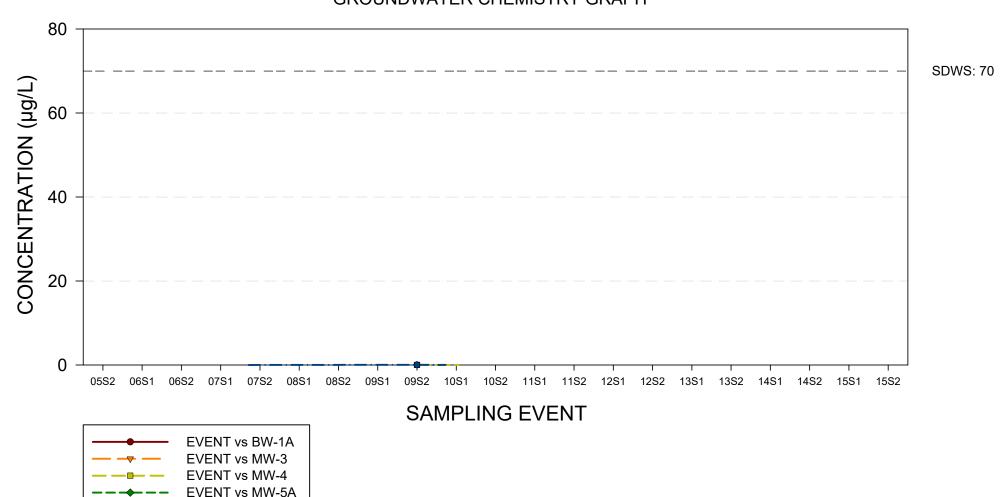






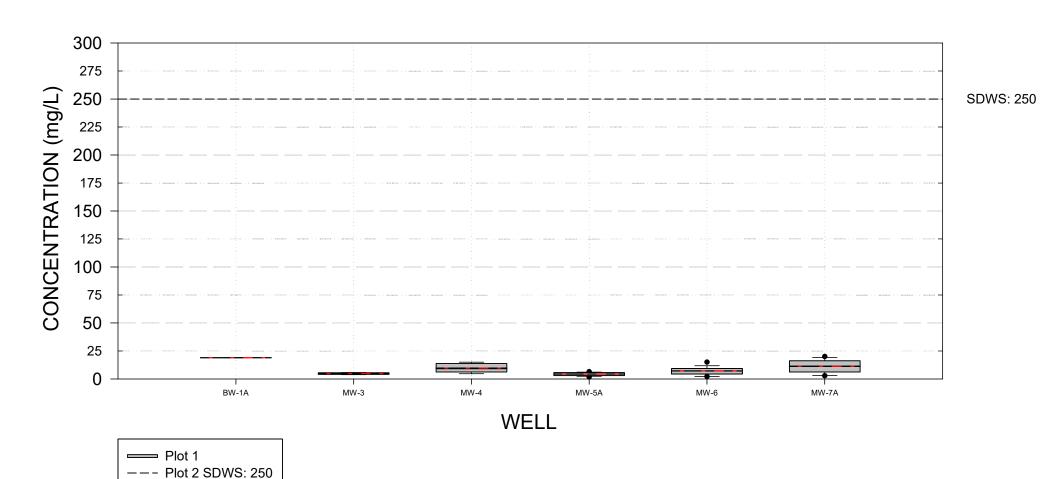
1,2-DIBROMOETHANE

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



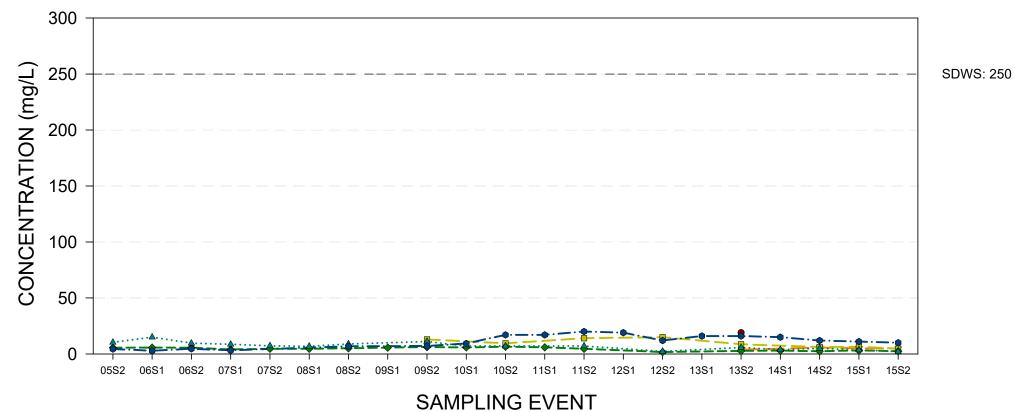
EVENT vs MW-6 EVENT vs MW-7A Plot 1 SDWS: 70

CHLORIDE



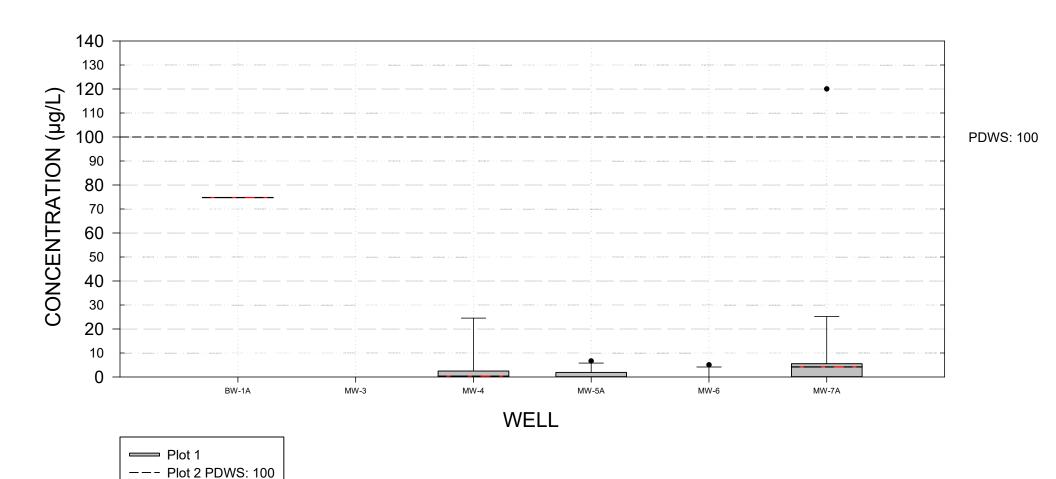
CHLORIDE

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



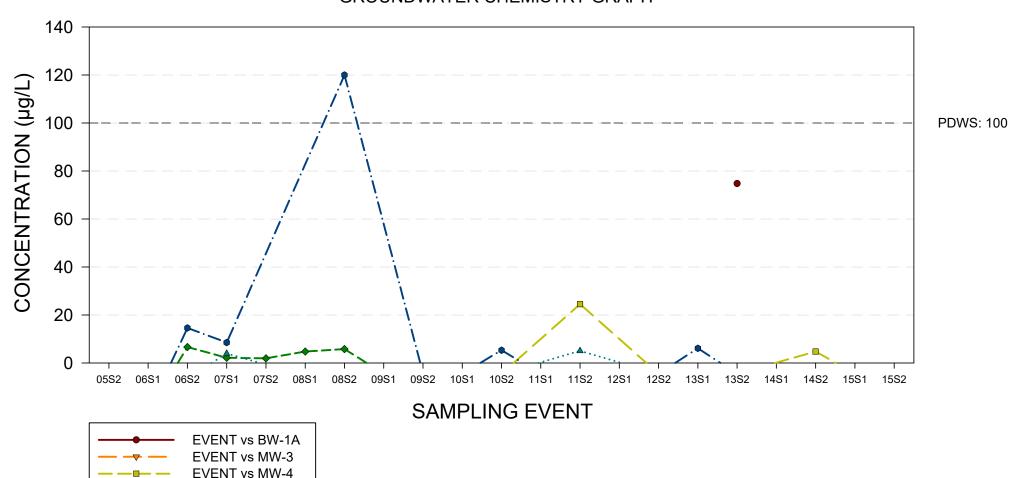
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A
Plot 1 SDWS: 250

CHROMIUM



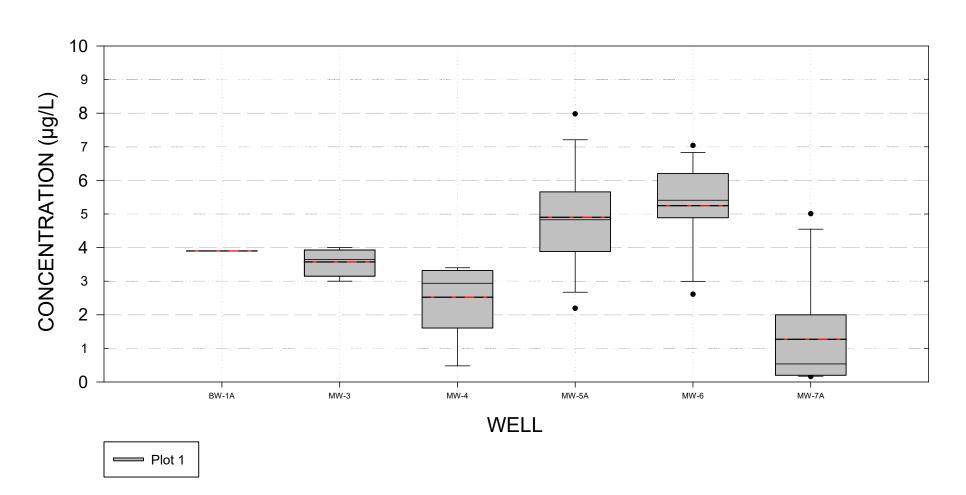
CHROMIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



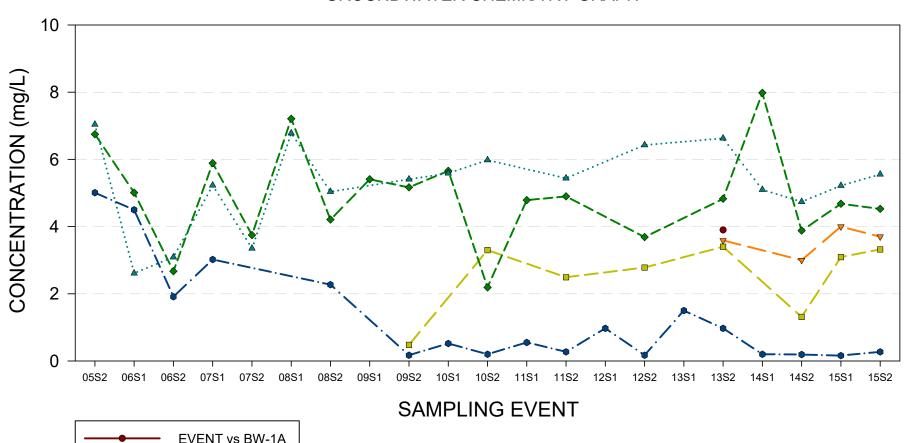
EVENT vs MW-5A EVENT vs MW-6 EVENT vs MW-7A Plot 1 PDWS: 100

DISSOLVED OXYGEN

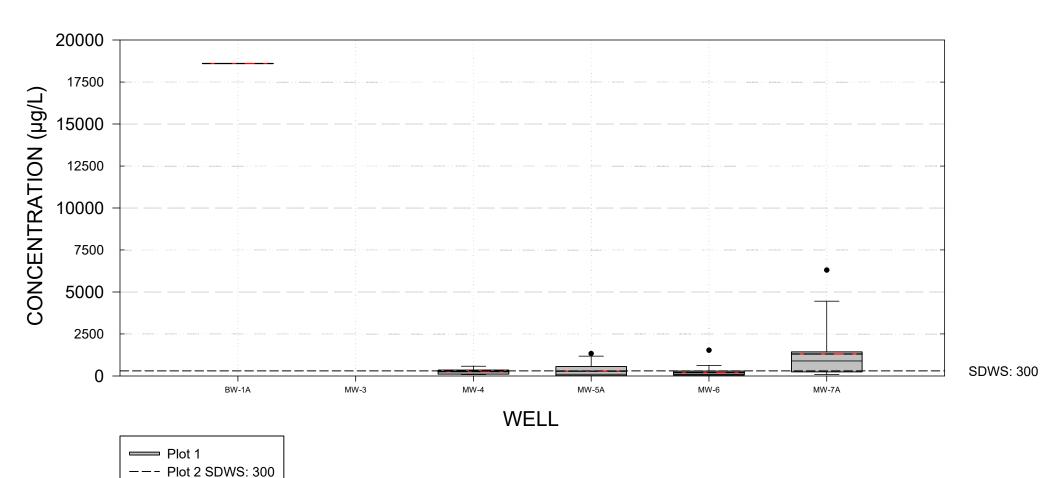


DISSOLVED OXYGEN

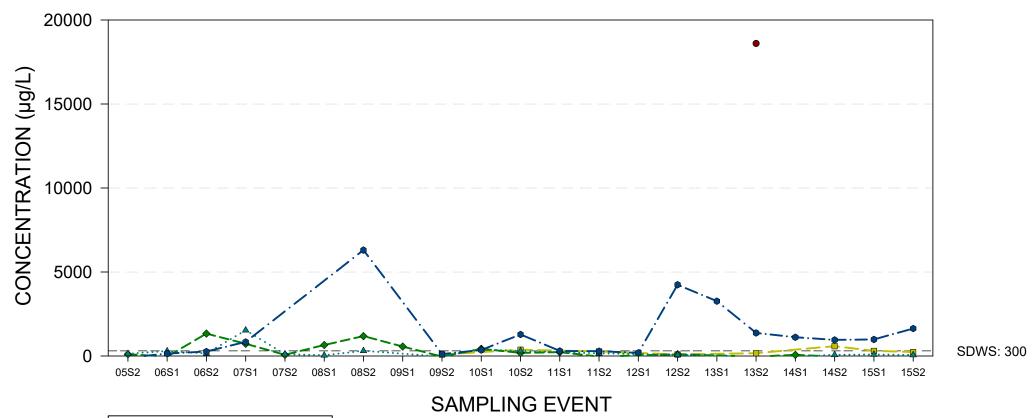
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH

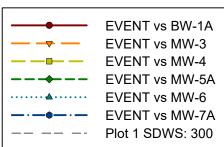


EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A

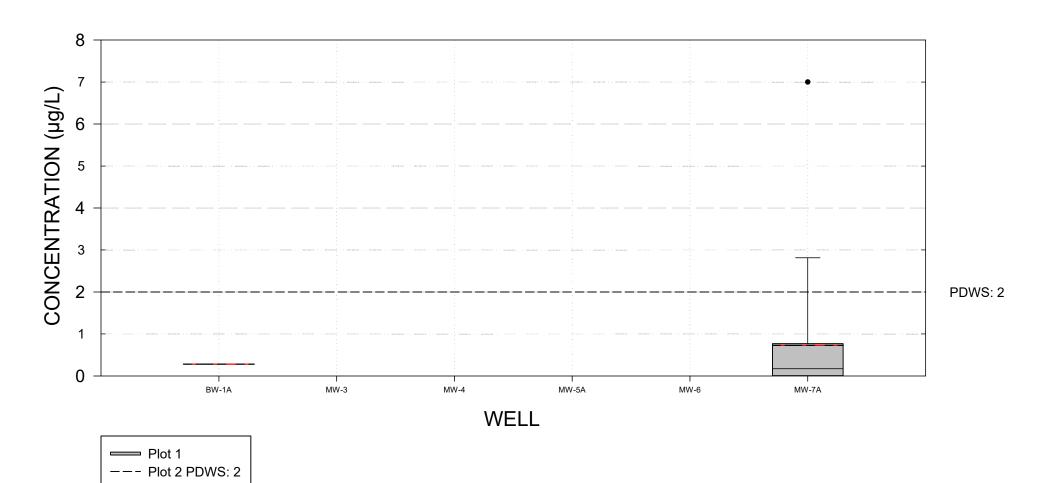


IRON



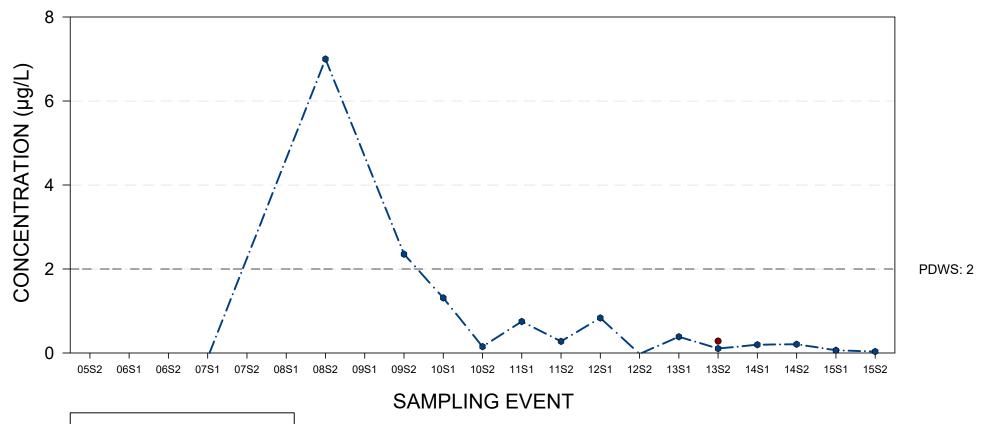


MERCURY



MERCURY

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1A

EVENT vs MW-3

EVENT vs MW-4

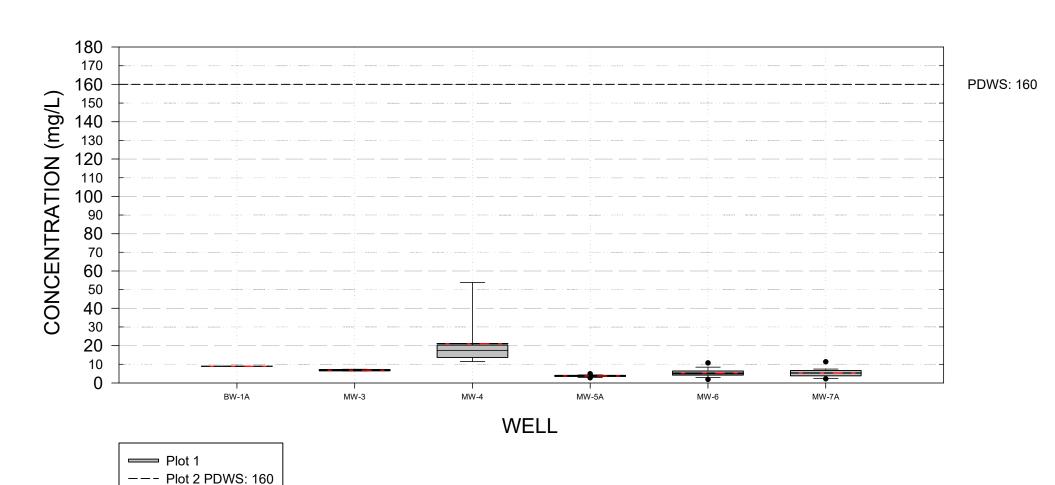
EVENT vs MW-5A

EVENT vs MW-6

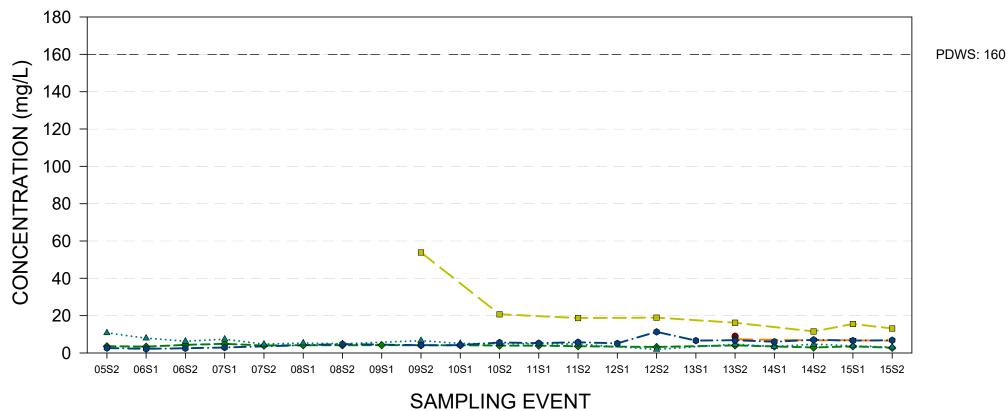
EVENT vs MW-7A

Plot 1 PDWS: 2

SODIUM

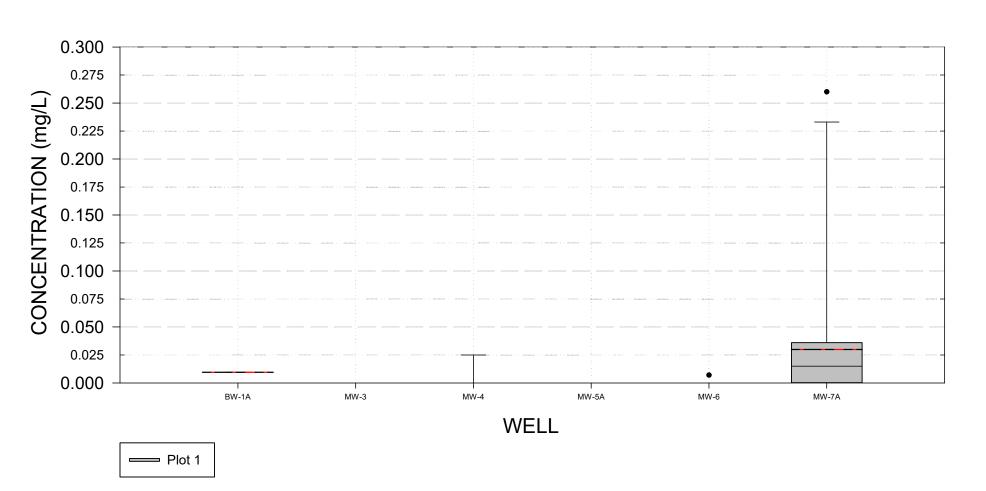


SODIUM



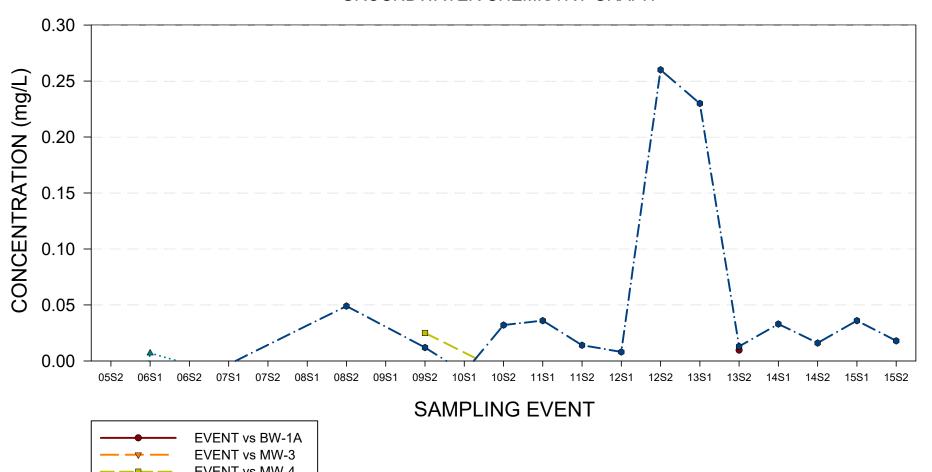
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A
Plot 1 PDWS: 160

AMMONIA AS NITROGEN



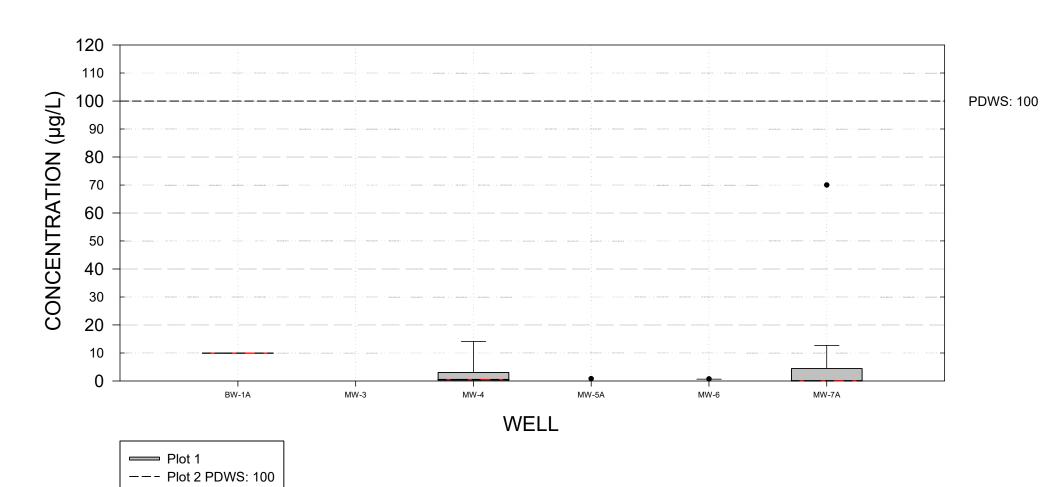
AMMONIA AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



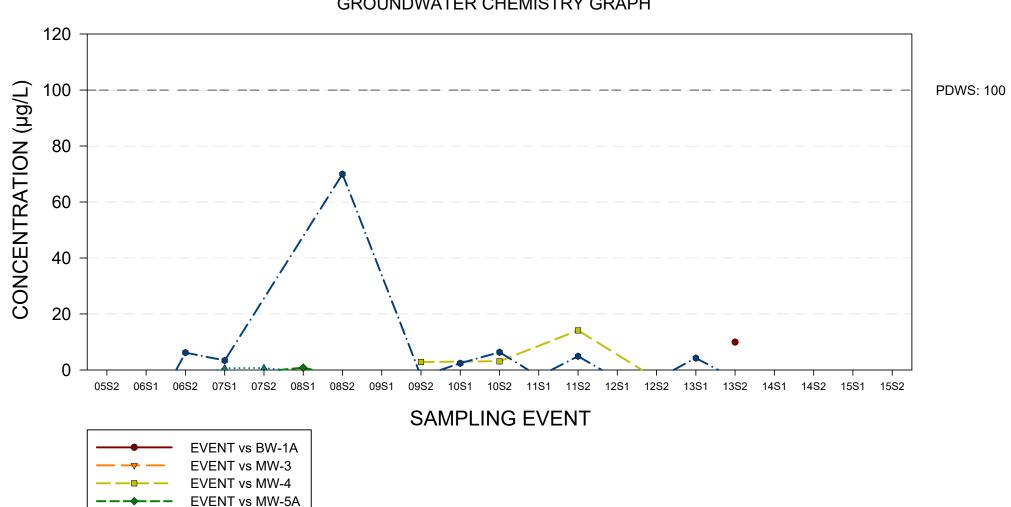
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A

NICKEL



NICKEL

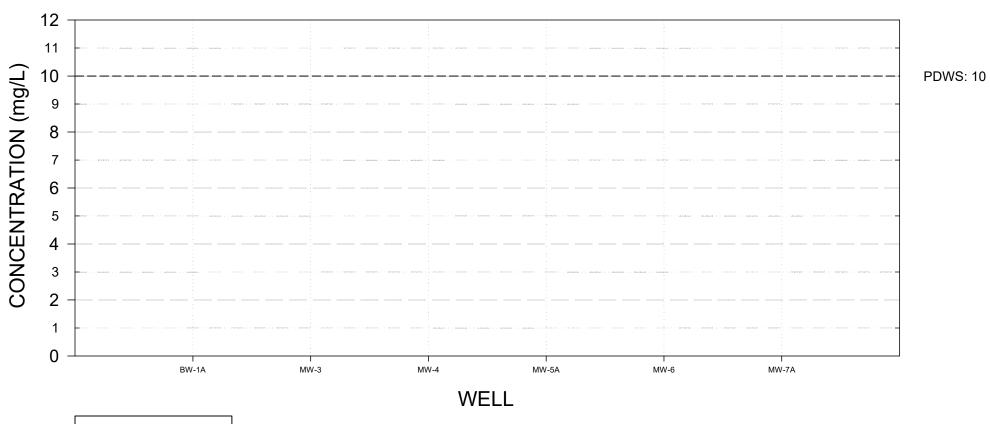
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs MW-6 EVENT vs MW-7A Plot 1 PDWS: 100

NITRITE AS NITROGEN

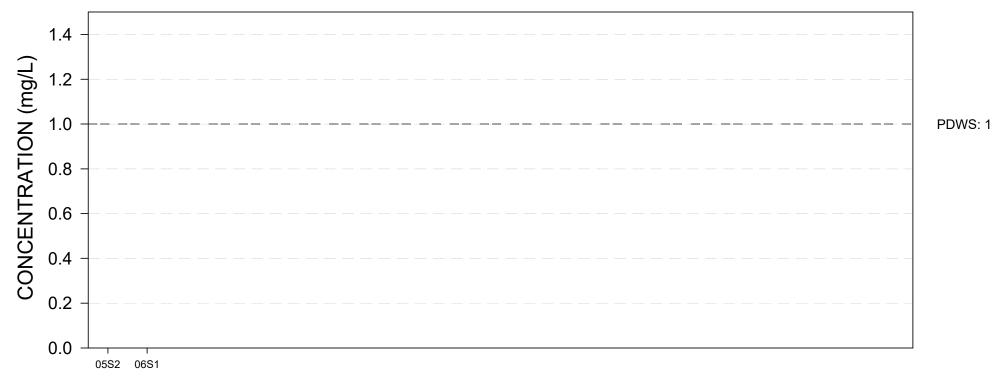
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH

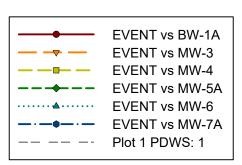


Plot 1
--- Plot 2 PDWS: 10

NITRITE AS NITROGEN

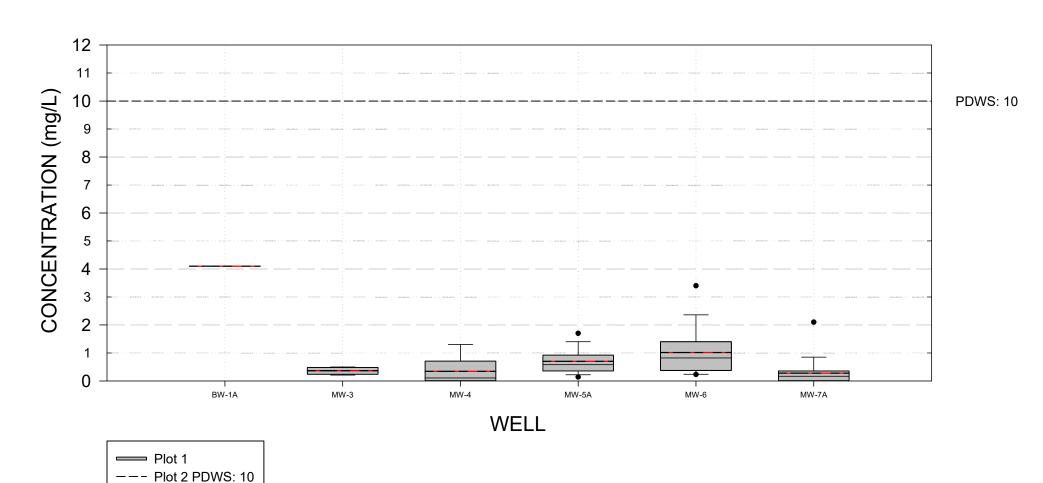
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH





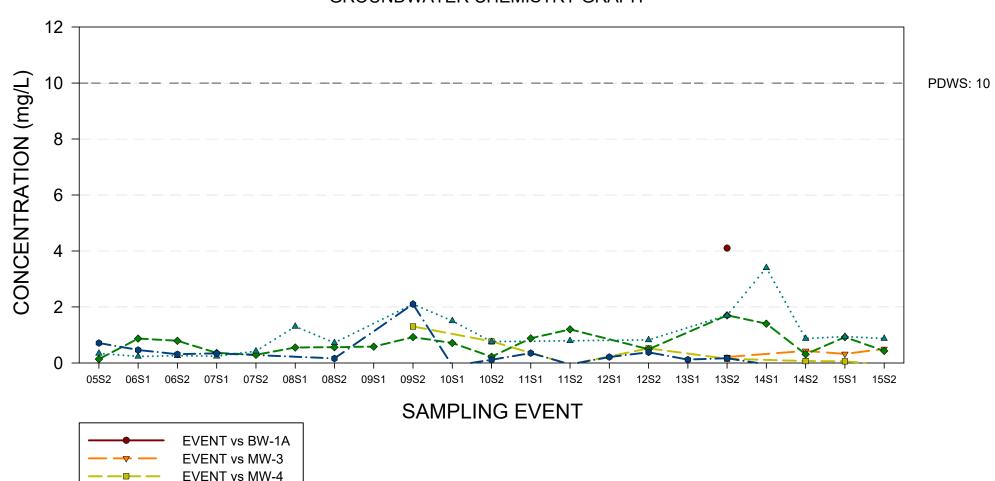
SAMPLING EVENT

NITRATE AS NITROGEN



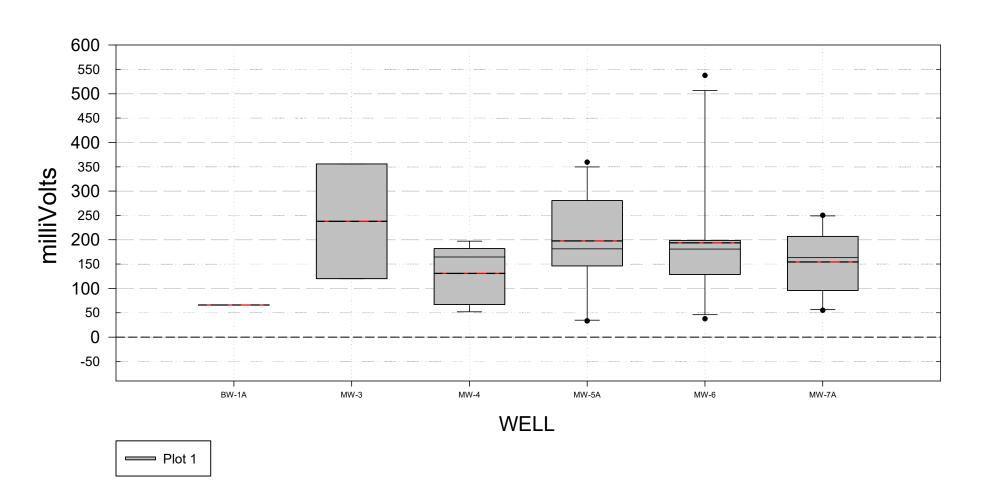
NITRATE AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



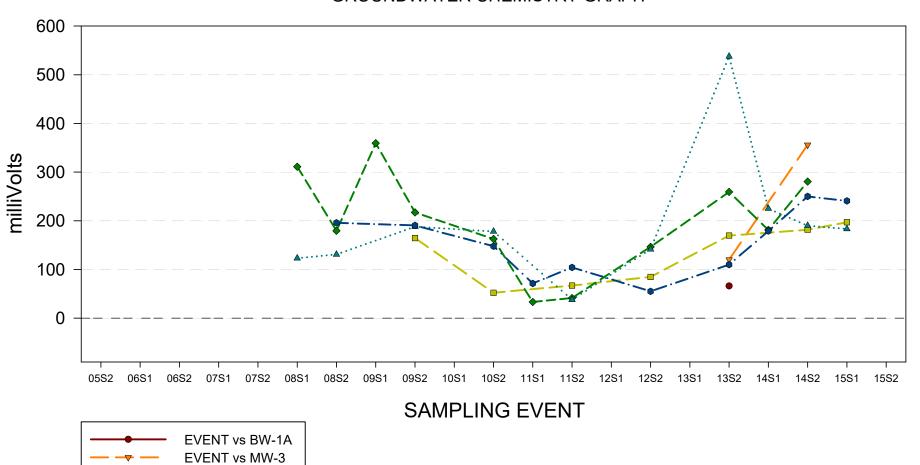
EVENT vs MW-5A EVENT vs MW-6 EVENT vs MW-7A Plot 1 PDWS: 10

OXIDATION / REDUCTION POTENTIAL



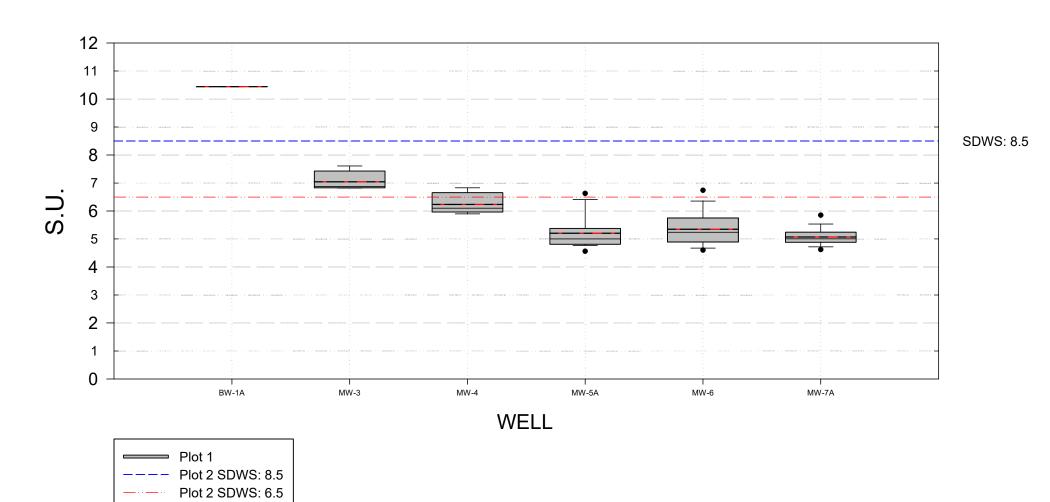
OXIDATION / REDUCTION POTENTIAL

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



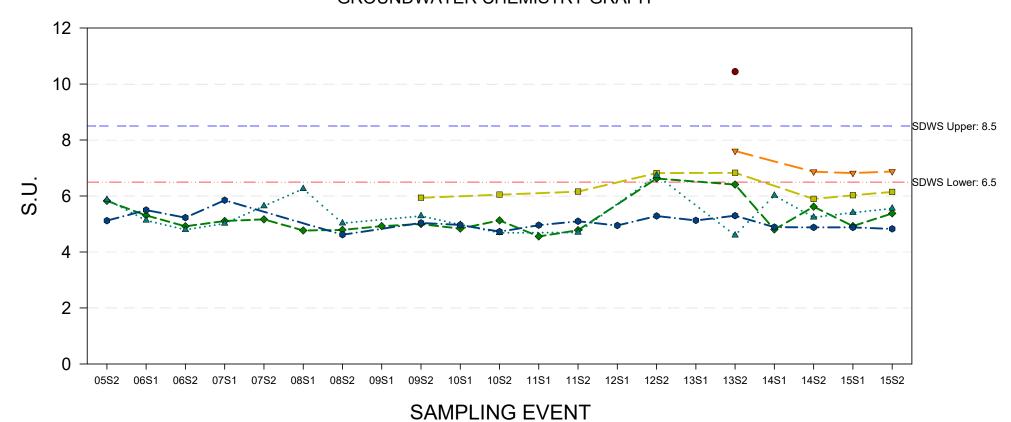
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A

PH
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING
FACILITY SURFICIAL AQUIFER
GROUNDWATER CHEMISTRY GRAPH



PH

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1A EVENT vs MW-3

EVENT vs BW-1A

EVENT vs MW-3

EVENT vs MW-4

EVENT vs MW-5A

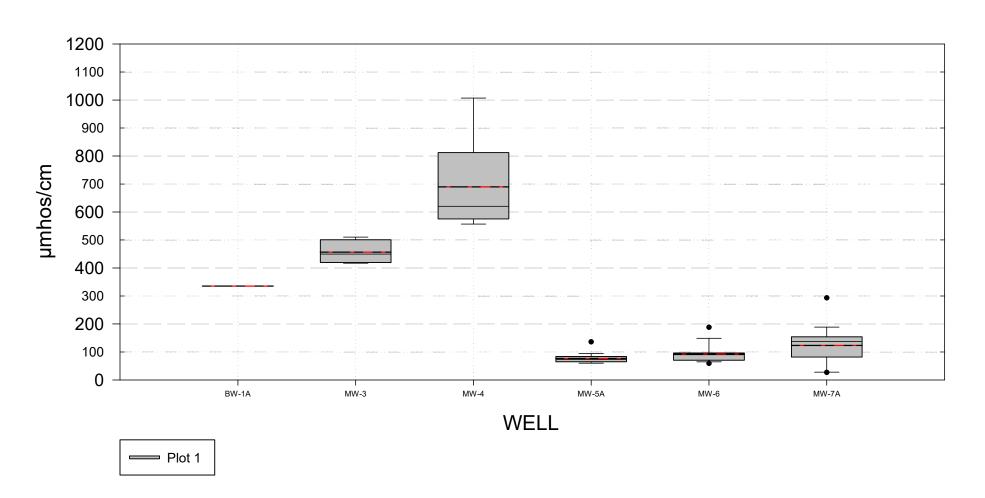
EVENT vs MW-6

EVENT vs MW-7A

Plot 1 SDWS Upper: 8.5

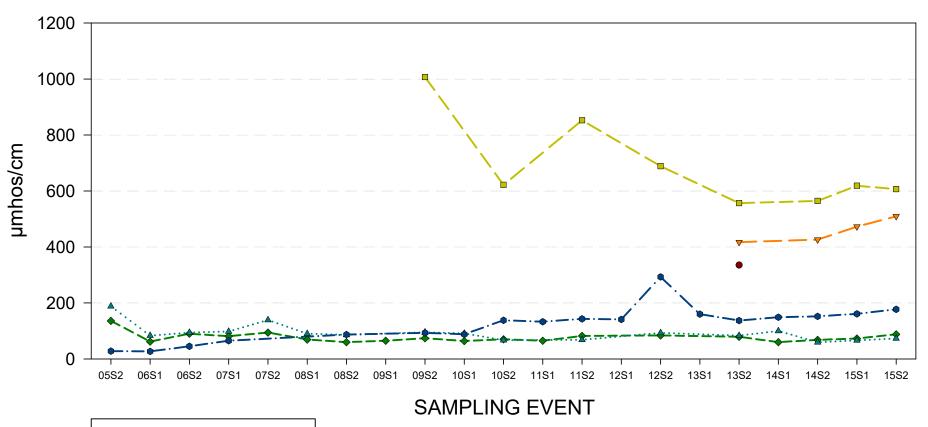
Plot 1 SDWS Lower: 6.5

SPECIFIC CONDUCTANCE



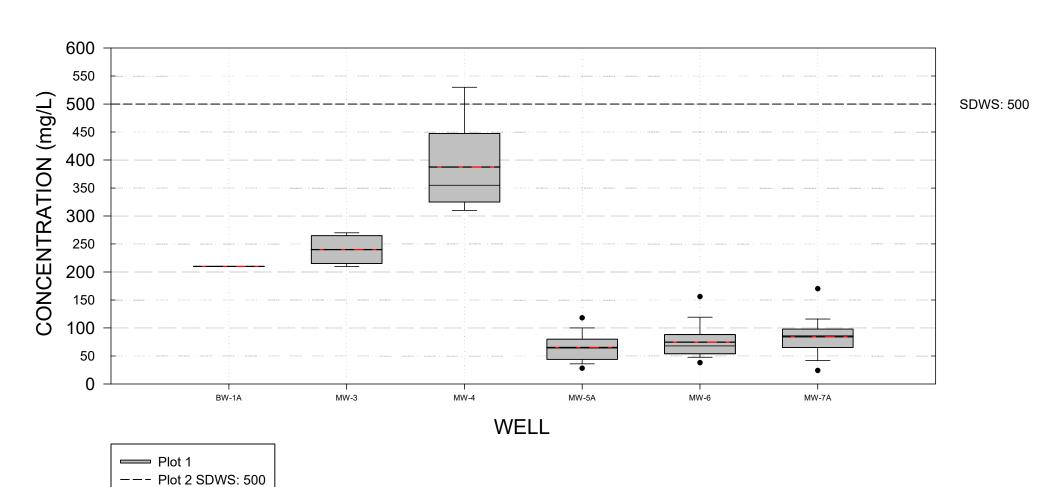
SPECIFIC CONDUCTANCE

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



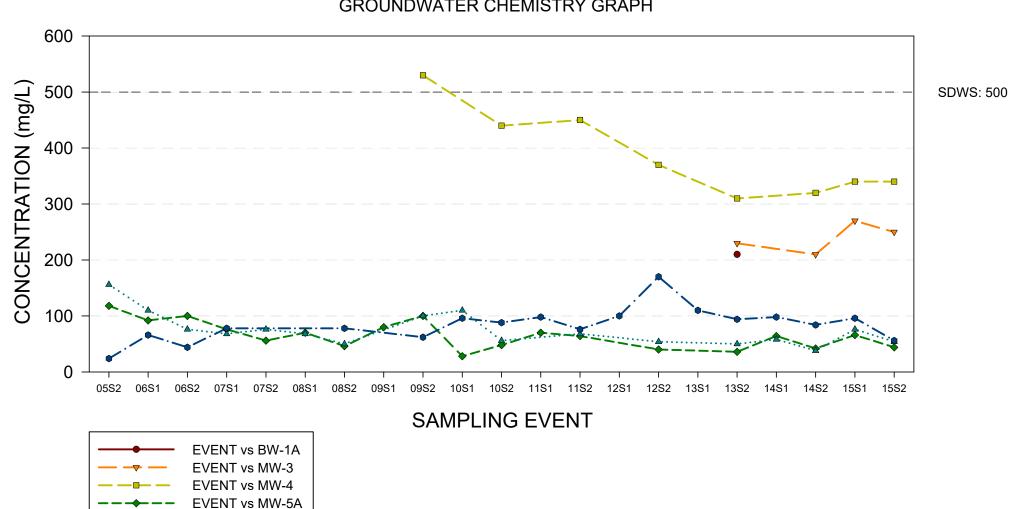
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A

TOTAL DISSOLVED SOLIDS



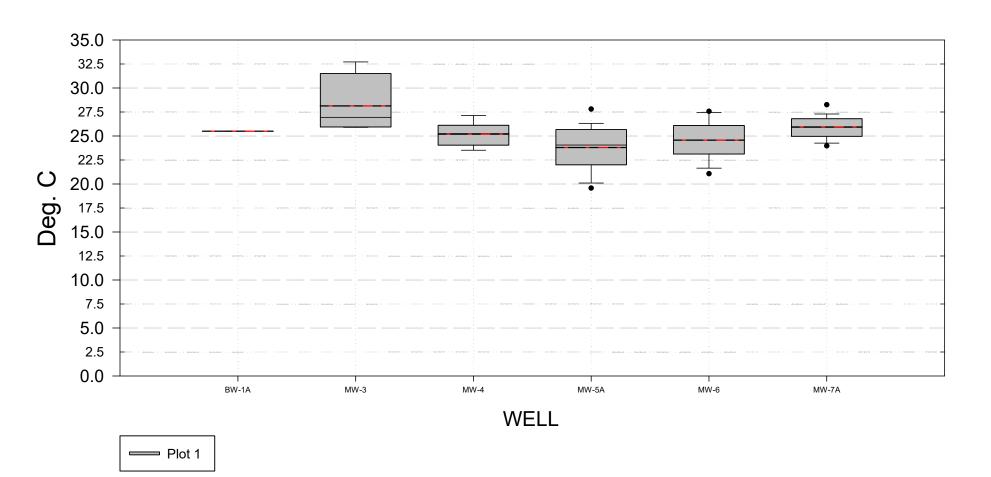
TOTAL DISSOLVED SOLIDS

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



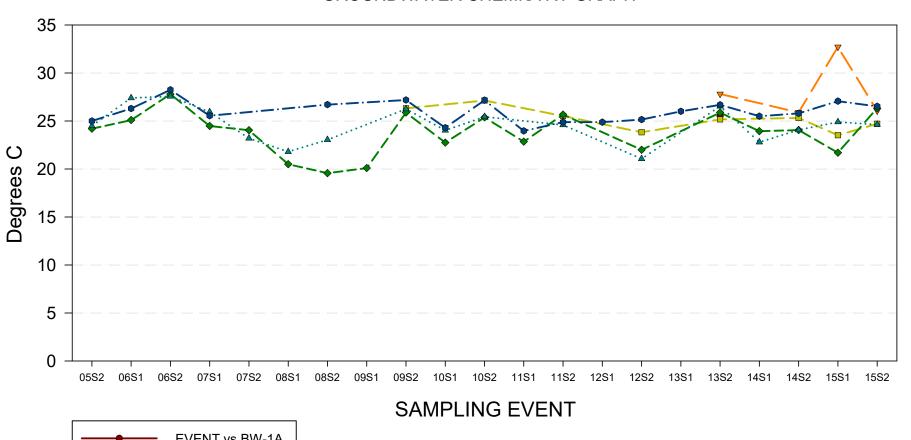
EVENT vs MW-6 EVENT vs MW-7A Plot 1 SDWS: 500

TEMPERATURE



TEMPERATURE

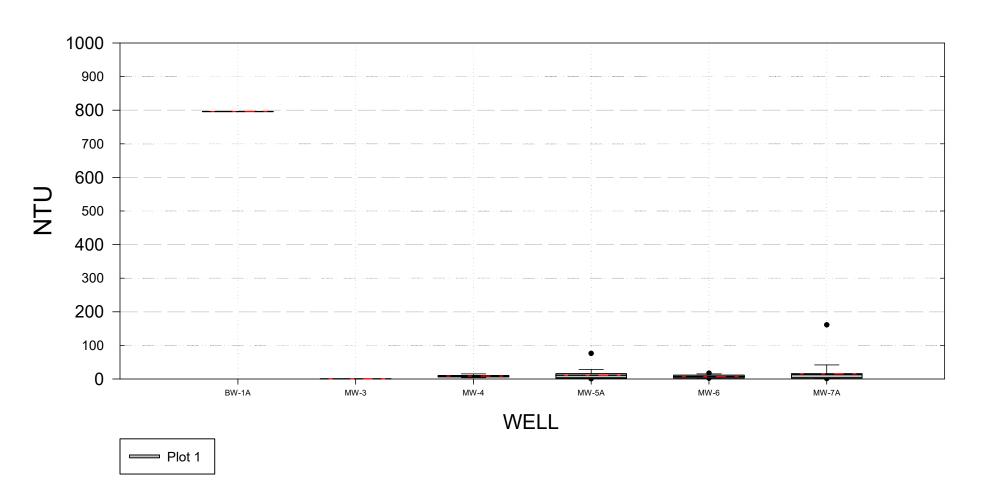
ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A

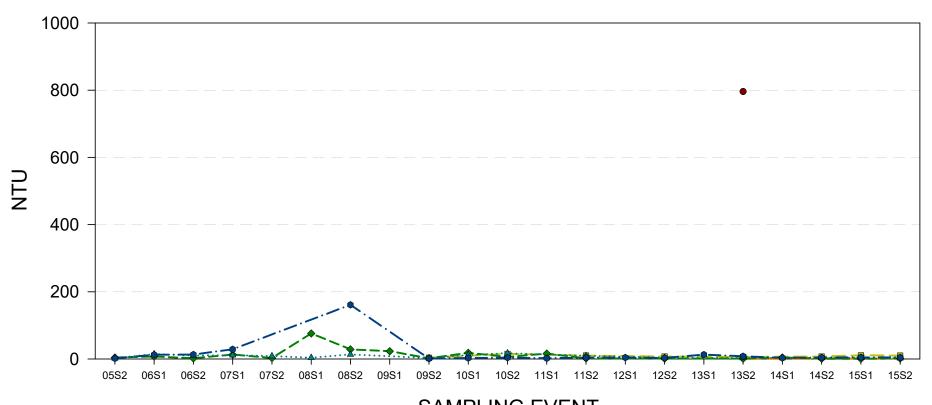
TURBIDITY

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



TURBIDITY

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH

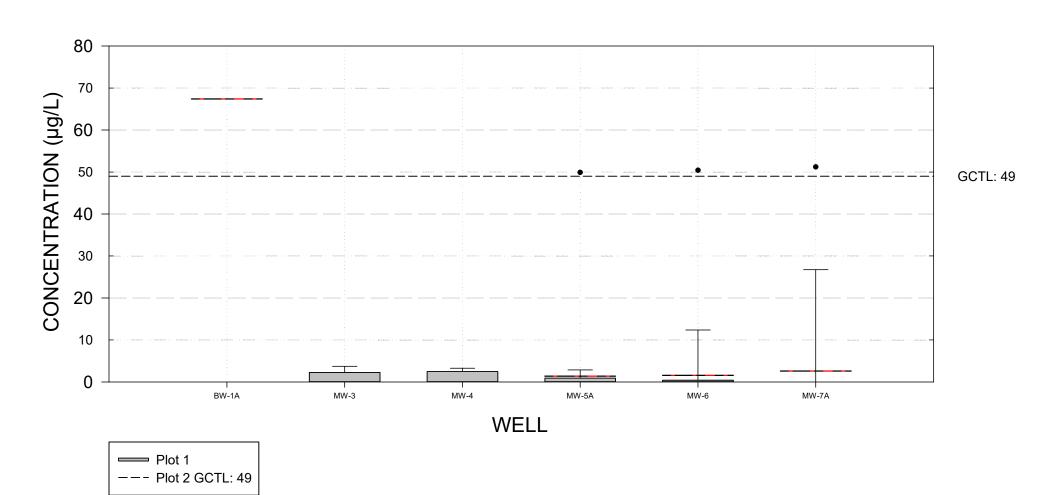


SAMPLING EVENT

EVENT vs BW-1A EVENT vs MW-3 EVENT vs MW-4 EVENT vs MW-5A EVENT vs MW-6 EVENT vs MW-7A

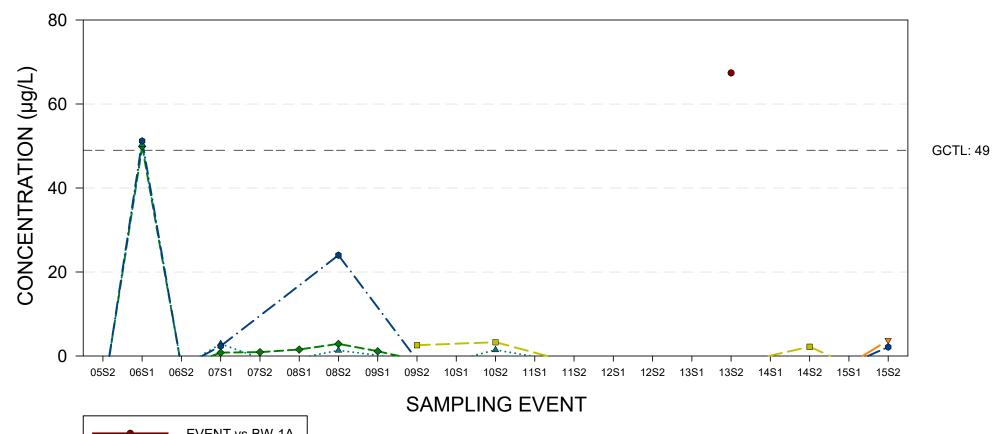
VANADIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



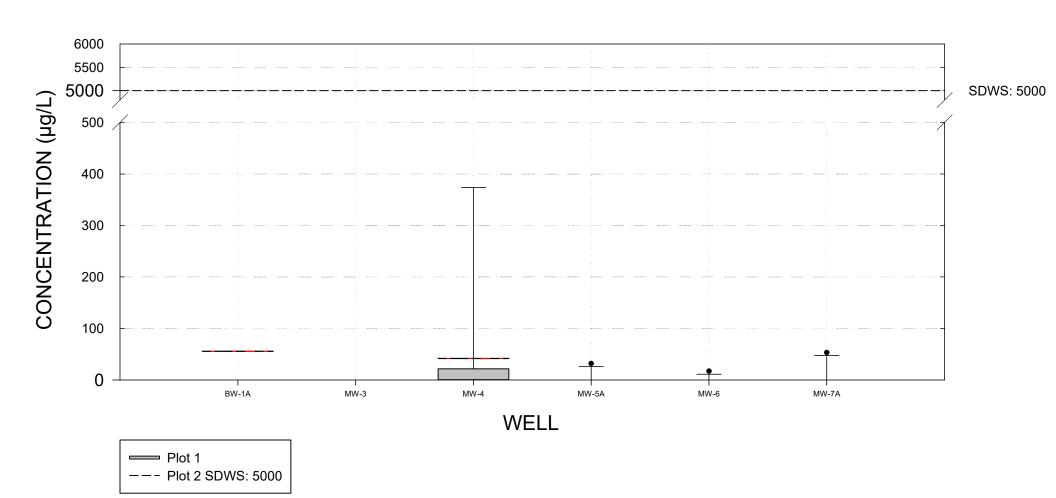
VANADIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



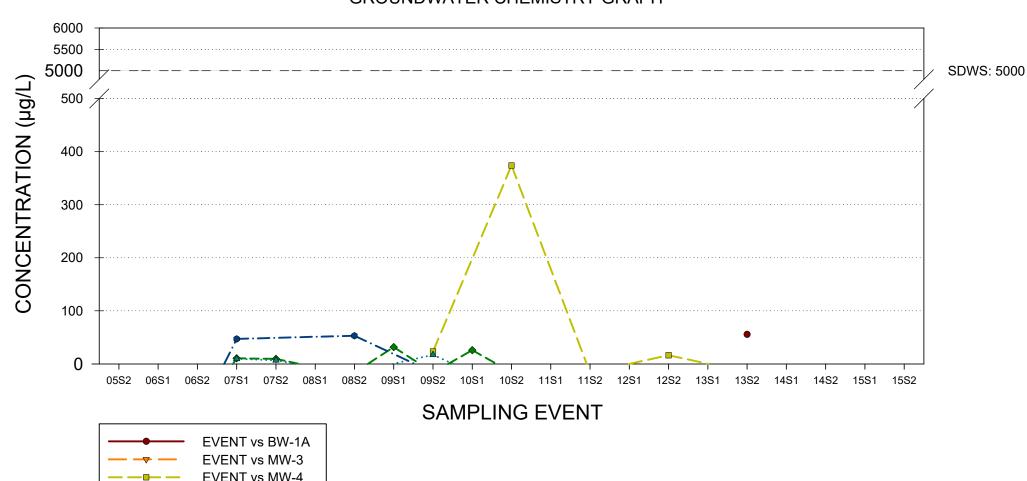
EVENT vs BW-1A
EVENT vs MW-3
EVENT vs MW-4
EVENT vs MW-5A
EVENT vs MW-6
EVENT vs MW-7A
Plot 1 GCTL: 49

ZINC ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



ZINC

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFICIAL AQUIFER GROUNDWATER CHEMISTRY GRAPH



EVENT vs BW-1A

EVENT vs MW-3

EVENT vs MW-4

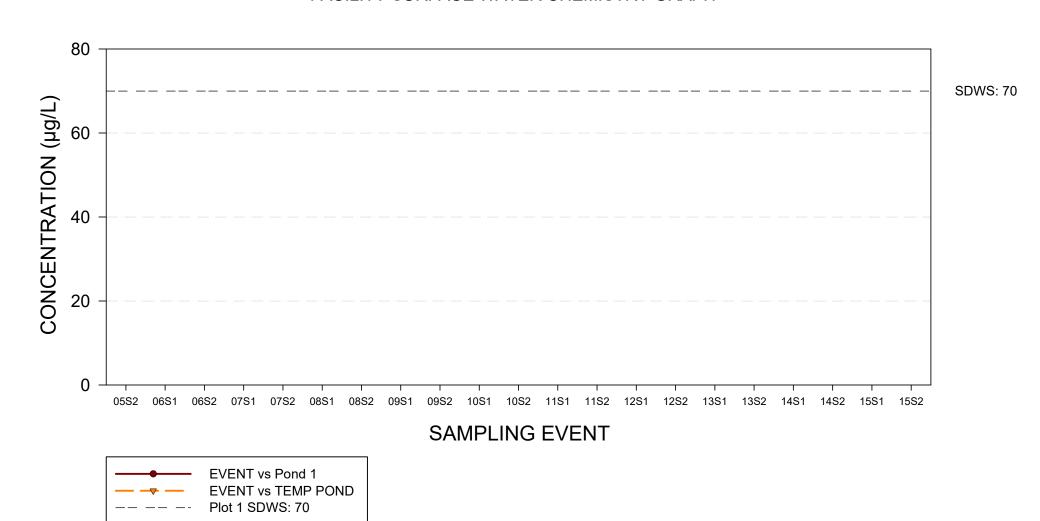
EVENT vs MW-5A

EVENT vs MW-6

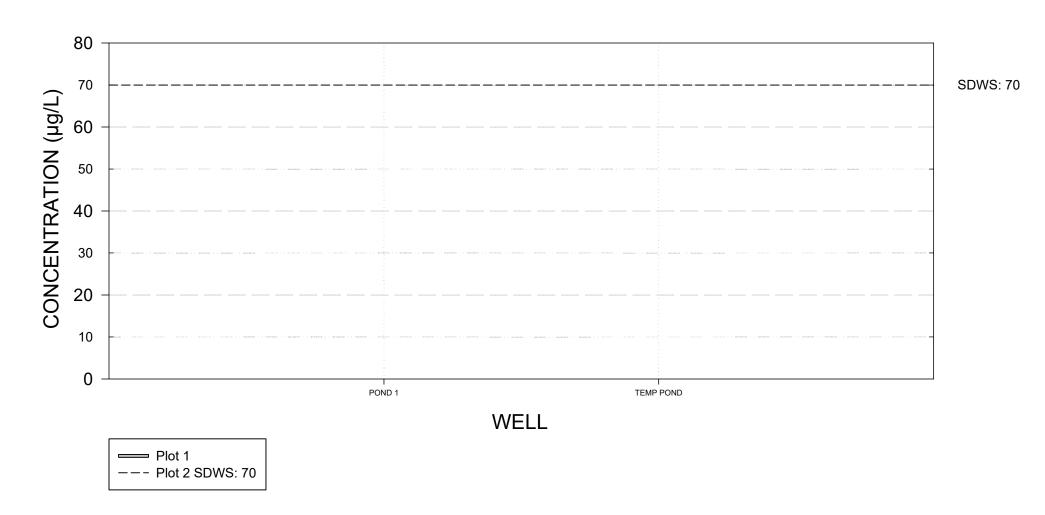
EVENT vs MW-7A

Plot 1 SDWS: 5000

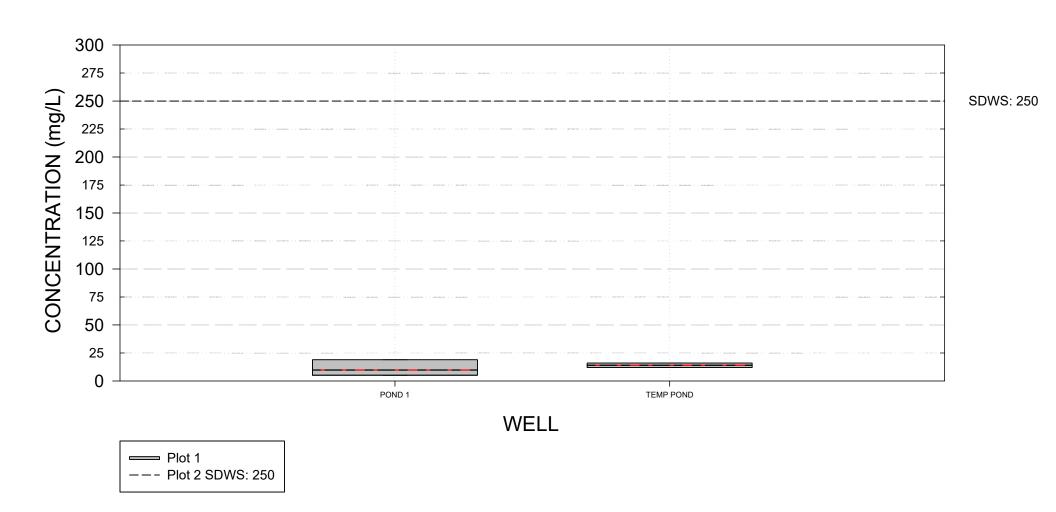
1,2-DIBROMOETHANE



1,2-DIBROMOETHANE

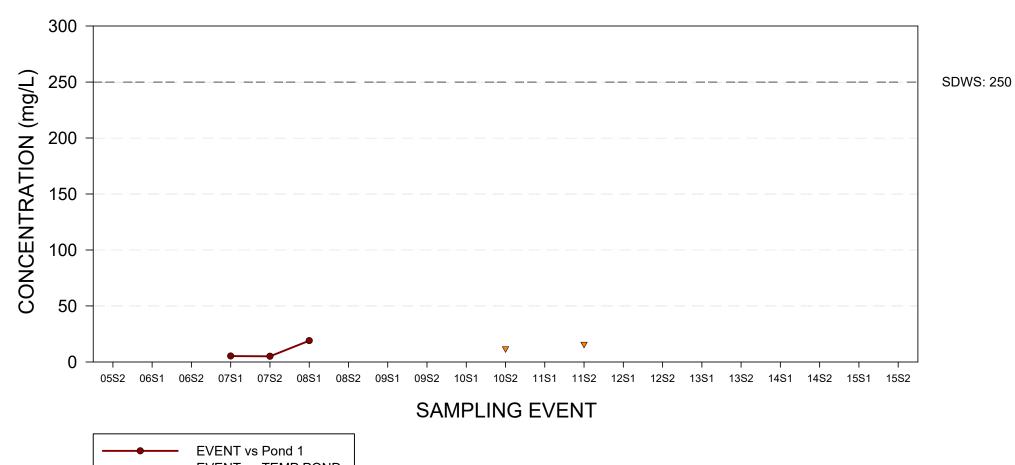


CHLORIDE



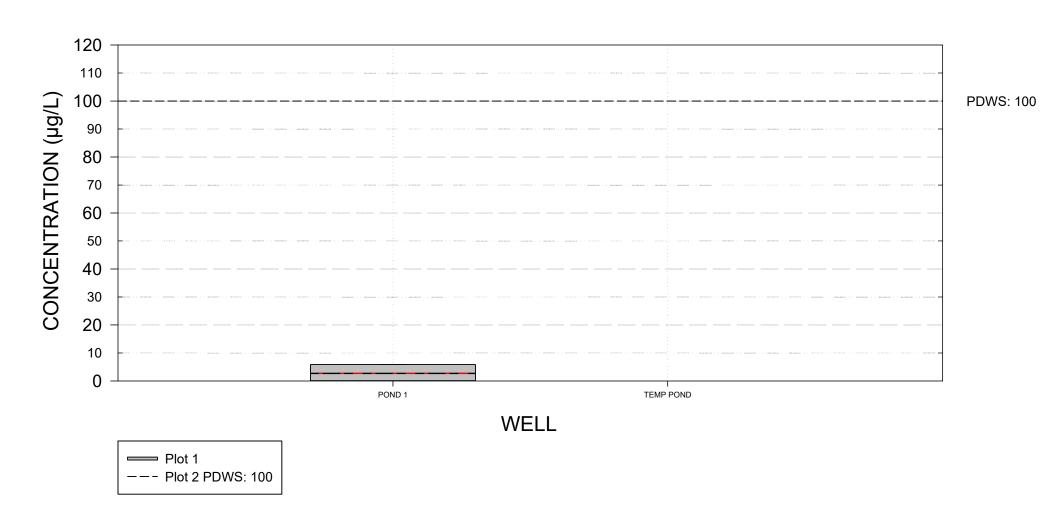
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ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

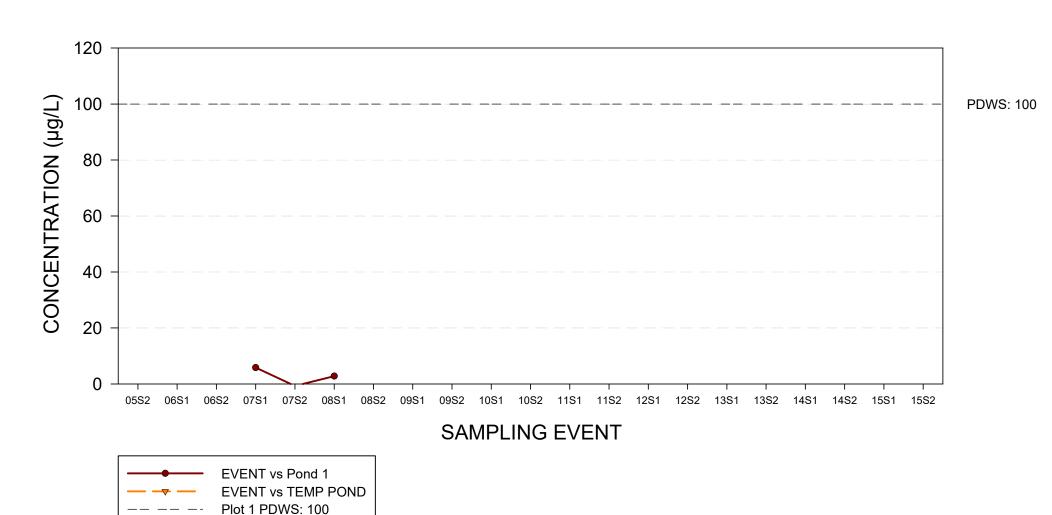


EVENT vs Pond 1
EVENT vs TEMP POND
Plot 1 SDWS: 250

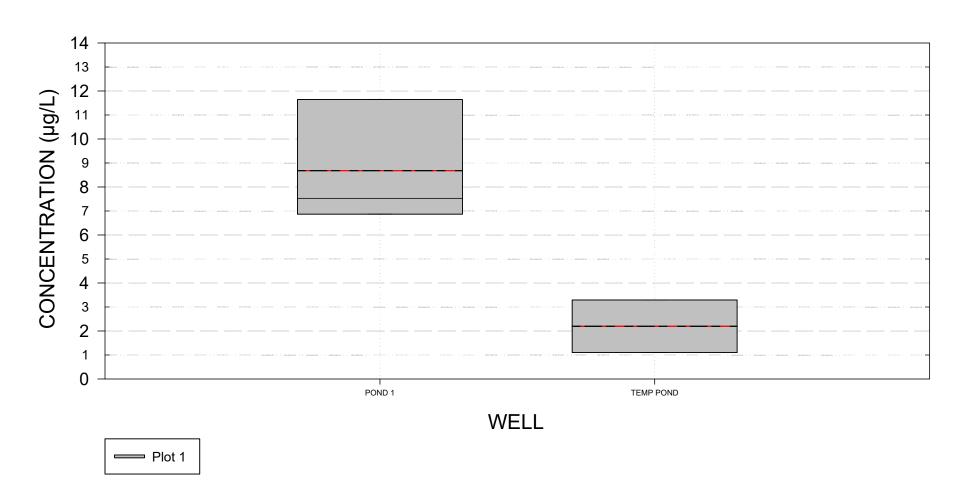
CHROMIUM



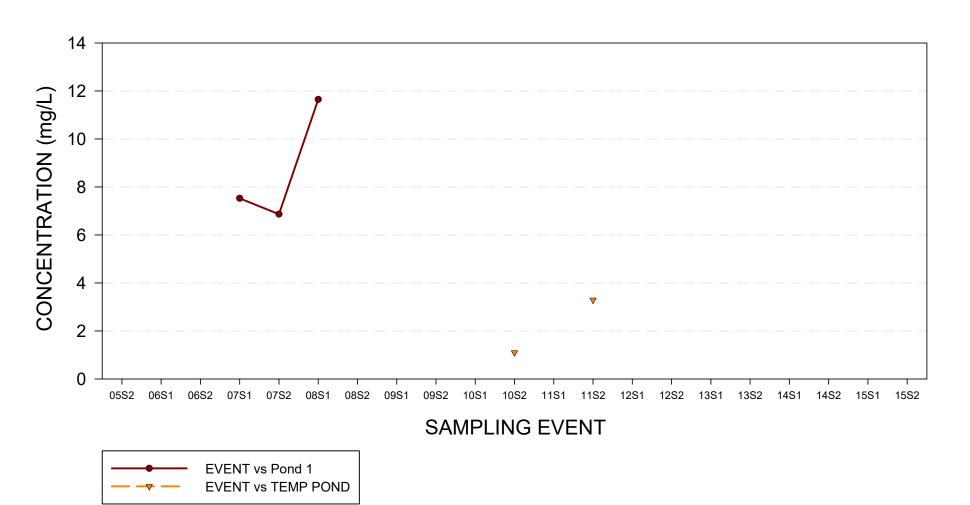
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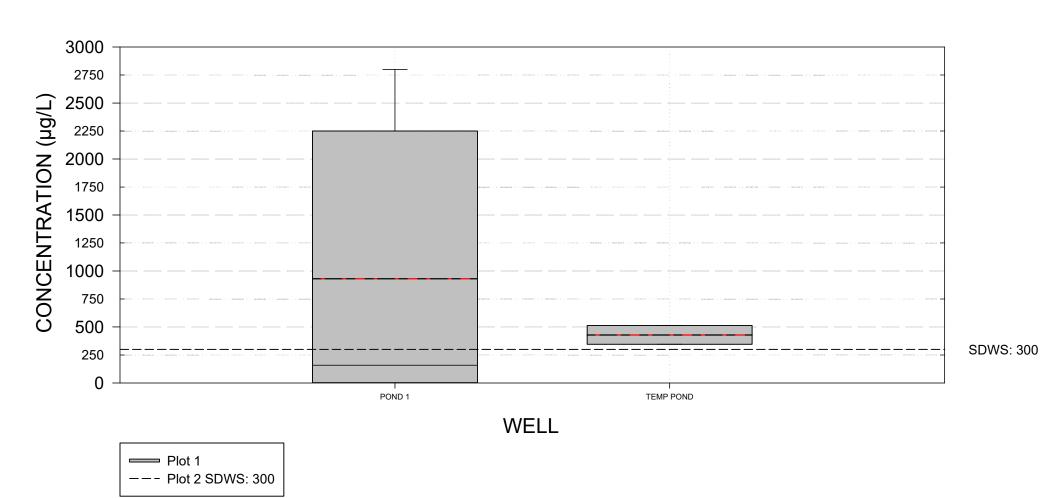
DISSOLVED OXYGEN



DISSOLVED OXYGEN

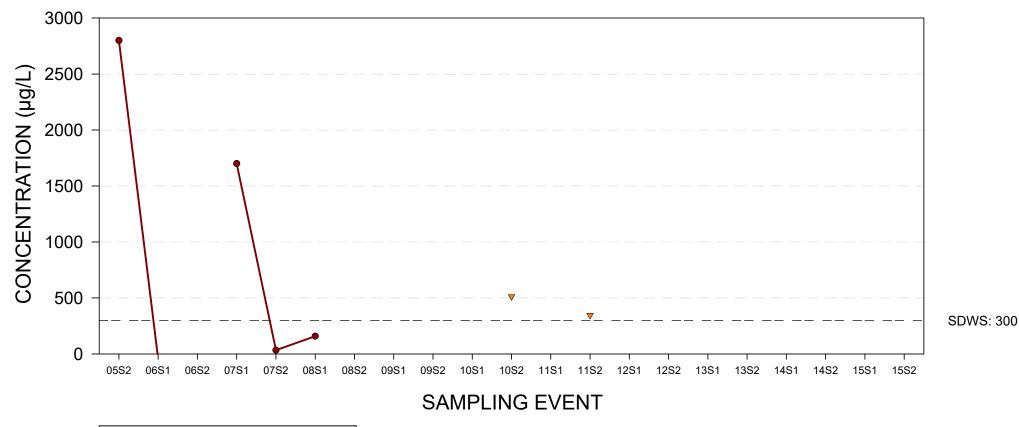


IRON



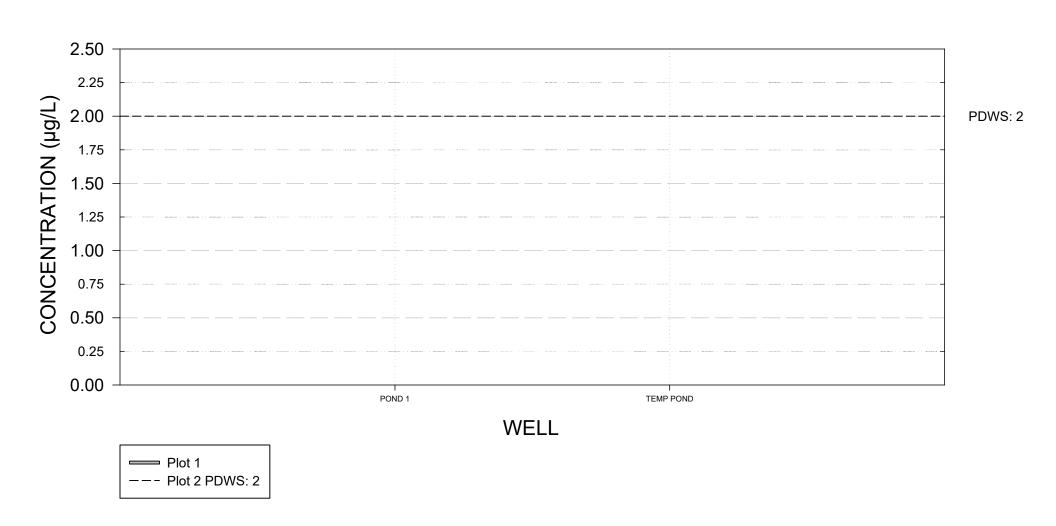
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ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH



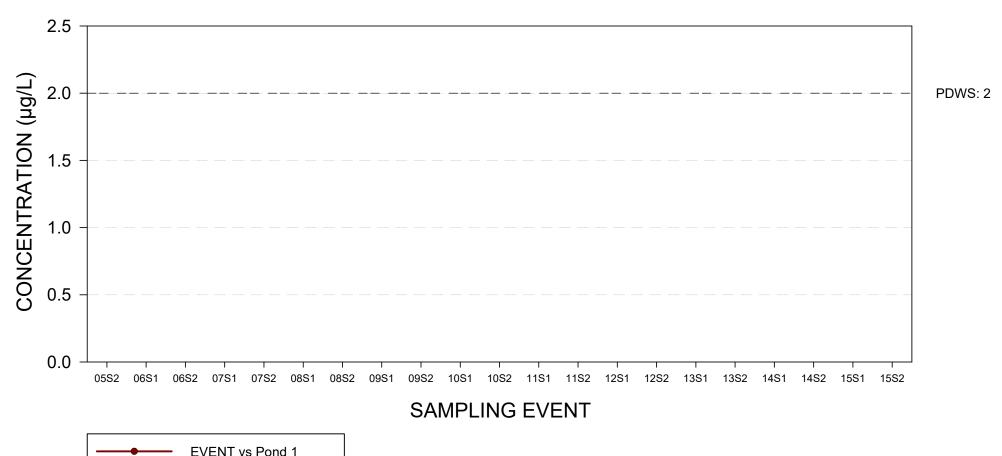
EVENT vs Pond 1
EVENT vs TEMP POND
Plot 1 SDWS: 300

MERCURY



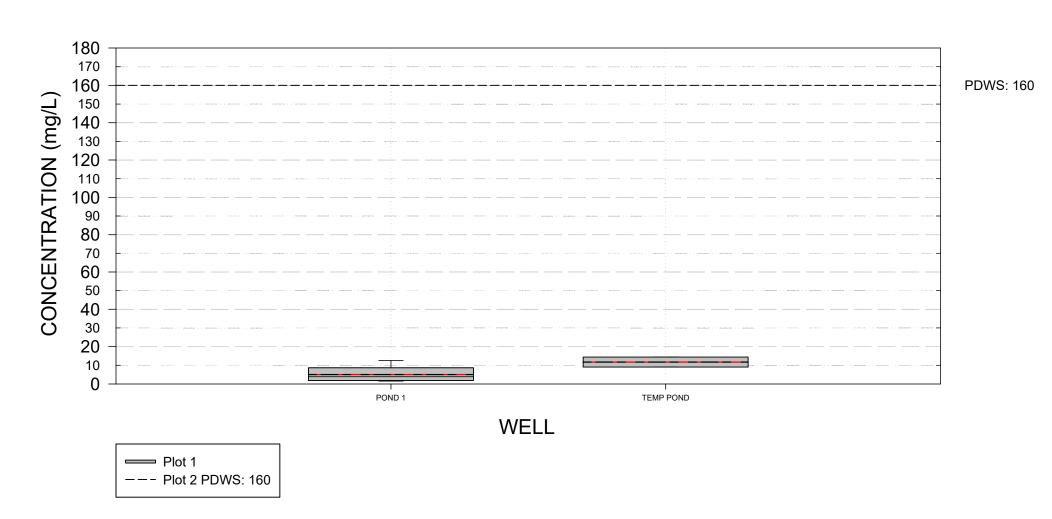
MERCURY

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH



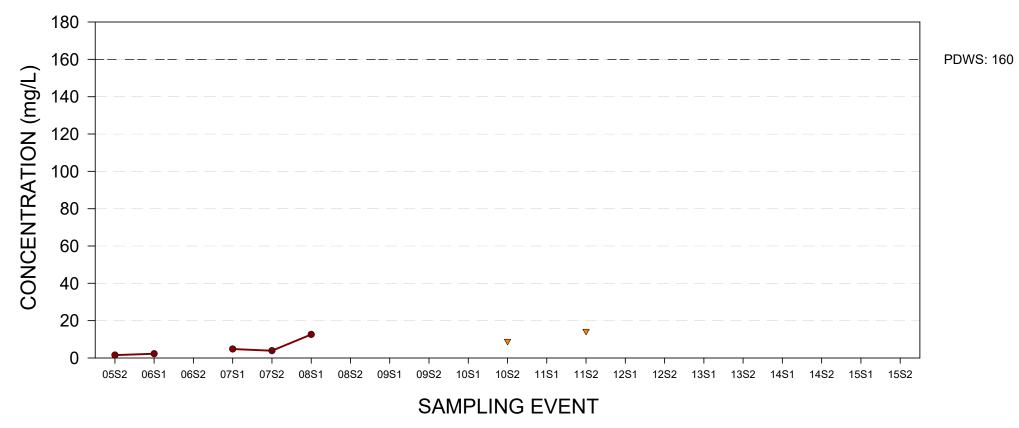
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EVENT vs TEMP POND
Plot 1 PDWS: 2

SODIUM



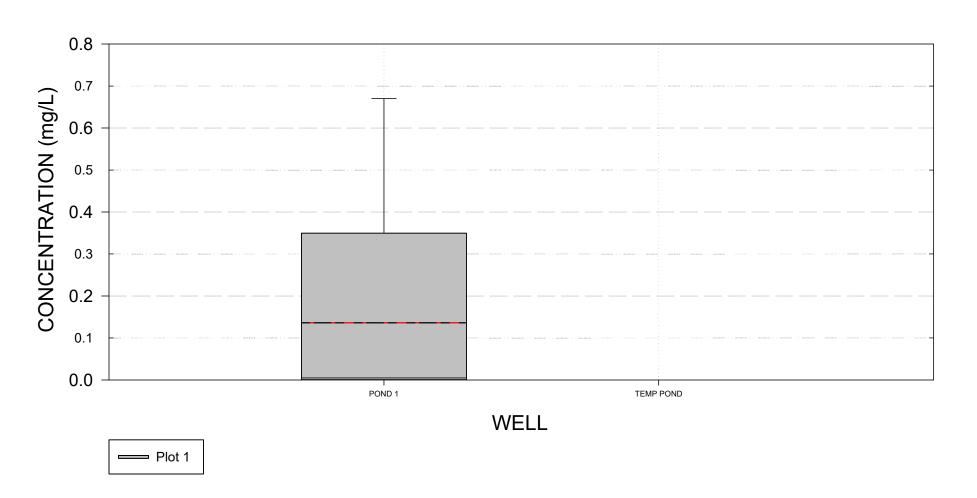
SODIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

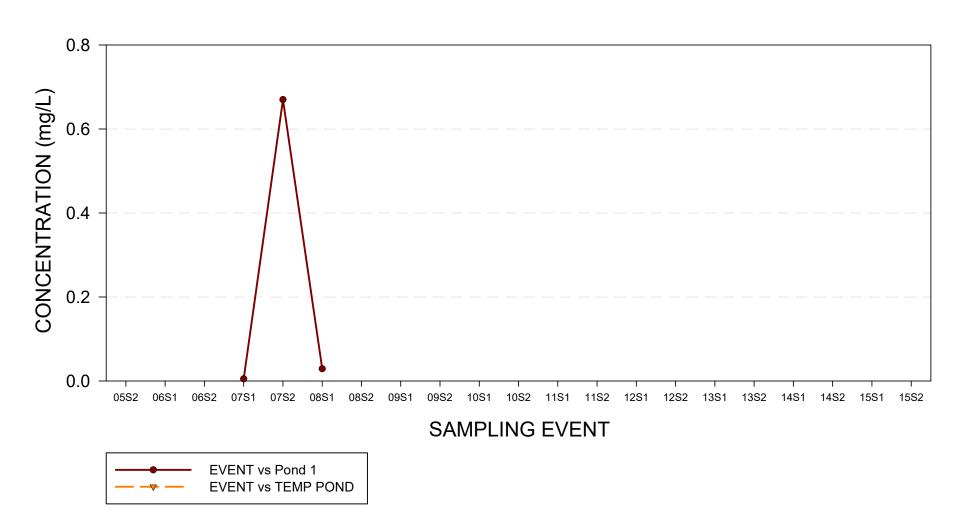


EVENT vs Pond 1
EVENT vs TEMP POND
Plot 1 PDWS: 160

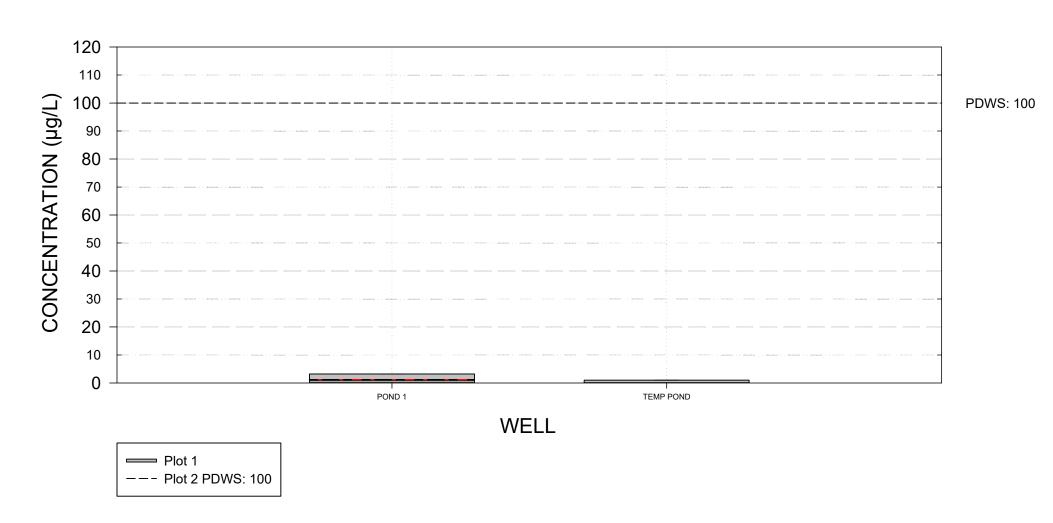
AMMONIA AS NITROGEN



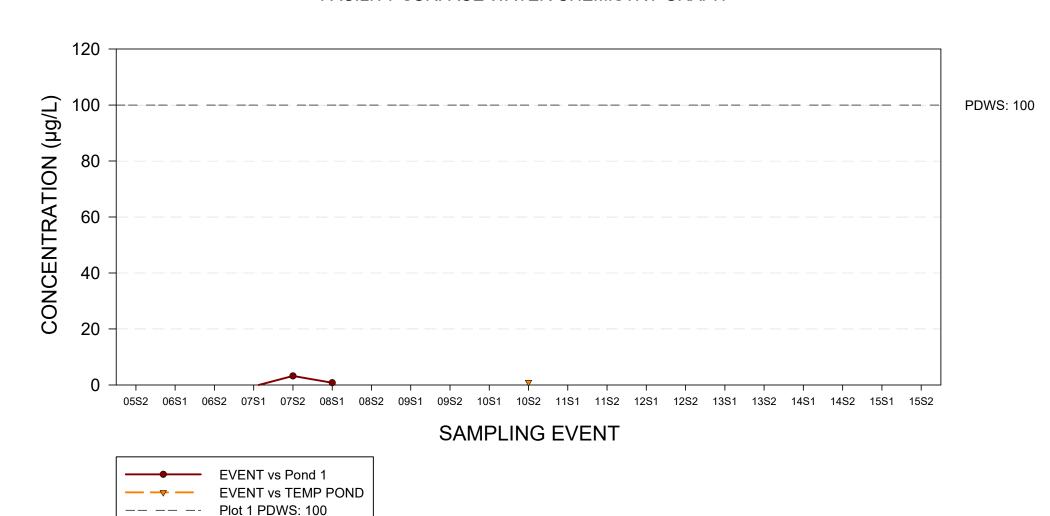
AMMONIA AS NITROGEN



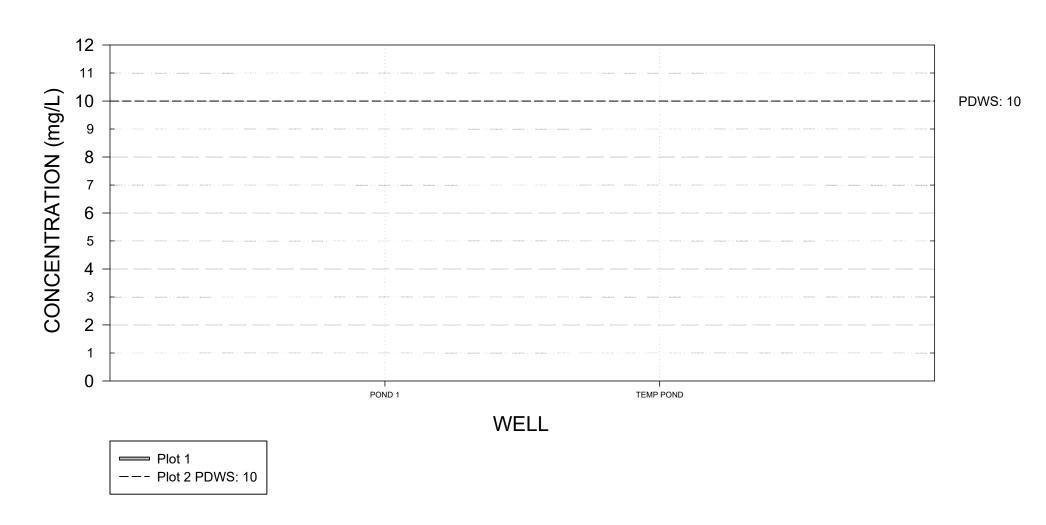
NICKEL



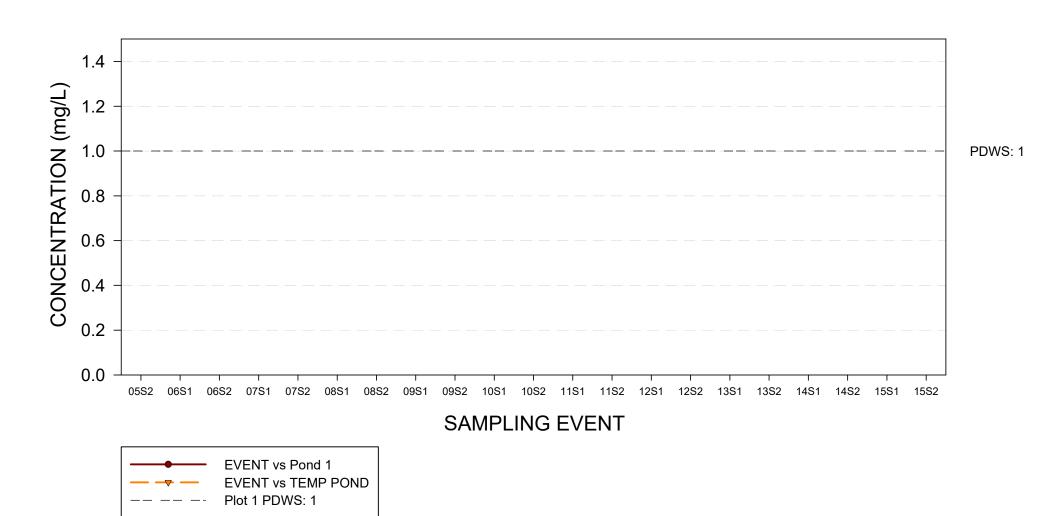
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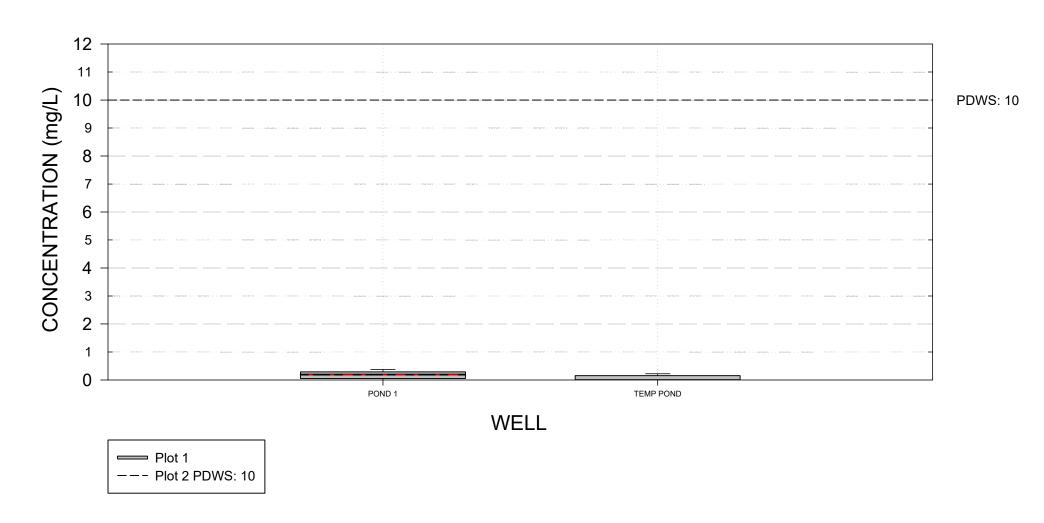
NITRITE AS NITROGEN



NITRITE AS NITROGEN

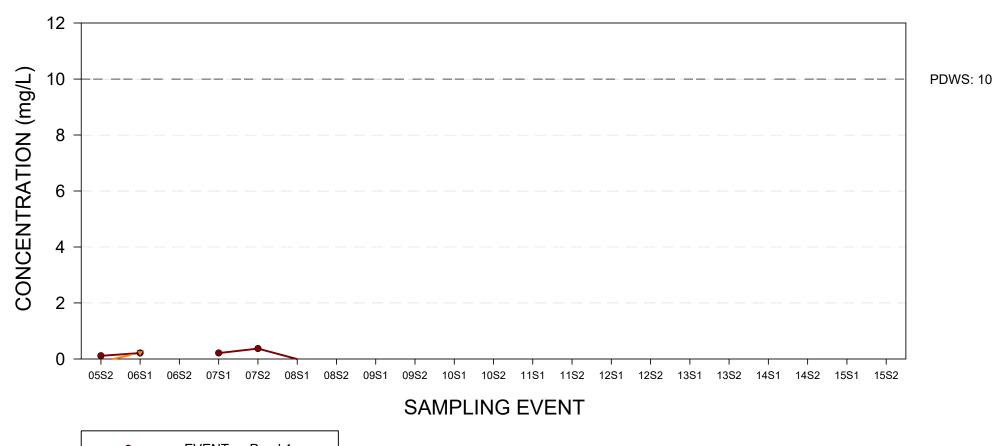


NITRATE AS NITROGEN



NITRATE AS NITROGEN

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

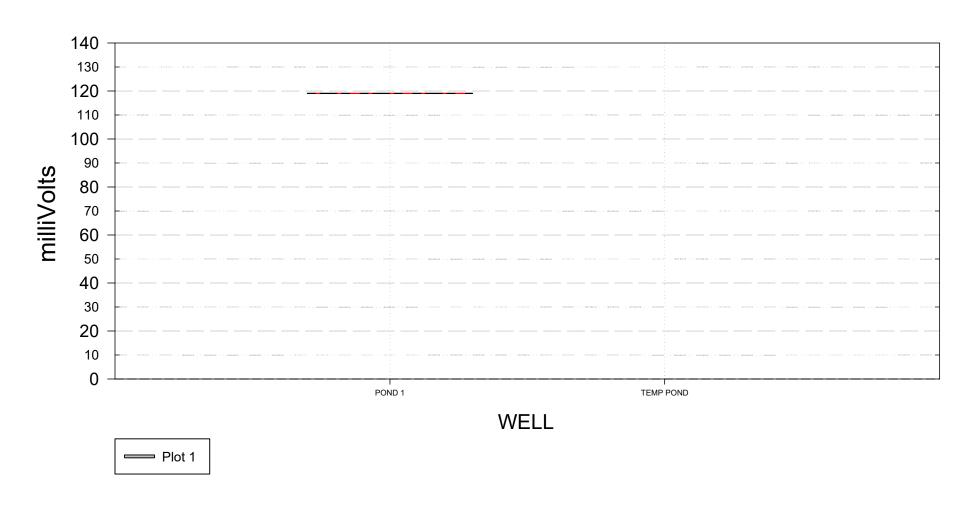


EVENT vs Pond 1

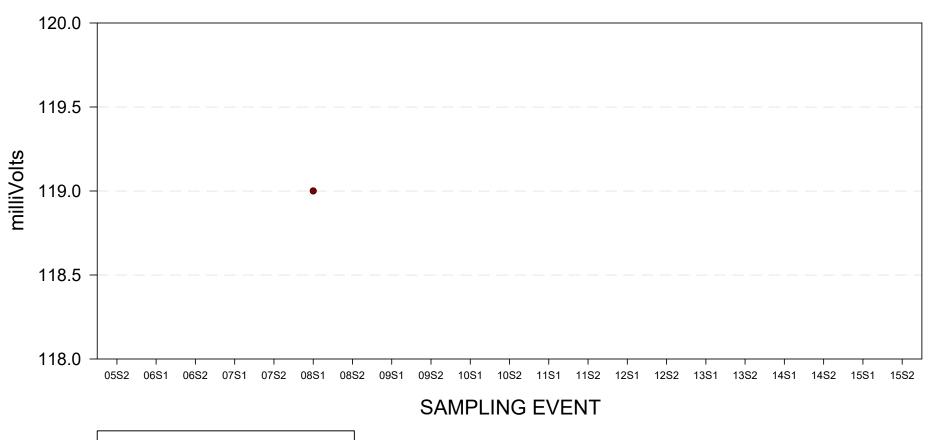
EVENT vs TEMP POND

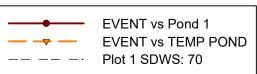
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OXIDATION / REDUCTION POTENTIAL

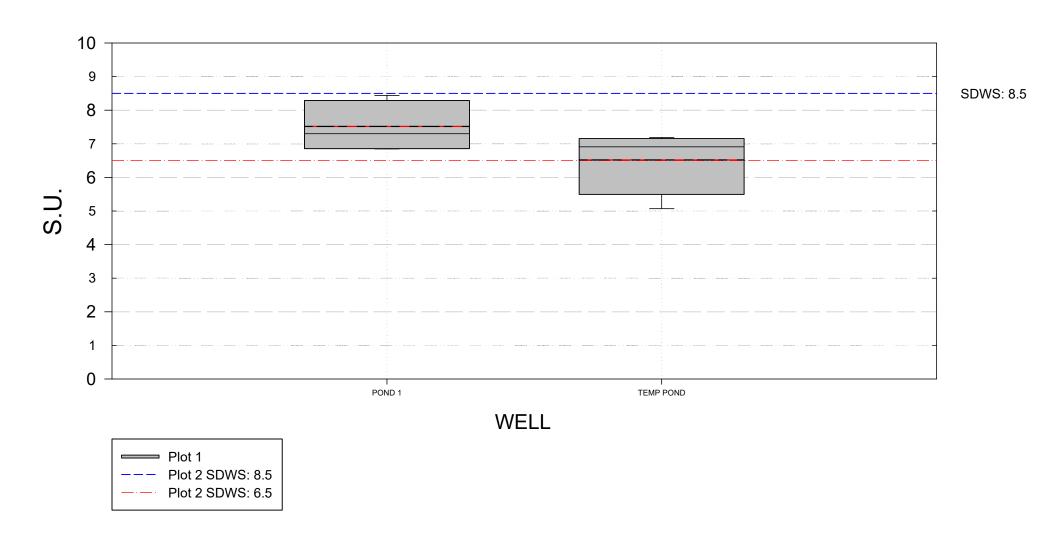


OXIDATION / REDUCTION POTENTIAL

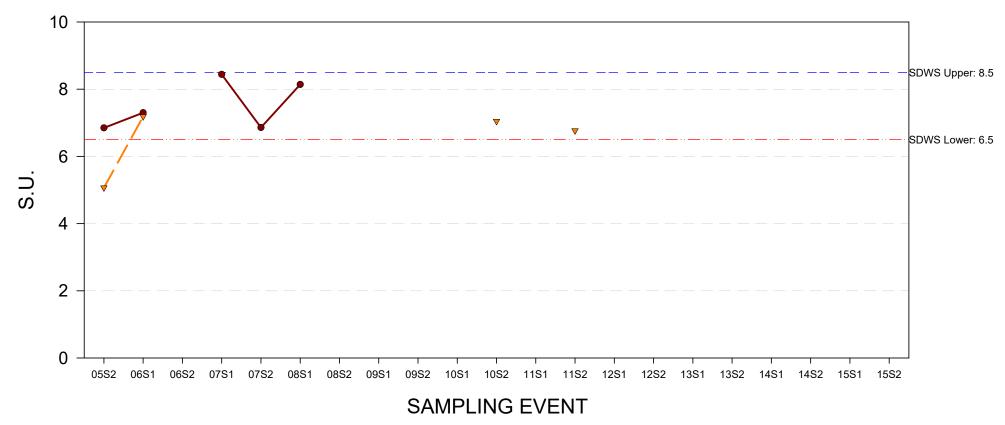




PH

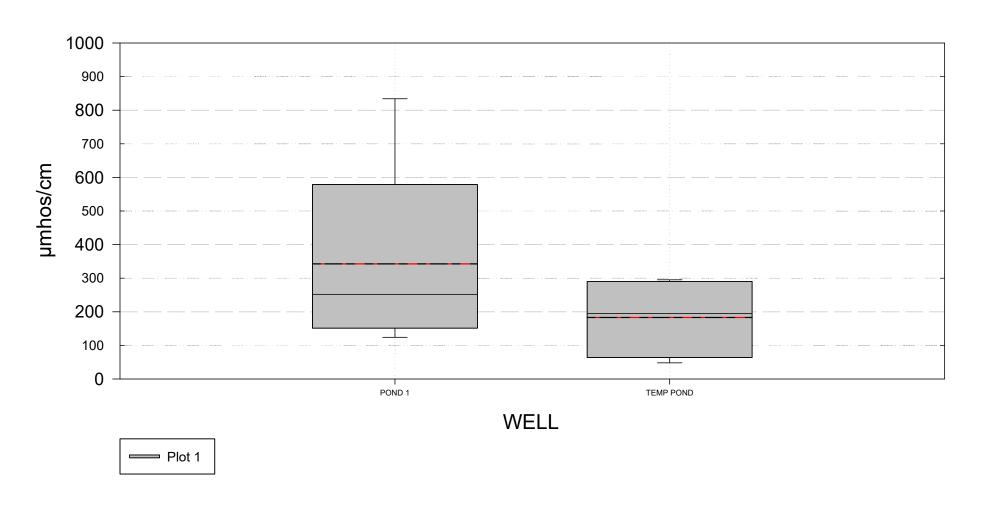


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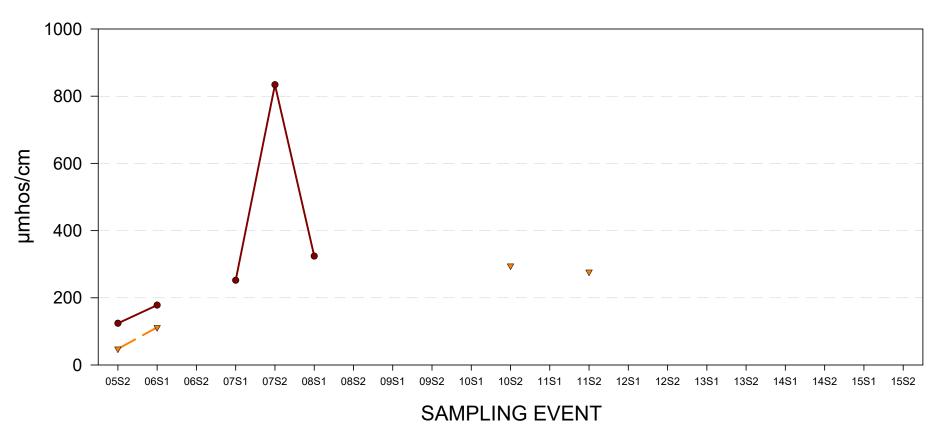




SPECIFIC CONDUCTANCE

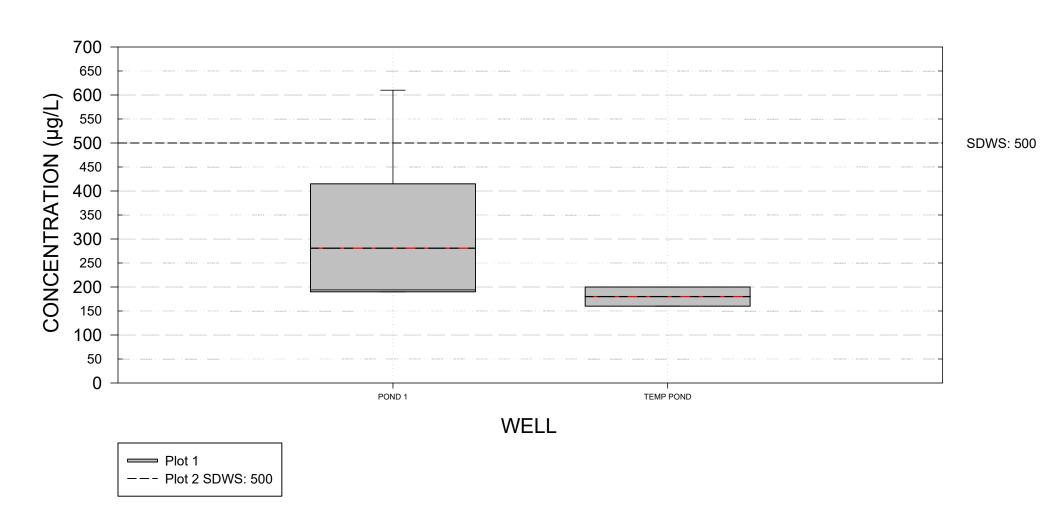


SPECIFIC CONDUCTANCE



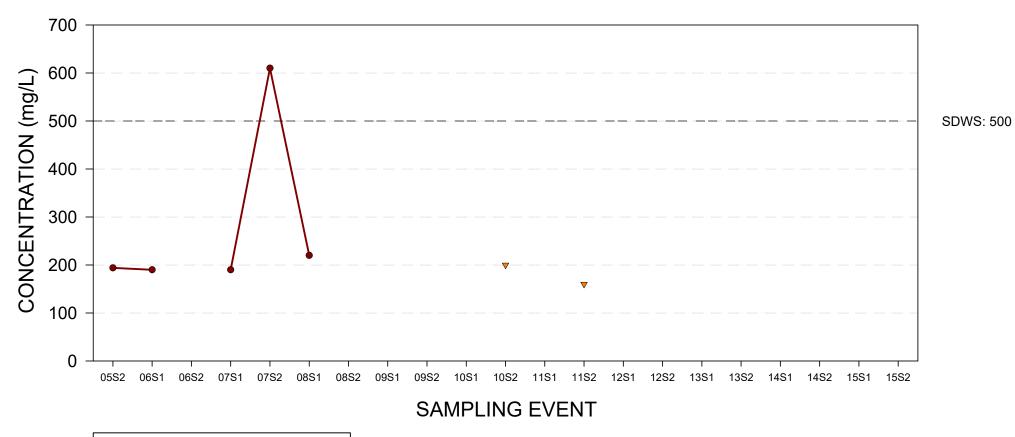


TOTAL DISSOLVED SOLIDS



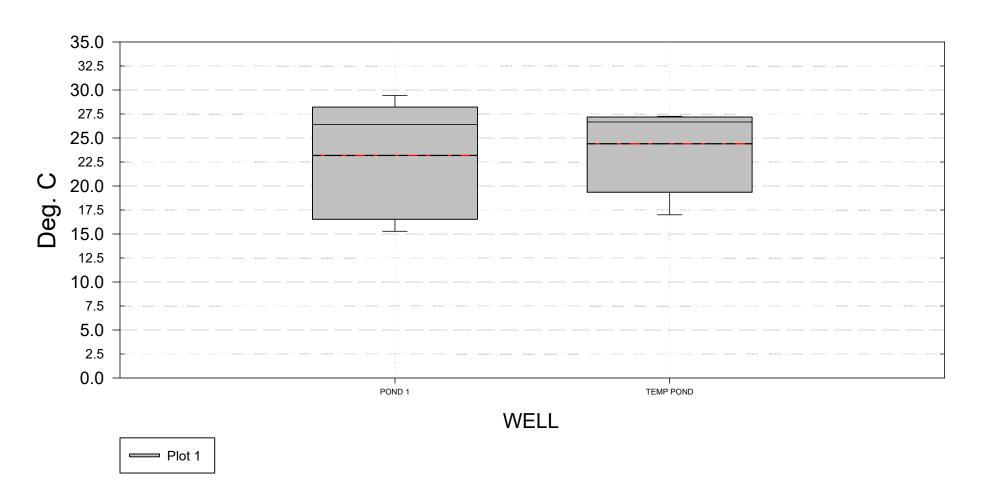
TOTAL DISSOLVED SOLIDS

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

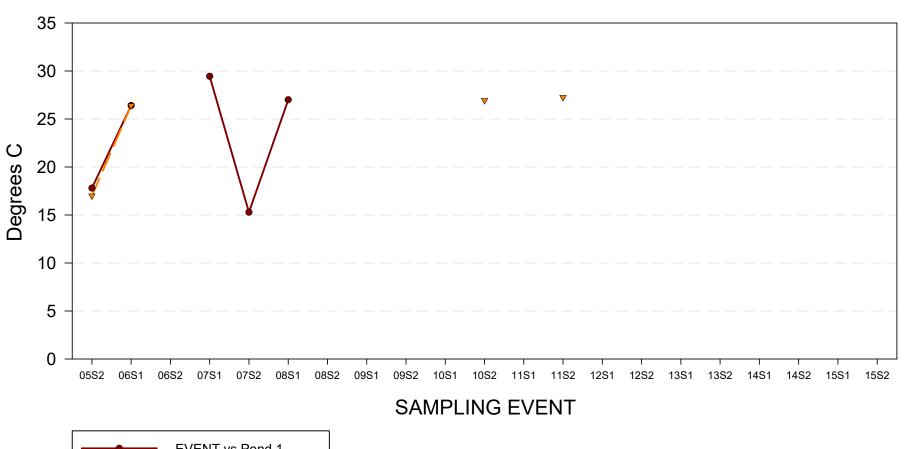


EVENT vs Pond 1
EVENT vs TEMP POND
Plot 1 SDWS: 500

TEMPERATURE

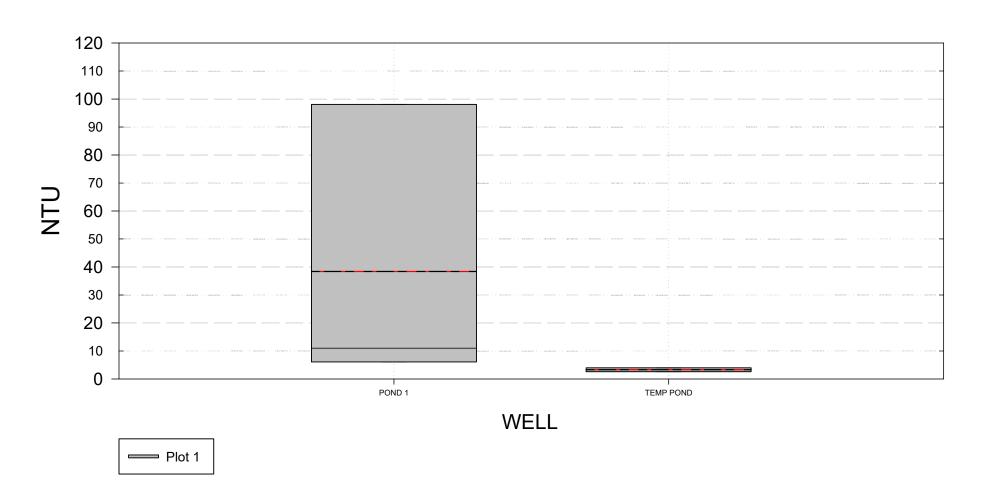


TEMPERATURE

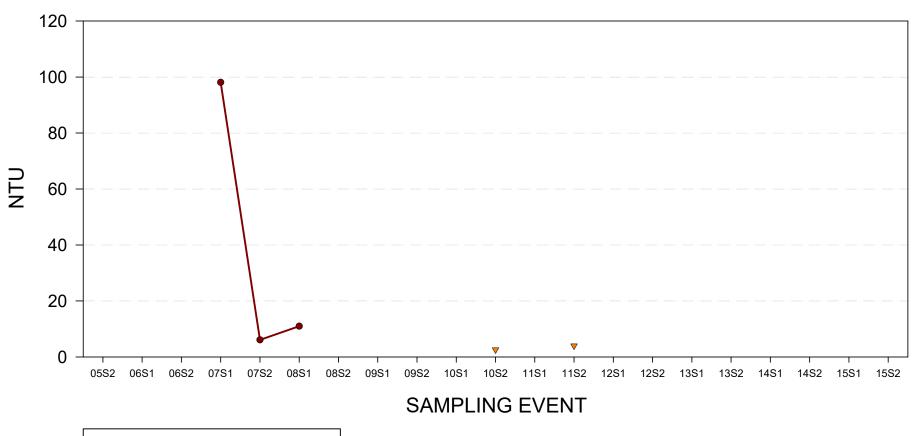




TURBIDITY

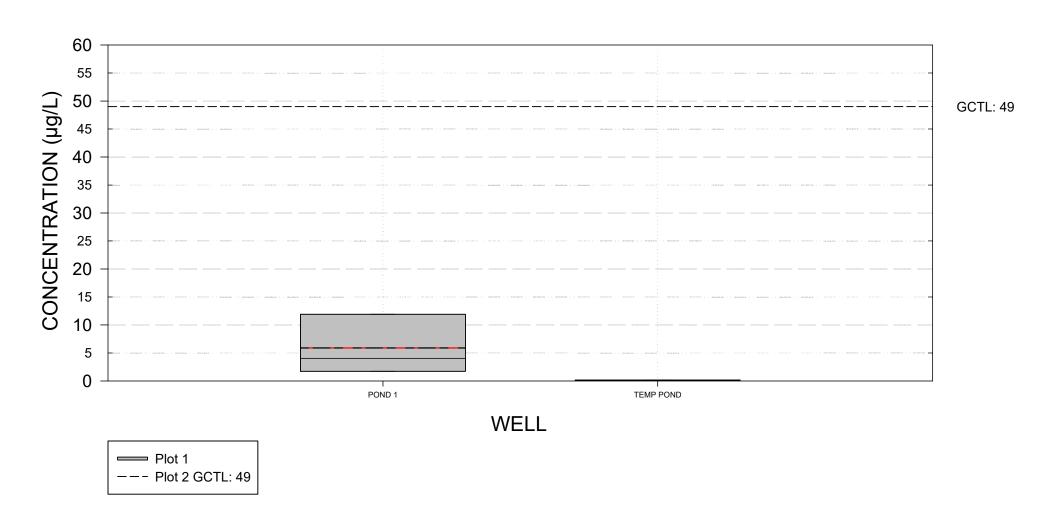


TURBIDITY



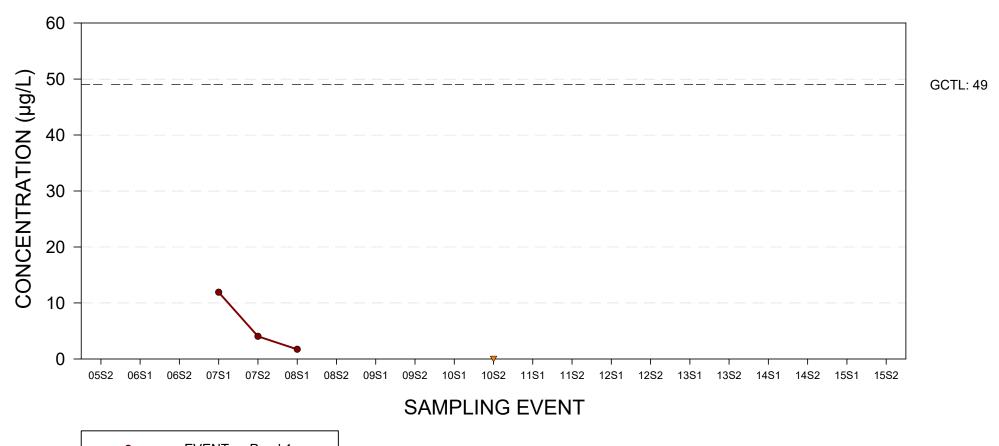


VANADIUM



VANADIUM

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

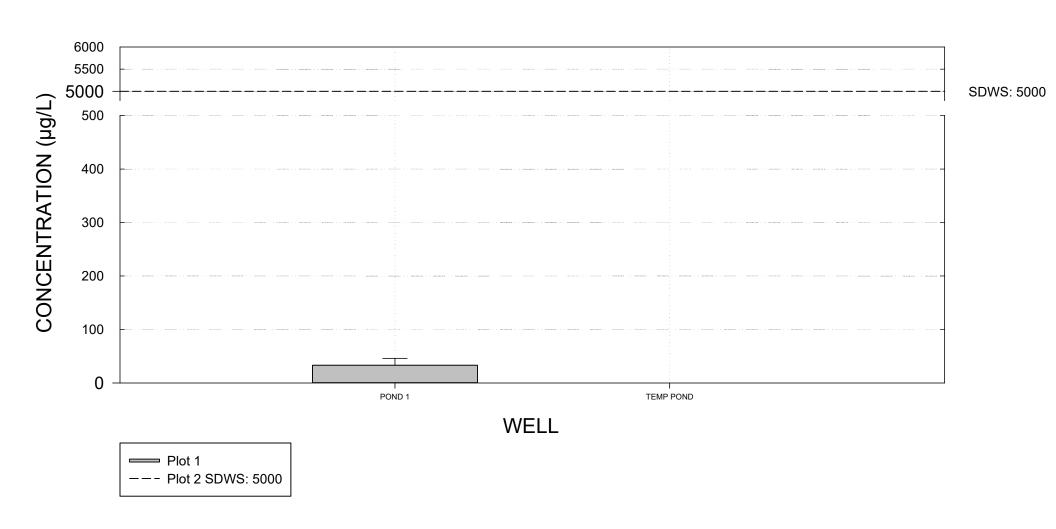


EVENT vs Pond 1

EVENT vs TEMP POND

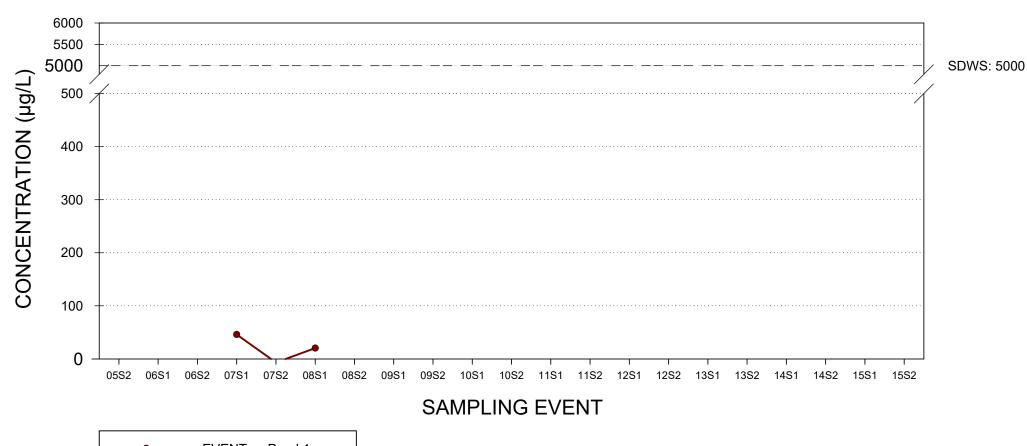
Plot 1 GCTL: 49

ZINC



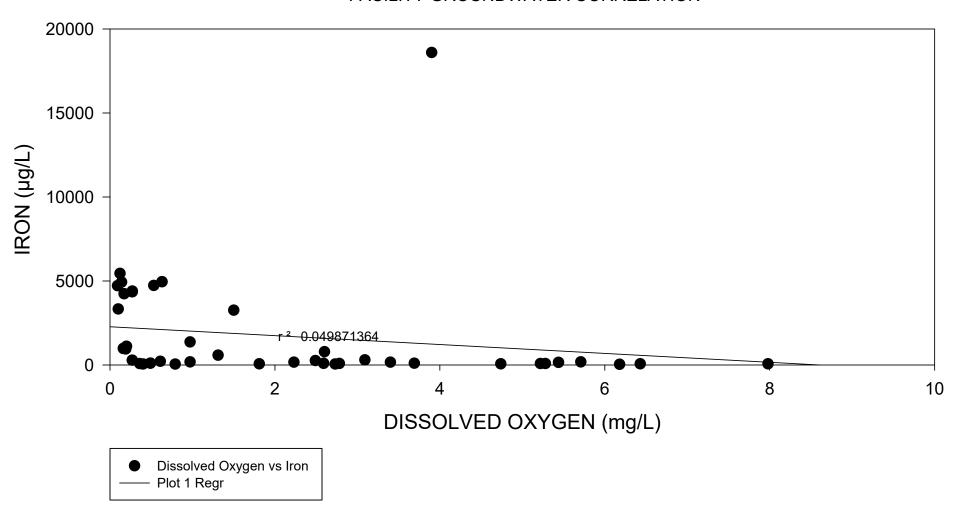
ZINC

ENTERPRISE ROAD CLASS III LANDFILL AND RECYCLING FACILITY SURFACE WATER CHEMISTRY GRAPH

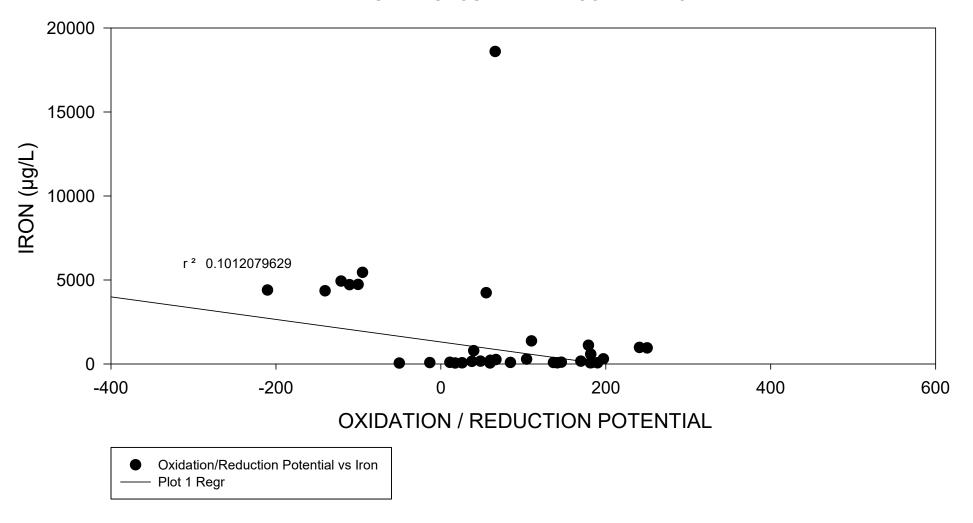


EVENT vs Pond 1
EVENT vs TEMP POND
Plot 1 SDWS: 5000

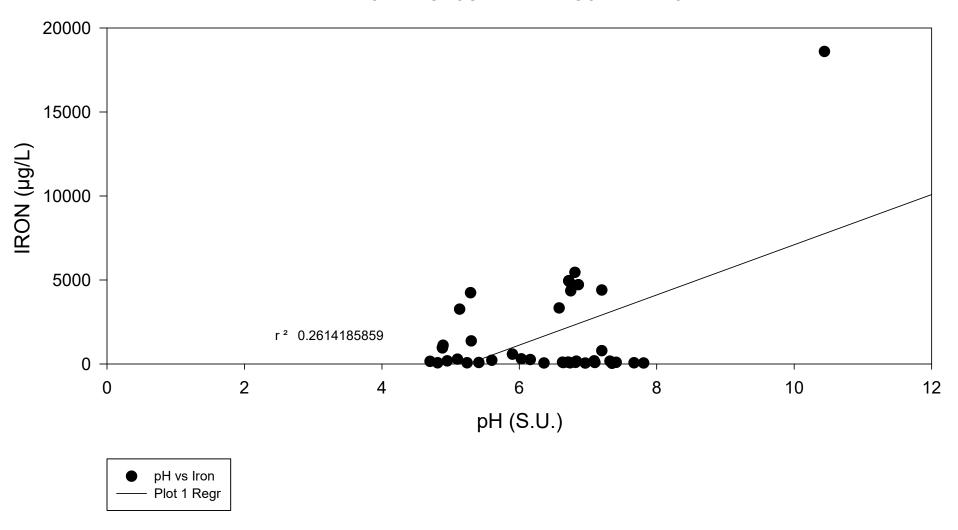
DISSOLVED OXYGEN VS IRON



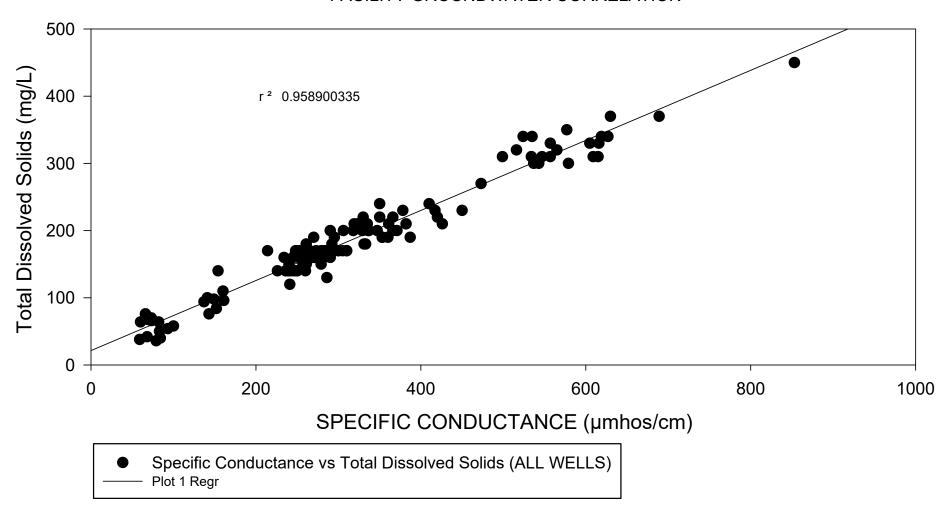
OXIDATION / REDUCTION POTENTIAL VS IRON



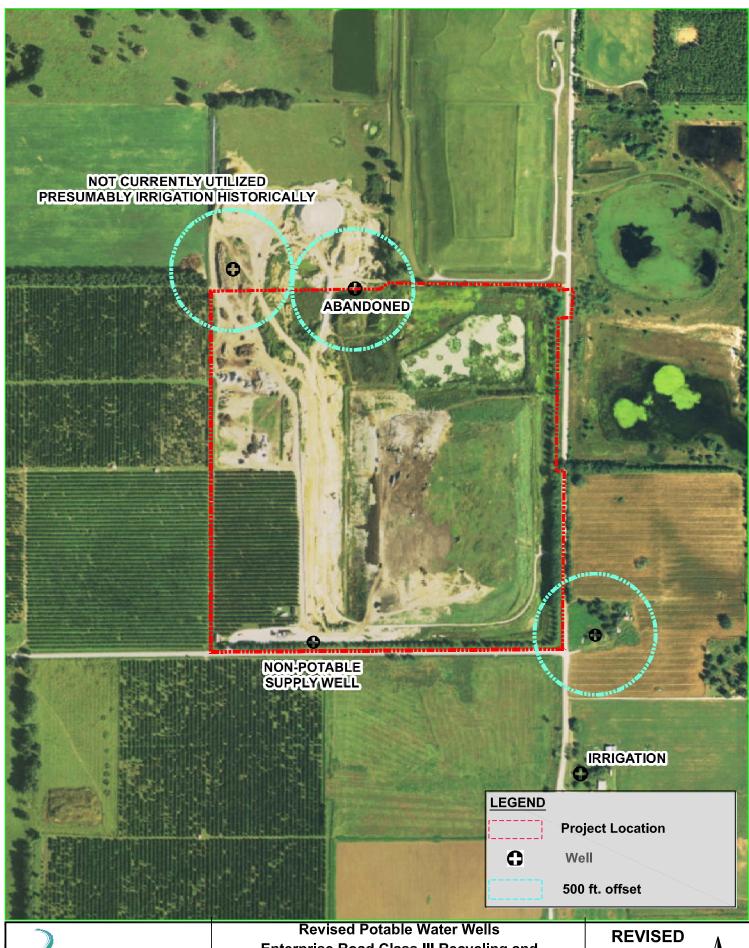
pH VS IRON



SPECIFIC CONDUCTANCE V TOTAL DISSOLVED SOLIDS



ATTACHMENT 3 POTABLE WELL SURVEY





Revised Potable Water Wells Enterprise Road Class III Recycling and Disposal Facility Permit Modification Dade City, Pasco County, Florida REVISED FIGURE



SOURCE: FDEP

PART I

I-1 Universal Engineering Sciences Report



UNIVERSAL ENGINEERING SCIENCES

GEOTECHNICAL EXPLORATION

Enterprise Class III Landfill Dade City, Florida

UES Project No. 0830.1500202

PREPARED FOR:

Angelo's Materials c/o Lockler & Associates 4140 NW 37th Place, Suite A Gainesville, FL 32606

PREPARED BY:

Universal Engineering Sciences 9802 Palm River Road Tampa, Florida 33619 (813) 740-8506

> January 29, 2016 (Revised May 31, 2016)



Consultants In: Geotechnical Engineering • Environmental Sciences Geophysical Services • Construction Materials Testing • Threshold Inspection Building Inspection • Plan Review • Building Code Administration

(Revised May 31, 2016)

January 29, 2016

Orlando (Headquarters) Palm Coast

Daytona Beach Fort Myers Fort Pierce Gainesville Jacksonville

- Miami Ocala
- Panama City
- Pensacola

LOCATIONS: Atlanta

- Rockledge
- Sarasota
- St. Petersburg
- Tampa Tifton
- West Palm Beach

Angelo's Materials c/o Lockler & Associates 4140 NW 37th Place, Suite A Gainesville, FL 32606

Attention:

John Locklear, P.E.

Reference:

Geotechnical Services/Documentation Review

Dade City Landfill, Cell 16

NWC of Ente rprise Rd. and Auton Rd. Dade City, Pasco County, Florida UES Project No. 0830.1500202 UES Report No. 1306524

Dear Mr. Locklear:

As requested Universal Engineering Sciences, Inc. (UES) has completed the review of documentation and field conditions related to the Permit Renewal Applications being prepared by Locklear & Associates, Inc. (L&A).

This report contains the results of our study, an engineering interpretation of the subsurface data obtained with respect to the project characteristics described to us, geotechnical design recommendations, and general construction and site preparation considerations.

We appreciate the opportunity to have worked with you on this project and look forward to a continued association with Angelo's Materials. Please do not hesitate to contact us if you should have any questions, or if we may further assist you as your plans proceed.

Respectfully submitted,

UNIVERSAL ENGINEERING SCIENCES, INC.

Certificate of Authorization No. 549

Dušan Jovanović

Senior Project Manager

Mark KEHardy

Regional Manager

Professional Engineer No

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1.0 INTRODUCTION

Universal Engineering Sciences, Inc. (UES) has completed the review of documentation and field conditions related to the permit modification application being prepared by Locklear & Associates, Inc. (L&A). We understand the permit modification involves the construction of a lateral expansion of the landfill north of existing Cell 15 into the area referred to as Cell 16. Furthermore, we understand the Department has requested a re-evaluation of the geotechnical conditions present in the area of Cell 16.

A general location map of the project area appears in Appendix A: Site Location Map. Also included in Appendix A for your reference are a Site Aerial Photographs, USGS Site Topographic Map and SCS Soil Survey Map.

2.0 DOCUMENT REVIEW

2.1 GENERAL

The following documents, provided to us by the applicant and L&A, were reviewed for this reevaluation report:

- January 19, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- February 11, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- February 18, 2004 Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E.
- March 30, 2004 (Revised July 15, 2004) Hartman & Associates, Inc (HAI) Correspondence to Ms. Susan Pelz, P.E. Grouting Completion Report
- Site Map, prepared by L&A with cell boundaries (existing and future) superimposed on it.
- January 6, 2011 letter from John Arnold, P.E. to Ms. Susan Pelz, P.E., subject: Enterprise Class III Landfill and Recycling Facility, Permit No.: 177982-007-SOfT3 & 177982-008-SCfT3, Response to January 5, 2011 email.
- October 2011 Enterprise Recycling and Disposal Facility Cell 6 Construction Completion Certification Report, prepared by John P. Arnold, P.E.
- December 7, 2011 letter from Steven Morgan to Mr. John Arnold, subject: Certification of Construction – Cell 6 Construction Enterprise Recycling and Disposal Facility, Permit No.: 177982-008-SCfT3, Pasco County, WACS No.: SWD/51/87895.



- March 2, 2012 letter from John Arnold, P.E. to Mr. Steve Morgan, subject: Enterprise Recycling and Disposal Facility, Cell 6 Construction Completion Report
 – RAI No. 1 Response, Angelo's Aggregate Materials, Ltd., FDEP Permit Nos. 177982-008-SCfT3 and 177982-007-SOfT3, WACS No.: 87895, Pasco County, Florida.
- March 26, 2012 letter from John Locklear, P.G. to John Morris, P.G., subject: Cell 6 Monitoring Well Installation, Enterprise Class III Landfill and Recycling Facility, Permit No. 177982-007-SOfT3, WACS No. 87895.
- April 24, 2012 letter from Steve Morgan to Mr. John Arnold subject: Certification of Construction – Cell 6 Construction Enterprise Recycling and Disposal Facility, Permit No.: 177982-008-SC/T3, Pasco County, WACS No.: SWD/51/87895.
- May 11, 2012 letter from John Arnold, P.E. to Mr. Steve Morgan subject: Enterprise Recycling and Disposal Facility Cell 6 Construction Completion Report – Response to RAI#2.
- June 2015 plan set from L&A compiling previous geotechnical boring data for the Cell 16 area.
- June 2015 plan set from L&A of geologic cross sections for the Cell 16 area.

In addition we revisited the following reports previously prepared by UES:

- Geotechnical Exploration, Proposed Dade City Class 111 Landfill, prepared for Hartman & Associates, Inc. (UES Project No. 80010-002-01), dated May 5, 2000.
- Geotechnical Exploration Update, Dade City Class III Landfill (UES Project No. 80010-002-01), prepared for Hartman & Associates, Inc. dated January 26, 2006.

2.2 GENERAL GEOLOGY

2.2.1 GEOLOGY

According to the Geologic Map of the State of Florida, 2001, the surficial deposits underlying the site and the general vicinity are classified as the Hawthorn Group (Th) of Miocene geologic age. The Hawthorn Group sediments are light olive gray and blue gray, poorly to moderately consolidated, clayey sands to silty clays.

The Oligocene Suwannee Limestone (Ts) generally lies below the Hawthorn Group sediments in the region. The Suwannee Limestone generally consists of a white to cream, poorly to well indurated, fossiliferous limestone. The upper portion of the limestone is highly variable due to paleo-weathering it is not uncommon for limestone to be found at relatively shallow depths (< 50 feet) or at depths greater than 100 feet below the land surface.



2.2.2 HYDROGEOLOGY

The Floridan aquifer is semi-confined in this area of Pasco County. The Floridan aquifer system consists of the Upper and Lower Floridan aquifers separated by the middle confining unit. The middle confining unit and the Lower Floridan aquifer in west-central Florida generally contain highly mineralized water. The water-bearing units containing fresh water are herein referred to as the Upper Floridan aquifer. The Upper Floridan aquifer is the principal source of water in the Southwest Florida Water Management District (SWFWMD) and is used for major public supply, domestic use, irrigation, and brackish water desalination in coastal communities (SWFWMD, 2000).

According to the Potentiometric Surface of the Upper Floridan Aquifer, West Central Florida, September 2008, groundwater flow is generally towards the west and depth to water is approximately 5 feet NGVD 1929

2.3 CELL 16 BORINGS AND GEOLOGIC CROSS SECTIONS

All geotechnical data collected within and immediately adjacent to the proposed Cell 16 lateral expansion area was compiled and reviewed. Sources of information included the following: (1) mining exploration borings performed prior to 2000; (2) borings performed during initial 1999/2000 geotechnical investigation; (3) borings performed as part of the 2004 subsidence remediation; (4) borings performed in conjunction with groundwater monitoring well installations. Because many of these borings were performed prior to mining and landfilling activities, the site land surface has changed significantly. As a result, the original borings include lithology which is no longer present. In order to update this information and provide a more accurate representation of what actually exists in the area, each boring log was reviewed relative to the current topographic elevation. In locations where natural material has been removed (either from mining or landfilling activities), the log has been revised to remove the portions of the column which no longer exist. Copies of the revised boring logs are provided in Appendix B. Also, geologic cross sections were generated with the boring log data and are provided in Appendix B. The cross sections also include the existing and proposed clay liner and cell boundaries to assist in visualizing the proposed expansion concept.

A total of 51 borings have been performed in the Cell 16 area and vicinity. The majority of the borings were performed as Standard Penetration Test Borings and include the required blow count and N values. N values are shown on the boring logs provided in Appendix B. It should be noted that the boring logs were prepared by different people and the lithologic descriptions are variable.

Geologic Cross Section A-A'

Cross section A-A' extends north to south through the approximate center of the Cell 16 area. The northern extent (A) begins with boring SSA-29 approximately 50 feet south of the northern cell boundary. The section ends with boring DCL01-12 located in the southern portion of Cell 15. Boring SSA-29 was completed to a depth of 55 feet, NGVD. The geology encountered consisted of silty sands and silty clays. Progressing south along the section the next boring is



B-32, which was completed to a depth of 35 feet, NGVD. The geology encountered consisted of alternating layers of silty sands to sandy clays until limestone was observed at an elevation of 36 feet, NGVD. The next two borings, B-26 and B-22, show deeper silty sands underlain by silty to sandy clays. Limestone was not encountered in either of the borings which terminated at elevations of 15 and 30 feet, NGVD, respectively. The two southernmost borings, DCL01-13 and DCL01-12, were completed within the existing Cell 15 footprint. Sandy clays were observed in both borings, with limestone encountered at an elevation of 65 feet, NGVD in DCL01-13.

N-values for the borings comprising cross section A-A' are provided in Appendix B. Of the six borings, all but SSA-29 included SPT data. N-values for B-22 ranged from 7 to 58. N-values for B-26 and B-32 ranged from 3 to 12 and 10 to 23, respectively. N-values for DCL01-12 and DCL01-13 ranged from 2 to 18 and 2 to 9, respectively. Note that discussions of N-values include values for those intervals that still remain in place. Therefore, the range discussed herein may be different than the full range displayed on the original boring logs.

Geologic Cross Section B-B'

Cross section B-B' extends from the southwest corner to the northeast corner of the Cell 16 area. The southwestern extent of the section begins with boring L-14 located within the Cell 1 footprint. The section ends in the northeastern corner of the proposed Cell 16 footprint with boring B-21. Borings L-14 and SSA-25 were both completed to depths of 65 feet, NGVD. The lithology described for both borings consists of sandy clays. As we move north in the proposed Cell 16 footprint, boring B-23 shows interbedded clayey sand, sandy clays and clays to a depth of 55 feet, NGVD. Borings B-33 and B-31 were completed to depths of 43 and 40 feet, NGVD, respectively. Both columns show similar interbedded clayey sands, sandy clays and clays. Boring B-33 shows a limestone marl underlain by limestone beginning at an elevation of 47 feet, NGVD. The limestone marl is seen at the same elevation in B-31 but is underlain by clayey sand rather than limestone. The section terminates with boring B-21 which was completed to a depth of 55 feet, NGVD. This column shows interbedded clayey sands and silty clays with a thin limestone marl layer from 64 to 61 feet, NGVD.

N-values for the borings comprising cross section B-B' are provided in Appendix B. Of the six borings, B-21, B-23, B-31 and B-33 included SPT data. N-values for B-21 ranged from 4 to 9. N-values for B-23 ranged from 5 to 19. N-values for B-31 ranged from 8 to 18. N-values for B-33 ranged from 3 (at the limestone contact) to 33. It is very common to observe lower blow counts and N-values at the contact between two differing lithologic units.

Geologic Cross Section C-C'

Cross section C-C' extends from the northwest corner to the southeast corner of the Cell 16 area. The section begins with boring B-34 in the northwest corner of the proposed Cell 16 footprint and extends to MW-6 just outside of the southeastern corner of Cell 16. Boring B-34 was completed to a depth of 50 feet, NGVD and consists of silty sand overlying interbedded clayey sand, silty clay and sandy clay. Boring SSA-26 was completed to a depth of 55 feet, NGVD. It consists of silty to clayey sands overlying silty clay. The upper portion of boring B-32 shows similar lithology to SSA-26 which is then underlain by more sandy clay and clayey sands



and ultimately limestone at a depth of 36 feet, NGVD. Boring B-31 shows a very similar column to that of B-32, though a thin limestone marl layer is encountered at approximately 47 feet, NGVD. SSA-30 is the last boring located within the Cell 16 footprint. SSA-30 was completed to a depth of 55 feet, NGVD. The column consists of silty clay underlain by a thin clayey sand layer and then silty clay with limestone fragments. Limestone was encountered at an elevation of 56 feet, NGVD. The boring performed during construction of monitoring well MW-6B represents the southern extent of the section. The boring was completed to a depth of 30 feet, NGVD. The column consists of sandy clay to clay underlain by limestone starting at an elevation of 55 feet, NGVD.

N-values for the borings comprising cross section C-C' are provided in Appendix B. Of the six borings, B-21, B-23, B-31 and B-33 included SPT data. N-values for B-21 ranged from 4 to 9. N-values for B-23 ranged from 5 to 19. N-values for B-31 ranged from 8 to 18. N-values for B-33 ranged from 3 (at the limestone contact) to 33. It is very common to observe lower blow counts and N-values at the contact between two differing lithologic units.

Geologic Cross Section D-D'

A geologic cross section (D-D') running north to south through the southeastern corner of Cell 16 is provided in Appendix B. The northern extent of the section is represented by boring B-42 and the southern extent by boring B-39. Boring B-42 was completed to a depth of 55 feet, NGVD. The column consists of sandy clay underlain by clay to clayey sand limestone marl at an elevation of 60 feet, NGVD. Boring B-41 shows sandy clay overlying limestone marl, followed by limestone at an elevation of 57 feet, NGVD. Borings B-40, B-36 and B-35 show a similar sequence though B-35 was completed deeper than the other borings (40 versus 57 feet, NGVD). Boring B-39 shows a slightly thinner layer of sandy clay underlain by limestone at an elevation of 70 feet, NGVD.

N-values for the borings comprising cross section D-D' are provided in Appendix B. All six borings included SPT data. N-values for B-42 ranged from 9 to 23. N-values for B-41 ranged from 7 to 36. N-values for B-40 ranged from 3 to refusal. N-values for B-36 ranged from 8 to refusal. N-values for B-35 ranged from 1 (at the limestone contact which is common) to 21. Boring B-39 N-values ranged from 9 to 36.

Geologic Summary

Collectively, the SPT borings show dense to very dense sediments and indicate no significant signs of active sinkholes, such as raveling soils, voids and large areas of soft soils. There is evidence of the typical loss of circulation at the soil-limestone interface at depth, and a few one to two foot thick layers of soft sediments (one to three blow counts). However, in all borings dense to very dense sediments have surrounded these softer soil layers in a stable setting.

The low blow count and even weight-of-rod/hammer strength material near the top of the limestone is a normal occurrence associated with the ancient weathering or erosional features of the epikarst. Epikarst is the zone of weathering at the upper surface of a limestone stratum. Weathering of limestone results in development of rubble, fine-grained carbonate-rich silt and clay, karren (including pinnacles and valleys in the limestone rock surface), and other features.



Epikarst is frequently associated with losses of drilling fluid circulation, low blow counts, weight of rod or hammer events, and recovery of gravel-sized particles of rock. The epikarst can occur at the land surface or be buried under later sediments. Raveling of soil or sediments into the voids within the epikarst formation can lead to sinkhole activity, but in most cases there is no evidence of on-going or contemporaneous raveling and the epikarst is not synonymous with sinkhole activity.

2.4 EVALUATION OF 2004 SUBSIDENCE FEATURE

In 2004, a small (12 feet in diameter) subsidence feature was observed by Hartman & Associates, Inc. (HAI) in the southeastern portion of the Cell 16 area. The area was investigated through the advancement of additional SPT borings.

The feature was subsequently remediated through grouting. The purpose of the grouting program was to seal the upper limestone zones and compact, fill and improve loose soil conditions encountered at this location. The grouting operation was conducted using present industry standards.

The remediation included 26 grout injection points. The casing depths of the injection points generally ranged from 25 to 45 feet below land surface (bls), with the exception of injection point 26 which extended to 60 feet, bls. The higher quantities of grout were generally injected in the points with deeper casing depths. The largest quantity of grout was injected in point 26. The initial grout take within the lower portion of this grout injection point, at depths between 60 and 42 feet, was relatively large per foot of depth. The grout take was significantly less per linear foot within the upper portion of this grout injection point with much higher line pressures. Based on the above observation we believe the upper limestone zone was sealed and the cavity was filled with low slump grout.

For the remaining grout injection points the njection pressures were generally higher at shallow depths.

A copy of Grouting Completion Report as presented to Department of Environmental Protection by Hartman & Associates in 2004 is attached.

Since completion of the grouting remediation, the entire area around the feature has been hydraulically loaded by the temporary stormwater pond. The feature has been stable for more than 10 years under conditions which are considered conducive to the formation of subsidence features.

3.0 CONCLUSIONS

As a result of our review process we concluded the following:

 Both reports issued by UES conform to the requirements of the Florida Administrative Code including the assessment of potential for sinkhole occurrence presented in our May 5, 2000 report.



- O UES report Geotechnical Exploration Update, dated January 25, 2006 was a result of the proposed change in the landfill geometry (fill thickness and change in slopes) and questions raised by FDEP. The report provided analysis and conclusions related to the soil bearing capacity and total settlement of foundation soils, slope stability analysis and potential for sinkhole occurrence related to loss of circulation (LOC) events at the time of our geotechnical exploration.
- No additional information presented in the documentation provided to us warranted any changes, revisions or additions to analysis and/or conclusions and recommendations presented in our reports.

Generally our conclusions can be summarized as:

- This report confirms the conclusion drawn in previous geotechnical site investigations and that the site meets geotechnical requirements of Rule 62-701.410 F.A.C.
- Sinkhole risk in the proposed disposal footprint is low. This conclusion is particularly applicable to the temporary retention pond area (Cell 15 and Cell 16) based on ten years of monitoring under conditions which are considered conducive to the formation of subsidence features.
- Placement of three feet of clay layer in the proposed fill areas including Cell #16 is adequate to meet the geotechnical requirements for the site.

We also performed a site visit on June 10, 2014 accompanied by Mr. John Arnold. The area of the former subsidence received a clay liner and was used as a temporary stormwater pond. Based on the site reconnaissance and information provided by Mr. Arnold no ground subsidence or indications of surficial expressions of sinkhole activity were observed within the temporary stormwater pond (future Cell 14 and 16) or anywhere at the site.

4.0 LIMITATIONS

During the early stages of most construction projects, geotechnical issues not addressed in this report may arise. Because of the natural limitations inherent in working with the subsurface, it is not possible for a geotechnical engineer to predict and address all possible subsurface variations. An Association of Engineering Firms Practicing in the Geosciences (ASFE) publication, "Important Information About Your Geotechnical Engineering Report" appears in Appendix C, and will help explain the nature of geotechnical issues. Further, we present documents in Appendix C: Constraints and Restrictions, to bring to your attention the potential concerns and the basic limitations of a typical geotechnical report.

Do not apply any of this report's conclusions or recommendations if the nature, design, or location of the facilities is changed. If changes are contemplated, UES must review them to



Angelo's Materials UES Project No. 0830.1500202. January 29, 2016, (Revised May 31, 2016) Page 8

assess their impact on this report's applicability. Also, note that UES is not responsible for any claims, damages, or liability associated with any other party's interpretation of this report's subsurface data or reuse of this report's subsurface data or engineering analyses without the express written authorization of UES.

* * * * * * * * *



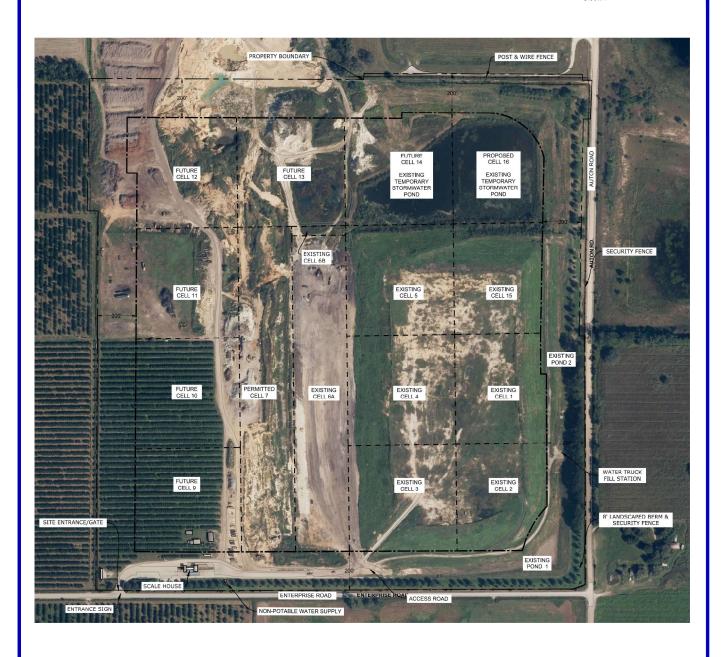
APPENDIX A

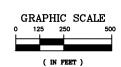




SITE LOCATION MAP				
CLIENT: ANGELO'S MATERIALS	DRAWN BY: SB DATE: AUG 10, 2015	j		
SCALE: NOT TO SCALE PROJECT NO: 0830.1500202	REVIEWED BY: SS APPENDIX: A			



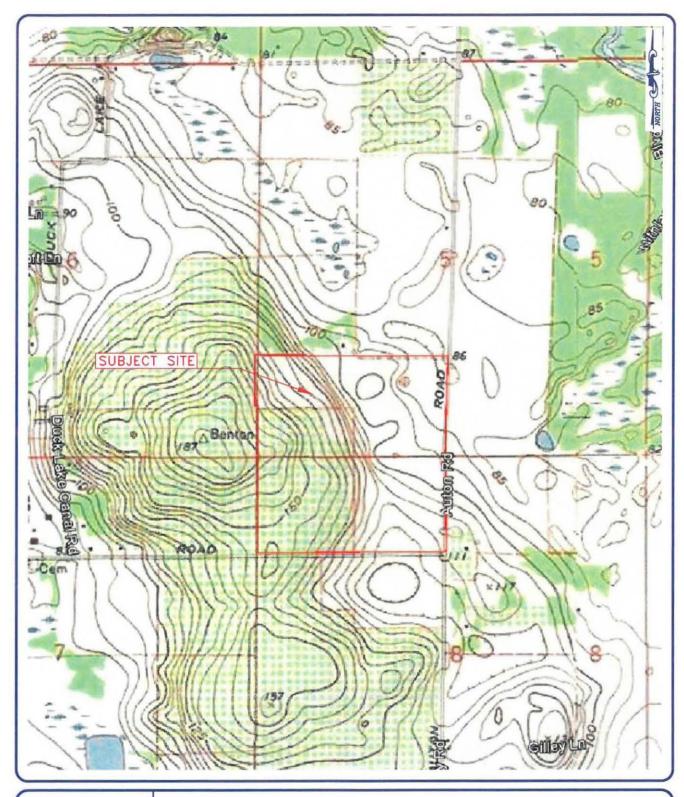






SITE AERIAL PHOTOGRAPH

CLIENT: ANGELO'S MATERIA	ALS	DRAWN BY: SB	DATE: MAY 6, 2016
SCALE: 1" = 500'	PROJECT NO: 0830.1500202	REVIEWED BY: SS	APPENDIX: A





	SITE TOPOG	RAPHIC MAP	
CLIENT: ANGELO'S MATER	ALS	DRAWN BY: SB	DATE: AUG 10, 2015
SCALE: NOT TO SCALE	PROJECT NO: 0830.1500202	REVIEWED BY: SS	APPENDIX: A

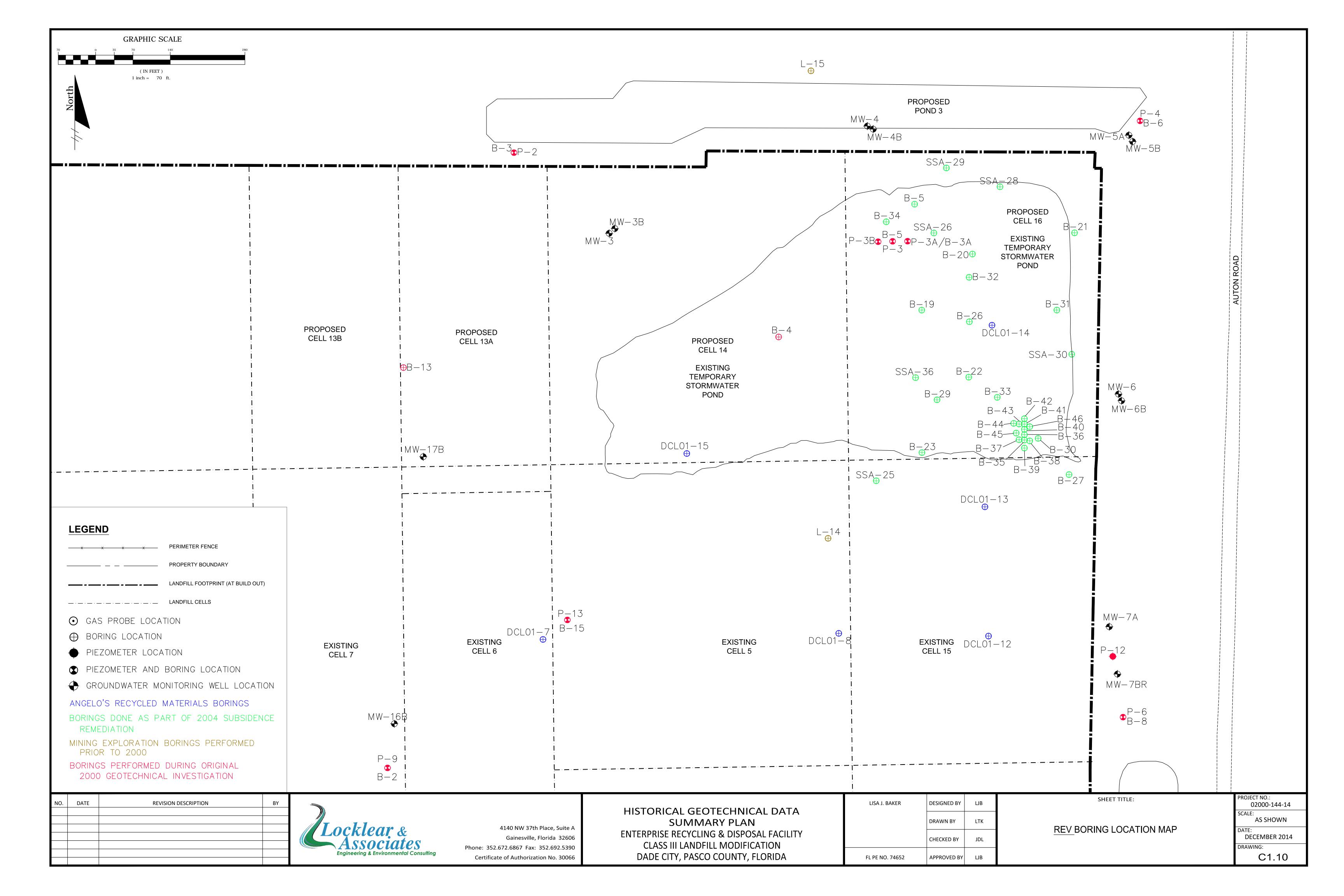


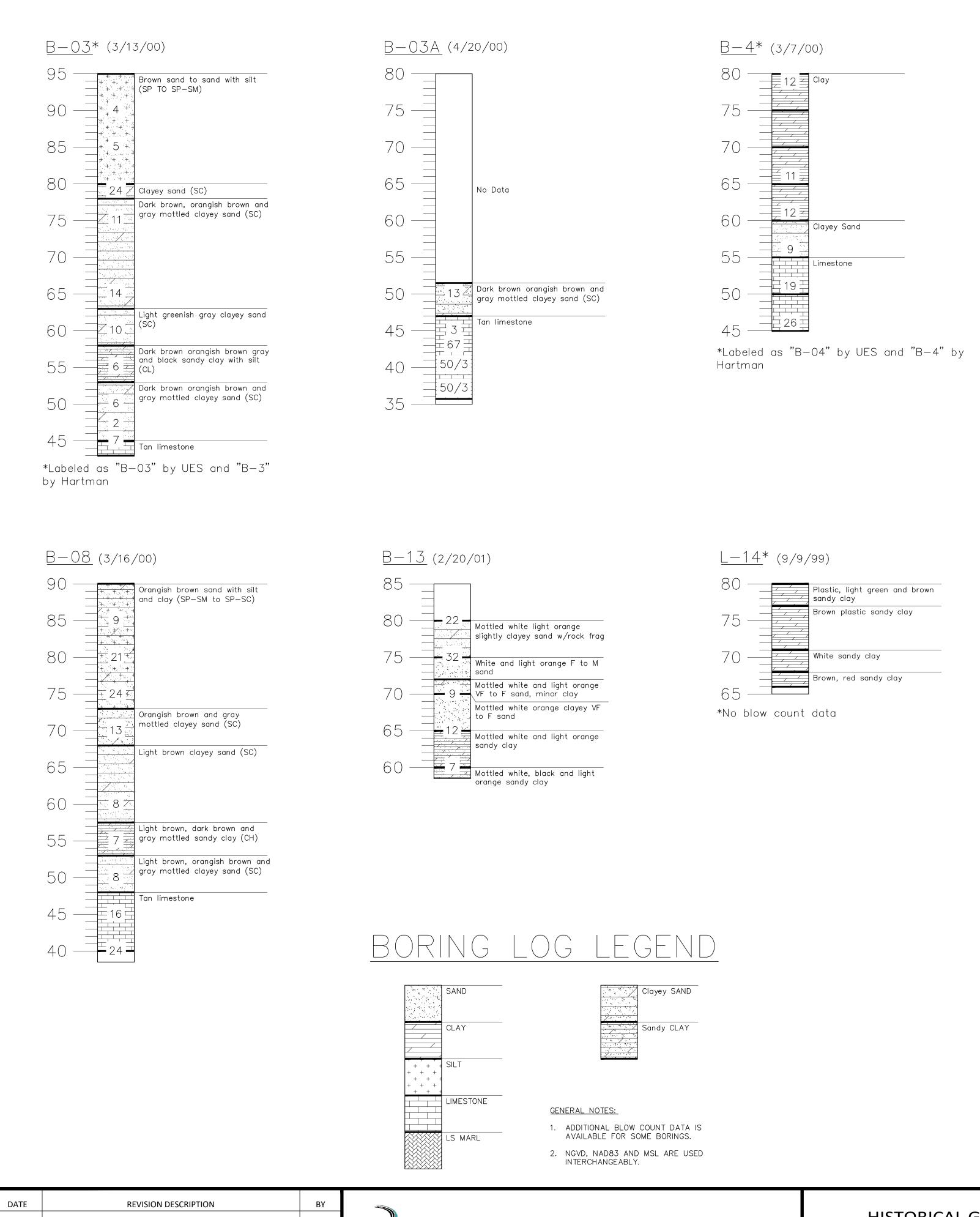


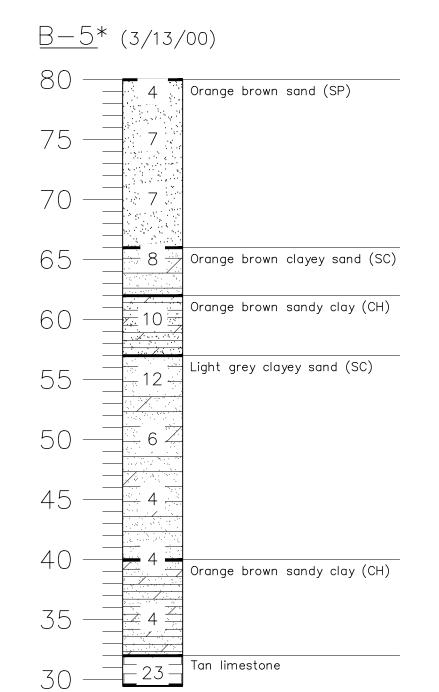
SCS SOIL SURVEY MAP

CLIENT: ANGELO'S MATERIALS			DRAWN BY: SB		DATE:	AUG 10, 20	115	
SCALE:	NOT TO SCALE	PROJECT NO:	0830.1500202	REVIEWED BY:	ss	APPENDIX:	Α	

APPENDIX B







by Hartman **Ground elevation listed as 77' MSL on

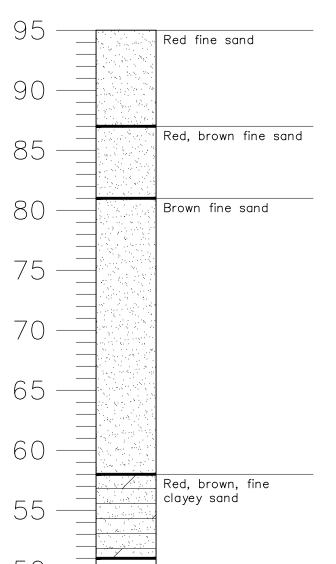
*Labeled as "B-05" by UES and "B-5"

boring log, however based on elevations of surrounding borings performed during the same time frame an elevation of 95' MSL was used.

B - 06 (3/15/00)

		Light brown sand (SP)
80 -		
		Light brown dayly brown and
¬ _	+ 7 +	Light brown, dark brown and gray mottled sand with silt
75 -	+ / _ +	(SP-SM)
70 -	14	
7 0		Light brown, dark brown and gray mottled sandy clay (CH)
		Light brown, dark brown and
65 -		gray mottled clayey sand (SC)
	16	Gray and dark brown mottled
\sim		sandy clay (CH)
60 -		
55 -	8	
00		
		Light brown, dark brown and
50 -	5	gray mottled clayey sand (SC)
	t. Val. 14 14 14 1	Gray sand with silt (SP—SM)
15	+ + +	ordy same with sire (Si Sim)
45 -	+ + + + + + + + + + + + + + + + + + + +	
	7	Brown, yellowish brown and gray
40 -	27 🚆	mottled sandy clay (CL)
. •		
7 _		Light brown orangish brown and white sandy clay (CH)
35 -	13	
	50 /2	
30 -	50/2	
\mathcal{O}		

<u>L-15</u> (9/9/99)



B-15 (2/21/01)

	<u>)</u> (2/21/	01)
85 -		1
80 -	- 21 	
		Orange V fine sand, minor black mottled slightly silty
7 =	+ + + +	
75 –	19	Orange brown F-VF sand
70 -	15/3.	Orange light brown sand with
		rock fragment
65 -	13 -	Ossara kaswa E asad
		Orange brown F sand
60 -		
00		Orange to brownish VF-F sand with black fragments
Γ		
55 –	34 -	Orange to light brown VF-M
		sand with minor clay rock fragments
50 -	34 =	Orange to light brown VF—F
		sand
45 -	59	Light brown to rusty F sand
		Light brown to rusty i saila
40 -		
+0		
7 E	<u> </u>	
35 –	+ + +	Orange to dark brown F sand, slightly silty
- 0	+ · · · · · · · · · · · · · · · · · · ·	Singificity Sincy
30 -	50/3	
25 -	73 + 73	Orange F—VF sand with minor
		clay materials
20 -	65	Orango to light has well 1/5 1/
	# (Orange to light brown VF-V sand, slightly silty
15 -		Orange to light brown V sand, slightly silty
1)	*************************************	30. my - 11. y
1 (# # # # # # # # # # # # # # # # # # #	
10 –	4	Orange F—VF sand slightly silty and minor clay
_		and minor ordy
5 –	12 ***	Dark brown VF sand slightly
	**************************************	silty, minor clay
0 -	15 🛨	Brownish to light VF sand,
	#	slightly silty
<u>-5</u> -	7	Slightly eilty VE E agad black
-	* + * + * + * + * + * + * + * + * + * +	Slightly silty, VF—F sand, black pigment of minor clay
10	+ 33 +	
ı O		Light to gray VF to M sand with black pigment of rock
1 🗔	= 50/3	fragments
	E . 11 1 1 1	

Gray to white F-VF sand well

Light brown VF to F sand, well

Gray to light brown VF to F sand, well rounded, sorted

Gray sandy clay, slightly silty,

sorted, slightly silty

Gray to white sandy clay,

slightly silty

Dark gray clay

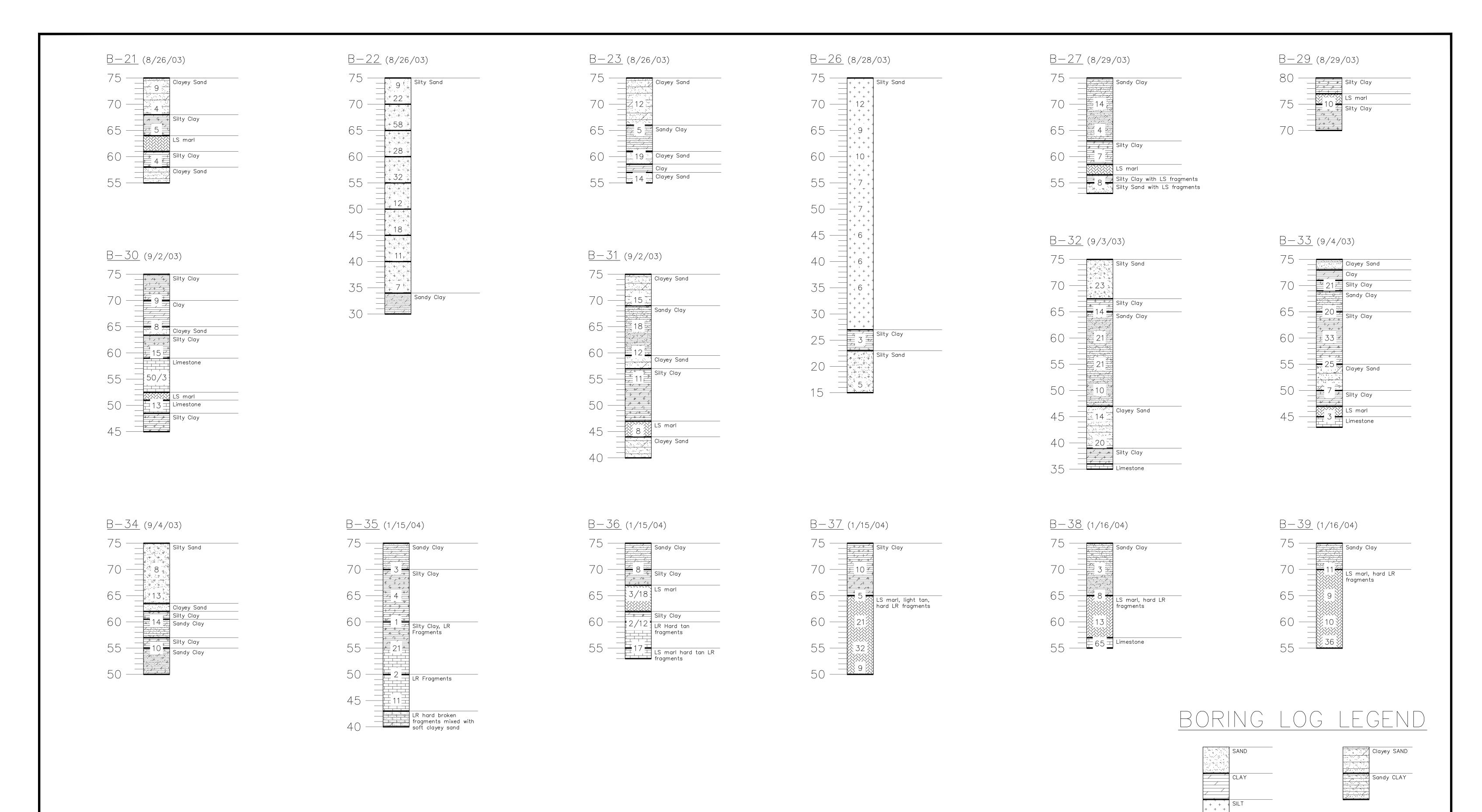
Locklear & Associates
ASSOCIATES Engineering & Environmental Consulting

4140 NW 37th Place, Suite A Gainesville, Florida 32606 Phone: 352.672.6867 Fax: 352.692.5390 Certificate of Authorization No. 30066

HISTORICAL GEOTECHNICAL DATA SUMMARY PLAN ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LTK
	CHECKED BY	JDL
FL PE NO. 74652	APPROVED BY	LJB

SHEET TITLE: 02000-144-14 **AS SHOWN BORING LOGS** DECEMBER 2014 DRAWING: C1.11



NO.	DATE	REVISION DESCRIPTION	ВҮ



4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

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FL PE NO. 74652	APPROVED BY	LJB

BORING LOGS

GENERAL NOTES:

 ADDITIONAL BLOW COUNT DATA IS AVAILABLE FOR SOME BORINGS.

2. NGVD, NAD83 AND MSL ARE USED INTERCHANGEABLY.

LIMESTONE

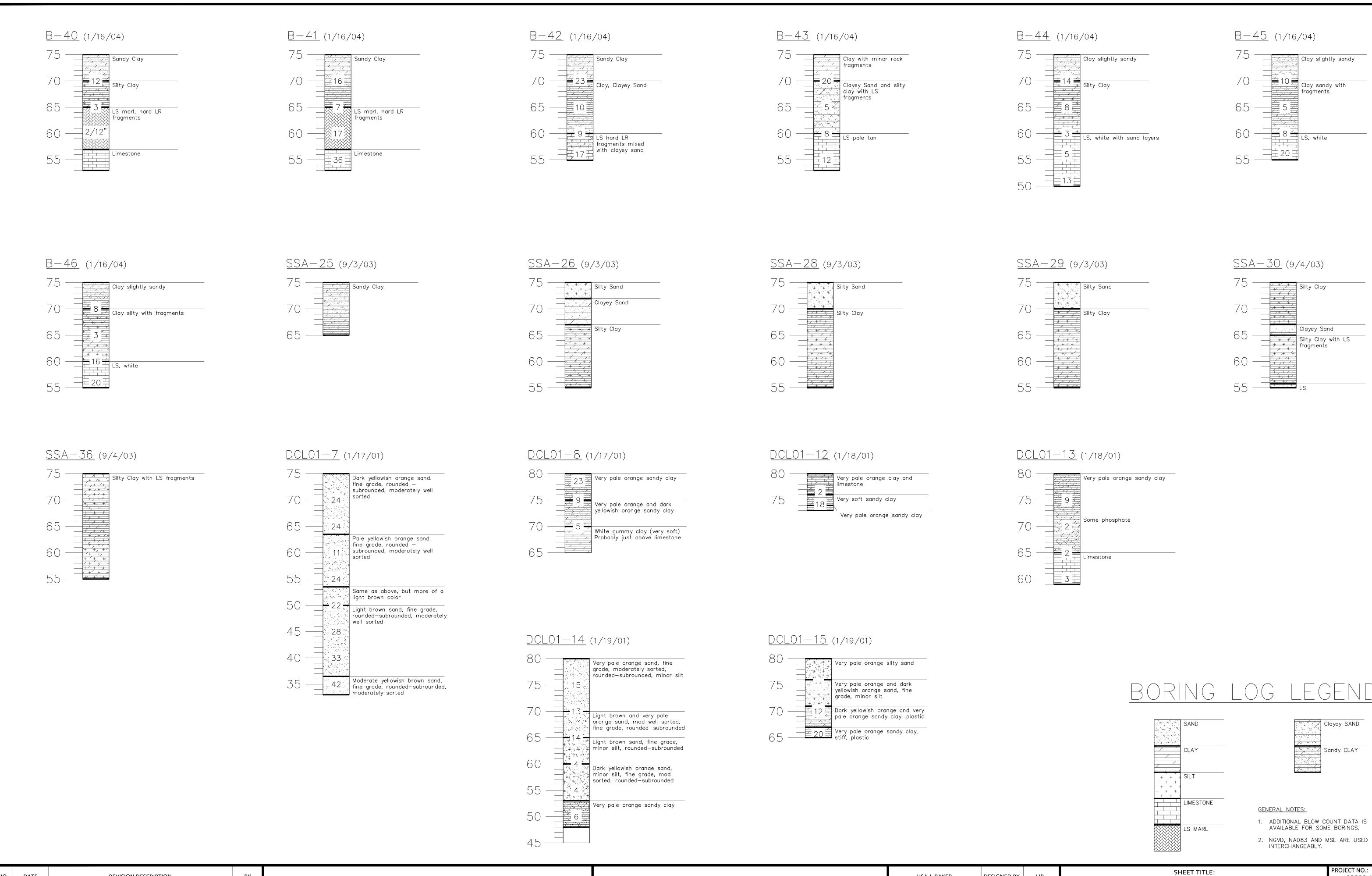
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PROJECT NO.:
02000-144-14

SCALE:
AS SHOWN

DATE:
DECEMBER 2014

DRAWING:
C1.12



NO.	DATE	REVISION DESCRIPTION	BY	



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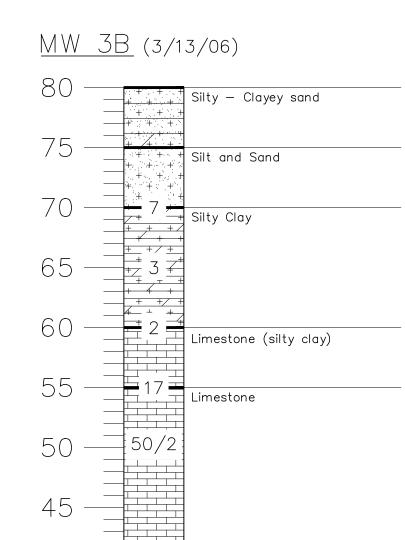
HISTORICAL GEOTECHNICAL DATA SUMMARY PLAN ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

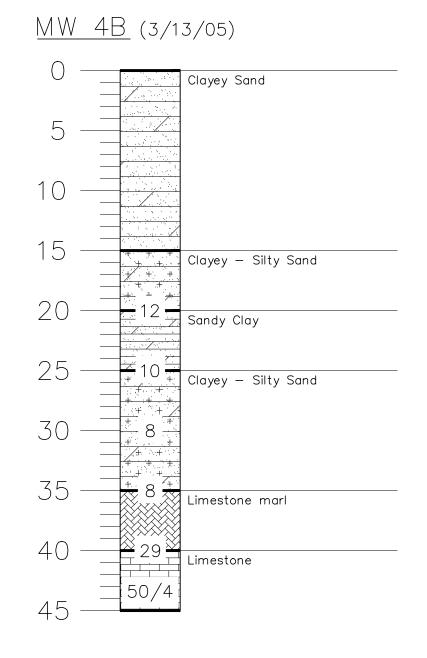
LISA J. BAKER	DESIGNED BY	LJB	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

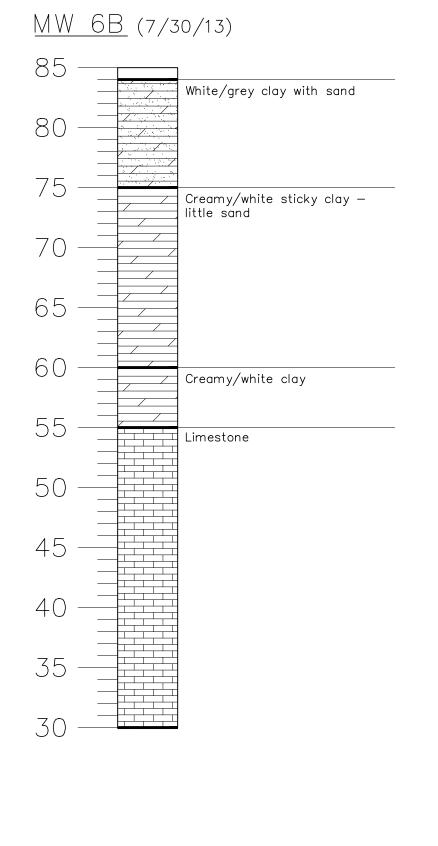
BORING LOGS

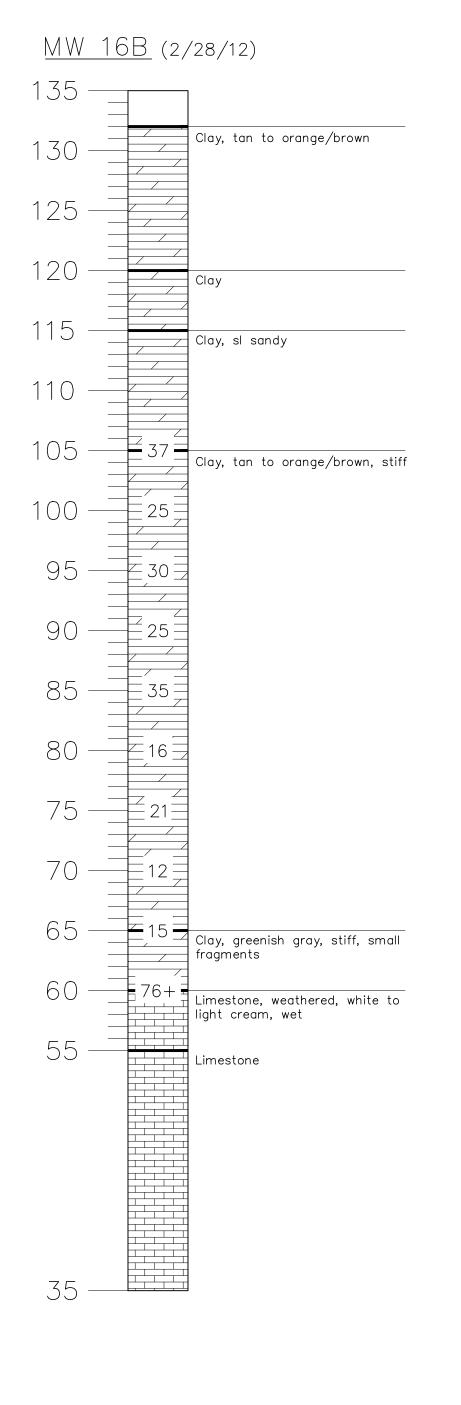
02000-144-14 **AS SHOWN** DECEMBER 2014 DRAWING: C1.13

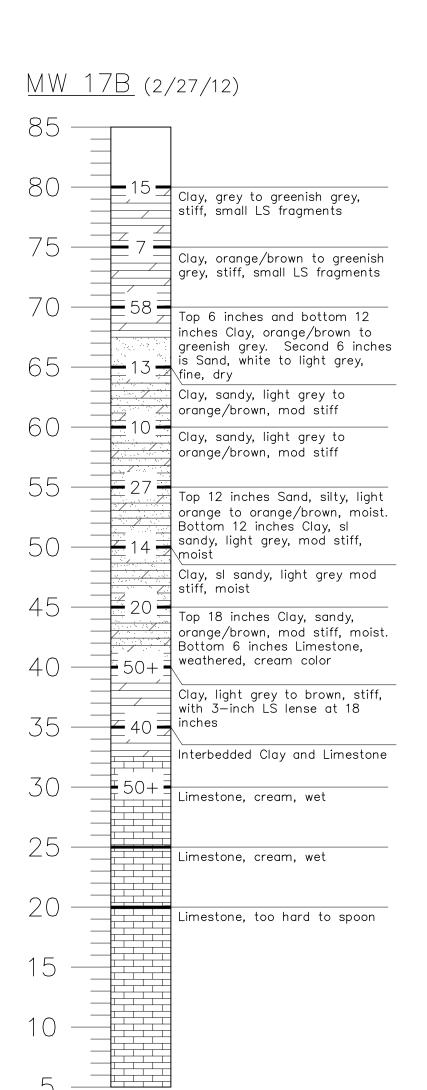
Sandy CLAY

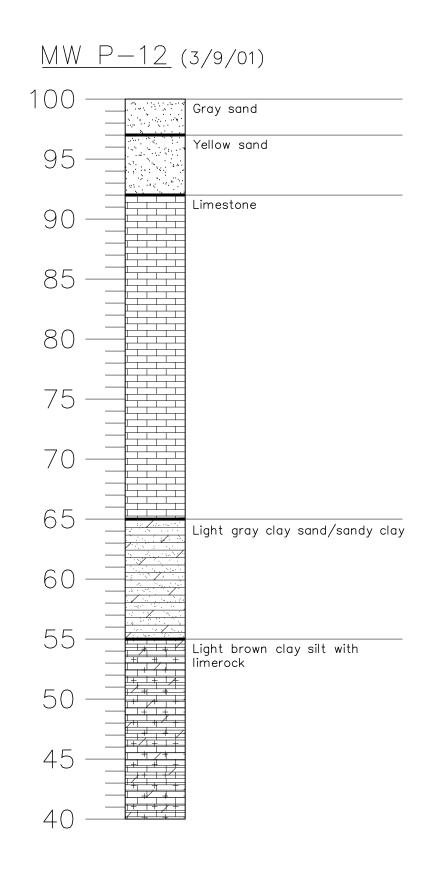




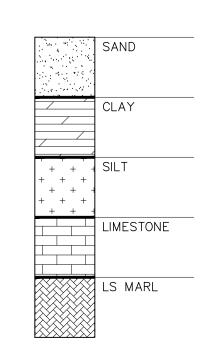








BORING LOG LEGEND



Clayey SAND
Sandy CLAY

GENERAL NOTES:

- 1. ADDITIONAL BLOW COUNT DATA IS AVAILABLE FOR SOME BORINGS.
- 2. NGVD, NAD83 AND MSL ARE USED INTERCHANGEABLY.

NO.	DATE	REVISION DESCRIPTION	ВҮ



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Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
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HISTORICAL GEOTECHNICAL DATA
SUMMARY PLAN
ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

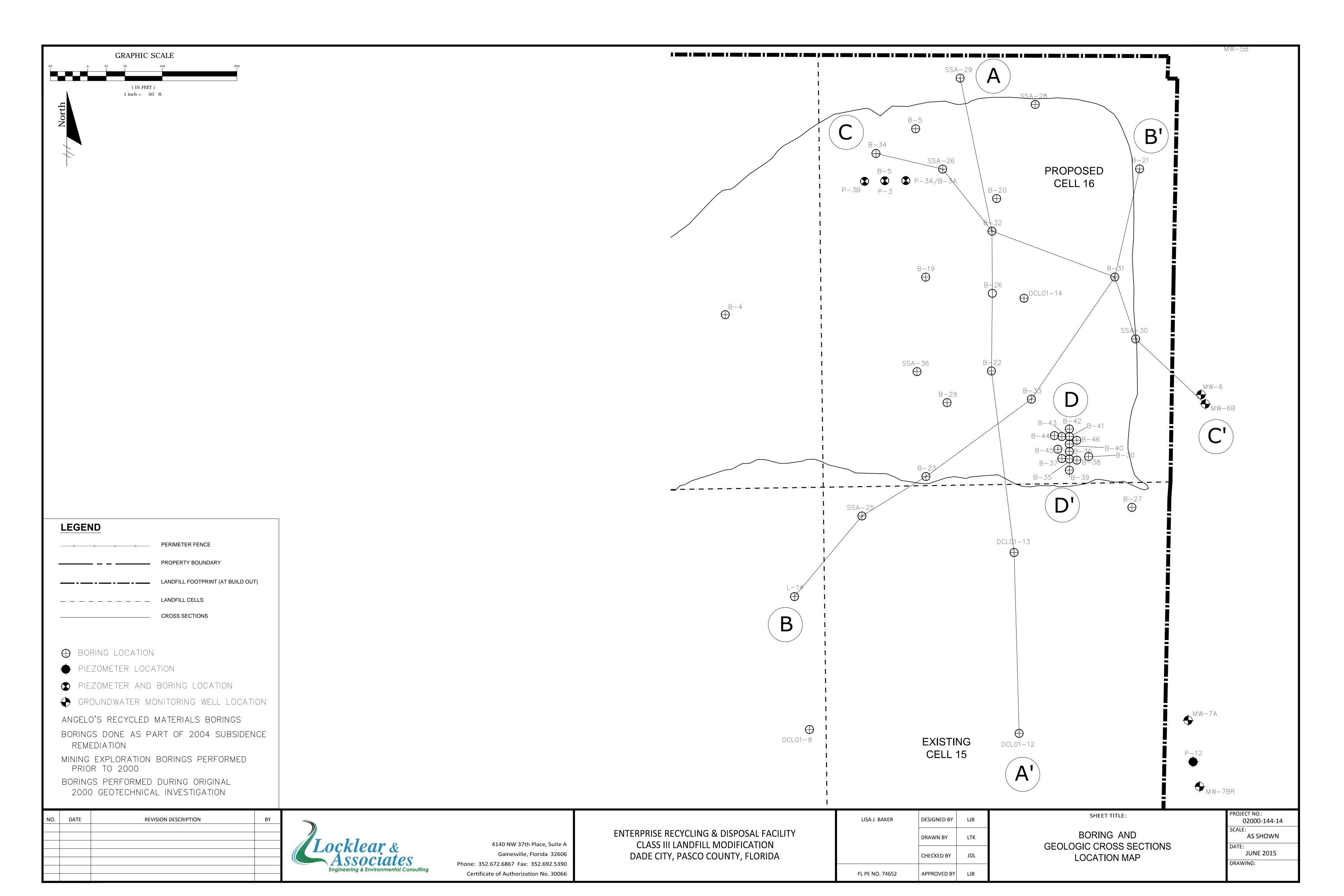
LISA J. BAKER	DESIGNED BY	IJВ	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

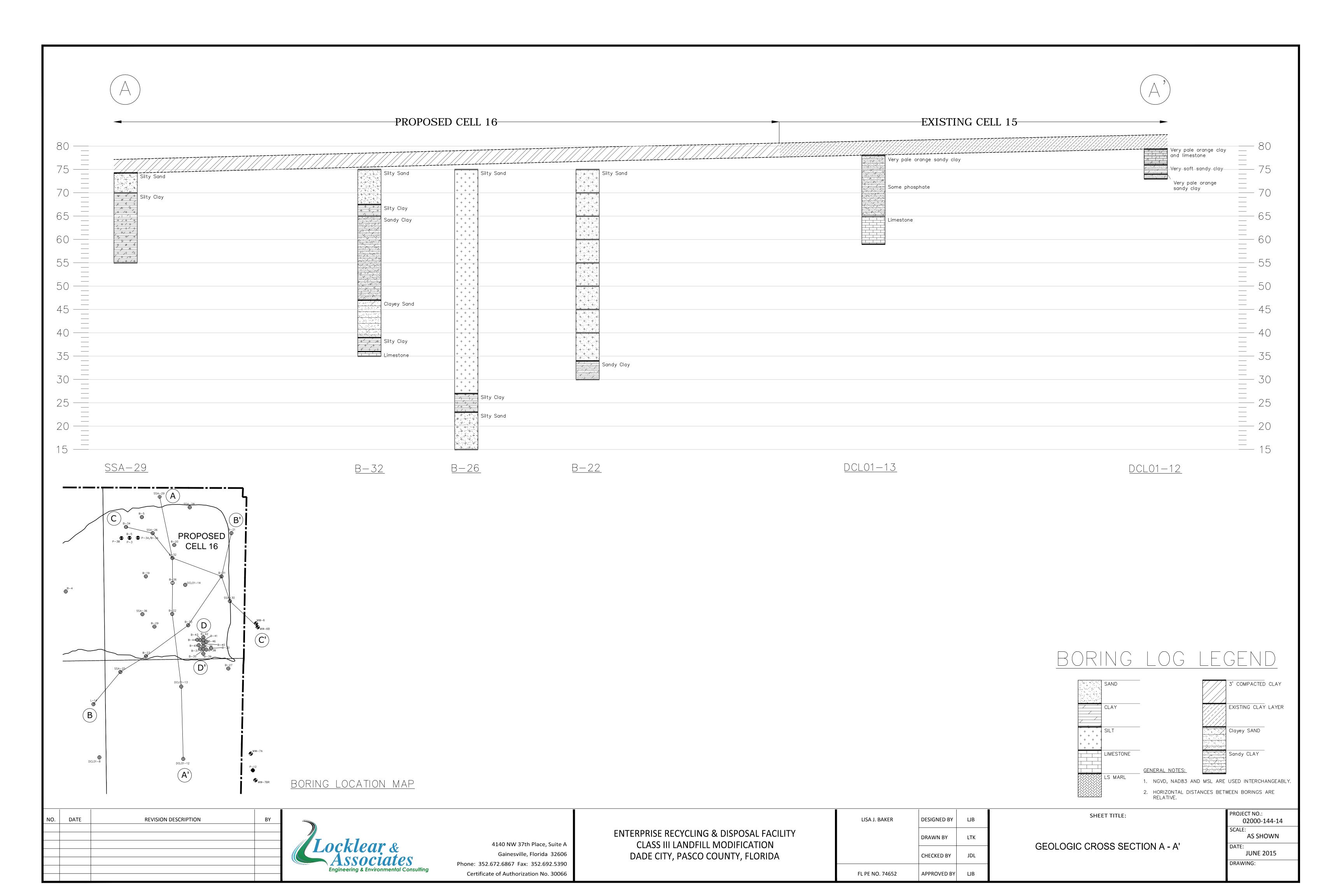
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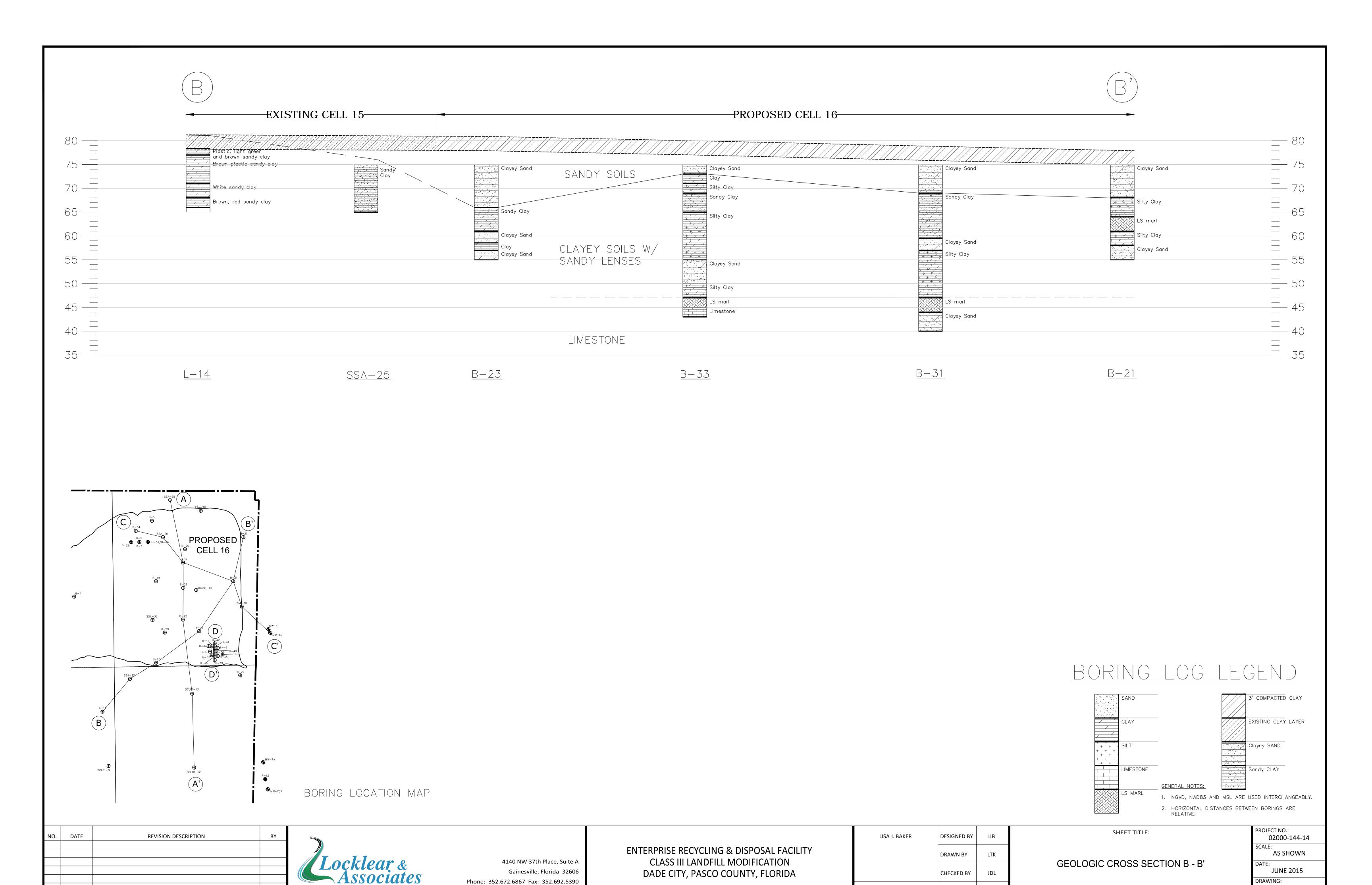
SHEET TITLE:

DECEMBER 2014

C1.14



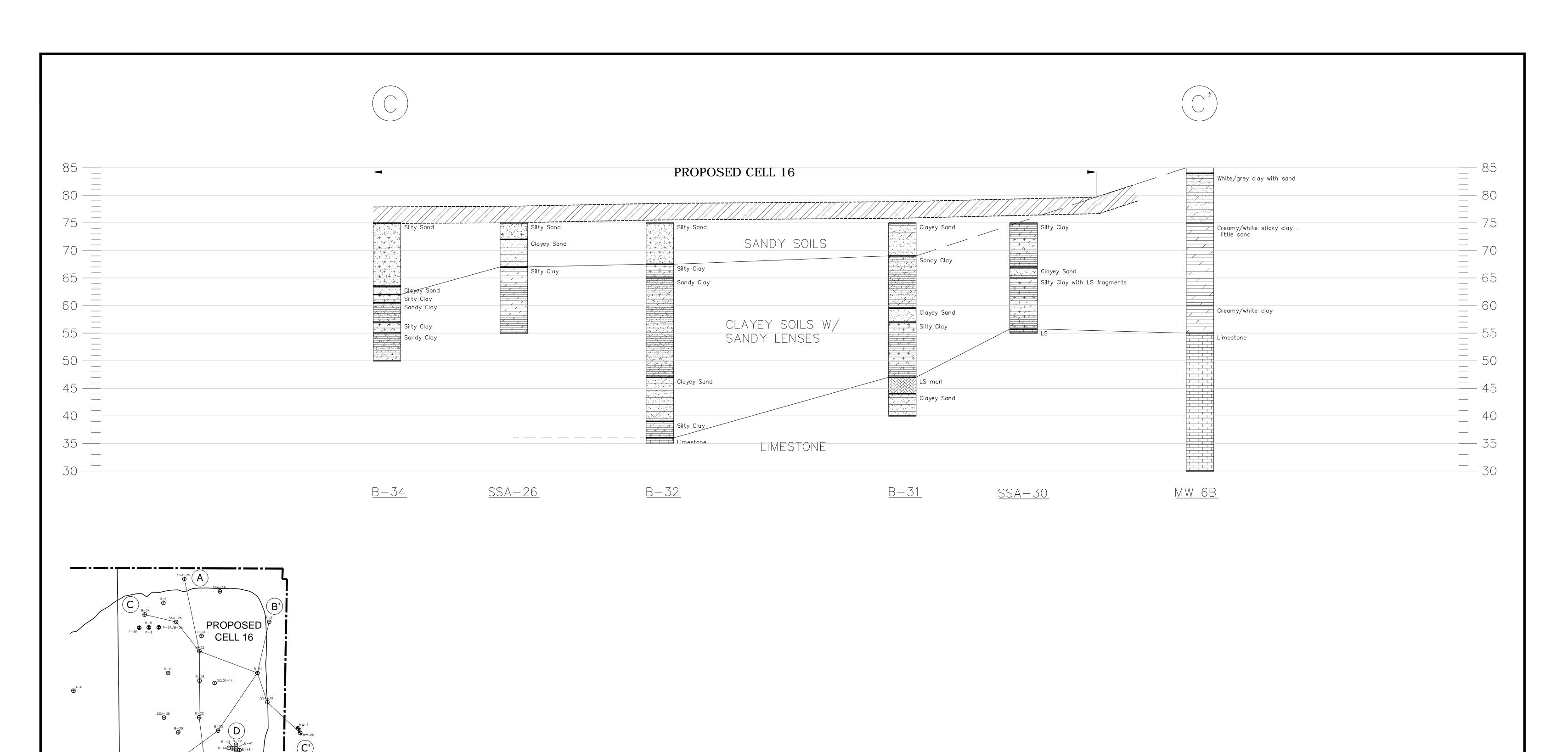




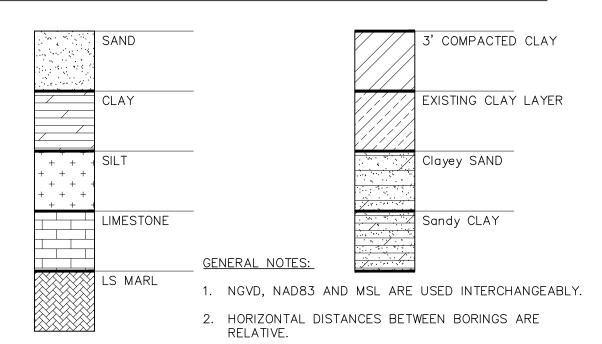
FL PE NO. 74652

APPROVED BY LJB

Certificate of Authorization No. 30066







NO.	DATE	REVISION DESCRIPTION	BY	
				Locklear Associa
				Associa
				Engineering & Environme

Locklear &

Gainesville, Florida 32606

Associates

Engineering & Environmental Consulting

4140 NW 37th Place, Suite A

Gainesville, Florida 32606

Phone: 352.672.6867 Fax: 352.692.5390

Certificate of Authorization No. 30066

BORING LOCATION MAP

ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

GEOLOGIC CROSS SECTION C - C'

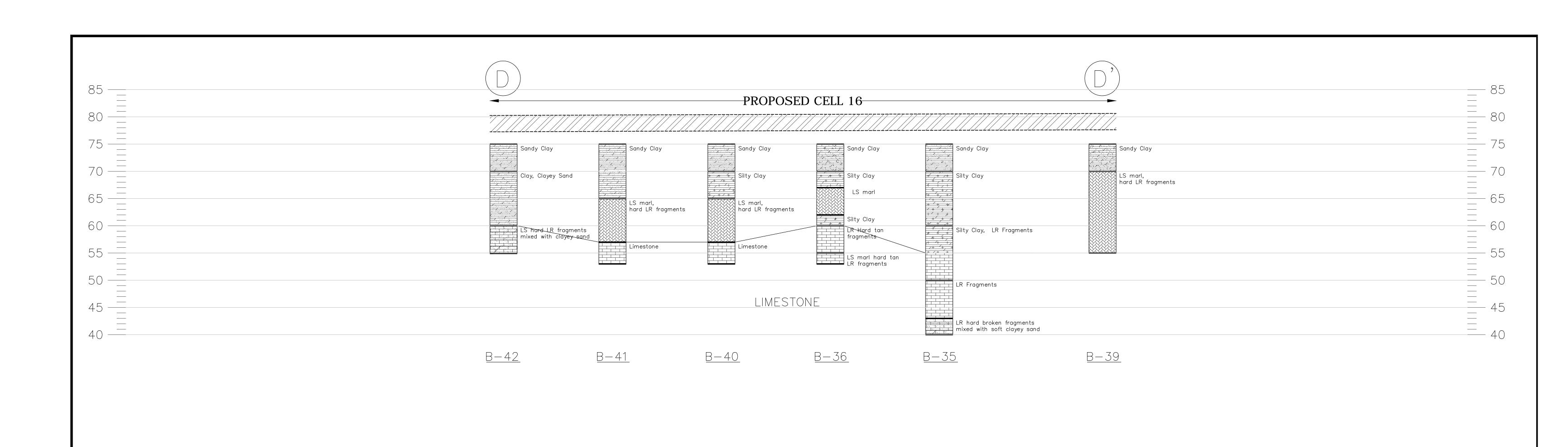
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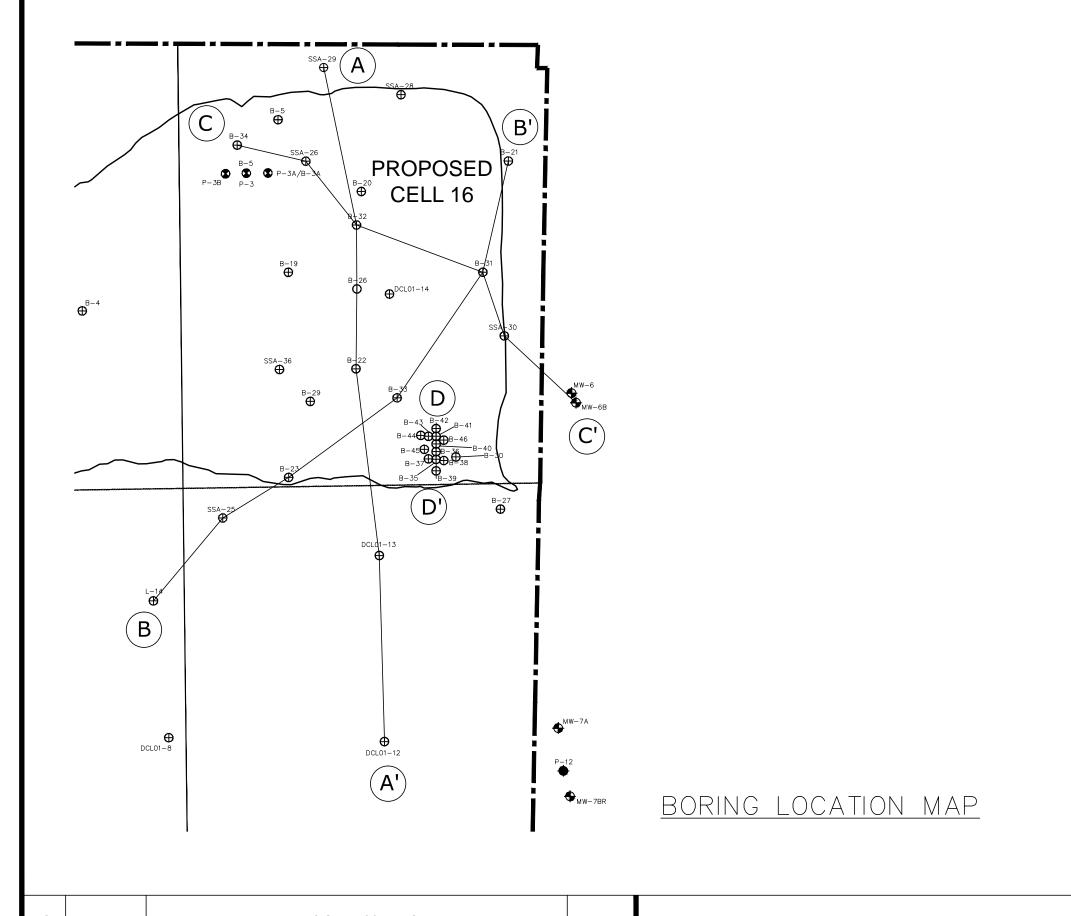
PROJECT NO.:
02000-144-14

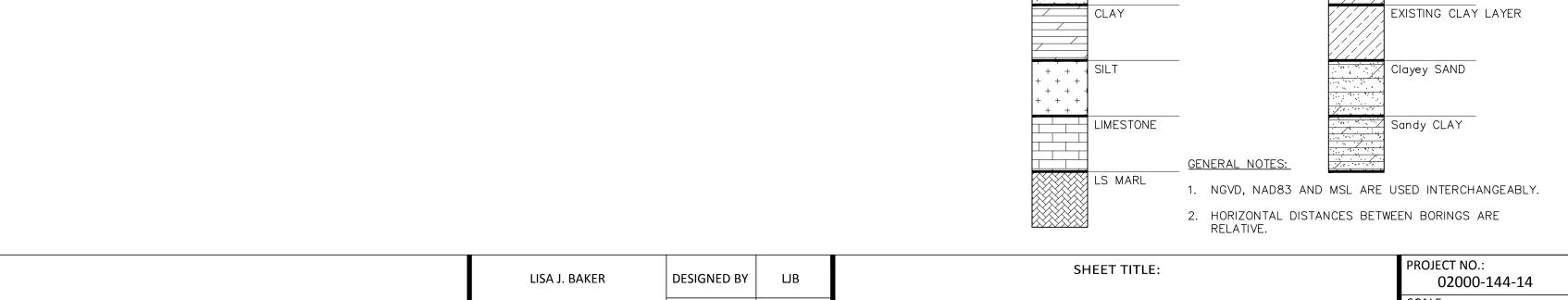
SCALE:
AS SHOWN

DATE:
JUNE 2015

DRAWING:







NO. DATE REVISION DESCRIPTION

BY

Locklear & Associates

Engineering & Environmental Consulting

4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

ENTERPRISE RECYCLING & DISPOSAL FACILITY
CLASS III LANDFILL MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB	
	DRAWN BY	LTK	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	LJB	

GEOLOGIC CROSS SECTION D - D'

BORING LOG LEGEND

O2000-144-14

SCALE:
AS SHOWN

DATE:
JUNE 2015

DRAWING:

3' COMPACTED CLAY



UNIVERSAL ENGINEERING SCIENCES 9802 Palm River Road Tampa, Florida 33619

(813) 740-8506

SOIL CLASSIFICATION CHART

TERMS DESCRIBING CONSISTENCY OR CONDITION

COARSE-GRAINED SOILS (major portions retained on No. 200 sieve); includes (1) clean gravel and sands and (2) silty or clayey gravels and sands. Condition is rated according to relative density as determined by laboratory tests or standard penetration resistance tests.

Descriptive Terms	Relative Density	SPT Blow Co	
Very loose	0 to 15 %	< 4	
Loose	15 to 35 %	4 to 10	
Medium dense	35 to 65 %	10 to 30	
Dense	65 to 85 %	30 to 50	
Very dense	85 to 100 %	> 50	

FINE-GRAINED SOILS (major portions passing on No. 200 sieve): includes (1) inorganic and organic silts and clays, (2) gravelly, sandy, or silty clays, and (3) clayey silts. Consistency is rated according to shearing strength, as indicated by penetrometer readings, SPT blow count, or unconfined compression tests.

Unconfined Compressive

Strength kPa	SPT Blow Count
< 25	< 2
25 to 50	2 to 4
50 to 100	4 to 8
100 to 200	8 to 15
200 to 400	15 to 30
> 400	> 30
	< 25 25 to 50 50 to 100 100 to 200 200 to 400

GENERAL NOTES

- 1. Classifications are based on the United Soil Classification System and include consistency, moisture, and color. Field descriptions have been modified to reflect results of laboratory tests where deemed appropriate.
- 2. Surface elevations are based on topographic maps and estimated
- Descriptions on these boring logs apply only at the specific boring locations and at the time the borings were made. They are not guaranteed to be representative of subsurface conditions at other locations or times.

SOIL SYMBOLS

FIL	ES ES Y ES TOPSOIL	ASPHALT	CONCRETE	SANO	SAND W	SAND W	SILTY SANO	CLAYEY SAND
E ES PEAT	Sut LOW 2 4510	SLT HIGH B ASTC	ORGANIC SILT	GLAV LOW	GLAY HIGH BLASTIF	LIMESTONE HIGHLY	LINESTONE	DOLOWITE

ОТ	HER SYMBOLS		
<u></u>	Measured Water	$\bar{\nabla}$	Estimated Seasonal

Ma	jor Divi	isions	Group Symbols	Typical Names			Laboratory Classification	Criteria						
	raction size)	gravel no fines)	GW	Well-graded gravels, gravel-sand mixtures, little or no fines			$C_u = \frac{D_{60}}{D_{10}}$ greater than 4; $C_c =$	$\frac{\left(\ D_{30}\right)^2}{D_{10} \ x \ D_{60}} \text{between 1 and 3}$		Sieve sizes	200	#200 to #40	#40 to #10	N# 01 01#
(exe size)	vels if coarse fr o 4 sieve	Clean g (Little or r	GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines	curve,	ols*	Not meeting all gradation require	rements for GW	0)	Sieve	* >	#500	#401	*
No. 200 s	Gravels (More than half of coarse fraction is larger than No. 4 sieve size)	Gravel with fines (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures	ain size curthan No.	dual symb	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are border-	Particle Size		1			_
arger than	(More is larg	Gravel w (Appre amount	GC	Clayey gravels, gravel-sand-silt mixtures	vel from gr on smaller 1 as follow: N, SP SM, SC	requiring	Atterberg limits above "A" line or P.I. greater than 7	line cases requiring use of dual symbols	Part			45	0	a
(More than half the material is larger than No. 200 sieve size)	irse fraction sieve size)	sands no fines)	sw	Weil-graded sands, gravelly sands, little or no fines	Determine percentages of sand and gravel from grain size of Depending on percentage of fines (fraction smaller than No. sieve) coarse-grained soils are classified as follows: Less than 5 percent	Borderline cases requiring dual symbols*	$C_U = \frac{D_{80}}{D_{10}}$ greater than 6, $C_C =$	$\frac{\left(\ D_{30}\right)^2}{\ D_{10}\ x\ D_{60}}\ \ \text{between 1 and 3}$		mm	< 0.074	0.074 to 0.42	0.42 to 2.00	2 L 04 00 C
n half the r	nds of coarse fr No. 4 sieve	Clean (Little or	SP	Poorly-graded sands, gravelly sands, little or no fines	ages of sar entage of t ed soils ar cent G	Borde	Not meeting all gradation requir	rements for SW						
(More than	Sands (More than half of coarse fraction is smaller than No. 4 sieve size)	Sands with fines (Appreciable amount of fines)	SM	Silty sands, sand-silt mixtures	etermine percentages of apending on percentage save) coarse-grained soils Less than 5 percent More than 12 percent	2 percent	Atterberg limits below "A" line or P.I. less than 4	Above "A" line with P.I. between 4 and 7 are border-	10,0	ā	clay		En	-
	(More the is smalls	Sands w (Appre amount			Atterberg limits above "A" line or P.I. greater than 7	line cases requiring use of dual symbols	Moto	Material	Silt or	Fine	Medium	Control		
size)	s,	0	ML	Inorganic silts and very fine sands, rock floor, silty or clayey fine sands or clayey silts with slight plasticity	80 FOR	R CLA	RIFICATION OF FINE-GRAINED SOIL AND	1.4.			Gravel Grave	_ ⊑	ū	ci ci
200 sieve	Silts and Clays	ss than 50	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	70 - FINE	E-GRA	AINED FRACTION OF COARSE-GRAINED SOIL	"The	9	Sieve	MA 12 21A	3/4 in to 3 in.	3 in. to 12 in.	40 to 10 to
r than No.	S	- je	OL	Organic silts and organic silty clays of low plasticity	NDEX (PI)		100	100	Particle Size	\perp				
sterial is smaller th	s,	20)	МН	Inorganic silts, micaceous or disto- maceous fine sandy or silty soils, organic silts	PLASTICITY INDEX (PI)				Par	mm	40.4	19.1 to 76.2	76.2 to 304.8	X X 10 0 10 0 10 0
the materia	Silts and Clays	ater than	СН	Inorganic clays of high plasticity, fat clays	20 -	/	100	MH OR OH		F	37.4	19.1	76.2 tc	304 8
(More than half the material is smaller than No. 200 sieve size)	IS.	gre	ОН	Organic clays of medium to high plasticity, organic silts		10	ML = OL 1620 30 40 50 60 LIQUID LIMIT (LL)	70 80 90 100 110		a la	76	se	ole	940
(More	Highly	Soils	Pt	Peat and other highly organic soils			Plasticity Cha	art	Mato	Maleria	Grave	Coarse	Cobble	Rouldere

When the percent passing a No. 200 sieve is between 5% and 12%, a dual symbol is used to denote the soil. For example; SP-SC, poorly-graded sand with clay content between 5% and 12%.

HARTMAN & ASSOCIATES, INC.

OFFICERS

Gerald C. Hartman, P.E., DEF Harold F. Schmidt, Jr., P.E., DEF James E. Christopher, P.E. Charles W. Drake, P.G. Mark A. Rynning, P.E., M.B.A. William D. Musser, P.E., P.H. Michael B. Bomar, P.E. Lawrence, E. Jenkims, P.S. M.

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> March 30, 2004 (Resubmitted July 15, 2004)

ASSOCIATES

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W Bruce Liferna, PG
Alexis K Stewart, PE
Ada R Terrero

HAI #99.0331.007

We Brace Lairenz, Palexis K Stewart, I Alexis K

Via UPS Ground

Ms. Susan Pelz, P.E. Florida Department of Environmental Protection Southwest District 3804 Coconut Palm Drive Tampa, Florida 33619

Subject:

Grouting Completion Report

Enterprise Recycling & Disposal Facility Angelo's Aggregate Materials, Ltd.

FDEP Permit Nos. 177982-001-SC, 177982-002-SO

Pasco County, Florida

Dear Ms. Pelz:

On behalf of Angelo's Aggregate Materials, Inc. (AAM), Hartman & Associates, Inc. (HAI) is submitting for your review the grouting completion report for the remediation of the subsidence area in cell 16, at the subject site in Dade City, Florida.

The subsidence area was discovered during an HAI site visit on January 12, 2004. The Department was notified about the existing site conditions within 24-hours, as required by the approved Construction Permit. AAM was advised by one of its consultants to fill in the subsidence area with clay immediately to prevent any additional slumping and to create areas stable enough to accommodate a drill rig. The approximate location of the subsidence area prior to being filled and the top of the excavated slope was marked and surveyed by Foresight Surveyors, Inc. A map showing the surveyed location of the subsidence area is included as Figure 1. HAI was onsite from January 15 through 17, 2004 with UES drillers to complete SPT borings in an effort to delineate the lateral and vertical extent of the subsidence area.

Using the lithologic description and blow count data from the SPT borings, engineers from UES calculated the approximate volume of grout required to remediate the subsidence area. LRE Ground Services, Inc. was onsite from March 2 through 9, 2004 to complete the grouting operation. A total of 357 cubic yards of grout was injected into a total of twenty-seven (27) grout injection points, within and adjacent to the original subsidence area.

Universal Engineering Sciences, Inc. (UES) observed the remedial grouting operation at the site, performed by LRE Ground Services, Inc. A grouting completion report, signed and sealed by a UES engineer has been included in Attachment A. Field notes completed by the onsite UES technician during the remedial grouting are included in Attachment B.



Ms. Susan Pelz, P.E. March 30, 2004 Page 2

We trust that we have provided the adequate information required for the submittal of the grouting completion report for the subject site in Dade City, Florida. Please feel free to contact us if you require additional information or have any questions.

Very truly yours,

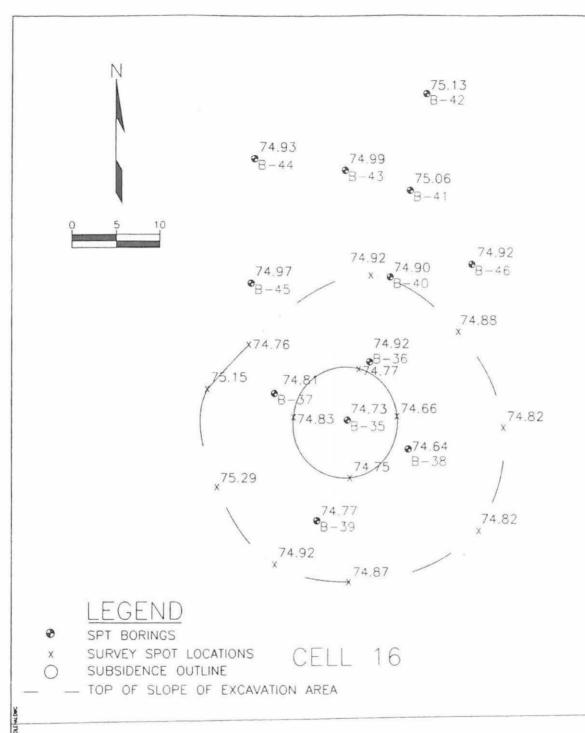
Hartman & Associates, Inc.

Miguel A. Garcia Project Hydrogeologist Bruce W. Lafrenz Project Hydrogeologist/Associate

MAG/cr/99.0331.007/corresp/grouting completion.doc

CC'

Dominic Iafrate, Angelo's Recycled Materials, Inc., Warren, MI Craig Bryan, Angelo's Aggregate Materials, Inc., Largo, FL



CELL 15



HARTMAN & ASSOCIATES, INC. engineers, hydrogeologists, surveyors & management consultants

201 EAST PINE STREET - SUITE 1000 - ORLANDO, FL 32801 TELEPHONE (407) 839-3955 - FAX (407) 839-3790

SUBSIDENCE AREA ENTERPRISE LANDFILL & DISPOSAL FACILITY PASCO, FLORIDA

FIGURE 1



ATTACHMENT A





March 10, 2004

Mr. Dominic lafrate Angelo's Recycled Materials, Inc. 1755 20th Avenue SE Largo, FL 34641

Reference:

Grouting Completion Report

Dade City Class III Landfill NEC Enterprise Rd. and Auton Rd.

Dade City, Florida

UES Project No. 80626-002-02

Dear Mr. lafrate:

As authorized, Universal Engineering Sciences, Inc. (UES) observed remedial grouting operation at the proposed retention area at Dade City landfill, performed by LRE Ground Services, Inc. The purpose of the grouting operation was to remediate suspected sinkhole conditions below the portion of the retention area by filling of any subsurface voids encountered in the general vicinity of the soil subsidence that occurred recently at this location.

UES developed the grouting program based on geotechnical subsurface exploration at the subject site directed by Hartman and Associates. The assessment regarding the remedial scope of work was made based upon the subsurface information provided by the SPT borings performed within the general vicinity of the soil subsidence.

A total of twenty seven (27) grout injection points were used during the grouting program. The approximate location, depth of installed casing, and actual pumped grout quantity for each grout injection point location are presented on the attached Grout Injection Point Location Plan. The installed length of the grout injection points generally varied from 10 to 46 feet, reflecting the variable subsurface conditions encountered during the geotechnical exploration. Grout injection point #26 however, was installed within a major void or partially filled void within limestone, believed to have contributed to the recent sinkhole related subsidence. A total of 68.6 yards of grout (nearly 20% of the grout total) was injected through this grout injection point alone. Total of 886 feet of casing was used to inject 357 cubic feet of grout. Approximately 8 cubic yards of grout was returned after completion of the grouting program.

The completion date, installed length of each grout injection point and the amount of grout pumped is presented in the following table. The grout injection points are listed in numerical order.

Angelo's Recycled Materials, Inc. UES Project No. 80626-002-02 March 10, 2004

GIP#	DATE COMPLETED	CASING LENGTH (FT)	TOTAL GROUT PUMPED (YDS ³
1	March 3, 2004	45	27.2
2	March 2, 2004	45	27.0
3	March 2, 2004	38	19.9
4	March 2, 2004	34	7.1
5	March 3, 2004	26	3.0
6	March 8, 2004	30	26.0
7	March 8, 2004	46	32.5
8	March 5, 2004	32	9.4
9	March 5, 2004	34	14.5
10	March 3, 2004	26	17.2
11	March 9, 2004	22	1.8
12	March 9, 2004	27	1.2
13	March 5, 2004	31	7.0
14	March 5, 2004	32	17.9
15	March 9, 2004	35	4.1
16	March 9, 2004	35	3.8
17	March 5, 2004	29	0.2
18	March 4, 2004	33	10.2
19	March 8, 2004	34	0.2
20	March 8, 2004	35	6.8
21	March 8, 2004	36	1.4
22	March 9, 2004	10	0.1
23	March 5, 2004	38	19.0
24	March 8, 2004	30	16.5
25	March 8, 2004	43	14 4
26	March 5, 2004	60	68.6
	TOTAL	886	357.0

Based on the grout take and depth of grout injection points, it appears that one major cavity and several zones of very loose soil conditions indicating possible sinkhole activity may have existed in the immediate vicinity and to the north of the occurred subsidence

Angelo'S Recycled Materials, Inc. UES Project No. 80626-002-02 March 10, 2004

Based on our observation of the grouting program performed within the proposed retention area, and our subsequent analysis of data gathered during the grouting, we feel that the intent of the remedial program was met. In our opinion, the subsurface grouting met the goals of the remedial program, by improving the overall subsurface conditions within the treated area and reducing the risk of future soil subsidences. We note that measures such as subsurface grouting are intended to treat, in a practical and cost-effective manner, potentially detrimental subsurface conditions which could affect the ground surface. However, evaluation of the effectiveness of treatment is subject to inference and interpretation of the end result and cannot be predicted with certainty.

It has been a pleasure assisting you with this phase of your program. If you have any questions regarding this report or when we can be of further assistance please contact the undersigned at (813) 740-8506.

Respectfully submitted,

UNIVERSAL ENGINEERING SCIENCES, INC.

Certificate of Authorization No. 549

Dusan Jovanovic

Senior Project Manager

Mark Hardy, P.E.

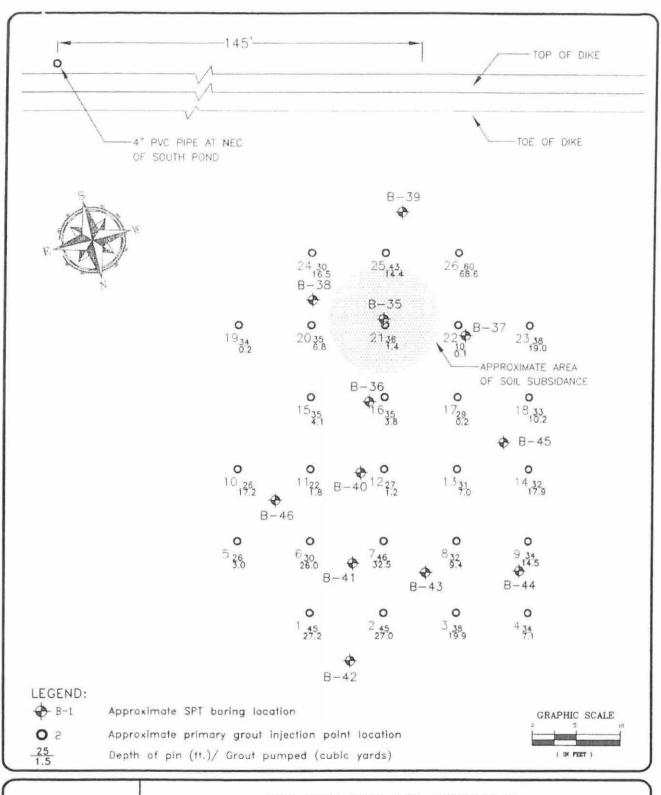
Tampa Regional Manager

Professional Engineer No. 57233

Date_ 3-10-04

Attachment: Grout Injection Point Location Plan

cc: Client (3)





RETENTION POND SOIL SUBSIDENCE DADE CITY CLASS III LANDFILL DADE CITY, FLORIDA

FINAL GROUT INJECTION POINT LOCATION PLAN

DRAWN BY: C.C.	DATE: MAR.	10, 2004	CHECKED BY: D.J.	DATE: MAR. 10, 2004
SCALE: 1" = 10'	PROJECT NO:	80626-002	-02 REPORT NO:	APPENDIX:



9802 Palm River Road
Tampa, Florida 33619-4438
Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.ues@com
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Tampa, Florida 33619-4438
Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.ues@com
Tampa, Florida 33619-4438 Universal Engineering Sciences, Inc.

onent.		DADE CITY LANDFILL				Injection Points								
roject:		DADE CI	TY LANDFI						Injection Point:					
Csng. Depth	Grou	ut Time	Max. Pressure	Pump	R	leasor pum	n to sto	op						
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks					
45	← TOTAL C	ASING DEPTH	1	8					Soit much					
1/5	10:11	1037	200	496					End Time Comes	(9.0				
				60 t . 52					New Truck					
42	1129		5004	5					00057					
38			256/40	86					00007					
38		1:56	220	192					End Truck Piece 16	(90				
				3-7	ş Î				NEW Truck BRES					
32	1210	1237	200	490			/		End Truck BRE 5	90				
				7-2										
27	1036		JUD+	2					00017					
25			17	1/					R6017					
22	1315	13/1	300+	9				X	completed	(.2				
2 1500									Go To 10					
										The state of the s				
		GH - Groun	d Heave;	GP - Grout	out				Communication					
upervis ompany		LRE			1	「otal			:27 1					
e: 0.5	tal To Date (Cu. Yd.):													



Universal Engineering Sciences, Inc. 9802 Palm River Road

Tampa, Florida 33619-4438

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Client: Project:	ANG							1	Injection Point: 2	-
Csng. Depth	Grou	t Time	Max. Pressure Pump		F	Reasor	n to ste	op		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks	
45	← TOTAL C	ASING DEPTH		2					Continue Truck	
115	1401	1126	160	1168					End Truck BEET	9.0
				5.4%					Now Truck	
42	14 33	1433	4014	5	X				0015	-
110			400+	1.	X				10057 10055	-
38	1434	1458	140	427					End Trycle 11th 10	90
				C.					NEW Tirck	
32	1531	15 58	216	523					Earl Truck BPK5	(9,0
27							X	1	Ret 5	_
22		16 18						X	Flusti	_
									Comple Ted	1
									EDD DAY	
										_
										_
HP - Higi	h Pressure;	GH - Groun	d Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication	
Supervis	upervisor:			_		Insp	ecto	r: JOHN MOTKO	_	
Compan	ompany: LRE				Total	l (Cu	. Yd.): 27.0		
Total To	Fotal To Date (Cu. Yd.):				-					



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GROUT MONITORING LOG

DAYONE

Client:	ANG	ELO'S RECY	CLING					[Date: . 3-2-04	
Project:	-	DADE CIT	TY LANDEL	<u> </u>					Injection Point: 3	
Csng.	Grou	ıt Time	Max	Pump	F	Reasor		op qu		ĺ
(ft.)	Start	Finish	Pressure (psi)	Strokes	H	G H	G P	C M	Remarks	
38	← TOTAL C	ASING DEPTH		进事					STORT Tivek	
37	1028	1050	180	446					End Truck BRY 5	9.0
32	1131	1156	200	1/94					X/ Tul Terek End Truck Part	9.0
				3.7					New Time	
27	125/	1251	400+	3	X				P.p. 2147 3 FT	
22			400+	8	χ				REKIO	
17	1301	12 (1)	200	53	ſ				Water put Ground IP 8	
13	1305	1307	200	110	X	X			South Side of I.P.	
									completed	(1.9
									Co To 4	
		GH - Groun	d Heave;	GP - Grout	tout				Communication	
Supervisor: Company: LRE						Total			r: JOHN MOTKO):	
Total To	Data (Cir V	d).								



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Client: Project:	ANGELO'S RECYCLINGDADE CITY LANDFILL							ı	Injection Point:
Csng. Depth	Grout Time		Max. Pressure	Pump	F	leasor purr	n to ste	ор	
(ft.)	Start	Finish	(psi)	Strokes 3-9	H	G H	G P	C M	Remarks
34	← TOTAL C	ASING DEPTH		110					Continue Twee
32	1321		200	1.5					WATER OUT GOILS AT IP
32		1341	220	511					End Truck BAKT (7
27							X		End Truck BAKT (7
22							X		BEKS
17									
				雙中					New Truck
17	1351	1351	100	2				X	
									compleTell
									Go TO 2
HP - High	n Pressure;	GH - Grour	nd Heave;	GP - Grout	out	of Pi	ipe;	CM -	Communication
Supervis	upervisor:						Insp	ecto	r: JOHN MOTKO
Company	y:	LRE			Total (Cu. Yd.)): 7.1
Total To	otal To Date (Cu. Yd.):			i.					



Universal Engineering Sciences, Inc. 9802 Palm River Road

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Client:	ANGELO'S RECYCLING							1	Date: 3 3 0 7
Project:		DADE CIT	TY LANDFII	<u> </u>					Injection Point: 5
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to ste	ор	
(ft.)	Start	Finish	(psi)	Strokes 5-9	H	G H	G P	C M	Remarks -
26	← TOTAL C	ASING DEPTH		459					Continue True
26	1501		160	465					Food Truck Out Groved IP
		1503	160	492					End Truck
				(5) (F. 7)					NEW Truck
26	1517	1504	210	125		X			Bet 5
22				, ,			X		cer 5
17	15.7.1	1532	180	132		X			Deet
12							X		completed 6
									Go To 26
		-15-75-75-75-75-75-75-75-75-75-75-75-75-75							
HP - High	Pressure;	GH - Groun	d Heave; (GP - Grout	out	of P	ipe;	CM -	- Communication
Supervis	or:						Insp	ecto	or: JOHN MOTKO
Company	y:	LRE			. 1	Tota	(Cu	Yd.	.):
Total To	Date (Cu. Y	d.):							



Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client:	ANGELO'S RECYCLING					Date: 3- 5-04							
Project:	\ <u></u>	DADE CI	TY LANDFII	<u> </u>					Injection Point:				
Csng. Depth	Grou	ut Time	Max. Pressure	Pump	F	Reason	n to st	ор					
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks				
30	← TOTAL C	ASING DEPTH	1	460					CLAT TOUCK (7.	<u> </u>			
	1130	1502	200	647									
30	1516	1547	Crary.	430					NAW TRUCK port 10.	7			
27	1214	12 (1	1-77	450			X			_			
							-		Plant Stap sender Trucks				
			KEYS						Continue Truck from				
27	1423	1644	280	435		χ			I.P. 21				
22							X	-	BRICT	_			
12	1458	1700	300	456				X	End Tivil	2			
HP - Hig	h Pressure;	GH - Groun	d Heave;	GP - Grou	tout	of P	ipe;	CM -	Communication				
Supervis	sor:				-		Insp	ecto	or: JOHN MOTKO				
Compan	Company: L.RE			-	Tota	l (Cu	. Yd.):26.0					
Total To	Date (Cu. Y	'd.):			-1								



Tampa, Florida 33619-4438 Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client: Project:	ANG	ANGELO'S RECYCLING DADE CITY LANDFILL						[Date: 3-8-04 Injection Point: 7	
i rojedi.		DADE OII	TEARDIN						injection (vint.	
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to sto	pp		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks	
46	← TOTAL CA	ASING DEPTH	CCMEY	100					STAIT TIVILE	
42	10114	1116	160/	672					End Truck nows 10	
37	1159	15.11	Cemix.						That Truck BRKS 10	
3/	1159	1231							Altw Truck BRIES 10.	
32	13 63	1327	180 god	462	V				BEIT	
27	1326	1348	160	668					End Truck BAY (10	
									Alin Trock	
22	1412	1405	JOD 300	451	X	X		-	- BW 5	
17		7 . 2					У		BRY	
12	1439	1444	201/	160		X			(bm ple fel 2.	
		(at mail							(D) TO (D	
HP U:al	Procesure	GH Groun	d Hoover	GD Gra	1.0114	of P	ine: /	- BA	Communication	
Supervis		on - Groun	u nedve; (3r - G10u	i out	UI P			r: JOHN MOTKO	
Çompan	Company: LRE				Total (Cu. Yd.): 32.5					



Universal Engineering Sciences, Inc. 9802 Palm River Road

Tampa, Florida 33619-4438

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Client:	ANG					I	Date: 3-5-04			
Project:	1	DADE CI	TY LANDFIL						Injection Point: 8	
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F	Reasor purr	n to sto	op		
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks	
32	← TOTAL C	ASING DEPTH		30		12			Commune Testes	
32	1725	1738	180/200	198		X			nert	
27		1					X		CPE	
22	17:15	1749	200	317		1			not:	
17	175#	1757	200	493						
12							X		End Tives per	
									END MAY	
									60 70 7	
								_		
								_		
HP - High	n Pressure;	GH - Groun	d Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication	
Supervis	or:				_		Insp	ecto	r: JOHN MOTKO	
Compan	y:	LRE			_	Total	(Cu	. Yd.): 9.4	_
Total To	Date (Cu. Y	d.):			-					



Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client: Project:	ANG	ELO'S RECY DADE CI	CLING						Date: 3-5-29 Injection Point: 9
Csng. Depth	Grou	it Time	Max. Pressure				n to st	op q	
(ft.)	Start	Finish	BeTin	Strokes	H P	G H	G P	C M	Remarks
34	← TOTAL C	ASING DEPTH		群和			T		STORT TOURS
34	12/12	1229	190/100		X				OPY
32							X		OPT
27	1234	1236	180/100	391	X		,		RPET
22	1210	1249	150	624					End opull
			B-mix	10-10		_	\vdash		How Trick
22	1319	13-6	1:0/80	255		X			FEE -
17	1271						1		Dev -
/2									
			-			_			60 10 14
		<u> </u>				_	-		
_			-						
		-	-		_	-	-		
-	-	-	-		-	-			
		-	-						
			1						
	***************************************		-						

P - High	Pressure;	GH - Grour	nd Heave;	GP - Grout	t out	of P	ipe;	CM -	Communication
upervis	sor:						Insp	ecto	r: JOHN MOTKO
ompany	ny: _ LRE					Tota	I (Cu	. Yd.)	14.5
otal To	Date (Cu. Yd.):								



Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client: Project:	ANG	ELO'S RECY	CLING					ı	Date: 3-3-04 Injection Point: /0	
Csng. Depth	Grou	It Time	Max. Pressure	Pump	F	Reasor	n to st	ор		
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks	
33	← TOTAL C	ASING DEPTH		9			T		Continue Truck	
	1378 1401		160	48/					End Truck BRES	
				金子					How Truck	
27	11/13		180	139					WATER OUT Grand I.P. 6	
27	1		374	X		_		BRE 5		
22			459		X			BAKT		
17							X		BPIT	
12							X		campleteel	
									/	18.4
									Go To 5	9
						_				
						-		_		
						-				
						-				
							-			
							-			
				_			_			
HP - High	P - High Pressure; GH - Ground Heave; GP - Grou				t out	of P	ipe;	CM -	Communication	
Supervis	upervisor:				_		Insp	ecto	r: JOHN MOTKO	
Compan	ompany: LRE				Tota	l (Cu	. Yd.):17.2		
Total To	tal To Date (Cu. Yd.):									



Universal Engineering Sciences, Inc. 9802 Palm River Road

Tampa, Florida 33619-4438 Telephone: (813) 740-8506 Fax: (813) 740-8706 Website: www.uesorl.com

Client:	ANG	ANGELO'S RECYCLING						Date: 3-9-04									
Project:		DADE CI	TY LANDFIL	<u></u>					Injection Point: //								
Csng.	Grou	ut Time	Max.		Reason to			ор									
Depth (ft.)	Start	Finish	Pressure (psi)	Pump Strokes	Н	g G	g G P	С	Remarks								
22	← TOTAL C	TAL CASING DEPTH		249	P	Н	P	М	Continue Truck								
22	956	1001	170	35/		X			BRKT								
17							X		BEET								
12	1006	1006	170	359				X		8							
			-							1							
									GO TO 12								
	ř																
		-															
			-														
							_										
HP - High	h Pressure;	GH - Groun	d Heave; (GP - Grout	tout	of Pi	pe; (CM -	Communication								
Supervis	or:						Insp	ecto	r: JOHN MOTKO								
Compan	y:	LRE	10	Number of the second		Γotal	(Cu.	Yd.)	1.8								
Total To	otal To Date (Cu. Yd.):																



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Client: Project:	ANG					[Date: 3-9-04 Injection Point: 12							
Csng.			T	leason										
Depth (ft.)	Groun	rime	Pressure (psi)	Pump Strokes			ping	ф	Remarks					
1007	Start	Finish	(551)	1-10	H P	G H	G P	C M	7.07.07.10					
27	← TOTAL CASING DEPTH 359						Continue Truck							
27	10 18		210	1/26		X			CONTINUE TRUCK					
22							Y							
17	10 27	1028	210	43/		χ		X	completed	1.2				
									GO TO 16					
							_							
HP - Higl	Pressure;	GH - Groun	d Heave; (GP - Grou	t out	of Pi	ipe; (CM -	Communication					
Supervisor:						Inspector: JOHN MOTKO								
Company: LRE				Total (Cu. Yd.): 1.2										
Total To	otal To Date (Cu. Yd.):													



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Client: Project:	ANG	ELO'S RECY	CLING TY LANDFII					1	Date: 3-5-01/						
Csng Depth	Grou	t Time	Max. Pressure	Pump	Reason to stop pumping			op							
(ft.)	Start	(psi)		Strokes		G H	G P	C M	Remarks						
3/	← TOTAL CA	ASING DEPTH						Centino Trock							
3/	1639	1456	180 180	557					Contine Truck	4					
			B-mix	(B) (B)					Mrw Truck						
31	1701	176	500+	2	Y				Pipe Dest						
29	1702		300+	5	X				Pro 11/9 Bric 15 /	,					
22	1768	1709	160	30				X	completed (1)	0					
									60 10 8						
HP - Higl	n Pressure;	GH - Groun	d Heave;	GP - Grout	out	of P	ipe;	CM -	Communication						
Supervis	Supervisor:							ecto	r: JOHN MOTKO						
Compan	Company: LRE						Total (Cu. Yd.): 7.0								
Total To	otal To Date (Cu. Yd.):														



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GROUT MONITORING LOG

Client:	ANG	ELO'S RECY		Date: 3- 5-04									
Project:	-	DADE CI	TY LANDFIL						Injection Point:				
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F	Reasor pum	n to sto	op	Consider				
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks				
32	← TOTAL C	ASING DEPTH	1	255					C. Teuck				
	1340	1355	150/20	572					C. Teuck Eny Truck	2.5			
			KIYS	w Salaya					Nrw Truck				
32	1408	1438	160/160	630					End Tive BOLT	7.0			
			B-MIX	\$4=100°					Min Tivile				
27	15 58	11,04	130/400	126	X				BECT				
25				1.0			X		DRET				
17	16 10	16 13	160/180	189		X			CALT	-			
12							X			ξ. 1) Ξ			
							-						
									Co TO 17				
						_							
UD Uint	B. High Brassura CH. Count House CD. Cou				- 6 P	in a : /	CM	Communication					
	P - High Pressure; GH - Ground Heave; GP - Grou				ut out of Pipe; CM - Communication Inspector: JOHN MOTKO								
Company					Total (Cu. Yd.): 17. 9								
Total To	Date (Cu. Y	d.):											

H:\djovanovic\GroutIng\Grout Monitoring 7 oaks.wpd



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Client:	ANG	ELO'S RECY	CLING					ı	Date: 3-9-04		
Project:		DADE CI	TY LANDFII	LL					Injection Point:		
Csng. Depth (ft.)	Grou	Grout Time		Pump	F	Reasor	to sto	эр	Remarks		
(11.7	Start	Finish	(psi)	Strokes GMIX	H P	G H	G P	C M	Remarks		
35	← TOTAL CA	ASING DEPTH		(1)					STUPT TINCK		
35									TIGHT PIPE BAYT		
32									TIGHT PIPE BRKT		
27	930	939	160	181		X			pret 5		
22							Х			1	
17	9 44	919	160	249				X	campleted	[4].	
									60 TO 11		
									,		
	V										
-		GH - Grour	nd Heave;	GP - Grout	out				Communication		
Supervis	or:				-		insp	ecto	r: JOHN MOTKO		
Company: LRE				Total (Cu. Yd.): 4.)							
Total To	Date (Cu. Y	d.):			-						



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Client:	ANG	ELO'S RECY	CLING					1	Date: 3-9-04							
Project:	-	DADE CI	TY LANDFIL						Injection Point: / 6							
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F		n to sto	pp								
(ft.)	Start Finish (psi) Strokes 1-10 ← TOTAL CASING DEPTH		(psi)	100000000000000000000000000000000000000	H P	G H	G P	СМ	Remarks							
35							Continue Touck									
			X													
			11	467	У											
		1037	11	441	У				DPY5							
32	10341	1041	500+	169	X				nout							
31	1059	10:63	210/	540		X			BRK 5							
27	10 30	1027	210	605		1			End Touch	2.9						
										7						
			PT-15	2-9					New Trull.							
27	1112	12.7	200	36		1/.			Ordes							
22	1150	1151	577/	40		X			· nout							
17	1 2 2			1-2-			X		BRILL	.9						
12									Chron letel							
									Co To 22							
HP - High	Pressure;	GH - Groun	d Heave; (GP - Grout	tout	of P	ipe; (CM -	Communication							
Supervis	upervisor:							Inspector: JOHN MOTKO								
Company: LRE							Total (Cu. Yd.): 3. 8									
Total To	Date (Cu. Y	d.):			-,											



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Client:	ANGELO'S RECYCLING					ľ	Date:	3.	-5-09				
Project:	-	DADE CIT	TY LANDFIL		Injection Point: / 7								
Csng. Depth	Start Finish (psi) Strokes			F	Reasor pum	to sto	op						
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M		Remarks			
29	← TOTAL C	ASING DEPTH		189					ConTinue	Truck			
29	1425	1626	240	195					Continue Track Pipe 2117 Bet T				
27							X				BAKT		
25	1631	163/	200	198				L,	Post 1	(T	,		
20	1433	1630	200	200				X	(om)	n le Tru	/	\Box (,2	
							_		Go 10	13	, ,		
							_					_	
												_	
												_	
					-	-		-					
						\vdash							
						-							
												\dashv	
						-							
					-								
HP - High Supervis		GH - Groun	d Heave; (GP - Grout	t out				Communicati			_	
							100		-	0.2			
Company: LRE				-	Total	(Cu	. Yd.):					
Total To	Date (Cu. Y	d.):		TA I	-								



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Client: Project:	ANG	ELO'S RECY	CLING TY LANDFII					Ì	Date: 3.4-04 Injection Point: 18				
Csng.	Grou	t Time	Max.	I	F	Reasor	to ste	op					
Depth (ft.)	Start	Finish	Pressure (psi)	Pump Strokes	H		G P	C	Remarks				
33	← TOTAL C	ASING DEPTH		4					Mru Truck				
33	1420		240	468					End Truck BERT 90				
				4.91					1/w Tirk				
27	15.16	1549	300	47		X		*	DROUGH IN BRES				
77	1211	1021	500	43					Completed 1.2				
									60 10 23				
								-					
HP - High Pressure: GH - Ground Heave: GP - Grou					Out	of P	ine:	CM -	Communication				
HP - High Pressure; GH - Ground Heave; GP - Grout Supervisor:									or: JOHN MOTKO				
Company: LRE				Total (Cu. Yd.): 10. 2									
Total To Date (Cu. Yd.):													



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Client: Project:	ANG	SELO'S RECY	CLING					,	Date: 3-8-04 Injection Point: 19		
i rojeci.	944	DADE O	III EARDIII						injection i diffe		
Csng Depth	Grou	ut Time	Max. Pressure	Pump	R		to sto	эр	Remarks		
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks		
31/	← TOTAL C	ASING DEPTH	l	37					Continue Truste		
34									Dest		
32	1415		300 F	39	X				noon		
50			500 T	45	4				BRY		
27			5001	47	X				BERT		
22			5001	49	X				Brr		
17			2001	70	Y				BRIET		
12.		1450	5001	71	Y				1 umpleted		
				_							
									Gn 70 20		
		<u></u>	1								
HP - High	h Pressure;	GH - Groun	nd Heave;	GP - Grou	t out	of P	ipe;	CM -	Communication		
Supervis	upervisor:							ecto	r: JOHN MOTKO		
Company: LRE					Total (Cu. Yd.):						
Total To	Date (Cu. Y	(d.):					14				



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Client:	ANG	LO'S RECY	CLING		Date: 3 - 8 - 7004 Injection Point: 28								
Project:		DADE CI	TY LANDFIL	L					Injection Point: 20				
Csng	Depth Pressure Pump		Reasor	n to sto	op								
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	СМ	Remarks				
35	← TOTAL CA	SING DEPTH	-	7/					Cent Treck				
32	1956	1456		72	X				13625				
78				73	X								
27	1459		300+	78	X				Det T				
55		1509	400+	285	1				124				
112	1514	1521	180/	422		X			DEKS				
17			,				X		1000				
12							y		Completed	6.8			
							1						
									GD TO 21				
-						-		_					
-						-	-	_					
-							-	-					
							-						
						-							
-													
-													
-													
HP - High	Pressure;	GH - Groun	d Heave; (GP - Grout	tout	of P	ipe; (CM -	Communication				
Supervisor:							Insp	ecto	r: JOHN MOTKO				
Company: LRE				Total (Cu. Yd.): 6. g									
Total To Date (Cu. Yd.):													



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Client: Project:	ANG					ľ	Injection Point: 2/					
Cono	Grow	I Time	I May		T	Reasor	, to sk		Remarks			
Csng. Depth (ft.)	Grou	i rime	Max. Pressure (psi)	Pump Strokes			nping	J.	Remarks			
	Start	Finish	387 - 5	1/- 9	H P	G H	G P	C M				
36	← TOTAL CA	ASING DEPTH		437					Continue Trucke	(
	1536	1540	150	480					End Truck news	(.9		
32							X					
			KEYS	347					STUT TIVEK			
27	1600	1600	180	2		V			nelet			
25	1608	1609	180	24		7			DEKT DEKT			
17	1600	1607	150	27		H	X		BRKS	1.5		
12									Direc.)			
12												
									GO TO 6			
									50 10 0			
						-		-				
						-						
							-	_				
						_						
						_						
					_							
						<u></u>						
HP - High	d Heave;	GP - Grout	tout	of P	ipe; (CM -	Communication					
Supervis					Insp	ecto	r: JOHN MOTKO					
Company: LRE						Total (Cu. Yd.):						
Total To												



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,11,0

Client:	ANG	ELO'S RECY	CLING									
Project:		DADE CI	TY LANDFII						Injection Point: 22			
Csng	Grou	ut Time	Max.		F	Reason		op				
Depth (ft.)	Start	Finish	Pressure (psi)	Pump Strokes	H	G H	G P	СМ	Remarks			
10	← TOTAL C	ASING DEPTH		40		H		Ī	Can Trase Tench			
1159	1159	1139	200	116				X	Completed			
									Job Completed			
		-										
									SFAT BACK 804			
-												
HP - High	h Pressure; GH - Ground Heave; GP - Gro				t out	of P	ipe; (CM -	Communication			
Supervis	sor:						Insp	ecto	or: JOHN MOTKO			
Company	Company: LRE				Total (Cu. Yd.):							
Total To	Date (Cu. Y	'd.):										



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GROUT MONITORING LOG

Client: Project:	ANG	DADE CI	CLING TY LANDFII					j	Date: 3-1/-01/ Injection Point: 23		
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F	teasor	to ste	op			
(ft.)	Start	Finish	(psi)	Strokes	H	G H	G P	C M	Remarks		
38	← TOTAL CA	ASING DEPTH	63	(2009)					CINTIADE TINCE		
38	1609	1631	140	491					FACTIVIC CKES		
Supervis	or:	LRE	d Heave; (GP - Grout	rout out of Pipe; CM - Communication Inspector: JOHN MOTKO Total (Cu. Yd.): 7.8 +						

H:\djovanovic\Grouting\Grout Monitoring 7 oaks.wpd



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Client:	ANG				Date: 3.5.04 (autinity Injection Point: 23							
Project:		DADE C	ITY LANDFI	LL			(4	11/1	115 m 3 1/- 05			
Csng. Depth	Grou	t Time	Max. Pressure	Pump	F	Reason	n to st	ор				
(ft.)	Start	Finish	(psi)	Strokes	HP	G G C H P M						
	+ TOTAL C	ASING DEPTH	1	产业共和国					STAIT Truck			
22	1217	124/	160						End Truck DRE- (10			
			Keys	7.4					New Truck			
27	1247	1249	140/100	4/	X				0x165			
22	1255	1255	1100 +	1/3	X			X	New Truck ORIUS Completed			
									Go BACK TO 26 (1:			
			-			-						
									4			
			-									
HP - Higi	h Pressure;	GH - Groun	nd Heave;	GP - Grout	out	of P	ipe;	CM -	Communication			
Supervis	sor:						Insp	ecto	r: JOHN MOTKO			
Compan	ompany: LRE							. Yd.)	1: 7.8 + 11.2 = 19.0			
Fotal To	Date (Cu. Y	'd.):		-	e.							



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Client:	ANGELO'S RECYCLINGDADE CITY LANDFILL					Date: 2-8-04									
Project:		DADE CIT	TY LANDFIL						Injection Point:						
Csng.	Grout	Time	Max. Pressure	Pump	R		to sto	op.							
(ft.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks						
30	← TOTAL CA	SING DEPTH	1	135					Continue Truck						
30	1225	12110	140/	459					End Truck Driet	6.4					
									Ktw Teach						
27	1205	1327	180	441					End Tirel DRICT	9.0					
			K879	Marie					1/7W Trick						
22	1355	13 = +	160	21				1	WATER AND GENERA IP 20						
17		12-6	160/	5/			¥	X	CompleTeel	(1.1					
		- Aurio							,						
									Co To 19						
HP - High Pressure; GH - Ground Heave; GP - Grou					out	of P	ipe;	CM -	Communication						
Supervisor:							Insp	ecto	г: ЈОНИ МОТКО						
Company: LRE					Total (Cu. Yd.): 16.5										
Total To Date (Cu. Yd.):															



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Client:	ANG	ELO'S RECY	CLING					ľ	Date: 3-504 Injection Point: 25	
Project:		DADE CI	TY LANDFII	LL					Injection Point: 25	
Csng. Depth	epth Pressure Pump		F	Reason pum	to sto	op q	Remarks			
(ft.)	Start	Finish	(psi)	6-9	H P	GH	G P	C M		
43	← TOTAL C	ASING DEPTH		325					Con Tavell	
47									TISKT PY: NEES	
42									11	_
37	1756	1802	180/	469					End Truck 2	,8
32									Cont Tarell Tight par 100 5 Track Fract Track Flush BRK 0	
32									End Dist	
									,	
		-	-					_		
		1								
								-		
									,	
HP - High	n Pressure;	GH - Groun	d Heave;	GP - Grou	t out	of Pi	ipe; (CM -	Communication	
Supervisor:							Insp	ecto	r: JOHN MOTKO	
Compan			Total (Cu. Yd.): 2.8 +							
Total To	Date (Cu. Y	'd.):			4					



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Client:	ANG	ELO'S RECY	CLING				_	-	Date: 3-804			
Project:							(0)	7111	from 3-5-04			
Csng. Depth (ft.)	Grou	ut Time	Max Pressure	Pump Strokes	F		n to st	op	Remarks			
(11.)	Start	Finish	(psi)	Strokes	H P	G H	G P	C M	Remarks			
	← TOTAL C	ASING DEPTH	R8-15	阿兴等					STEPT TIVE			
32										0		
27	1026	1048	200	461					End Truck Ext	90		
			KEYS	my Sayes					NEW TIVE			
22	1150	1156	200/	126		X			AT I.P. BREST			
17							X		124-	6		
12	1205	1205	200	135		X			Completed	2.1		
									Go TO 24			
HP - High	n Pressure;	GH - Groun	d Heave; (GP - Grout	out	of P	ipe;	CM -	Communication			
Supervis	or:					Insp	ecto	r: JOHN MOTKO				
Compan	company: LRE						Total (Cu. Yd.): 2.8 + 11.6 = 14.4					
Total To	Date (Cu. Y	'd.):										



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Client:	ANG	ELO'S RECY	CLING		Date: 3.3-04 Injection Point: 26							
Project:	·	DADE CIT	TY LANDFIL	<u> </u>			Injection Point: 26					
Csng. Depth	Grou	t Time	Max. Pressure	Pump	R	Reason pum	to sto	ф				
(ft.)	Start	Finish	(psi)	Strokes	НР	G H	G P	C M	Remarks			
60	← TOTAL CA	ASING DEPTH		132					Con Tinue Time			
60	1551	1610	150	4/3					pump out of fuel			
		1622	150	487					pump out of such End Track			
									Flush nex			
60												
									ENLLY			
HP - Higl	h Pressure;	GH - Groun	d Heave; (GP - Grou	tout	of P	ipe; (CM -	- Communication			
Supervis	or:				-,		Insp	ecto	or: JOHN MOTKO			
Compan	y:	LRE				Total	(Cu	Yd.	.):6.6+			
Total To	Date (Cu. Y	d.):										



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Client:	ANG	ELO'S RECY	CLING						Date: 3-1/04				
Project:		DADE CIT	TY LANDFI	LL			Injection Point: 26 Continue from 2-3 a4						
Csng. Depth (ft.)	Grou	it Time	Max. Pressure (psi)	Pump Strokes	F		n to st	ор	Remarks				
(3.7)	Start	Finish	(1)		H P	G H	G P	C M	INCHIBINS.				
	← TOTAL C	ASING DEPTH							576.7 Tiel4				
60	1206	1232	140	485					End Truck BAG = 9.0				
									New Truck 90				
57	1332	/353	140	458				-	End Truck 9.0				
									Go To Point 18				
									Go To Point 18				
HP - Higl	n Pressure;	GH - Ground	d Heave; (GP - Grout	out	of Pi	ipe; (CM -	Communication				
Supervis	or:				-		Insp	ecto	r: JOHN MOTKO				
Compan	y:	LRE	-X		- 1	Total	(Cu	Yd.):6.6+18				
Fotal To	Date (Cu. Y	d.):											



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Client:	ANC		Date: 3-50/						
Project:	ct: DADE CITY LANDFILL (CATION C Injection Point: 26 floa 3 4-04								
Csng. Depth	Grout Time		Max. Pressure	Pump	F	Reasor pum	to sto	op	
(ft.)	Start	Finish	(psi)	Strokes 2-9	H	G H	G P	C M	Remarks
	← TOTAL C	ASING DEPTH		43					CLATIQUE TIME
57	1303	1324	110/	462		-			SICH TRUCK DEKS
				35-487					NEW Treck
52	1334	1400	200	572					End Truck URK ! 10
			C-1014	We lot					NEW Truck
47	1757	1517	200 200	543		-			End Truck But 10
				3-10					New Tires
1/2	16 18	16 23	200/44-	110	X				OFF
37	1,23	113)	1100	113	X				End Truck DIEK: (16
32	14 33	1652	189/	554					End Truck DIEK !
			7	L. STA					NEW Truck
27	1659	1714	200/200		7	X			AT IP BEKT
22	1721	1724	200/40		7				pert
17	1726	1726	400+	325	X	-			(mp)
									GOT 25
		-							
łP - Higl	h Pressure;	GH - Grour	d Heave;	GP - Grout	out	of P	ipe; (CM -	Communication
Supervis	or:	-					Insp	ecto	r: JOHN MOTKO
ompan	y:	LRE				Total	(Cu.	Yd.)	6.5 + 18 + 44 = 68.6
otal To	Date (Cu. \	(d.):							

APPENDIX C

Important Information about Your

Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared solely for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. And no one — not even you — should apply the report for any purpose or project except the one originally contemplated.

Read the Full Report

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

A Geotechnical Engineering Report Is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- · not prepared for your project,
- · not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

 the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure.
- composition of the design team, or
- project ownership.

As a general rule, always inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

subsurface conditions revealed during construction. The geolechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.

A Geotechnical Engineering Report Is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineering report. Reduce that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should never be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, but recognize that separating logs from the report can elevate risk.

Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. Be sure contractors have sufficient time to perform additional study. Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely.* Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform a *geoenviron-mental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else*.

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

Rely, on Your ASFE-Member Geotechncial Engineer for Additional Assistance

Membership in ASFE/THE BEST PEOPLE ON EARTH exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with your ASFE-member geotechnical engineer for more information.



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CONSTRAINTS AND RESTRICTIONS

WARRANTY

Universal Engineering Sciences has prepared this report for our client for his exclusive use, in accordance with generally accepted soil and foundation engineering practices, and makes no other warranty either expressed or implied as to the professional advice provided in the report.

UNANTICIPATED SOIL CONDITIONS

The analysis and recommendations submitted in this report are based upon the data obtained from soil borings performed at the locations indicated on the Boring Location Plan. This report does not reflect any variations which may occur between these borings.

The nature and extent of variations between borings may not become known until construction begins. If variations appear, we may have to re-evaluate our recommendations after performing on-site observations and noting the characteristics of any variations.

CHANGED CONDITIONS

We recommend that the specifications for the project require that the contractor immediately notify Universal Engineering Sciences, as well as the owner, when subsurface conditions are encountered that are different from those present in this report.

No claim by the contractor for any conditions differing from those anticipated in the plans, specifications, and those found in this report, should be allowed unless the contractor notifies the owner and Universal Engineering Sciences of such changed conditions. Further, we recommend that all foundation work and site improvements be observed by a representative of Universal Engineering Sciences to monitor field conditions and changes, to verify design assumptions and to evaluate and recommend any appropriate modifications to this report.

MISINTERPRETATION OF SOIL ENGINEERING REPORT

Universal Engineering Sciences is responsible for the conclusions and opinions contained within this report based upon the data relating only to the specific project and location discussed herein. If the conclusions or recommendations based upon the data presented are made by others, those conclusions or recommendations are not the responsibility of Universal Engineering Sciences.

CHANGED STRUCTURE OR LOCATION

This report was prepared in order to aid in the evaluation of this project and to assist the architect or engineer in the design of this project. If any changes in the design or location of the structure as outlined in this report are planned, or if any structures are included or added that are not discussed in the report, the conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and the conclusions modified or approved by Universal Engineering Sciences.

USE OF REPORT BY BIDDERS

Bidders who are examining the report prior to submission of a bid are cautioned that this report was prepared as an aid to the designers of the project and it may affect actual construction operations.

Bidders are urged to make their own soil borings, test pits, test caissons or other explorations to determine those conditions that may affect construction operations. Universal Engineering Sciences cannot be responsible for any interpretations made from this report or the attached boring logs with regard to their adequacy in reflecting subsurface conditions which will affect construction operations.

STRATA CHANGES

Strata changes are indicated by a definite line on the boring logs which accompany this report. However, the actual change in the ground may be more gradual. Where changes occur between soil samples, the location of the change must necessarily be estimated using all available information and may not be shown at the exact depth.

OBSERVATIONS DURING DRILLING

Attempts are made to detect and/or identify occurrences during drilling and sampling, such as: water level, boulders, zones of lost circulation, relative ease or resistance to drilling progress, unusual sample recovery, variation of driving resistance, obstructions, etc.; however, lack of mention does not preclude their presence.

WATER LEVELS

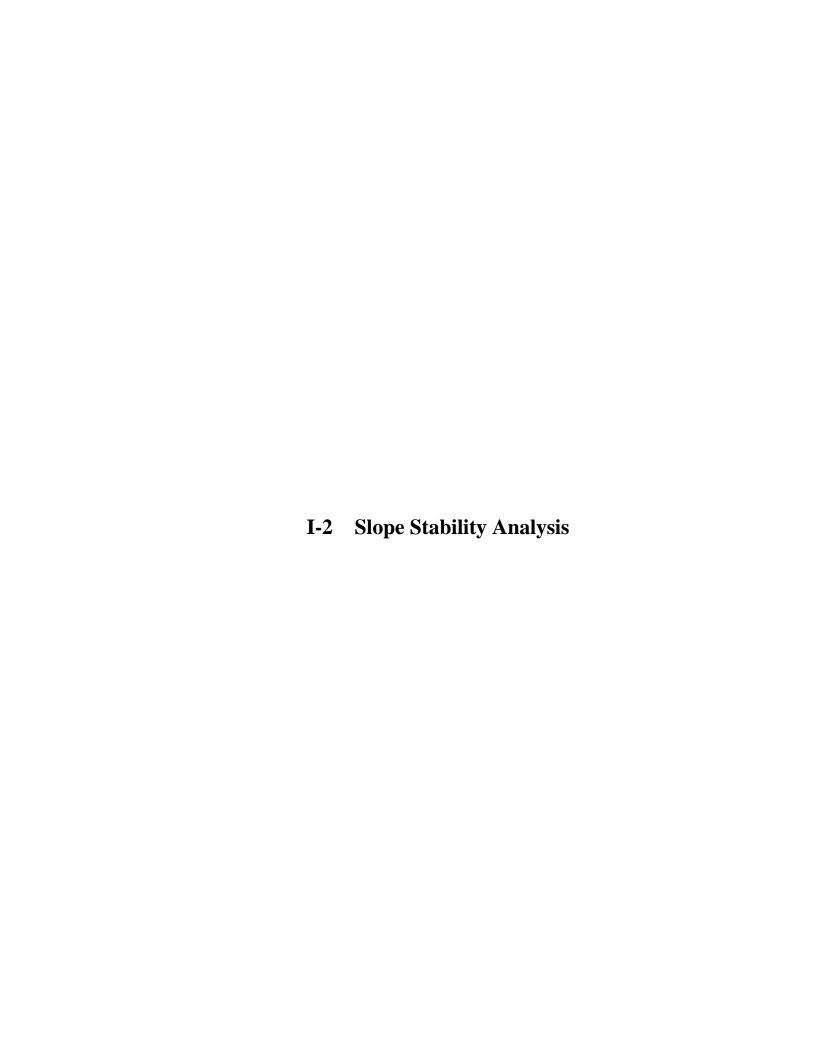
Water level readings have been made in the drill holes during drilling and they indicate normally occurring conditions. Water levels may not have been stabilized at the last reading. This data has been reviewed and interpretations made in this report. However, it must be noted that fluctuations in the level of the groundwater may occur due to variations in rainfall, temperature, tides, and other factors not evident at the time measurements were made and reported. Since the probability of such variations is anticipated, design drawings and specifications should accommodate such possibilities and construction planning should be based upon such assumptions of variations.

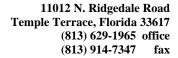
LOCATION OF BURIED OBJECTS

All users of this report are cautioned that there was no requirement for Universal Engineering Sciences to attempt to locate any man-made buried objects during the course of this exploration and that no attempt was made by Universal Engineering Sciences to locate any such buried objects. Universal Engineering Sciences cannot be responsible for any buried man-made objects which are subsequently encountered during construction that are not discussed within the text of this report.

TIME

This report reflects the soil conditions at the time of exploration. If the report is not used in a reasonable amount of time, significant changes to the site may occur and additional reviews may be required.







July 31, 2016 Project No. 16-01-0111.01

Mr. John Locklear, P.G. President Locklear & Associates, Inc. 4140 NW 37th Place, Suite A Gainesville, Florida 32606

RE: Slope Stability, Settlement, and Bearing Capacity Analysis

Enterprise Class III Landfill – Cell 16 Expansion – Response to FDEP RAI No. 1 Dade City, Florida

Dear Mr. Locklear,

Civil Design Services, Inc. (CDS) is submitting the following Slope Stability, Settlement, and Bearing Capacity Analysis Report (Report) to Locklear & Associates, Inc. (L&A) for the Cell 16 Expansion for continued Class III solid waste operations at the Enterprise Class III Landfill (Landfill), located in Dade City, Florida. It is our understanding that the following items are proposed as part of the expansion permit;

- Cell 16 will be constructed with 3(h):1(v) ratio sideslopes from the perimeter maintenance road to the first terrace at EL 125;
- 4(H):1(V) sideslopes will continue from the first terrace to s buildout elevation of Elevation 150 for of the Cell 16 area.
- The bottom of the Cell 16 area will be constructed with a compacted 3-foot clay layer that will be connected with the north end of Cell 15 and the bottom will slope toward the north. Water collected in the Cell 16 area will gradually flow toward the clay lined Pond 3 area located to the north and east of Cell 16.
- Grading as reference the Permit Drawings prepared by Locklear and Associates, Inc. for the Cell 16 Expansion, and revised per FDEP RAI No. 1.

The purpose and limitation of the scope of this Report is to evaluate the above proposed Cell 16 expansion and to evaluate the stability of the waste materials with the proposed geometry, estimate the settlement of the bottom area of the Cells 16 area, and estimate the bearing capacity of the foundation with the Cell 16 area, based upon boring information referenced in this Report. Previous geotechnical and hydrogeological reports, submitted by others, evaluated the subsurface conditions for potential activity in the karst layers beneath the site and are strictly the responsibility of others. Reference the Cell 16 Expansion Permit Application for additional evaluations and recommendations made by others to support the overall Cell 16 expansion.

Reference Documents

The following documents were reviewed and information contained within these reference documents were used as part of the analyses. The reference documents are as follows;

Reference No 1. Universal Engineering Sciences – Geotechnical Exploration dated January 14, 2004.

Reference No 2. Locklear and Associates, Inc. – Angelo's Class III Cell 16 Expansion Permit Application, dated July y 31, 2016.

Slope Stability Model Analysis

L&A prepared the permit modification Plans (Plans) for the Landfill. These Plans were used as the basis for modeling the slope geometry.

The boring logs referenced above were reviewed and similar soil types, with similar SPT N-values, were grouped together for the purpose of modeling. Breaks in soils types or SPT N-values were assigned to layers to differentiate between stronger or weaker soils. This allows for a better representation of failure planes, and thus stability of the foundation, as the failure planes shear through the different layers.

The estimated shear strength for the soils shown in the boring logs is contained in Attachment A.

The waste equipment used in the analyses were a CAT D8T WH dozer; a CAT 826H compactor; and a CAT 740B off-road dump truck. All equipment types are used onsite and/or are representative of typical waste and construction equipment used at landfills. Refer to Attachment B of this Report for equipment loads and manufacturer data.

The seasonal high groundwater table was estimated by L&A to be at EL 72. It is our understanding the previous measurements in local peizometers in the northeast corner of the Facility were not representative of the groundwater and may have been perched water tables.

Two sets of Slope Stability Models were completed as follows;

- ❖ Cell 16 Expansion The permit application is for the expansion of the Cell 16 area and models were prepared to demonstrate stability for the expansion.
 - Refer to Figure 1 Cell 16 Expansion, Boring Locations, and Cross Section
 - Refer to Figure 2 East/West Model Cross Section
 - Refer to Figure 3 North/South Model Cross Section

A review of the above reference information and the modeling assumptions made above are reasonable for completing the slope stability analyses prepared by CDS for the proposed expansion.

Slope Stability Analysis

PCSTABL was used to model and estimate slope stability of the Landfill during operational conditions using typical site waste equipment and waste filling during operations and final buildout. Both BLOCK and CIRCULAR failure modes were evaluated. BLOCK failure modes are used to evaluate sliding failure planes and

CIRCULAR failure modes are used to evaluate shallow and deep rotational stability of the waste and foundation soils.

All cross sections were modeled with, and without, temporary waste equipment loading conditions.

All equipment loads were modeled at the crest of the slope, a position that would induce the greatest stress on the slopes and thus generate the lowest Factor of Safety.

A typical input file of the slope stability models for the BLOCK and CIRCULAR searches has been placed prior to the graphical output of the models. In each scenario, the profile and failure search routines were adjusted to determine the lowest Factor of Safety.

The graphical output files of the slope stability analyses are contained in the following attachments;

- Attachment C East/West Section Cell 16 Expansion CIRCULAR & BLOCK Analysis
- Attachment D North/South Section Cell 16 Expansion CIRCULAR & BLOCK Analysis

Summary of Slope Stability Model Results

Table 1 summarizes the slope stability mode results. As shown in Table 1, the slopes are stable and have a factor of safety above 1.5.

Table 1. Summary of Slope Stability Models

Description		Configuration	West/Ea	st Section	North/South Section		
Cell 16			Circular	Block	Circular	Block	
	EL 150	Waste Only	2.2	2.9	2.5	3.1	
		CAT D8	2.2	2.7	2.1	2.5	
		CAT 826H	2.2	2.9	2.5	2.8	
		CAT 740B	2.2	2.6	2.3	2.6	

As shown in Table 1, the overall slope stability scenerios meet the minimum Factors of Safety of 1.5 and are therefore considered stable.

Settlement Estimates

Settlement of the foundation soil beneath the expansion was evaluated. The proposed drainage pattern is toward the north, sloping downward from Cell 15, northward across Cell 16, and toward Pond 3.

Settlement of the soils beneath the Cell 16 area will be a function of soil types, soil compressibility, and the change in stress induced on the soils after the overburden is removed and waste is added. Note: the Landfill is being excavated to form the bottom of the cells. In some cased, some of the soils shown in the boring have already been excavated; therefore, settlement estimates in these layers was not computed.

Settlement estimates were computed starting on the high end of Cell 16 at the interface with Cell 15 (using Boring B-22), and in the middle (using Boring B-26), and on the northside (using Boring B-20). Typical soil properties based upon soil types, relative in-situ density, and consolidation coefficients were made at each location and for each soil layer group.

Contained in Attachment E are the soil properties and settlement estimates at each location. Listed below in Table 2 is a summary of the estimated settlement.

Table 2. Settlement Summary

Boring ID	Location	Settlement	Drainage	Comment
		(ft)	Pattern	
B-22	Southside of Cell 16	0.54	Maintains slope	Top of the Clay Barrier is at EL 80.3;
			toward the north	0.54 ft of settlement; Top of Clay is
				at EL 79.76
B-26	Middle of Cell 16	1.07	Maintains slope	Top of the Clay Barrier is at EL 79.8;
			toward the north	1.07 ft of settlement; Top of Clay is
				at El 78.73.
B-20	Northside of Cell 16	0.49	Maintains slope	Top of the Clay Barrier is at EL
			toward the north	79.11.; 0.49 ft of settlement; Top of
				Clay at north edge is at El 78.62.

As shown in Table 2, the overall drainage is maintained toward the north.

Bearing Capacity Estimation

Bearing capacity is the capacity of the soils to support loads applied to the foundation soils. The bearing capacity of soil below the landfill disposal area is the maximum average contact loading, or pressure, exerted on the bottom of the landfill disposal cells and the loading (stress) on the foundation soils which should not produce a shear failure in the soil. This is a function of soil layers, waste unit weight, and depth of waste at that location.

To estimate the bearing capacity of the soils below the landfill disposal cell, the unit weight of the Class III waste was incrementally increased until the Factor of Safety reduced below the original FS in the Slope Stability Section above. Different unit weights for the waste materials were evaluated.

The results of the modeling indicate an increase in the unit weight for waste from 50 pounds per cubic foot (pcf) to 70 pcf for does not results in a decrease from the East/West or North/South slope stability models with a FS of 2.2 and 2.5, respectively. Based upon the model results, this would be representative of the ultimate bearing capacity of the foundation. Refer to Attachment F for bearing capacity models.

At the crest of the expansion, at EL 150, the underlying base of disposal Cell 16 at approximately El 79 (+/-), thus 71 feet of waste will be placed over the landfill foundation at this location. The ultimate bearing capacity (maximum bearing capacity) is therefore estimated to be 4,970 pounds per square foot (70 pcf * 71 feet). The proposed loading on the landfill foundation is only estimated to be 3,550 psf (50 pcf * 71 feet); therefore, the proposed expansion has sufficient additional foundation bearing capacity to accommodate the proposed design.

Conclusions

- ➤ Based upon the PCSTABL Model results, and the assumptions stated in this Report, a minimum Factor of Safety of 1.5 or greater was achieved for all waste configurations.
- The proposed expansions overall drainage pattern, sloping toward the north is maintained after settlement.
- Based upon the model results, the foundation soils beneath have sufficient bearing capacity strength for the proposed landfill modifications.

Please call the undersigned if you have any questions.

Sincerely,

Civil Design Services, Inc.

Joseph H. O'Neill, P.E.

Vice President

Attachment A – Soil Strength Estimates

Attachment B – Equipment Loading Data

Attachment C - E/W Section - Cell 16

Attachment D - N/S Section - Cell 16

Attachment E- Settlement Estimates

Attachment F- Bearing Capacity Models

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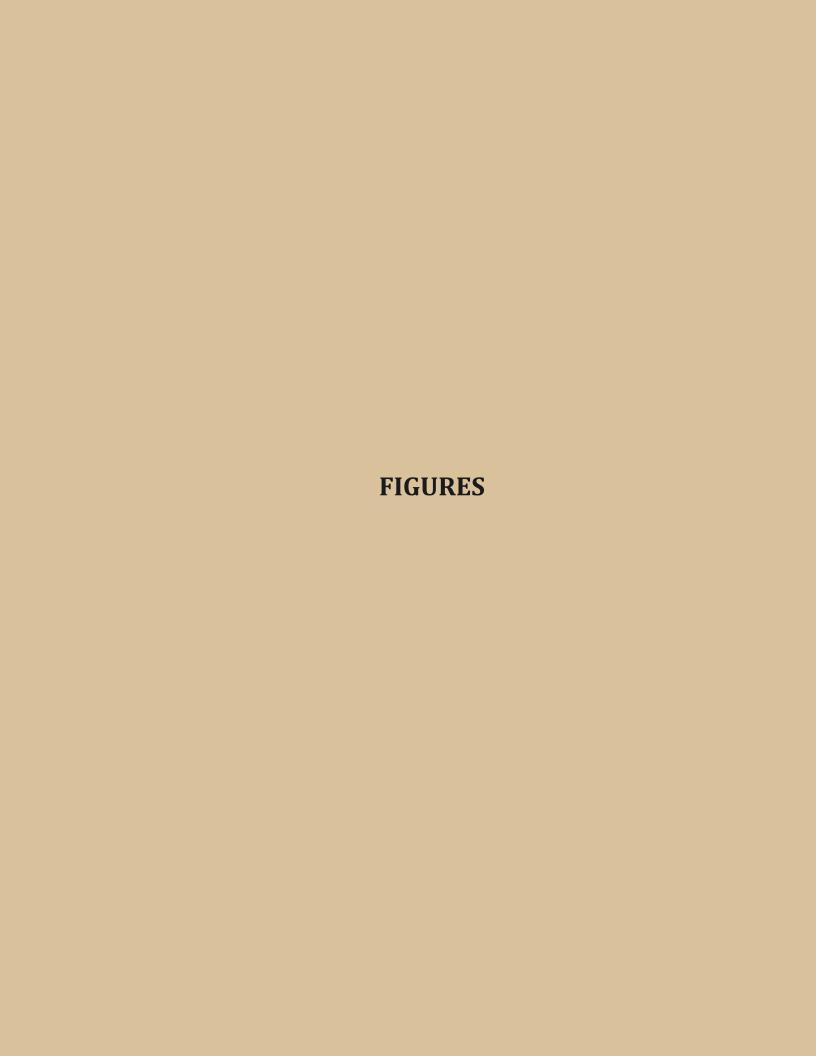
Joseph H. O'Neill, P.E.

Civil Design Services, Inc.

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Certificate of Authorization 28923



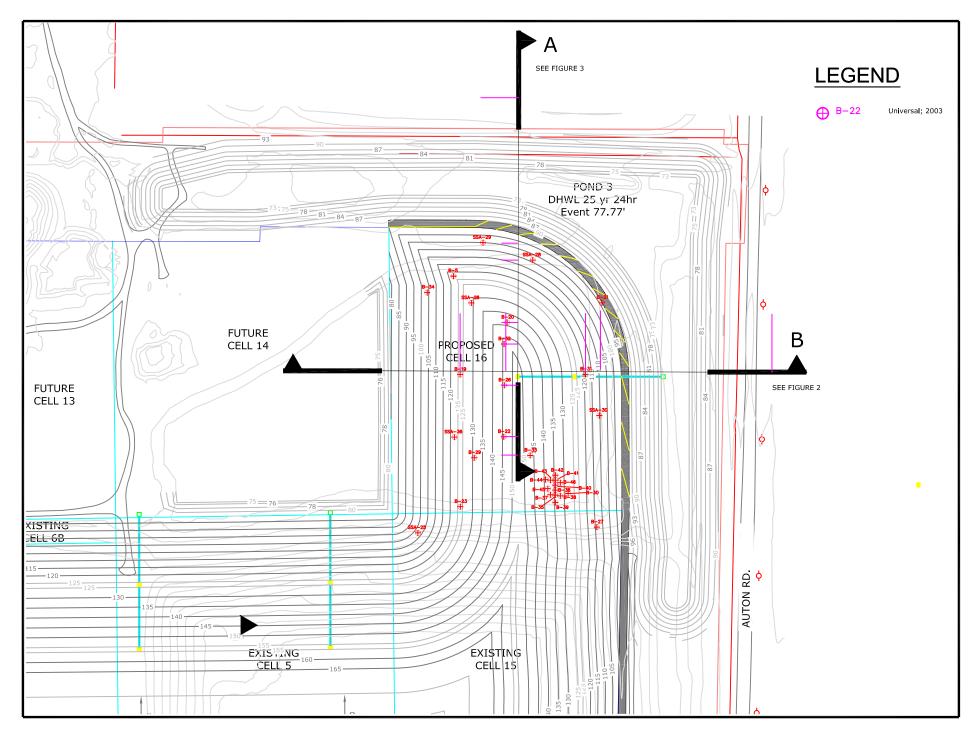
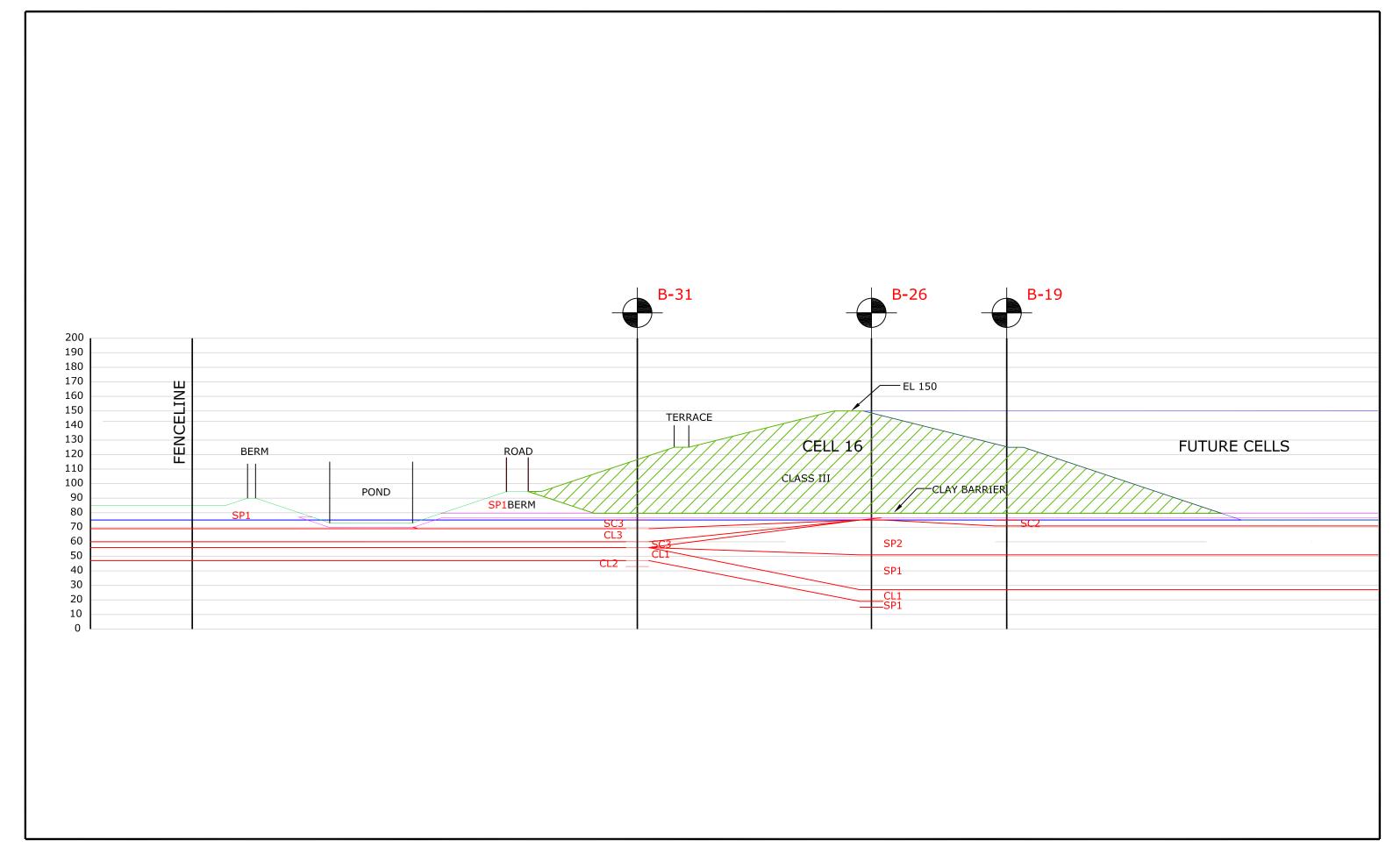
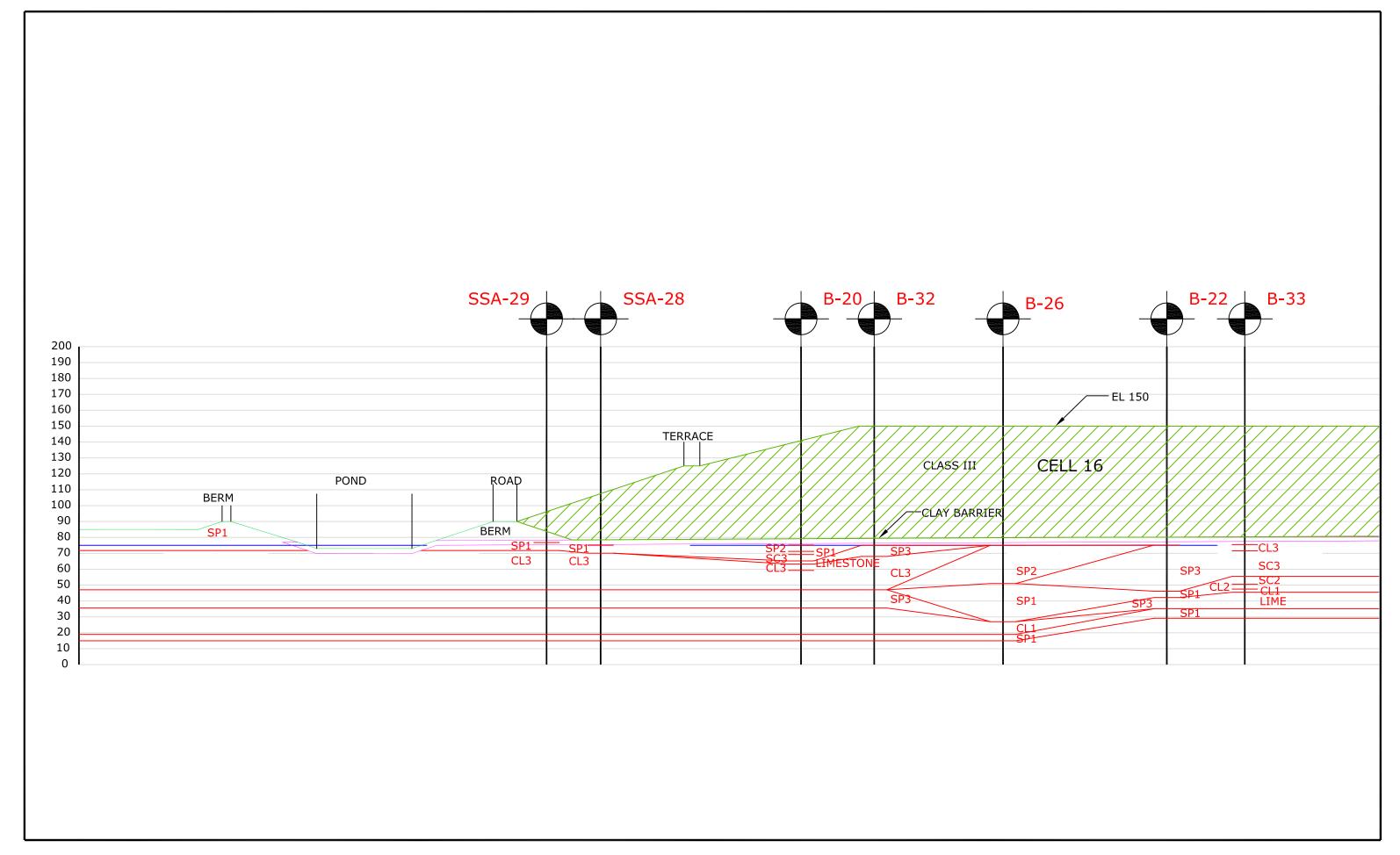
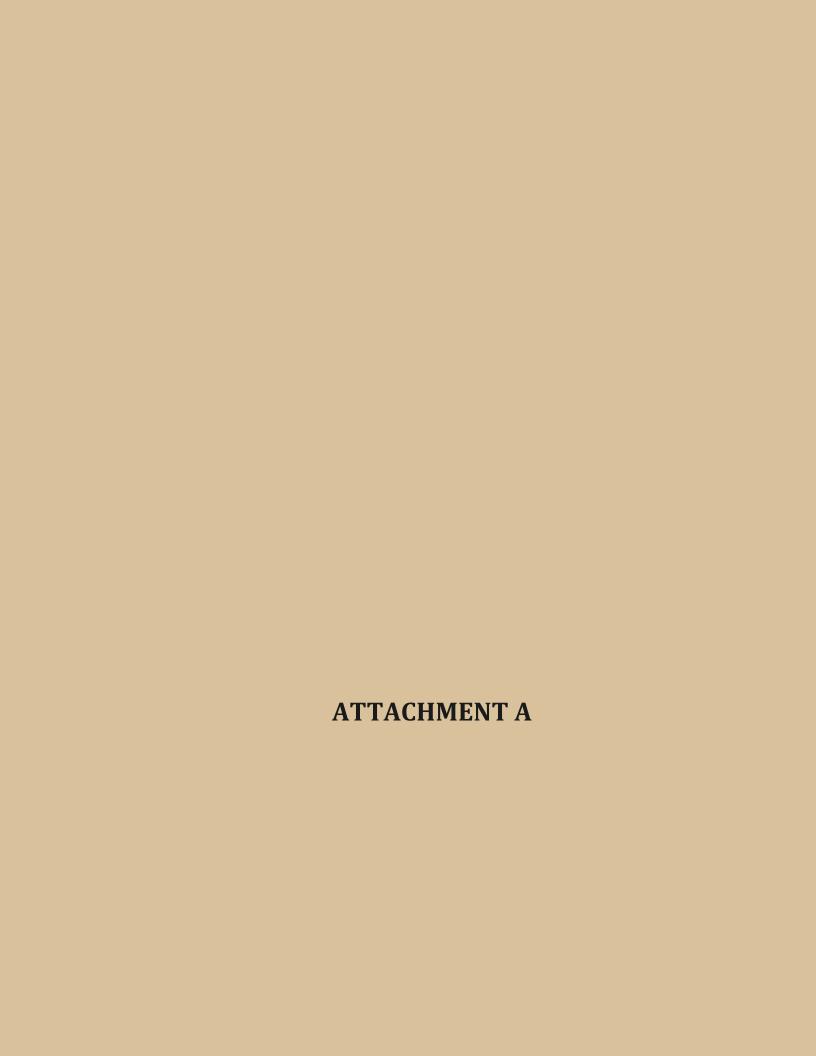


FIGURE 1. CELL 16 EXPANSION, BORING LOCATIONS, and SECTIONS







Soil Properties - Strength for Slope Stability

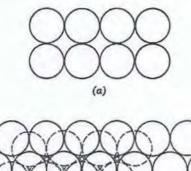
ınds, Silty Sands, (Clays				
SPT Blow Count	Description	Dr*	Dr avg	SPT Blow Count	Description	Dr avg	References:	1) SPT vs Soil Relative Density
								" Soil Mechanics; 1969 Lambe and Whitman, Table 3.3"
0-4	Very Loose	0-15	10	<2	Very Soft	10		
4-10	Loose	15-30	20	2-4	Soft	20		2) SPT vs Cohesive Soil Shear Strength, Soil Properties
10-30	Medium	35-65	50	4-8	Medium	50		" Soil Mechanics; 1969 Lambe and Whitman, Table 7.4"
30-50	Dense	65-85	75	8-15	Stiff	75		
>50	Very Dense	85-100	90	15-30	Very Stiff	90		
				>30	Hard	100		3) SPT vs Cohesionless Soil Shear Strength - "Principles of
								Geotechnical Engineering, 1985, B. Das, Table 13.3"

Soils for Slope Sta	bility Models						
					Shear Strengh Properties		
Model Soil ID	Soil Types	SPT N	Dr	Description	phi	С	Comment
1	SP1	0-4	Very Loose	Poorly Grade Sands, Fine Sand, Silty Sand	26	0	Model using "low strength" for conservative results
2	SP2	4-10	Loose		30	0	
3	SP3	10-30	Medium		34	0	
4	SC1	0-4	Very Loose	Very fine sands, sands with clays	26	0	Model using "low strength" for conservative results
5	SC2	4-10	Loose		30	0	
6	SC3	10-30	Medium		34	0	
7	CL1	0-4	Very Loose	clays with sand and silts, low PI index	28	0	Model using "low strength" for conservative results
8	CL2	4-10	Loose		30	0	Transition from Sands to Clays
9	CL3	10-30	Medium		34	0	
10	CH1	<2	Very Soft	Clays with High PI index	0	100	Model using "low strength" for conservative results
11	CH2	2-4	Soft		0	750	
12	CH3	4-8	Medium		0	1000	
13	SP 2		Loose-med	Perimeter Berm - Sandy to allow for flow	30	0	sandy soils - typ medium compaction
14	SP2		Loose-med	Closure Cap	30	0	Sandy to Sandy Clay soils available onsite
15	CL 3		Loose-med	Compacted Clay Barrier	30	0	Compacted sandy-clay - typ med to high strength
16	Waste			Class III waste	35	0	Typically higher strength - model low at 35
17	Foundation	>30-40	Dense	Limetone, fractured limestone	40	0	Hard, high strength soils - failure planes above this layer

Cohesionless Soils - S	SP, SP/SM. SM.	SC, (Transit	ion to CL)	Cohesive Soils -	CL, CH		
SPT N-values	Estimated	Modeled		SPT N-values	Estimated		Modeled
0-5	26-30	26-28	low SPT N values; low density, weak shear strenght layer	<2	< .25 tsf	<500 psf	100
5-10	28-35	30		2-4	0.25-0.50 tsf	500-1,000	750
10-30	35-42	34		4-8	0.50-1.00 tsf	1,000-2,000	1000
30-50	38-46	40		8-15	1.00-2.00 tsf	2,000-4,000 psf	
* Reference 3				15-30	2.00-4.00 tsf	4,000-8,000 psf	
				>30	>4.00 tsf	>8,000 psf	
				* Reference 2			

Reference 1 Soil Stength

Ch. 3 Description of an Assemblage of Particles



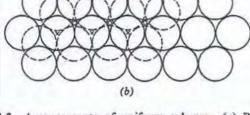


Fig. 3.2 Arrangements of uniform spheres. (a) Plan and elevation view: simple cubic packing. (b) Plan view: dense packing. Solid circles, first layer; dashed circles, second layer; o, location of sphere centers in third layer: face-centered cubic array; ×, location of sphere centers in third layer: close-packed hexagonal array. (From Deresiewicz, 1958.)

these simple packings can be computed from the geometry of the packings, and the results are given in Table 3.2.

This table also gives densities for some typical granular soils in both the "dense" and "loose" states. A variety of tests have been proposed to measure the maximum and

Table 3.2 Maximum and Minimum Densities for Granular Soils

	Void Ratio		Porosit	y (%)	Dry Unit Weight (pcf)	
Description	e_{max}	e_{\min}	n_{max}	n_{\min}	7d min	Ydmax
Uniform spheres	0.92	0.35	47.6	26.0	_	_
Standard Ottawa						
sand	0.80	0.50	44	33	92	110
Clean uniform						
sand	1.0	0.40	50	29	83	118
Uniform inorganic					100	
silt	1.1	0.40	52	29	80	118
Silty sand	0.90	0.30	47	23	87	127
Fine to coarse						
sand	0.95	0.20	49	17	85	138
Micaceous sand	1.2	0.40	55	29	76	120
Silty sand and	1000					100
gravel	0.85	0.14	46	12	89	146

B. K. Hough, Basic Soils Engineering. Copyright © 1957, The Ronald Press Company, New York.

minimum void ratios (Kolbuszewski, 1948). The test to determine the maximum density usually involves some form of vibration. The test to determine minimum density usually involves pouring oven-dried soil into a container. Unfortunately, the details of these tests have

not been entirely standardized, and values of the maximum density and minimum density for a given granular soil depend on the procedure used to determine them. By using special measures, one can obtain densities greater than the so-called maximum density. Densities considerably less than the so-called minimum density can be obtained, especially with very fine sands and silts, by slowly sedimenting the soil into water or by fluffing the soil with just a little moisture present.

The smaller the range of particle sizes present (i.e., the more nearly uniform the soil), the smaller the particles, and the more angular the particles, the smaller the minimum density (i.e., the greater the opportunity for building a loose arrangement of particles). The greater the range of particle sizes present, the greater the maximum density (i.e., the voids among the larger particles can be filled with smaller particles).

A useful way to characterize the density of a natural granular soil is with relative density D_r, defined as

$$D_r = \frac{e_{\text{max}} - e}{e_{\text{max}} - e_{\text{min}}} \times 100\%$$

$$= \frac{\gamma_{d \text{max}}}{\gamma_d} \times \frac{\gamma_d - \gamma_{d \text{min}}}{\gamma_{d \text{max}} - \gamma_{d \text{min}}} \times 100\% \quad (3.1)$$

 e_{\min} = void ratio of soil in densest condition

 $e_{\text{max}} = \text{void ratio of soil in loosest condition}$

e = in-place void ratio

where

 $\gamma_{d \max} = dry \text{ unit weight of soil in densest condition}$

 $\gamma_{d \min}$ = dry unit weight of soil in loosest condition

 γ_d = in-place dry unit weight

Table 3.3 characterizes the density of granular soils on the basis of relative density.

===	y Description	Table 3.3 Densit
	Descriptive Term	Relative Density (%)
	Very loose	0-15
MOISTURE TE	Loose	15-35
	Medium	35-65
Mi	Dense	65-85
W= MW	Very dense	85-100

Values of water content for natural granular soils vary from less than 0.1% for air-dry sands to more than 40% for saturated, loose sand.

Typical Values of Phase Relationships for Cohesive Soils

The range of values of phase relationships for cohesive soils is much larger than for granular soils. Saturated sodium montmorillonite at low confining pressure can exist at a void ratio of more than 25; saturated clays

Table 7.4 Standard Penetration Test

Relative of Sa		Strength of Clay				
Penetration Resistance N (blows/ft)	Relative Density	Penetration Resistance N (blows/ft)	Unconfined Compressive Strength (tons/ft²)	Consistency		
0-4	Very loose	<2	<0.25	Very soft		
4-10	Loose	2-4	0.25-0.50	Soft		
10-30	Medium	4-8	0.50-1.00	Medium		
30-50	Dense	8-15	1.00-2.00	Stiff		
>50	Very dense	15-30	2.00-4.00	Very stiff		
		>30	>4.00	Hard		

In certain countries, such as Holland, subsoil conditions are such that penetration testing has proved to be a relatively reliable technique. More sophisticated techniques [such as the friction jacket cone (Begemann,

1953)] have been widely used.

The vane test has proved to be a very useful method of determining the shear strength of soft clays and silts. Figure 7.6 shows various sizes and shapes of vanes which have been used for field testing. The vane is forced into the ground and then the torque required to rotate the vane is measured. The shear strength is determined from the torque required to shear the soil along the vertical and horizontal edges of the vane.

As later chapters in this book will show, a proper subsoil investigation should include the determination of water pressure at various depths within the subsoil. Methods of determining pore water pressure are discussed in Part IV. Part IV also notes how the permeability of a subsoil can be estimated from pumping tests.

Various load tests and field compaction tests may be highly desirable in important soil projects. In this type of test, a small portion of the subsoil to be loaded by the prototype is subjected to a stress condition in the field which approximates that under the completed structure. The engineer extrapolates the results of the field tests to predict the behavior of the prototype.

7.7 SUBSOIL PROFILES

Figures 7.7 to 7.17 present a group of subsoil profiles and Table 7.5 gives some information on the geological history of the various profiles. The purposes of presenting these profiles are to:

- Indicate how geological history influences soil characteristics.
- 2. Give typical values of soil properties.

- Show dramatically the large variability in soil behavior with depth.
- 4. Illustrate how engineers have presented subsoil data.

Three considerations were used in the selection of the profiles: first, examples were chosen with different types of geological history; second, most of the profiles are ones for which there are excellent references giving considerably more detail on the characteristics of the soil and engineering problems involved with the particular profile; and finally, most of the profiles selected have been involved in interesting and/or important soil engineering projects.

Some of the soil characteristics shown in the profiles have already been described in this book. These characteristics include water content, unit weight, void ratio, porosity, Atterberg limits, and particle size. Other characteristics, particularly those referring to strength and compressibility, will be discussed in detail in later portions of this book. Reference will then be made back to these profiles.

The profiles illustrate many concepts presented in the preceding parts of this book; some of them are discussed in the remaining part of this section.

Stress History

In a normally consolidated sedimentary soil both the void ratio and water content decrease with depth in the profile, and the strength therefore increases. This characteristic is illustrated in several of the profiles, e.g., the Norwegian marine clay (Fig. 7.7), the Thames Estuary clay (Fig. 7.10), and the Canadian clay (Fig. 7.11). The London clay is overconsolidated since it was compressed by a greater overburden than now exists. Erosion removed some of the original overburden. As would be expected, the overconsolidated London clay does not

43.5 Correlations for Standard Penetration Test

Table 13.3 Approximate Relation Between Corrected Standard Penetration Number, Angle of Friction, and Relative Density of Sand

Corrected standard penetration number, N	Relative density, D_r (%)	Angle of friction, ϕ (degrees)
0-5	0-5	26-30
5-10	5-30	28-35
10-30	30-60	35-42
30-50	60-95	38-46

Refernce No. 3 Soil Strength

The standard penetration number is a very useful guideline in soil exploration and assessment of subsoil conditions, provided that the results are interpreted correctly. Note that all equations and correlations relating to the standard penetration numbers are approximate. Since soil is not homogeneous; a wide variation in the N-value may be obtained in the field. In soil deposits

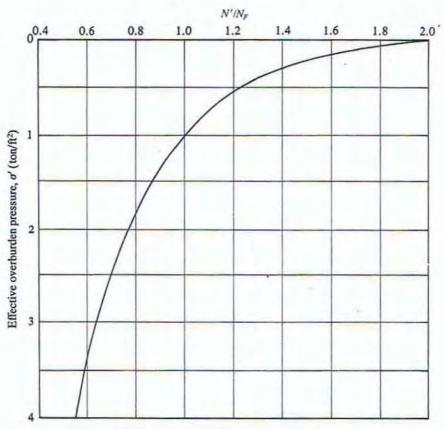
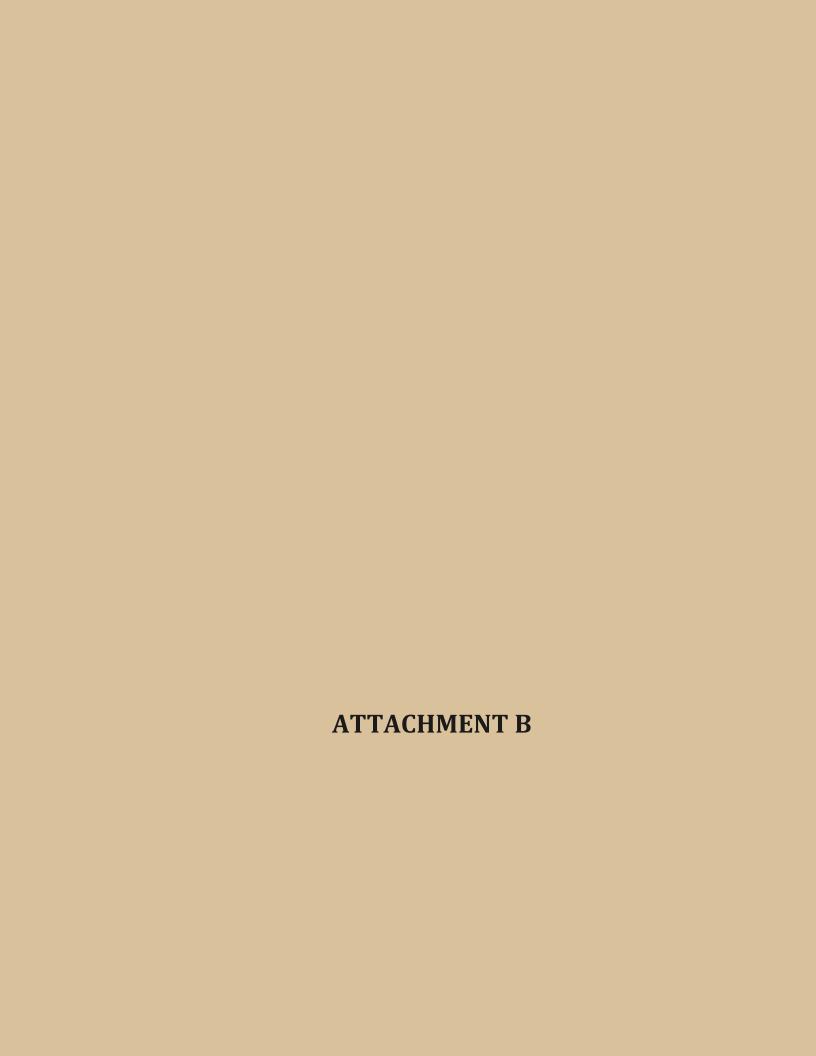


Figure 43.41 Variation of N'/N_F with vertical effective stress, σ' (after Peck, Hanson, and Thornburn, 1974)

verburden presrected standard sands.





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Project Name

Angleos Recycling and Disposal Facility

Class III Modification 41111 Enterprise Road Dade City, Florida 33525-1589

Slope Stability Evaluation

Estimated Equipment Surface Loads

Equipment Surface Loads

Operations and Closure

CAT 8T WH Dozer



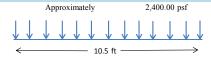
91,270.0 lbf Equipment Weight (Operating) = Weight per Track = 45,635.0 lbf (2 tracks) Load = Area = Track Contact Area 5,554.0 in²

> (both tracks) 2,777.0 in² Per Track

Track Length = 10.5 ft Surface Loading

45,635.0 lbf 2,777.0 in2 Contact Pressure (Force/Area) = 16.43 psi 2,366.38 psf

LOADING PATTERN



CAT 826H Compactor



Equipment Weight (Operating) = 81,498.0 lbf Weight per Drum = 20,374.5 lbf (4 drums)

> Drum Width = 3.94 ft Drum Diameter = 5.03 ft Drum Radius = 2.515 ft





Assumption on Wheels

73.51 degrees (from CADD) Drum Length on Ground L = 3.23 ft <

Drum Width = 3.94 ft Drum Length on Ground L = 3.23 ft Area of Each Drum = 12.71 sf

Distance Centerline to Centerline Drum = 12.1 ft Surface Loading

6 in Wheel pentration into waste (compacted)

Load = 20,374.5 lbf 12.7 sf Area = Contact Pressure (Force/Area) = 1,602.61 psf

LOADING PATTERN



1,700.00 psf Approximately

Equipment Surface Loads



CAT 740B 17.0 19.25

Operations and Closure

Fully Loaded

Equipment Weight (Operating) = 165,311.0 lbf

50,977.0 lbf per tire ===> 25.488.5 lbf Front Axle 57,997.0 lbf per tire ===> 28,998.5 lbf Center Axle Rear Axle 56,335.0 lbf per tire ===> 28,167.5 lbf 165,309.0 lbf

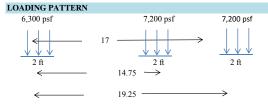
(negligible difference of 2 lbf)

Tires 29R 25 Contact Area

Tires (Contact Area) 4.049 ft^2 583 in² 30.4 in wide Front Axle 4.049 ft² Center Axle 583 in² 19.2 length Rear Axle 583 in² 4.049 ft^2

Pressure

Front Axle Load per axle/area 6,295.6 psf (Say 6,300 psf) 43.7 psi 49.7 psi 7,162.6 psf (Say 7,200 psf) Load per axle/area Center Axle 48.3 psi 6,957.3 psf (Say 7,000 psf) Rear Axle Load per axle/area





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CATERPILLAR D8R WHA CRAWLER TRACTOR

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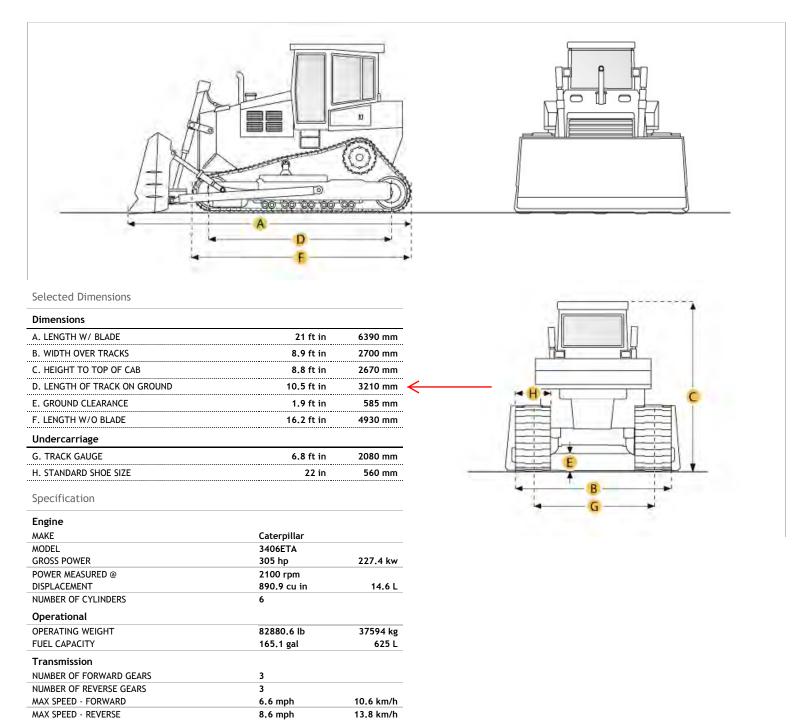
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D8T WH (TIER 4 INTERIM/STAGE IIIB)

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1 of 2

SPECIFICATIONS

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The Cat® D8T Waste Handler has earned a reputation for best-in-class versatility, productivity and resale value. Landfill customers choose the D8T WH because it excels at multiple tasks from pushing trash and spreading cover to cell construction and closing. Cat Waste Handlers are designed and built from the frame up to handle the demands of landfill work – and they do it with industry leading comfort and reliability. The D8T WH meets U.S. Tier 4 Interim/EU Stage IIIB emission standards.

ENGINE UNITS:

Engine Model	Cat® C15 ACERT™
Flywheel Power	310.0 hp
Bore	5.4 in
Stroke	6.75 in
Displacement	928.0 in3
Emissions	U.S. Tier 4 Interim/EU Stage IIIB
Global Emissions	U.S. Tier 4 Interim/EU Stage IIIB
Gross Power – ISO 14396	318.0 hp
Gross Power – ISO 14396 (DIN)	322.0 hp
Gross Power – SAE J1995	348.0 hp
Net Power – EU 80/1269	310.0 hp
Net Power – ISO 9249	310.0 hp
Net Power – ISO 9249 (DIN)	314.0 hp
Net Power – SAE J1349	310.0 hp
SERVICE REFILL CAPACITIES	
Cooling System	20.3 gal
Engine Crankcase*	10.0 gal
Final Drives (each)	3.3 gal
Hydraulic Tank	19.8 gal
Pivot Shaft Compartment	10.6 gal
Powertrain	41.0 gal
Roller Frames (each)	17.2 gal
Fuel Tank	170.0 gal

WEIGHTS

Operating Weight	85650.0 lb	
Operating Weight – LGP WHA	91270.0 lb	
Operating Weight – SU Blade WHA	85650.0 lb	
Shipping Weight – LGP WHA	77840.0 lb	
Shipping Weight – WHA	72220.0 lb	
NDERCARRIAGE		
Track Gauge	82.0 in	
Track Gauge – LGP	92.0 in	
Length of Track on Ground	10.5 ft	
Ground Contact Area	5554.0 in2	
Track Rollers/Side	8	
Ground Clearance	24.3 in	
Ground Contact Area – LGP	9576.0 in2	
Grouser Height	3.0 in	
Number of Carrier Rollers	1 per side (optional)	
Pitch	8.5 in	
Shoe Type	Moderate Service	
Shoes/Side	44	
Width of Shoe	24.0 in	
Width of Shoe – LGP	38.0 in	
BLADES		
Capacity (SAE J1265)	26.1 yd3	
Capacity (SAE J1265)	32.4 yd3	
Capacity (SAE J1265)	27.6 yd3	



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CATERPILLAR 826H COMPACTOR

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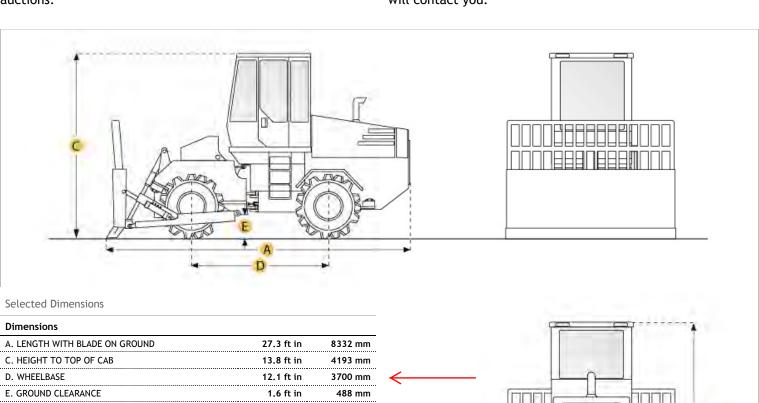
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Ε.	GROUN	D CLEA

FRONT WHEELS DRUM DIAMETER

REAR WHEELS DRUM DIAMETER

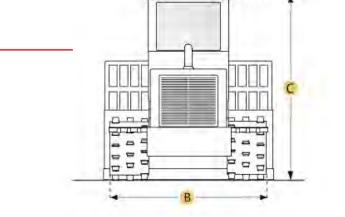
REAR WHEELS DRUM WIDTH

A. LENGTH WITH BLADE ON GROUND	27.3 ft in	8332 mm
C. HEIGHT TO TOP OF CAB	13.8 ft in	4193 mm
D. WHEELBASE	12.1 ft in	3700 mm
E. GROUND CLEARANCE	1.6 ft in	488 mm
	·····	

Specification		
Engine		
MAKE	Caterpillar	
MODEL	C15 diesel with ACER	T Technology
GROSS POWER	401 hp	299 kw
NET POWER	354 hp	264 kw
DISPLACEMENT	927.6 cu in	15.2 L
Operational		
OPERATING WEIGHT	81498 lb	36966.9 kg
FUEL CAPACITY	177.5 gal	672 L
HYDRAULIC SYSTEM FLUID CAPACITY	23.3 gal	88 L
ENGINE OIL CAPACITY	9 gal	34 L
COOLING SYSTEM FLUID CAPACITY	21.7 gal	82 L
TRANSMISSION FLUID CAPACITY	16.4 gal	62 L
Transmission		
NUMBER OF FORWARD GEARS	2	
NUMBER OF REVERSE GEARS	2	
MAX SPEED	6.6 mph	10.6 km/h
Wheels		
FRONT WHEELS DRUM WIDTH	47.2 in	1200 mm

60.3 in

47.2 in



1532 mm

1200 mm

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826H

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826H - 2011, Global Landfill Compactors

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SPECIFICATIONS

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Caterpillar put the first 826 landfill compactor to work in 1978. Since then, customers like you have helped us improve the safety, reliability and productivity of this very popular machine. Our H Series model has enhanced visibility and comfort from a new ergonomic cab. Operators have greater line of sight to areas around the machine, and with CAES installed, the 826H has the ability to be more efficient, lowering your operating costs.

ENGINE UNITS: US

US METRIC

:2)

at 826H Landfill Compactor Caterpillar	Page 2
Gross Power	401.0 hp
Net Power	354.0 hp
Engine Model	Cat® C15 ACERT™
Flywheel Power	354.0 hp
Torque Rise	19.0 %
Bore	5.4 in
Stroke	6.7 in
Displacement	927.56 in3
Peak Torque – Gross	1387.0 ft-lb
FRANSMISSION	
Forward 1	3.6 mph
Forward 2	6.03 mph
Reverse 1	4.1 mph
Reverse 2	6.59 mph
HYDRAULIC SYSTEM	
Vane Pump Output @ 2,000 rpm and 6900 kPa (1,000 psi)	93.0 gal/min
Relief Valve Setting	3506.29 psi
Lift Cylinder Bore x Stroke	120.65 mm × 915 mm (4.74 in × 36.02 in)
AXLES	
Front	Planetary – Fixed
Oscillating Rear	±5°
BRAKES	
Standards	Meet OSHA, SAE J1473 DEC84, ISO 3450:1985 standards

WHEELS - CHEVRON-PATTERN, CHOPPER BLADES

WHEELS - CHEVRON-PATTERN, CHOPPER BLADES	
Drum Width	3.94 ft
Drum Diameter	5.03 ft
Diameter with Blades	6.07 ft
Blades per Wheel	24
STRAIGHT BLADE	
Capacity	17.0 yd3
Width Over End Bits	14.77 ft
Moldboard Length	14.14 ft
Height	6.23 ft
U-BLADE	
Capacity	21.84 yd3
Height	6.81 ft
Moldboard Straight Length	6.81 ft
Moldboard U-Length	4.09 ft
U-Angle	25°
Width Over End Bits	14.43 ft
SEMI U-BLADE	
Capacity	18.97 yd3
Height	6.43 ft
Moldboard Semi U-Length	1.51 ft
Moldboard Straight Length	11.92 ft
Semi U-Angle	25°
Width Over End Bits	14.73 ft

SERVICE REFILL CAPACITIES

Fuel Tank	177.52 gal
Cooling System	21.66 gal
Crankcase	8.98 gal
Transmission	16.38 gal
Differentials and Final Drives – Front	23.78 gal
Differentials and Final Drives – Rear	23.78 gal
Hydraulic Tank	23.25 gal
WEIGHTS	
Operating Weight	81498.0 lb
САВ	
ROPS/FOPS	Meets SAE and ISO standards
SOUND PERFORMANCE	
Standards	Meet ANSI/SAE and ISO standards
DIMENSIONS (APPROXIMATE)	
Center Line of Rear Axle to Hitch	7.46 ft
Width over Wheels	12.5 ft
Width over Endbits (Blade)	14.77 ft
Turning Radius – Inside	10.57 ft
Turning Radius – Outside	24.06 ft
HYDRAULIC STEERING SYSTEM	
Piston Pump Output @ 2,000 rpm and 7000 kPa (1,015 psi)	49.0 gal/min
Relief Valve Setting	3499.0 psi



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CATERPILLAR 740B ARTICULATED DUMP TRUCK

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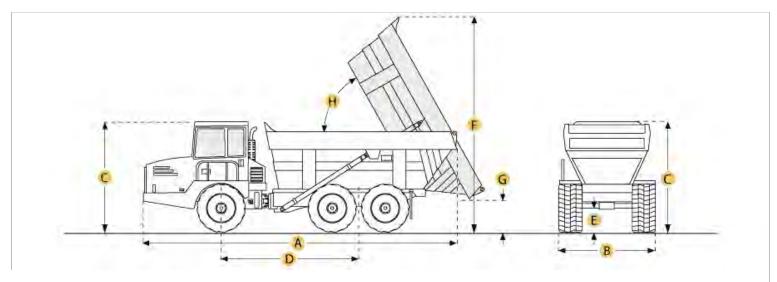
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Selected Dimensions

Dimensions		
A. OVERALL LENGTH	36.1 ft in	11000 mm
B. OVERALL WIDTH	12.4 ft in	3770 mm
C. OVERALL HEIGHT	13,3 ft in	4039 mm
D. WHEELBASE	17,2 ft in	5229 mm
E. GROUND CLEARANCE	1.9 ft in	577 mm
F. DUMP HEIGHT	23,3 ft in	7092 mm
G. DUMP GROUND CLEARANCE	2.3 ft in	697 mm

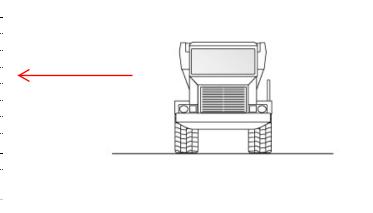
Dump

H. DUMP ANGLE	70 degrees
	•

Specification

Engine		
MAKE	Caterpillar	
MODEL	C15	
GROSS POWER	489 hp	364.6 kw
NET POWER	474 hp	353.5 kw
POWER MEASURED @	1700 rpm	
DISPLACEMENT	926 cu in	15.2 L
TORQUE MEASURED @	1200 rpm	
MAX TORQUE	1819 lb ft	2466.2 Nm
Operational		
FUEL CAPACITY	147.9 gal	560 L
HYDRAULIC SYSTEM FLUID CAPACITY	86.6 gal	328 L
COOLING SYSTEM FLUID CAPACITY	21.1 gal	80 L
ENGINE OIL CAPACITY	10 gal	38 L
TRANSMISSION FLUID CAPACITY	19 gal	72 L
TIRE SIZE	29 5R25	

Transmission



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740B Ejector Articulated Trucks

РНОТО

360 VIEW

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SPECIFICATIONS

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The new Cat® 740B ej with 38 tonnes (42 tons) rated payload offers proven reliability and durability, high productivity, superior operator comfort and lower operating costs. The spacious two-person cab with forward facing passenger seat and off road oil/nitrogen front suspension cylinders keep the operator comfortable through out the working day. The true "on-the-go" Automatic Traction Control (ATC) automatically modulates the correct level of Inter-Axle and Cross-Axle differential lock engagement which will improve cycle times and productivity. No operator interaction. Strong, durable Cat ACERT™ engines with the Tier 4 Interim/EU Stage IIIB exhaust emission solution and electronically controlled smooth shifting transmissions deliver high productivity with low fuel consumption. There are significant changes/improvements to the engine/transmission software that result in smoother gear changes.

ENGINE

UNITS: US METRIC

SOUND LEVELS

Forward 6

Forward 7

Reverse 1

Reverse 2

25.1 mph

34.0 mph

5.2 mph

7.2 mph

at 740B EJ Articulated Truck Cate	79.0 dB(A)	Page 3 o
THEORY CAD	10.0 dB(A)	
OPERATING WEIGHTS		
Front Axle – Empty	47357.0 lb	
Center Axle – Empty	17919.0 lb	
Rear Axle – Empty	16257.0 lb	
Total – Empty	81536.0 lb	
Front Axle – Rated Load	3620.0 lb	
Center Axle – Rated Load	40078.0 lb	
Rear Axle – Rated Load	40078.0 lb	
Total – Rated Load	83776.0 lb	
Front Axle – Loaded	50977.0 lb	
Center Axle – Loaded	57997.0 lb	
Rear Axle – Loaded	56335.0 lb	
Total – Loaded	165311.0 lb	
ODY PLATE THICKNESS		
Front	0.24 in	
Side	0.24 in	
Base	0.39 in	
SERVICE REFILL CAPACITIES		
Fuel Tank	149.3 gal	
Cooling System	21.1 gal	
Hydraulic System	89.0 gal	
Engine Crankcase	9.0 gal	
Transmission	19.0 gal	
Final Drives/Differential	60.8 gal	

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RL-4K (24/24)(L-4)



Tire Size: 29.5R25

Extra tread radial loader tire designed for use in rock or load and carry service.

For rock or load and carry service, here is a long wearing radial loader tire available in multiple tread configurations. The 24/24 (24 lugs per side) is ideally suited for both general and load and carry service.

Available in ply ratings: *, **

Available locations: North America, Europe / Africa / Mid East

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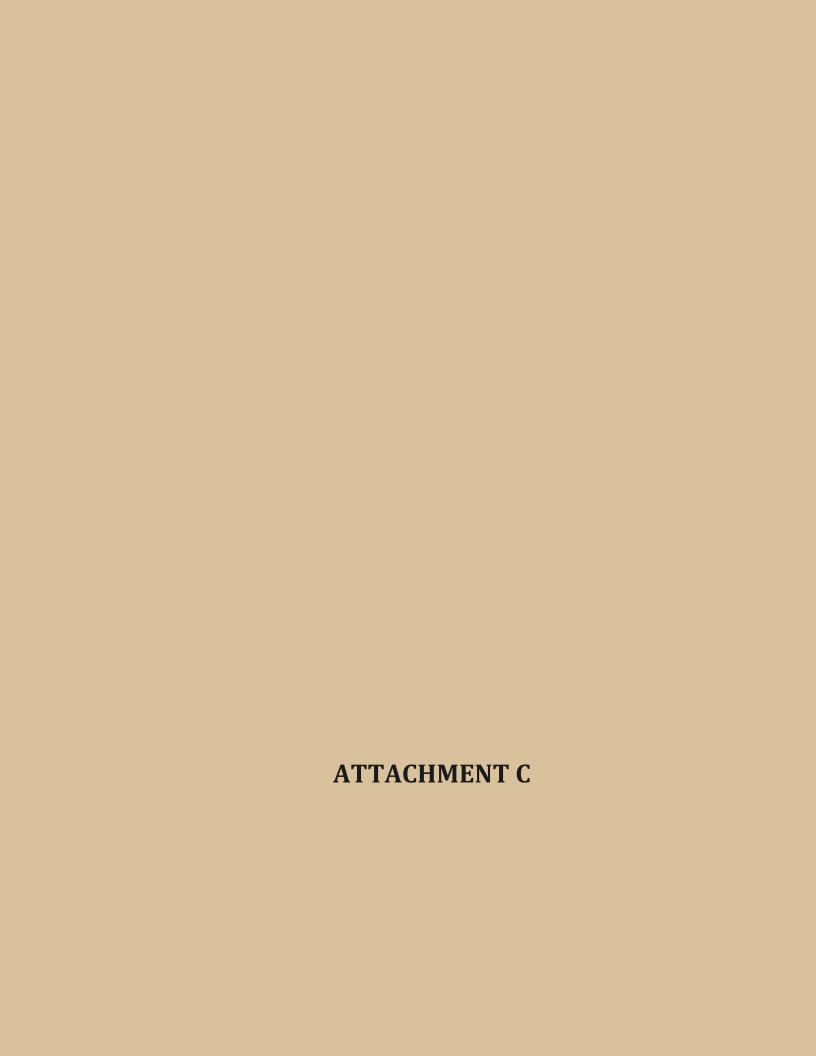
- 150-Level tread depth--50% deeper than standard L-3
- High tensile steel belt package
- Radial construction
- Tire available in multiple tread configurations
- Unique synthetic / natural rubber compound

Benefits

- Extra tread for long wear
- Impact and cut resistant
- Improved treadwear and cooler running than bias construction
- 24/24 (24 lugs per side) appropriate for both general or load and carry service
- Long wearing tread and advanced cut resistance

Change unit of measure: US O Metric												
Tiro Choos								1				
Tire Specs	Loads and In	flations										
Rim Width &	Min. Dual	Overall	Overall	Load Sect. &	Static Load	Revolution	_S Gross Contact	Tire Vol.	Tread Depth	TMPH	TMPH	TMPH
Flange	Spacing (in)	Width (in)	Diameter (in)	Growth (in)	Radius (in)	per Mi	Area (in²)	(gal)	(¹ / ₃₂ in)	(2S)	(4S)	(6S)
25.00-3.5		30.4	75.7	33.6	33	278	583	325	72		90	85

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** STABL6H **

by

Purdue University
--Slope Stability Analysis-Simplified Janbu, Simplified Bishop
or Spencer's Method of Slices

Run Date: 7/31/2016 Time of Run: 2:59PM

Run By: Civil Design Service, Inc

Input Data Filename: C:ew_cel~1.
Output Filename: C:ew_cel~1.OUT
Plotted Output Filename: C:ew_cel~1.PLT

PROBLEM DESCRIPTION Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section_ RAI No. 1

BOUNDARY COORDINATES
20 Top Boundaries
51 Total Boundaries

31 IOLAI	Boundaries				
Boundary	X-Left	Y-Left	X-Right	Y-Right	Soil Type
No.	(ft)	(ft)	(ft)	(ft)	Below Bnd
1	.00	85.00	93.00	85.00	1
2	93.00	85.00	108.00	90.00	1
3	108.00	90.00	113.50	90.00	1
4	113.50	90.00	152.50	77.00	1
5	152.50	77.00	164.50	73.00	15
6	164.50	73.00	221.50	73.00	15
7	221.50	73.00	241.00	79.50	15
8	241.00	79.50	286.00	94.50	13
9	286.00	94.50	301.00	94.70	13
10	301.00	94.70	310.50	94.70	16
		94.70			
11	310.50		401.40	125.00	16
12	401.40	125.00	411.40	125.00	16
13	411.40	125.00	511.40	150.00	16
14	511.40	150.00	531.40	150.00	16
15	531.40	150.00	631.40	125.00	16
16	631.40	125.00	641.40	125.00	16
17	641.40	125.00	777.90	79.50	16
18	777.90	79.50	786.90	76.50	15
	786.90	76.50	791.40		
19				75.00	2
20	791.40	75.00	1000.00	75.00	2
21	301.00	94.70	346.60	79.50	1
22	143.00	77.00	152.50	77.00	15
23	241.00	79.50	346.60	79.50	15
24	346.60	79.50	777.90	79.50	15
25	143.00	77.00	164.00	70.00	1
26	164.00	70.00	222.00	70.00	1
27	222.00	70.00	241.50	76.50	3
					3
28	241.50	76.50	543.60	76.50	2
29	543.60	76.50	786.90	76.50	5
30	222.00	70.00	225.00	69.00	1
31	.00	69.00	225.00	69.00	9
32	225.00	69.00	369.00	69.00	9
33	369.00	69.00	384.00	69.00	9
34	384.00	69.00	529.00	75.00	9
35	529.00	75.00	543.60	76.50	5
36	529.00	75.00	545.00	75.00	2
37	545.00	75.00		70.90	2
			622.00		
38	622.00	70.90	638.00	70.90	2
39	638.00	70.90	1000.00	70.90	2
40	.00	60.00	368.00	60.00	6
41	368.00	60.00	384.00	60.00	6
42	384.00	60.00	529.00	75.00	6
43	.00	56.00	368.00	56.00	7
44	368.00	56.00	384.00	56.00	7
45	384.00	56.00	529.00	75.00	2
46	384.00	56.00	529.00	51.00	1
47	529.00	51.00	545.00	51.00	1
48	545.00	51.00	1000.00	51.00	1
49	384.00	56.00	529.00	27.00	7
50	529.00	27.00	545.00	27.00	7
51	545.00	27.00	1000.00	27.00	7

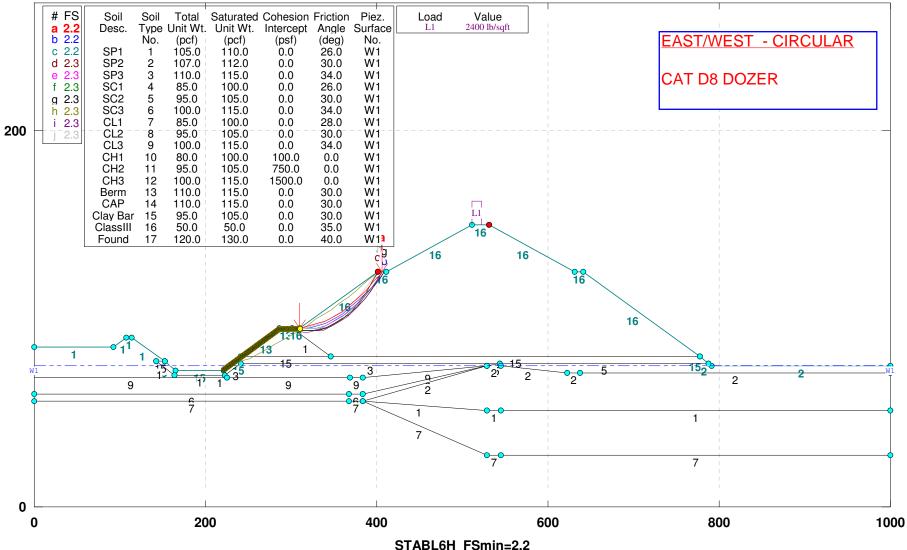
```
ISOTROPIC SOIL PARAMETERS
  17 Type(s) of Soil
  Soil Total Saturated Cohesion Friction Pore Pressure Piez.
  Type Unit Wt. Unit Wt. Intercept Angle Pressure Constant Surface
   No. (pcf)
                 (pcf) (psf)
                                          (deg) Param. (psf) No.
                             .0
  1 105.0 110.0 .0 26.0 .00
2 107.0 112.0 .0 30.0 .00
3 110.0 115.0 .0 34.0 .00
4 85.0 100.0 .0 26.0 .00
5 95.0 105.0 .0 30.0 .00
6 100.0 115.0 .0 34.0 .00
7 85.0 100.0 .0 28.0 .00
8 95.0 105.0 .0 30.0 .00
9 100.0 115.0 .0 34.0 .00
10 80.0 100.0 100.0 .0 34.0 .00
11 95.0 105.0 .0 30.0 .00
11 95.0 105.0 .0 30.0 .00
12 100.0 115.0 1500.0 .0 .00
13 110.0 115.0 1500.0 .0 .00
14 110.0 115.0 .0 30.0 .00
15 95.0 105.0 .0 30.0 .00
16 50.0 50.0 .0 35.0 .00
17 120.0 130.0 .0 40.0 .00
1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED
                                                                .0
    1 105.0
                 110.0
                                         26.0 .00
                                                                          1
                                                                  .0
                                                                           1
                                                                 .0
                                                                            1
                                                                  .0
                                                                            1
                                                                  .0
                                                                  .0
                                                                 .0
                                                                  .0
                                                                  . 0
                                                                  .0
                                                                  .0
                                                                           1
                                                                  .0
                                                                 .0
                                                                            1
                                                                  .0
                                                                            1
                                                                  . 0
                                                                            1
                                                                  .0
                                                                           1
                                                                  . 0
  1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED
 Unit Weight of Water = 62.40
Piezometric Surface No. 1 Specified by 2 Coordinate Points
                               Y-Water
    Point
                X-Water
                  (ft)
                                (ft)
     No.
                    .00
      1
                                75.00
              1000.00
                                75.00
      2
BOUNDARY LOAD(S)
   3 Load(s) Specified
 Load X-Left X-Right Intensity
No. (ft) (ft) (lb/sqft)
                                                           Deflection
                            .±911C
(ft)
                                                            (deg)
               511.40
                               513.40
                                            6300.0
                                                                 .0
   1
              526.15
                          528.15
532.65
    2
                                              7200.0
                                                                   .0
    3
                                              7200.0
               530.65
                                                                  . 0
  NOTE - Intensity Is Specified As A Uniformly Distributed
          Force Acting On A Horizontally Projected Surface.
  A Critical Failure Surface Searching Method, Using A Random
  Technique For Generating Circular Surfaces, Has Been Specified.
10000 Trial Surfaces Have Been Generated.
   50 Surfaces Initiate From Each Of200 Points Equally Spaced
  Along The Ground Surface Between X = 221.50 ft.
                                  and X = 310.50 ft.
 Each Surface Terminates Between X = 401.40 ft.
                                  and X = 531.40 ft.
 Unless Further Limitations Were Imposed, The Minimum Elevation
 At Which A Surface Extends Is Y = .00 ft.
  10.00 ft. Line Segments Define Each Trial Failure Surface.
  Following Are Displayed The Ten Most Critical Of The Trial
         Failure Surfaces Examined. They Are Ordered - Most Critical
         First.
         * * Safety Factors Are Calculated By The Modified Bishop Method * *
         Failure Surface Specified By 12 Coordinate Points
           Point X-Surf
                                   Y-Surf
            No.
                        (ft)
                                      (ft)
                        310.50
                                      94.70
             1
             2
                        320.46
                                       95.65
                                      97.06
                       330.36
             3
                                      98.93
             4
                       340.18
             5
                       349.91
                                      101.24
                      359.52
             6
                                      104.01
                       368.99
             7
                                      107.22
             8
                        378.30
                                      110.87
             9
                       387.43
                                    114.94
            1.0
                       396.37
                                    119.43
                                  124.33
            11
                       405.08
                       406.15
                                      125.00
            12
         Circle Center At X = 295.0; Y = 309.9 and Radius, 215.8
               *** 2.187 ***
```

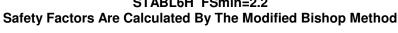
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1
C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:54PM # FS Total Saturated Cohesion Friction Piez. Soil Soil **a 2.2** b 2.2 Type Unit Wt. Unit Wt. Intercept Angle Desc. Surface (psf) 0.0 (deg) No. No. (pcf) (pcf) c 2.2 SP1 105.0 110.0 26.0 W1 d 2.3 SP2 107.0 112.0 0.0 30.0 W1 **NO WASTE** SP3 110.0 115.0 0.0 34.0 W1 f 2.3 SC1 100.0 W1 85.0 0.0 26.0 g 2.3 h 2.3 SC₂ 95.0 105.0 0.0 30.0 W1 115.0 100.0 0.0 W1 34.0 CL1 100.0 W1 i 2.3 85.0 200 CL2 8 95.0 105.0 0.0 30.0 W1 9 W1 CL3 100.0 115.0 0.0 34.0 CH1 10 100.0 100.0 W1 80.0 CH₂ 11 95.0 105.0 750.0 W1 CH3 12 100.0 115.0 1500.0 0.0 W1 13 115.0 0.0 30.0 W1 Berm 110.0 CAP 115.0 0.0 30.0 W1 14 110.0 Clay Bar 15 95.0 105.0 0.0 30.0 W1 50.0 W1 ClassIII 16 50.0 0.0 35.0 130.0 0.0 40.0 W13 Found 17 120.0 16 16 9 9 0 400 600 200 800 1000



STABL6H FSmin=2.2 Safety Factors Are Calculated By The Modified Bishop Method

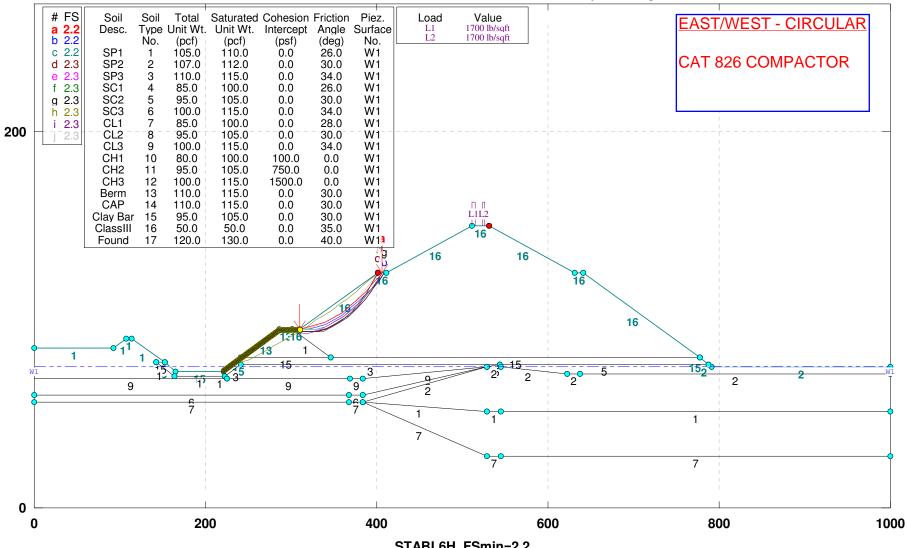
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section_ RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:53PM

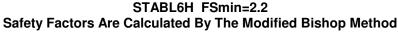






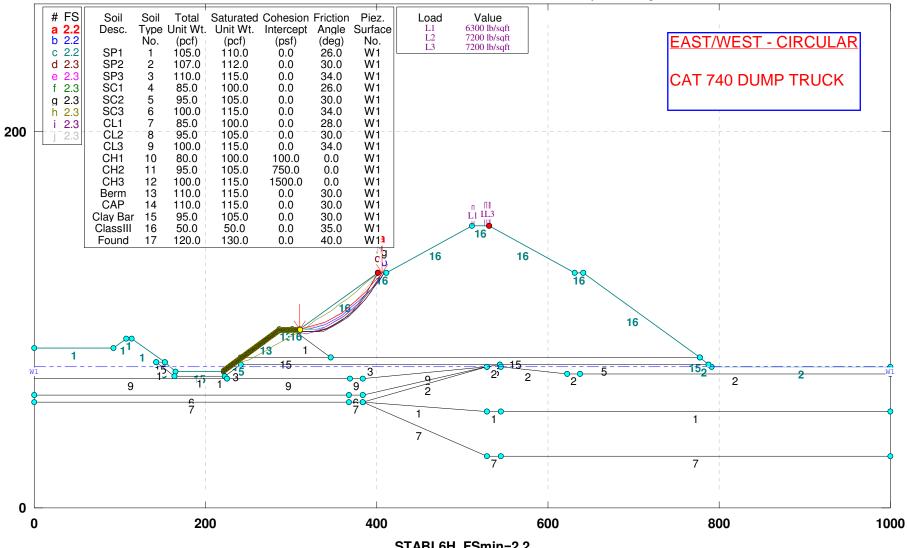
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:56PM

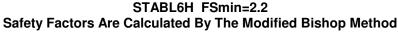


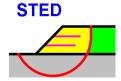




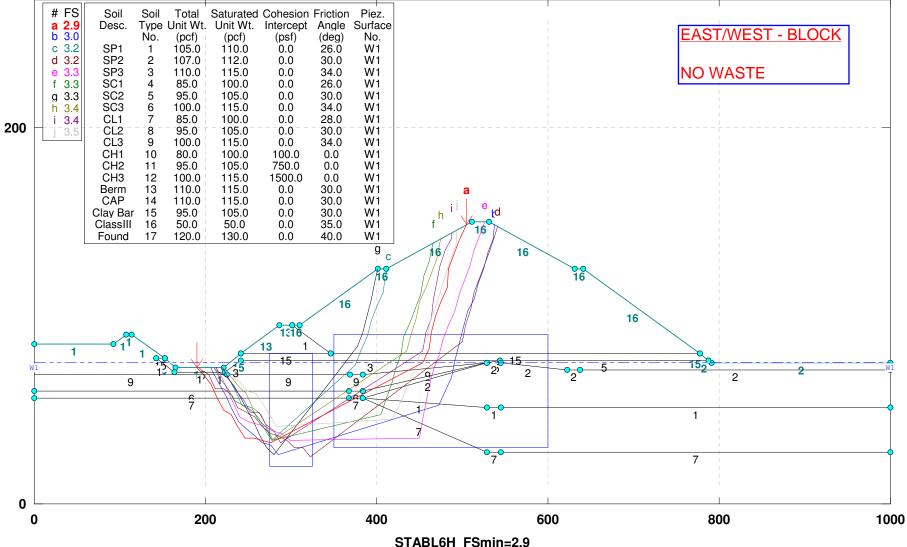
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:59PM

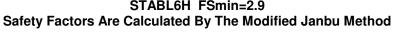


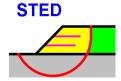




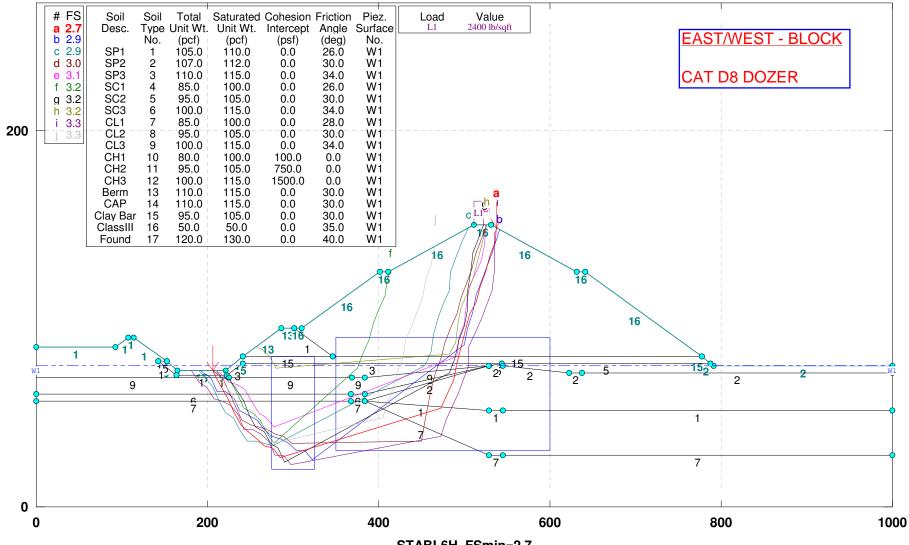
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:47PM

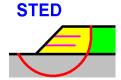






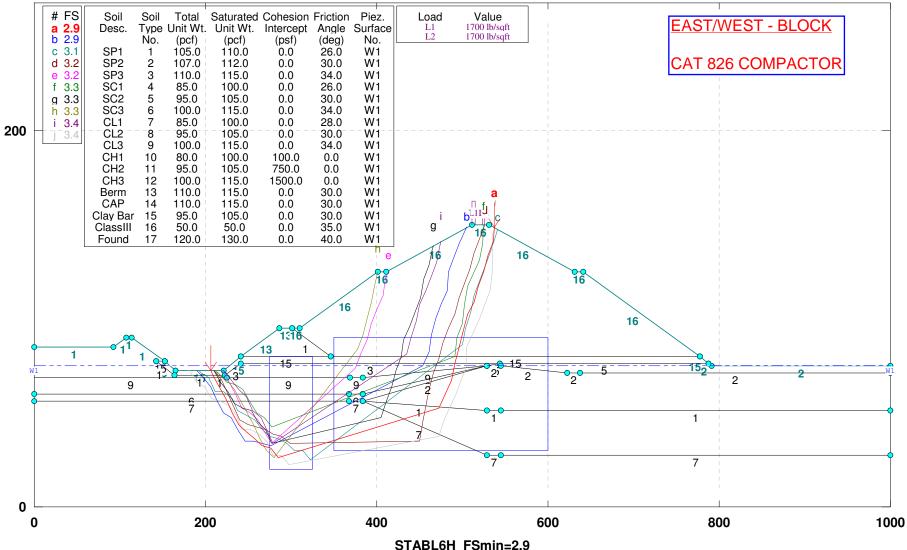
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:51PM

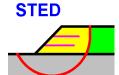




STABL6H FSmin=2.7 Safety Factors Are Calculated By The Modified Janbu Method

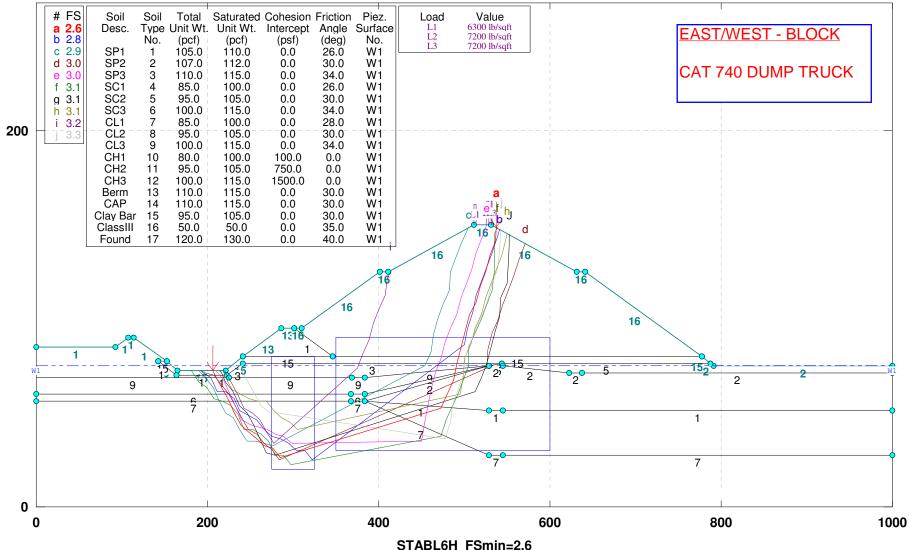
Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section_ RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:50PM

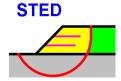




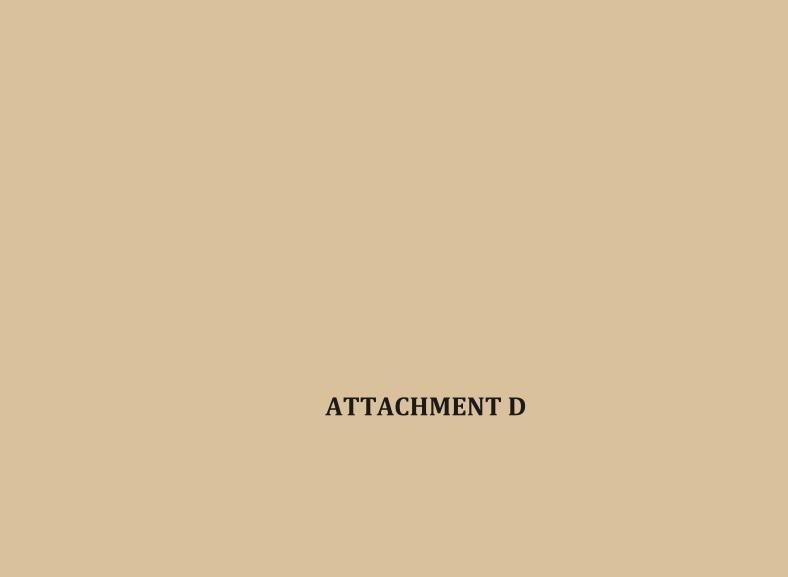
Safety Factors Are Calculated By The Modified Janbu Method

Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:48PM





Safety Factors Are Calculated By The Modified Janbu Method



** STABL6H **

by

Purdue University
--Slope Stability Analysis-Simplified Janbu, Simplified Bishop
or Spencer's Method of Slices

Run Date: 7/31/2016 Time of Run: 2:20PM

Run By: Civil Design Service, Inc

Input Data Filename: C:ns_cel~1.
Output Filename: C:ns_cel~1.OUT
Plotted Output Filename: C:ns_cel~1.PLT

PROBLEM DESCRIPTION Angelos Class III Cell 16 Expansion Cell 16 North/South Section - RAI No. 1

BOUNDARY COORDINATES

13 Top Boundaries
67 Total Boundaries

67 Total	Boundaries				
Boundary	X-Left	Y-Left	X-Right	Y-Right	Soil Type
No.	(ft)	(ft)	(ft)	(ft)	Below Bnd
1	.00	85.00	75.00	85.00	1
2	75.00	85.00	90.00	90.00	1
3	90.00	90.00	95.50	90.00	1
4	95.50	90.00	137.50	77.00	15
5	137.50	77.00	149.50	73.00	15
6	149.50	73.00	209.40	73.00	15
7	209.40	73.00	224.20	78.00	15
8	224.20	78.00	260.40	90.00	13
9	260.40	90.00	275.40	90.00	13
10	275.40	90.00	380.40	125.00	16
11	380.40	125.00	390.40	125.00	16
12	390.40	125.00	490.40	150.00	16
13	490.40	150.00	1100.00	150.00	16
14	275.40	90.00	310.10	78.40	1
15	128.00	77.00	137.50	77.00	15
16	224.20	78.00	310.10	78.40	15
17	310.10	78.40	840.50	81.00	15
18	840.50	81.00	1100.00	81.00	15
19	128.00	77.00	143.70	71.80	1
20	215.20	71.80	225.00	75.00	1
21	225.00	75.00	840.50	78.00	1
22	840.50	78.00	1100.00	78.00	1
23	.00	71.80	143.70	71.80	9
24	143.70	71.80	149.00	70.00	9
25	149.00	70.00	209.80	70.00	9
26	209.80	70.00	215.20	71.80	9
27	215.20	71.80	286.00	71.80	9
28	286.00	71.80	302.00	71.80	9
29	302.00	71.80	320.00	70.10	9
30	320.00	70.10	336.00	70.10	9
31	336.00	70.10	446.00	65.20	3
					ა ე
32	446.00	65.20	462.00	65.20	3
33	462.00	65.20	492.00	75.10	3
34	492.00	75.10	508.00	75.10	3
35	508.00	75.10	573.00	75.00	3
36	573.00	75.00	589.00	75.00	2
37	589.00	75.00	676.00	75.20	2
38	676.00	75.20	1100.00	75.20	3
39	336.00	70.10	446.00	63.20	9
40	446.00	63.20	462.00	63.20	9
41	462.00	63.20	492.00	68.10	9
42	492.00	68.10	508.00	68.10	9
43	508.00	68.10	573.00	75.00	9
44	.00	47.10	492.00	47.10	3
45	492.00	47.10	508.00	47.10	3
46			573.00	75.00	2
	508.00	47.10			
47	589.00	51.00	676.00	75.20	3
48	508.00	47.10	575.00	51.00	1
49	575.00	51.00	589.00	51.00	1
50	589.00	51.00	676.00	46.20	1
51	676.00	46.20	692.00	46.20	1

```
52
                                            725.00
                  692.00
                                 46.20
                                                           55.50
                                                                            1
                                                          55.50
27.00
42.20
      53
                  725.00
                                55.50 1100.00
                                                                            1
                                         573.00
676.00
      54
                  508.00
                                 47.10
      55
                 589.00
                                 27.00
                                           692.00
725.00
                                                          42.20
      56
                676.00
                               42.20
      57
                 692.00
                               42.20
                                                          45.50
                                                          45.50
      58
                 725.00
                                45.50 1100.00
                                                          35.60
35.60
                                         492.00
508.00
                    .00
      59
                                 35.60
                 492.00
      60
                                 35.60
                                           573.00
                                                           27.00
                508.00
                               35.60
                                                                            7
      61
                 573.00
                               27.00 589.00
                                                          27.00
      62
      6.3
                589.00
                                27.00
                                            676.00
                                                           35.20
                676.00
                                                           35.20
19.00
19.00
      64
                                35.20 1100.00
                                                                            1
                                         573.00
589.00
      65
                   .00
                                 19.00
                  573.00
                                19.00
      66
                                                                            1
      67
                  589.00 19.00
                                           676.00
                                                          35.20
 ISOTROPIC SOIL PARAMETERS
  17 Type(s) of Soil
  Soil Total Saturated Cohesion Friction Pore Pressure Piez.
  Type Unit Wt. Unit Wt. Intercept
No. (pcf) (pcf) (psf) (deg) Param. (psf) No.
1 105.0 110.0 .0 26.0 .00 .0 1
       (pcf) (pcf) (psf) (deg) Param.

105.0 110.0 .0 26.0 .00

107.0 112.0 .0 30.0 .00

110.0 115.0 .0 34.0 .00

85.0 100.0 .0 26.0 .00

95.0 105.0 .0 30.0 .00

85.0 100.0 .0 28.0 .00

95.0 105.0 .0 34.0 .00

85.0 100.0 .0 28.0 .00

95.0 105.0 .0 30.0 .00

100.0 115.0 .0 34.0 .00

95.0 105.0 .0 30.0 .00

100.0 115.0 .0 34.0 .00

95.0 105.0 .0 30.0 .00

100.0 115.0 .0 34.0 .00

95.0 105.0 750.0 .0 .0 .00

110.0 115.0 1500.0 .0 .0 .00

110.0 115.0 1500.0 .0 .00

110.0 115.0 .0 30.0 .00

110.0 115.0 .0 30.0 .00

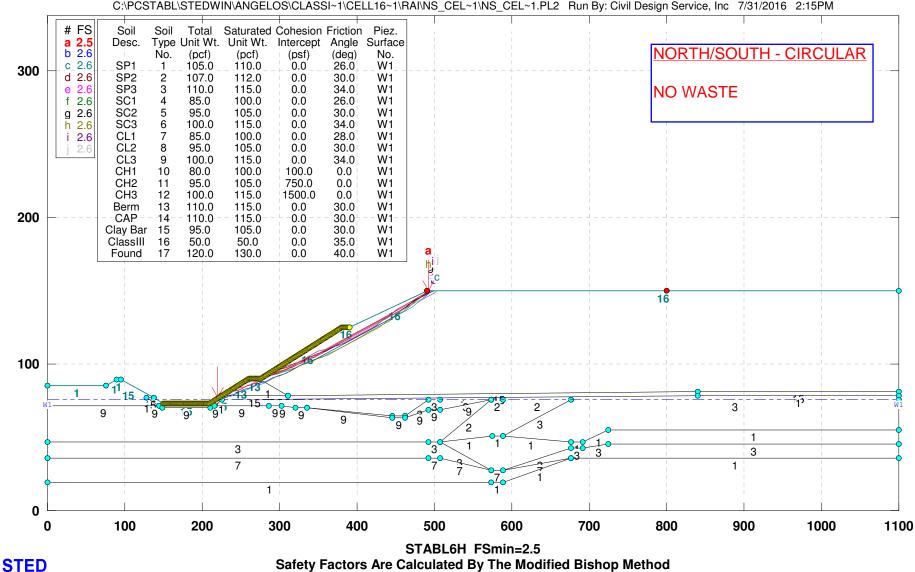
95.0 105.0 .0 30.0 .00

110.0 115.0 .0 30.0 .00

220.0 130.0 .0 35.0 .00

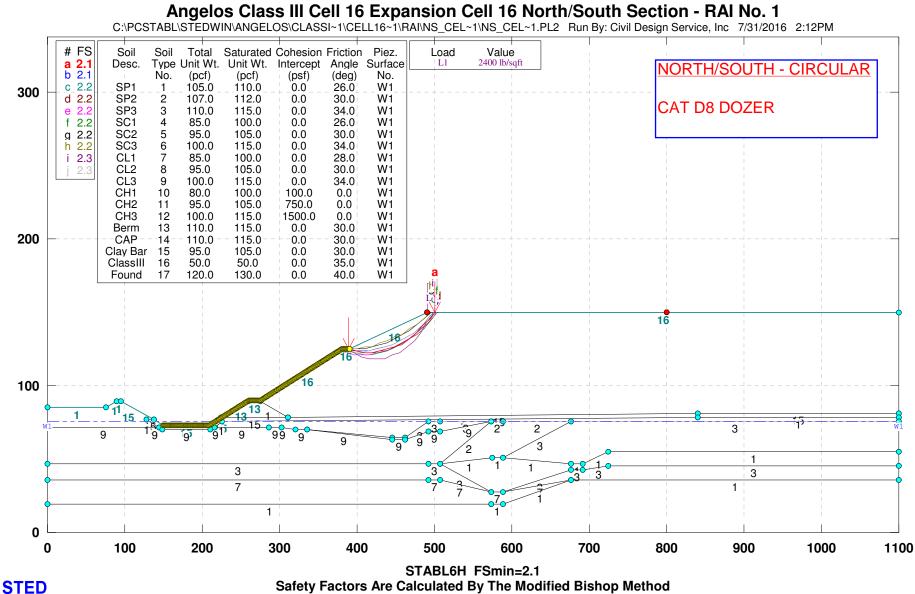
EZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED
                                                                      .0
     2.
                                                                               1
                                                                     .0
     3
                                                                              1
                                                                      .0
     4
                                                                      .0
     5
                                                                                1
                                                                     .0
     6
                                                                               1
                                                                     .0
     7
                                                                      .0
    8
                                                                                1
     9
                                                                      .0
                                                                                1
   10
                                                                      .0
                                                                      .0
   11
                                                                      .0
   12
                                                                      .0
   13
                                                                                1
                                                                      .0
   14
                                                                                1
   15
                                                                      .0
                                                                      .0
   16
                                                                                1
                                                                      .0
   17
  1 PIEZOMETRIC SURFACE(S) HAVE BEEN SPECIFIED
  Unit Weight of Water = 62.40
  Piezometric Surface No. 1 Specified by 2 Coordinate Points
    Point X-Water
                                Y-Water
                                  (ft)
     No.
                   (ft)
                                  75.00
      1
                     .00
       2
                1100.00
                                 75.00
 BOUNDARY LOAD(S)
      3 Load(s) Specified
                                            Intensity
(lb/sqft)
                X-Left X-Right
  Load
                                                              Deflection
                 (ft)
                                (ft)
   No.
                                                                (deg)
                                492.20
                                              6300.0
                                                                     .0
    1
                490.40
                                              7200.0
7200.0
    2
                                                                      .0
                505.15
                                507.15
    3
                509.65
                                511.65
                                                                      . 0
  NOTE - Intensity Is Specified As A Uniformly Distributed
          Force Acting On A Horizontally Projected Surface.
  A Critical Failure Surface Searching Method, Using A Random
  Technique For Generating Circular Surfaces, Has Been Specified.
10000 Trial Surfaces Have Been Generated.
   50 Surfaces Initiate From Each Of200 Points Equally Spaced
  Along The Ground Surface Between X = 149.50 ft.
                                    and X = 390.40 ft.
  Each Surface Terminates Between X = 490.40 ft.
                                    and X = 800.00 \text{ ft.}
  Unless Further Limitations Were Imposed, The Minimum Elevation
  At Which A Surface Extends Is Y = .00 ft.
  10.00 ft. Line Segments Define Each Trial Failure Surface.
  Following Are Displayed The Ten Most Critical Of The Trial
         Failure Surfaces Examined. They Are Ordered - Most Critical
          * * Safety Factors Are Calculated By The Modified Bishop Method * *
         Failure Surface Specified By 17 Coordinate Points
```

Angelos Class III Cell 16 Expansion Cell 16 North/South Section - RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\NS_CEL~1\NS_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:15PM



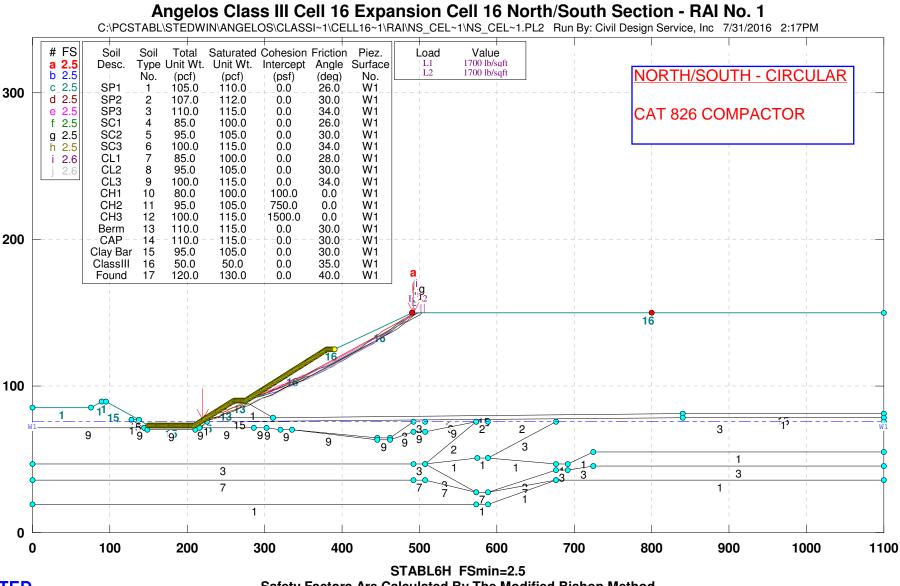


Safety Factors Are Calculated By The Modified Bishop Method





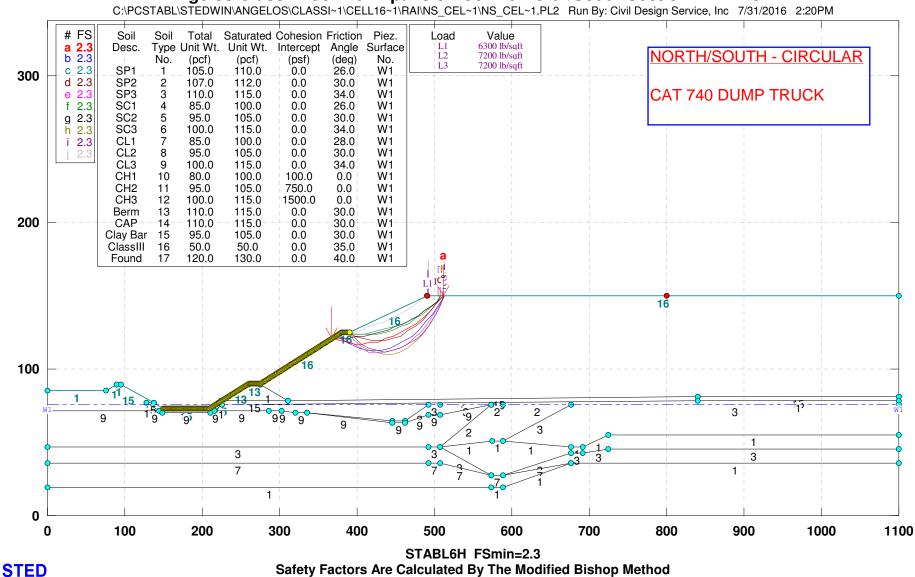
Safety Factors Are Calculated By The Modified Bishop Method





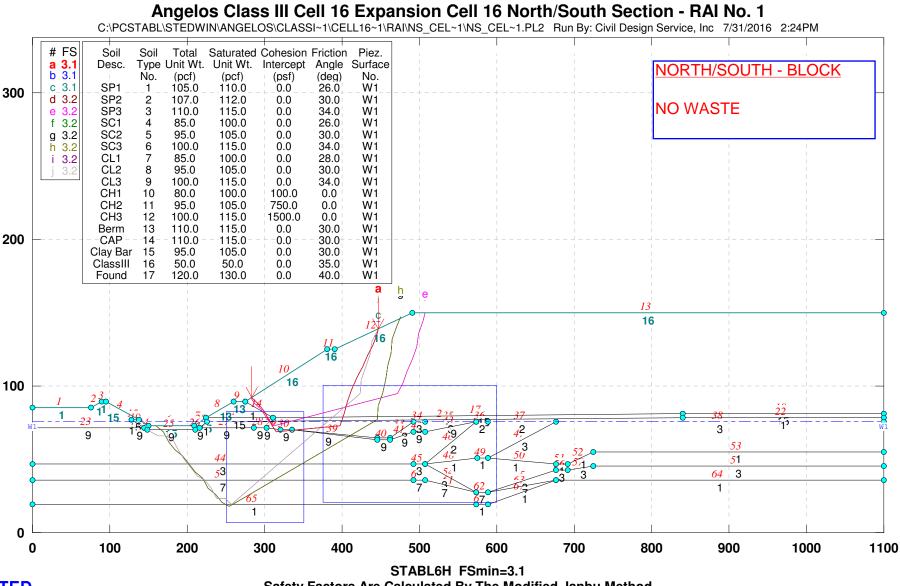
Safety Factors Are Calculated By The Modified Bishop Method

Angelos Class III Cell 16 Expansion Cell 16 North/South Section - RAI No. 1





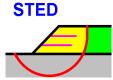
Safety Factors Are Calculated By The Modified Bishop Method





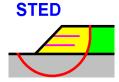
Safety Factors Are Calculated By The Modified Janbu Method

Angelos Class III Cell 16 Expansion Cell 16 North/South Section - RAI No. 1
C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\NS_CEL~1\NS_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:27PM # FS Total Saturated Cohesion Friction Piez. Load Soil Soil Value **a 2.5** b 2.5 Type Unit Wt. Unit Wt. Intercept Angle Surface 2400 lb/sqft Desc. NORTH/SOUTH - BLOCK No. (pcf) (pcf) (psf) (deg) No. c 2.9 SP1 105.0 110.0 0.0 26.0 W1_ 300 SP2 d 2.9 107.0 112.0 30.0 W1 0.0 SP3 SC1 CAT D8 DOZER 110.0 115.0 34.0 W1 85.0 26.0 W1 f 2.9 100.0 0.0 5 6 7 g 2.9 h 2.9 SC2 95.0 105.0 0.0 30.0 W1 SC3 34.0 100.0 115.0 0.0 W1 CL1 85.0 28.0 W1 i 3.0 100.0 0.0 CL2 95.0 105.0 30.0 W1 0.0 CL3 9 100.0 115.0 0.0 34.0 W1 CH1 W1 10 80.0 100.0 100.0 0.0 CH2 11 95.0 105.0 750.0 0.0 W1 CH3 12 1500.0 0.0 W1 100.0 115.0 13 115.0 30.0 W1 Berm 110.0 0.0 200 CAP -14 110.0 115.0 0.0 30.0 W1 Clay Bar 95.0 105.0 0.0 30.0 W1 15 ClassIII 16 50.0 50.0 35.0 W1 17 Found 120.0 130.0 40.0 W1 16 100 53 51 *64* 3 1 0 100 200 300 400 500 600 700 800 900 1000 1100 0 STABL6H FSmin=2.5

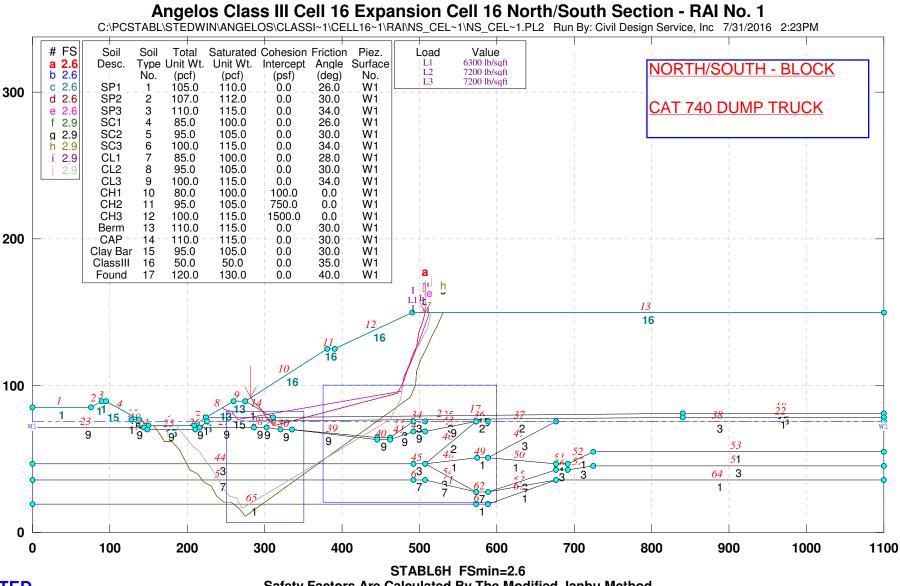


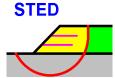
Safety Factors Are Calculated By The Modified Janbu Method

Angelos Class III Cell 16 Expansion Cell 16 North/South Section - RAI No. 1
C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\NS_CEL~1\NS_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 2:25PM # FS Total Saturated Cohesion Friction Piez. Load Value Soil Soil **a 2.8** b 2.8 1700 lb/sqft 1700 lb/sqft Type Unit Wt. Unit Wt. Intercept Angle Surface L1 NORTH/SOUTH - BLOCK Desc. L2 No. (pcf) (pcf) (psf) (deg) No. c_3.1 SP1 105.0 110.0 0.0 26.0 W1_ 300 SP2 d 3.1 107.0 112.0 30.0 W1 0.0 CAT 826 COMPACTOR SP3 SC1 110.0 115.0 34.0 W1 e 3.1 85.0 26.0 W1 f 3.1 4 5 6 7 100.0 0.0 g 3.1 h 3.1 SC2 95.0 105.0 0.0 30.0 W1 SC3 34.0 100.0 115.0 0.0 W1 CL1 85.0 28.0 W1 i 3.1 100.0 0.0 CL2 95.0 105.0 30.0 W1 j 3.1 0.0 CL3 9 100.0 115.0 0.0 34.0 W1 CH1 W1 10 80.0 100.0 100.0 0.0 CH2 11 95.0 105.0 750.0 0.0 W1 CH3 12 1500.0 0.0 W1 100.0 115.0 13 115.0 30.0 W1 Berm 110.0 0.0 200 CAP -14 110.0 115.0 0.0 30.0 W1 Clay Bar 95.0 105.0 0.0 30.0 W1 15 ClassIII 16 50.0 50.0 35.0 W1 17 Found 120.0 130.0 40.0 W1 16 100 53 51 *64* 3 1 0 100 200 300 400 500 600 700 800 900 1000 1100 0

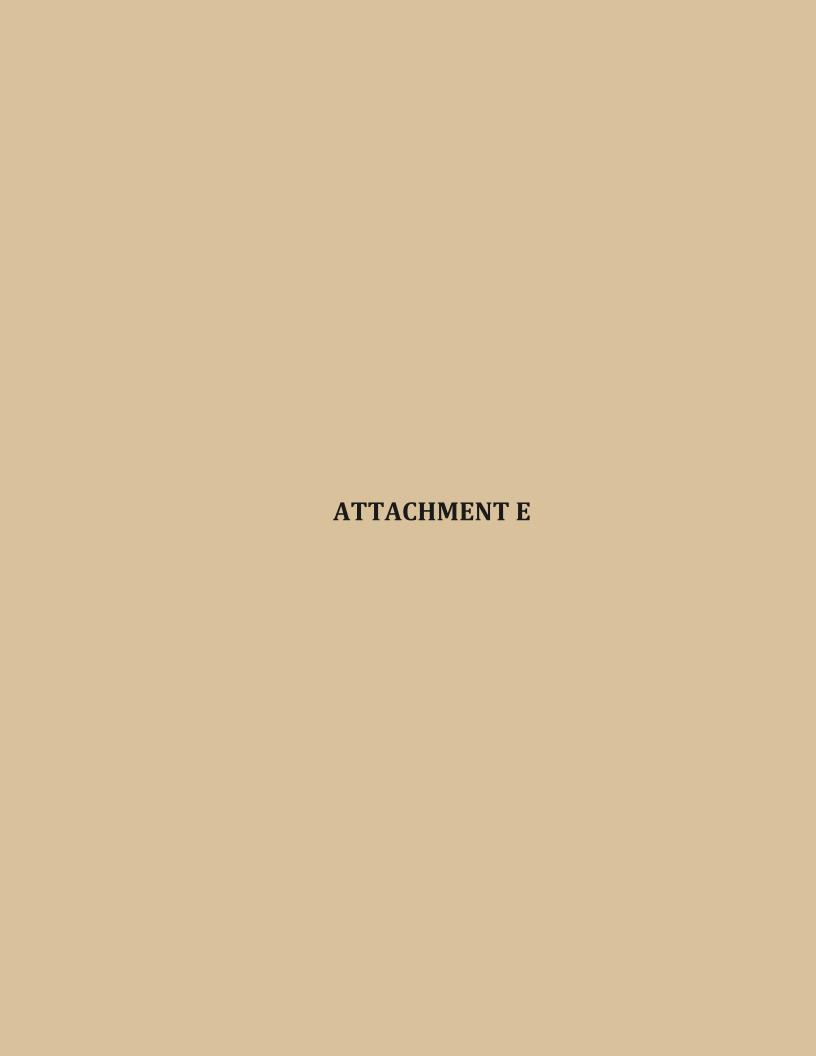


STABL6H FSmin=2.8 Safety Factors Are Calculated By The Modified Janbu Method





Safety Factors Are Calculated By The Modified Janbu Method



Soil Properties - Settlement Estimates

Sands, Silty Sands	, Clayey Sands			Clays			
SPT Blow Count	Description	Dr*	Dr avg	SPT Blow Count	Description	Dr avg	References: 1) SPT vs Soil Relative Density
							" Soil Mechanics; 1969 Lambe and Whitman, Table 7.4"
0-4	Very Loose	0-15	10	<2	Very Soft	10	
4-10	Loose	15-30	20	2-4	Soft	20	2) Soil Types, Soil Properties
10-30	Medium	35-65	50	4-8	Medium	50	" Soil Mechanics; 1969 Lambe and Whitman, Table 3.2"
30-50	Dense	65-85	75	8-15	Stiff	75	
>50	Very Dense	85-100	90	15-30	Very Stiff	90	3) Soil Consolidation Coefficent vs Soil Type
				>30	Hard	100	Sands - "Basic Soils Engineering, 1969 B.K. Hough, Table 5-1"

^{*}Dr - Relative Density (Reference 1)

Soil Types (Reference 2)

SP	emin	0.	2			SC	emin	0.	3		Clays	emin	0.4	1		
	emax	0.9	5				emax	0.	9			emax	2	2		
	Gs	2.6	5				Gs	2.6	5			Gs	2.65	5		
	Moisture	1	2				Moisture	1	2			Moisture	30)		
SPT N	Eo	γ dry	γ sat	γ moist		SPT N	Eo	γ dry	γ sat	γ moist	SPT N	Eo	γ dry	γ sat	γ moist	
0-4	0.875	88.2	117.3	98.8		0-4	0.84	89.9	118.4	100.7	<2	1.84	58.2	98.7	75.7	
4-10	0.8	91.9	119.6	102.9		4-10	0.78	92.9	120.2	104.0	2-4	1.68	61.7	100.8	80.2	
10-30	0.575	105.0	127.8	117.6		10-30	0.6	103.4	126.8	115.8	4-8	1.2	75.2	109.2	97.7	
30-50	0.3875	119.2	136.6	133.5		30-50	0.45	114.0	133.4	127.7	8-15	0.8	91.9	119.6	119.4	
>50	0.275	129.7	143.2	143.2	Saturated	>50	0.36	121.6	138.1	136.2	15-30	0.56	106.0	128.4	128.4	Saturated
											>30	0.4	118.1	135.9	135.9	Saturated
SP - Esimate	d Consolidation C	Coefficient				SC - Esimated	Consolidatio	n Coefficie	nt		Clay - Esi	imated Cons	solidation (Coefficient		
Cc	=a(Emax-b)				*Reference 3	Cc	=a(Emax-	b)		*Reference 3	Cc	= (0.156E	o)+0.107		*Referen	ce 4
	0.03375	a =	0.075	5			0.092	a =	0.2	.3						
		Emax =	0.95	5				Emax =	0.	.9	SPT N	Eo				
		b =	0.5	5				b =	0.	.5	<2	1.84	0.29774	1		
											2-4	1.68				
											4-8	1.2				
											8-15	0.8				
											15-30	0.56				
											>30	0.4	0.0731	<u>[</u>		

4) Clays - "Principles of Geotechnical Engineering, 1985, B. Das, Table 7.1"

Ch. 7 Soil Formation

Table 7.4 Standard Penetration Test

Relative of Sa		Strength of Clay								
Penetration Resistance N (blows/ft)	Relative Density	Penetration Resistance N (blows/ft)	Unconfined Compressive Strength (tons/ft²)	Consistency						
0-4	Very loose	<2	< 0.25	Very soft						
4-10	Loose	2-4	0.25-0.50	Soft						
10-30	Medium	4-8	0.50-1.00	Medium						
30-50	Dense	8-15	1.00-2.00	Stiff						
>50	Very dense	15-30	2.00-4.00	Very stiff						
		>30	>4.00	Hard						

From Terzaghi and Peck, 1948.

In certain countries, such as Holland, subsoil conditions are such that penetration testing has proved to be a relatively reliable technique. More sophisticated techniques [such as the friction jacket cone (Begemann, 1953)] have been widely used.

The vane test has proved to be a very useful method of determining the shear strength of soft clays and silts. Figure 7.6 shows various sizes and shapes of vanes which have been used for field testing. The vane is forced into the ground and then the torque required to rotate the vane is measured. The shear strength is determined from the torque required to shear the soil along the vertical and horizontal edges of the vane.

As later chapters in this book will show, a proper subsoil investigation should include the determination of water pressure at various depths within the subsoil. Methods of determining pore water pressure are discussed in Part IV. Part IV also notes how the permeability of a subsoil can be estimated from pumping tests.

Various load tests and field compaction tests may be highly desirable in important soil projects. In this type of test, a small portion of the subsoil to be loaded by the prototype is subjected to a stress condition in the field which approximates that under the completed structure. The engineer extrapolates the results of the field tests to predict the behavior of the prototype.

7.7 SUBSOIL PROFILES

Figures 7.7 to 7.17 present a group of subsoil profiles and Table 7.5 gives some information on the geological history of the various profiles. The purposes of presenting these profiles are to:

- Indicate how geological history influences soil characteristics.
- 2. Give typical values of soil properties.

- Show dramatically the large variability in soil behavior with depth.
- Illustrate how engineers have presented subsoil data.

Three considerations were used in the selection of the profiles: first, examples were chosen with different types of geological history; second, most of the profiles are ones for which there are excellent references giving considerably more detail on the characteristics of the soil and engineering problems involved with the particular profile; and finally, most of the profiles selected have been involved in interesting and/or important soil engineering projects.

Some of the soil characteristics shown in the profiles have already been described in this book. These characteristics include water content, unit weight, void ratio, porosity, Atterberg limits, and particle size. Other characteristics, particularly those referring to strength and compressibility, will be discussed in detail in later portions of this book. Reference will then be made back to these profiles.

The profiles illustrate many concepts presented in the preceding parts of this book; some of them are discussed in the remaining part of this section.

Stress History

In a normally consolidated sedimentary soil both the void ratio and water content decrease with depth in the profile, and the strength therefore increases. This characteristic is illustrated in several of the profiles, e.g., the Norwegian marine clay (Fig. 7.7), the Thames Estuary clay (Fig. 7.10), and the Canadian clay (Fig. 7.11). The London clay is overconsolidated since it was compressed by a greater overburden than now exists. Erosion removed some of the original overburden. As would be expected, the overconsolidated London clay does not

Reference No. 2 Settlement

Ch. 3 Description of an Assemblage of Particles

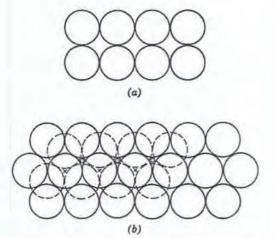


Fig. 3.2 Arrangements of uniform spheres. (a) Plan and elevation view: simple cubic packing. (b) Plan view: dense packing. Solid circles, first layer; dashed circles, second layer; o, location of sphere centers in third layer: face-centered cubic array; x, location of sphere centers in third layer: close-packed hexagonal array. (From Deresiewicz, 1958.)

these simple packings can be computed from the geometry of the packings, and the results are given in Table 3.2.

This table also gives densities for some typical granular soils in both the "dense" and "loose" states. A variety of tests have been proposed to measure the maximum and

Table 3.2 Maximum and Minimum Densities for Granular Soils

	Void	Ratio	Porosit	y (%)	Dry Unit Weight (pcf)			
Description	e_{max}	e_{\min}	n_{max}	n_{\min}	7d min	7d max		
Uniform spheres	0,92	0.35	47.6	26.0	-	-		
Standard Ottawa								
sand	0.80	0.50	44	33	92	110		
Clean uniform								
sand	1.0	0.40	50	29	83	118		
Uniform inorganic			1					
silt	1.1	0.40	52	29	80	118		
Silty sand	0.90	0.30	47	23	87	127		
Fine to coarse								
sand	0.95	0.20	49	17	85	138		
Micaceous sand	1.2	0.40	55	29	76	120		
Silty sand and								
gravel	0.85	0.14	46	12	89	146		

B. K. Hough, Basic Soils Engineering. Copyright © 1957, The Ronald Press Company, New York.

minimum void ratios (Kolbuszewski, 1948). The test to determine the maximum density usually involves some form of vibration. The test to determine minimum density usually involves pouring oven-dried soil into a container. Unfortunately, the details of these tests have not been entirely standardized, and values of the maximum density and minimum density for a given granular soil depend on the procedure used to determine them. By using special measures, one can obtain densities greater than the so-called maximum density. Densities considerably less than the so-called minimum density can be obtained, especially with very fine sands and silts, by slowly sedimenting the soil into water or by fluffing the soil with just a little moisture present.

The smaller the range of particle sizes present (i.e., the more nearly uniform the soil), the smaller the particles, and the more angular the particles, the smaller the minimum density (i.e., the greater the opportunity for building a loose arrangement of particles). The greater the range of particle sizes present, the greater the maximum density (i.e., the voids among the larger particles can be filled with smaller particles).

A useful way to characterize the density of a natural granular soil is with relative density D_r , defined as

$$D_r = \frac{e_{\text{max}} - e}{e_{\text{max}} - e_{\text{min}}} \times 100\%$$

$$= \frac{\gamma_{d \text{max}}}{\gamma_d} \times \frac{\gamma_d - \gamma_{d \text{min}}}{\gamma_{d \text{max}} - \gamma_{d \text{min}}} \times 100\% \quad (3.1)$$

where

 $e_{\min} = \text{void ratio of soil in densest condition}$

 e_{max} = void ratio of soil in loosest condition

e = in-place void ratio

 $\gamma_{d \max} = dry$ unit weight of soil in densest condition

 $\gamma_{a_{\min}} = dry unit weight of soil in loosest condition$

 γ_d = in-place dry unit weight

Table 3.3 characterizes the density of granular soils on the basis of relative density.

Table 3.3 Density Description

Relative Density (%)	Descriptive Term	
0-15	Very loose	
15-35	Loose	MOISTURE 7945
35-65	Medium	
65-85	Dense	NI:
85-100	Very dense	W= MW

Values of water content for natural granular soils vary from less than 0.1% for air-dry sands to more than 40% for saturated, loose sand.

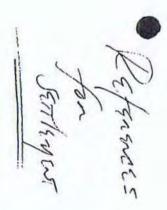
Typical Values of Phase Relationships for Cohesive Soils

The range of values of phase relationships for cohesive soils is much larger than for granular soils. Saturated sodium montmorillonite at low confining pressure can exist at a void ratio of more than 25; saturated clays B. K. Hough, formerly Professor of Civil Engineering at Cornell University and Lehigh University, is presently a consulting engineer with his own consulting firm in Ithaca, N. Y. He has also taught at Massachusetts Institute of Technology. He received his undergraduate and graduate degrees from Massachusetts Institute of Technology. A former student of Professor Terzaghi at M. I. T., he has worked chiefly in soil mechanics ever since, and now has a record of forty years of extensive and varied experience in professional practice, teaching, and research.

BASIC SOILS ENGINEERING

B. K. HOUGH

SECOND



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5-111

values () and 0.270, respectively; a curve plotted on this basis is included in Fig. 5-12 for comparative purposes.

Values of the constants a and b of Eq. (5-7) obtained from tests on laboratory prepared specimens of many different soil types, including those described above, are summarized in Table 5-1. The values given

TABLE 5-1 Values of the Constants of Equation (5-7) for Typical Materials Value of Constant Type of Soil Uniform cohesionless material (C. ≤ 2) Clean gravel 0.05 Coarse sand 0.06 0.50 Medium sand 0.07 SP Fine sand 0.08 Inorganic silt 0.10 Well-graded, cohesionless soil Silty sand and gravel 0.00 35 Clean, coarse to fine sand 0.12 0125 D. 15--- Coarse to fine silty sand 0.18 0.21 Sandy silt (inorganic) 10,23 Inorganic, cohesive soil 0 20 - Sill, some clay; silty clay; clay Organic, fine-grained soil 0.35 Organic silt, little clay * The value of the constant h should be taken as emin whenever the latter is known or can conveniently be determined. Otherwise, use tabulated values as a rough approximation.

for materials such as sand and gravel, which are too coarse for testing in consolidometers of conventional size, represent assumptions based on study of available settlement records.

5-16. GENERALIZATIONS AS TO COMPRESSIBILITY

Before describing procedures for utilizing Eq. (5-7) for evaluation of the compression index in practical applications, it may be instructive to consider certain general aspects of compressibility which are evident from the discussion which has thus far been presented. These generalities may be stated in the following manner.

At a given void ratio, a (confined) uniform material is less compressible than one which is well graded.

Conidering (confined) uniform materials at a given void ratio, the

Soils in general with bulky, angular, or rounded part's are iess compressible than those with flat particles.

Clays with needle-shaped particles, such as attapulgite (and to a lesser degree, halloysite), are less compressible than those with plate-shaped particles, montmerillenite (plate-shaped particles plus expanding lattice) in particular.

Materials of any given type which include significant amounts of mica and/or organic matter are more (sometimes considerably more) compressible than those of the same type which do not.

As an overall generalization, the greater its void ratio prior to loading, the greater is the compressibility of any given soil type; and vice versa.15

5-17. INITIAL DENSITY OF SOIL FORMATIONS

It is evident that information on the original, "no-load" void ratio of a formation must be available if the C_c , c_c relationship is to be used directly for estimating soil compressibility. A rather general impression apparently exists to the effect that sedimentary formations, at least, are laid down initially in a condition approximating their maximum void ratio. Skempton's work suggests that this is true in the case of fine-grained sedimentary formations, clay in particular. Coupled with this belief is the assumption that the present, in-place condition of such formations is entirely the result of loading subsequent to deposition. If these assumptions could be completely accepted, the value c_{max} could be substituted for c_0 in Eq. (5-7) and application of the equation would be greatly simplified.

Unfortunately, there are many reasons for doubting the general appearability of such assumptions as the above. For example, in a texturally uniform deposit of fine-grained sand or silt, if these assumptions were valid, the void ratio of the material would steadily decrease with depth and at any given depth would have the same value at points which laterally are some distance apart. The finding of such a condition in a natural formation, however, is very much more the exception than the rule. In many cases, void ratio varies quite unpredictably both laterally and with depth. Most surprising to the layman, perhaps, is the finding that void ratio often increases with depth, loose sand layers being found beneath more compact surface layers and soft clay intervals underlying stiff clay.

The construction of conversion diagrams based on use of the C_c , c_a relationship in the manner described in the next section is often helpful

[&]quot;This, of course, is the je i cation for the expenditure of siderable sums of money to compact both car a till and natural soil formations to leading.

rield Compression Diagrams

-18. DEFINITION

As the term is used in this book, a field compression diagram is a essure-void ratio curve originating at or passing through a point which presents the in-place density of an element in a natural soil formation earth fill and the existing overburden pressure.

-19. CONSTRUCTION AND UTILIZATION

The recommended construction should be performed on semilog paper ith pressure and void ratio scales appropriate to the conditions of the roblem. The void ratio scale should cover the range from cmay to cmin or the material in question. For the pressure scale, it is usually sufficient make provision for two logarithmic cycles ranging from 0.1 to 1.0 and om 1.0 to 10.0 tons per sq. ft., respectively.

A pressure-void ratio curve originating at $e = c_{max}$ and p = 0.1 ton er sq. ft. is then constructed as shown in Fig. 5-14, by utilization of ic relationship,

$$C_e = a(c_{\max} - b)$$

or clay soils, enax can be taken as the void ratio at the liquid limit. or other soil types, an indication of emar can be obtained by reference Table 2-3 or by test on representative material. Although of less ractical importance, it may be of interest to draw a second diagram, riginating at emin. The latter may be assumed to be a horizontal line. The two diagrams described above establish limits on the area within hich a point representing the in-place condition of the soil will fall cept in a very few cases, which are mentioned later. Points A, B, nd C in Fig. 5-14 represent examples of in-place condition points for dinary situations.

If a plotting of the in-place void ratio and overburden pressure for soil element of any type results in a point such as point A, close the uppermost limiting diagram, it may reasonably be assumed that e material was laid down in an approximation of its loosest condition id that the subsequent reduction in void ratio was due entirely to eight of present overburden. If the soil is a cohesive type it would

tio and pressure plot at point B, it should be pressure a, that it is precompressed and that the field compression diagr

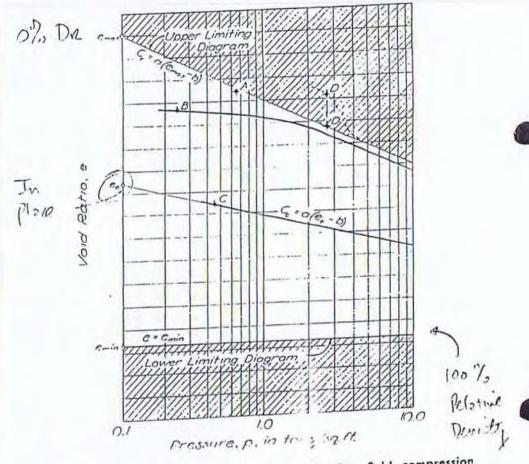


Illustration of procedure for contracting field compression Fig. 5-14. dingrams.

will resemble that shown by the full line day am through B in Fig. 5-14. This plotting provides a reasonable tues for recommending a program of undisturbed sampling and labor or testing even though greater than ordinary expense may be involve-

7.9 Swell Index (C,)

However, if the e vs. log p curve is given, it is possible to simply pick Δe off the plot for the appropriate range of pressures. This figure may be substituted into Eq. (7.18) for calculation of settlement, S.

Reference No. 4

Settlement

7.8

Compression Index (Cc)

The compression index for calculation of field settlement due to consolidation can be determined by graphic construction (as shown in Figure 7.12) after obtaining laboratory test results for void ratio and pressure.

Terzaghi and Peck (1967) suggest the following empirical expressions for compression index:

for undisturbed clays

$$C_o = 0.009\langle IL - 10 \rangle \tag{7.24}$$

for remolded clays

$$C_c = 0.007(LL - 10)$$
 (7.25)

where LL = liquid limit, in percent

In the absence of laboratory consolidation data, Eq. (7.24) is often used for approximate calculation of primary consolidation in the field.

Several other correlations for compression index are also available now. They have been developed by testing various clays. Some of these correlations are given in Table 7.1.

7.9

Swell Index (C,)

The swell index is appreciably smaller in magnitude than the compression index and can generally be determined from laboratory tests. In most cases

$$C_s = \frac{1}{5} \text{ to } \frac{1}{10}C_c$$
 (7.26)

Table 7.1 Correlations for Compression Index, C.

Equation	Reference	Region of applicability
$C_c = 0.007(LL - 7)$	Skempton	Remolded clays
$C_c = 0.01 w_N$		Chicago clays
$C_e = 1.15(e_O - 0.27)$	Nishida	All clays
$C_c = 0.30(e_O - 0.27)$	Hough	Inorganic cohesive soil: silt, silty clay, clay
$C_c = 0.0115 w_N$		Organic soils, peats, organic silt, and clay
$C_c = 0.0046(LL - 9)$		Brazilian clays
$C_c = 0.75(e_O - 0.5)$		Soils with low plasticity
$C_c = 0.208e_O + 0.0083$		Chicago clays
$C_c = 0.156e_O + 0.0107$		All clays

^{*}After Rendon-Herrero (1980)

Note: $e_0 = in situ$ void ratio; $w_N = in situ$ water content

(7.17)

(7.18)

igure 7.12)

(7.19)

ssion index

(7.20)

ided into a parately for e given as

layer i

e vs. log p proximately und curve,

(7.21)

(7.22)

(7.23)

Boring B-20

Final Stress

Top EL	Floor	Material	Depth	Unit Weight	Stress	Floor	Top of Boring	Material	Depth	Jnit Weigh	Stress	Total Final
(ft)	(ft)		(ft)	(pcf)	(psf)	(ft)	(ft)		(ft)	(pcf)	(psf)	
142	79.11	Class III	62.89	50	3,144.5	79.11	75.23	Clay Barrier	3.88	104	403.5	3,548.0

						End Layer	Mid-Layer	Initial	Final			Computed	Adjusted	
					Weight	Stress	Stress	Stress	Stress	Eo	Cc	Settlement	Settlement	Comment
Soil Layers	Type	(ft-total)	(ft-mid)	SPT N	(pcf)	(psf)	(psf)	(psf)	(psf)			(ft)	(ft)	
Ground EL 75.23								0						Note: Settlement numbers are conservative
	SP1	3.23	1.615	2-10	102.9		166.2	166.2						since ground level in 2004 used to compute
SHGWT EL 72						166.2		332.3						initial stress in soils; however, no adjustment
	SP1	2.77	1.385	2-10	119.6		79.2	411.6	3,548.0	0.875	0.03375	0.05		made to ground surface (ie. prior to
EL 69.23						79.2		490.8						excavation of soils, Borings in 2001, DCL01-
	SC3	4	2	16	126.8		128.7	619.5	3,548.0	0.6	0.092	0.19		13&-15, recorded ground EL of 94 to 99 in
EL 65.23						128.7		748.2						this area), thus soils previously under higher
	CL3	6	3	13-50	128.4		198.0	946.2	3,548.0	0.56	0.09806	0.26		stress. Settlement is based on the net
EL 59.23						198.0		1,144.2						increase in soil stresses from initial
														conditions.
	END	16			•									
												0.49	ft - Estimate	d Settlement

Boring B-26

Final Stress

Top EL	Floor	Material	Depth	Unit Weight	Stress	Floor	Top of Boring	Material	Depth	Jnit Weigh	Stress	Total Final
(ft)	(ft)		(ft)	(pcf)	(psf)	(ft)	(ft)		(ft)	(pcf)	(psf)	
150	79.8	Class III	70.2	50	3,510.0	79.8	75	Clay Barrier	4.8	104	499.2	4,009.2

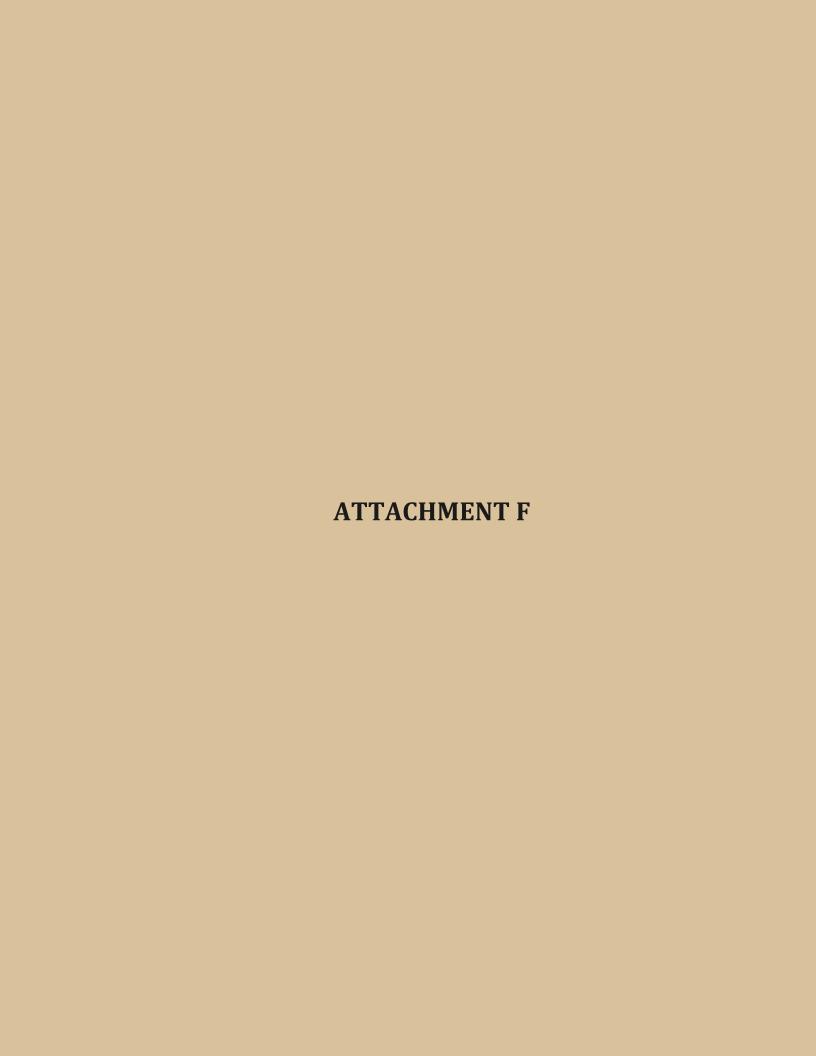
						End Layer	Mid-Layer	Initial	Final			Computed	Adjusted	
					Weight	Stress	Stress	Stress	Stress	Eo	Cc	Settlement	Settlement	Comment
Soil Layers	Type	(ft-total)	(ft-mid)	SPT N	(pcf)	(psf)	(psf)	(psf)	(psf)			(ft)	(ft)	
Ground EL 75								0						Note: Settlement numbers are conservative
	SP2	3	1.5	7-16	117.6		176.4	176.4						since ground level in 2004 used to compute
SHGWT EL 72						176.4		352.8						initial stress in soils; however, no adjustment
	SP2	20.82	10.41	7-16	127.8		680.5	1,033.3	4,009.2	0.575	0.03375	0.31		made to ground surface (ie. prior to
EL 51.18						680.5		1,713.8						excavation of soils, Borings in 2001, DCL01-
	SP1	23.98	11.99	2-7	119.6		685.8	2,399.6	4,009.2	0.03375	0.03375	0.33		13&-15, recorded ground EL of 94 to 99 in
EL 27.2						685.8		3,085.5						this area), thus soils previously under higher
	CL1	12.2	6.1	3-5	100.8		234.3	3,319.8	4,009.2	1.68	0.27278	0.43		stress. Settlement is based on the net
EL 15						234.3		3,554.2						increase in soil stresses from initial
														conditions.
	END	60												
												1.07	ft - Estimate	d Settlement

Boring B-22

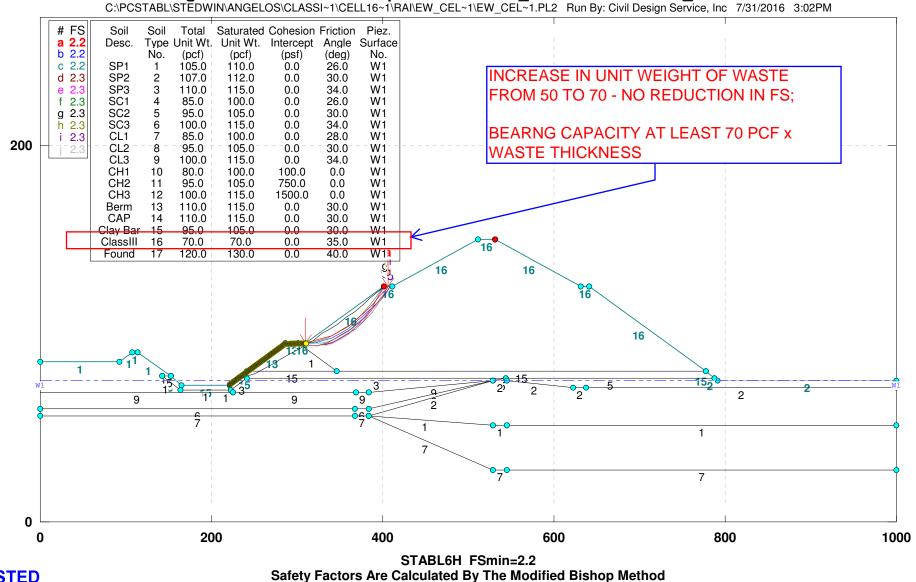
Final Stress

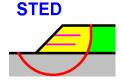
Top EL	Floor	Material	Depth	Unit Weight	Stress	Floor	Top of Boring	g Material	Depth	Jnit Weigh	Stress	Total Final
(ft)	(ft)		(ft)	(pcf)	(psf)	(ft)	(ft)		(ft)	(pcf)	(psf)	
150	80.3	Class III	69.7	50	3,485.0	80.3	75.18	Clay Barrier	5.12	104	532.5	4,017.5

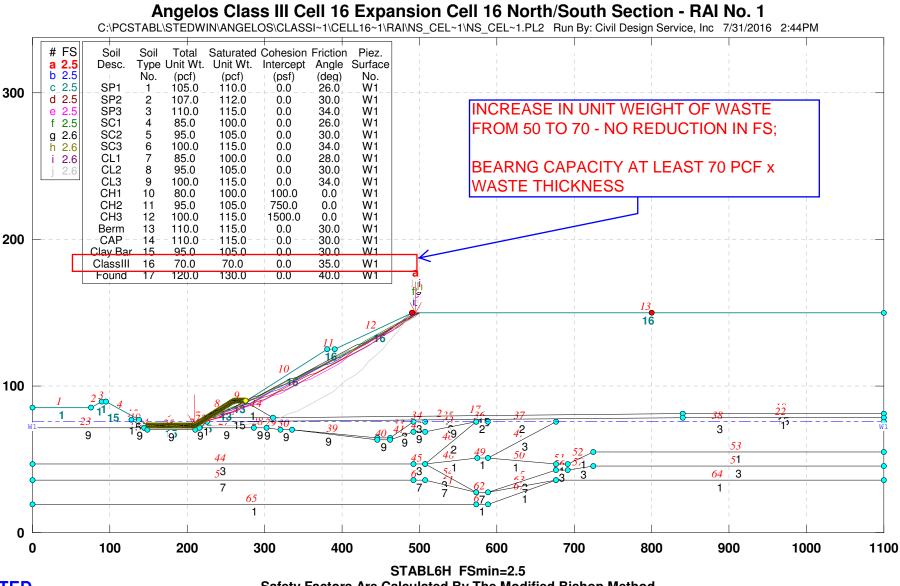
						End Layer	Mid-Layer	Initial	Final			Computed	Adjusted	
					Weight	Stress	Stress	Stress	Stress	Eo	Cc	Settlement	Settlement	Comment
Soil Layers	Type	(ft-total)	(ft-mid)	SPT N	(pcf)	(psf)	(psf)	(psf)	(psf)			(ft)	(ft)	
Ground EL 75.18								0						Note: Settlement numbers are conservative
	SP3	3.18	1.59	16-58	117.6		187.0	187.0						since ground level in 2004 used to compute
SHGWT EL 72						187.0		373.9						initial stress in soils; however, no adjustment
	SP3	25.82	12.91	16-58	127.8		843.9	1,217.9	4,017.5	0.3875	0.03375	0.40		made to ground surface (ie. prior to
EL 46.18						843.9		2,061.8						excavation of soils, Borings in 2001, DCL01-
	SP1	4	2	10-18	119.6		114.4	2,176.2	4,017.5	0.575	0.03375	0.04		13&-15, recorded ground EL of 94 to 99 in
EL 42.18						114.4		2,290.6						this area), thus soils previously under higher
	SP3	7	3.5	11	100.8		134.5	2,425.1	4,017.5	0.8	0.03375	0.06		stress. Settlement is based on the net
EL 35.18						134.5		2,559.5						increase in soil stresses from initial
	SP1	6	3	7	119.6		171.6	2,731.1	4,017.5	0.8	0.03375	0.04		conditions.
EL 29.18						171.6		2,596.7						
	END	46												
												0.54	ft - Estimate	d Settlement



Angelos Class III Cell 16 Expansion Cell 16 _ East/West Section _ RAI No. 1 C:\PCSTABL\STEDWIN\ANGELOS\CLASSI~1\CELL16~1\RAI\EW_CEL~1\EW_CEL~1.PL2 Run By: Civil Design Service, Inc 7/31/2016 3:02PM









Safety Factors Are Calculated By The Modified Bishop Method

SECTION 3

ENGINEERING REPORT

Appendix 3-A	Operations Plan
Appendix 3-B	Contingency Plan

Appendix 3-C Figures

Appendix 3-D Well Abandonment

Documentation

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY MAJOR PERMIT MODIFICATION ENGINEERING REPORT

Prepared for:

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March 2016 March 2016 Revised July 2016 (RAI 1 Response)

ENTERPRISE RECYCLING AND DISPOSAL FACILITY ENGINEERING REPORT

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3.10.3

APPENDIX D	GROUNDWATER MONITORING PLAN
APPENDIX E	SLOPE STABILITY ANALYSIS
APPENDIX F	CLOSURE AND RECLAMATION PLAN
APPENDIX F-1	FINANCIAL ASSURANCE COST ESTIMATES
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SECTION 3 ENGINEERING REPORT

3.1 GENERAL

This Engineering Report is part of a comprehensive Florida Department of Environmental Protection (FDEP or Department) permit modification application for the Enterprise Road Class III Recycling and Disposal Facility (Facility) submitted by Locklear & Associates, Inc. (L&A) in March 2016 on behalf of Angelo's Aggregate Materials, Ltd. (Applicant). The Engineering Report is designed to meet the requirements of Rule 62-701, F.A.C. and Pasco County's Land Development Code (LDC) and includes the following major components (and their respective location within this Engineering Report):

- Plan Set dated March 2016, titled 2016 Plan Set, by Locklear & Associates, Inc. (Appendix ASection 4) (Appendix A);
- Figures (Appendix B 3-C) (Appendix B);
- An evaluation of the applicability of bottom liner and leachate collection system requirements (Appendix CSection 2, Part G, G-1) (Appendix C);
- Updated report evaluating geotechnical site conditions (Appendix C, Attachment 1Section 2, Part I, I-1) (Appendix C, Attachment 1);
- Updated Groundwater Monitoring Plan (Appendix D) (Appendix D);
- An analysis of slope stability (Appendix ESection 2, Part I, I-2) (Appendix E);
- Updated Closure and Reclamation Plan (Appendix FSection 7) Appendix F;
- Updated financial assurance cost estimates (Section 7 Appendix F-1 7-A) (Appendix F-1);
- Updated Operations Plan (Section 3 Appendix G 3-A) (Appendix G);
- Updated Contingency Plan (Section 3 Appendix H 3-B) (Appendix H).

3.2 SITE LOCATION AND DESCRIPTION

The facility receives approximately 550 tons per day of Class III waste, which includes Construction and Demolition debris, from Pasco County and other surrounding Counties (including Pinellas, Hernando, Hillsborough and Polk). The Facility was originally permitted by the Department on October 5, 2001.

The subject site is located in Sections 5 and 8, Township 25 South, Range 22 East, in Pasco County, Florida, as shown on the United States Geological Survey (USGS) quadrangle map presented in Figure 1 of Appendix B Figure 3-1 in Appendix 3-C Figure 1 of Appendix B. More specifically, the Facility is located at the northwest corner of the intersection of Enterprise Road and Auton Road, southeast of Dade City, Florida (Figure 3-1 in Appendix 3-C see Figures)

2 and 3 of Appendix B). The site occupies approximately 160 acres of land on the north side of Enterprise Road. The square property is approximately 2,640 feet on a side and is located in the southwest quarter of Section 5 and the northwest quarter of Section 8.

There are no airports within 5 miles of the site, see <u>Figure 4 (Appendix B)</u> <u>Figure S-4 (Appendix B)</u>.

3.2.1 <u>Prohibition Compliance</u>

In order to comply with Rule 62-701.300, F.A.C., the Facility will abide by the following:

- The Facility will not dispose of solid waste at the proposed site until proper permitting is obtained.
- Disposal of solid waste will not occur in areas that are: unable to provide support for the waste; geological formation or subsurface features that would allow unimpeded discharge to surface water on groundwater; are within 500 feet of an existing potable water well (Figure 5 in Appendix B) (Figure S-1 in Appendix 3-C) (Figure 5 in Appendix B); are within a dewatered pit; are in a frequently flooded area; are in a body of water; are within 200 feet of a surface water body that discharges offsite (Figure 6 in Appendix B) (Figure S-2 in Appendix 3-C) (Figure 6 in Appendix B); are on a right of way; are within 1,000 feet of an existing community potable water; or are within 3,000 ft. of Class I surface waters (Figures 5 and 6 in Appendix B) (Figure S-3 in Appendix 3-C) (Figures 5 and 6 in Appendix B).
- Open burning will not occur on the site unless the burning takes place in a permitted air curtain incinerator.
- Hazardous wastes, PCB's, biohazardous wastes, special wastes, liquids, and oily
 wastes will not be disposed of at the Facility. Random load checks and the use of
 spotters at the working face will ensure that these wastes are not placed for disposal
 at the Facility.

3.3 SURROUNDING LAND USES AND ZONING

<u>Figure 7 (Appendix B) Figure 3-2A in Appendix 3-C Figure 7 (Appendix B)</u> presents an aerial photograph map depicting the surrounding land uses and designated FDOT FLUCCS codes in the site vicinity. Open land, pastureland, row crop, tree crop, and upland hardwood forest land uses surround the site. A few scattered residences also surround the site. All adjoining properties

are zoned AC. To the north is the East Pasco County Class I Sanitary Landfill, which is closed. To the east is an old borrow pit and agricultural land. South of the site is agricultural land and orange groves, and to the west are orange groves. Figure 8 (Appendix B) Figure 3-2A in Appendix 3-C Figure 8 (Appendix B) presents an aerial photograph map with future land use classifications.

Current site zoning designation, AC with a conditional use, is consistent with the Class III Landfill use. Figure 5 Revised Figure S 1 in Appendix 3 C5 depicts the locations of five (5) two (2) water wells proximate to the landfill limit. The well north of Cell 13 has been abandoned. The on-site non-potable Supply Well is operated and maintained by the facility and only utilized to flush on-site toilets. The well approximately 1000' south of the southeast corner of the facility is identified as "irrigation" by SWFWMD. The 500-foot setback from the approved landfill footprint to_potable wells complies with the setback requirements of Rule 62-701.300(2)(C), F.A.C.

3.4 TOPOGRAPHY

The USGS 7.5 minute quadrangle map shown in Figure 1 (Appendix B) Figure 3-1 in Appendix 3-C Figure 1 (Appendix B) shows the land surface of the subject site has elevations ranging from 85 feet to 175 feet National Geodetic Vertical Datum (NGVD). Natural land surface generally slopes to the northeast on the northern half of the property and southeast on the southern half of the site. A 2013 site-specific topographic survey is shown on Sheets 1 and 2 of the 2016 Plan Set provided in Appendix ASection 4 Appendix A.

3.4.1 100-Year Flood Prone Areas

Figure 9-Figure S-5 of the 2013 permit renewal application (which refers to the July 2006 Enterprise Recycling and Disposal Class III Landfill Response to 2nd Request for Additional Information, dated July 5, 2006 prepared by Jones Edmunds) Figure 9, depicts a 100-year flood prone area map from the U.S. Federal Emergency Management Administration for the subject vicinity. As shown, the site is not within and would not be impacted by an estimated 100-year storm flood.

3.5 SOILS

According to the Soil Survey of Pasco County, Florida, published by the U.S. Department of Agriculture Soil Conservation Services (USDA-SCS), the majority of the subject site and surrounding areas are covered by fine sands. A copy of the USDA-SCS Soils Survey Map showing the mapped areas of the major soil types at the subject site and its vicinity is presented in Figure 10 Figure 3-5 Soil Survey Map, as referred to in the 2013 permit renewal application as

submitted as part of the 2005 Enterprise Recycling and Disposal Facility Class III Landfill Permit Renewal Application, Pasco County, dated August 2005, prepared by Tetra-Tech HAI (TTHAI).

USDA-SCS soil type 12- Astatula fine sands encompass a small portion in the northeast portion of the site. Astatula sands are nearly level to gently sloping, and excessively drained mainly in the sandhills. Seasonal high water table (SHWT) is typically at a depth of 72 inches in Astatula soil. The permeability is very rapid throughout the soil. Both the available water capacity and natural fertility of the Astatula soil are low.

USDA soil type 32 - Lake fine sands comprise the majority of the soils found on the property. These soils are nearly level to gently sloping and excessively well drained. They occur along ridgetops and on low hillsides in the uplands. Permeability is rapid throughout the soil and the water table is below a depth of 120 inches. The available water capacity is very low in all layers and the natural fertility and organic matter content are both low.

USDA soil type 72 - Orlando fine sands are found in a small area in the northeast portion of the property. These soils are nearly level to gently sloping and well drained. The water table is typically at a depth greater than 72 inches with permeability of the soil rapid throughout. The available water capacity is low in the surface layer and very low in the other layers.

3.6 LANDFILL SITE IMPROVEMENTS

Portions of the 160-acre landfill site are also currently being operated as orange groves. The following site improvements have been installed to meet landfill operational requirements.

3.6.1 Entrance Facilities

An office trailer (gatehouse) is located onsite for the gate attendant. This trailer has hand washing and toilet facilities. Potable bottled water is supplied to the trailer. Electric and telephone services are available to the trailer office. Site entrance improvements also include an all-weather entrance roadway, scales and perimeter road as shown in Sheet C0.02 of the 2016 Plan Set provided in Appendix A Section 4.

3.6.2 Roads

The primary haul route servicing the Facility is Enterprise Road. Enterprise Road is serviced by Clinton Avenue and C.R. 35A.

Enterprise Road has been improved to an all-weather access roadway from C.R. 35A to the

entrance of the Facility. All on-site roads are maintained by the Applicant to allow for all weather access. Access roads to the working face are constructed from on-site soils and/or recovered materials such as concrete and asphalt. This is done on an as needed basis

3.6.3 Effective Barrier

A 6-foot high security fence has been constructed along the south and east boundaries. The security fence consists of a 6-foot high-galvanized chain link fence, hereafter referred to as the "security fence." A five-foot wire fence runs along the north and west property boundaries. The chain link fence has been installed in accordance with the permit issued October 2001. Three (3) foot square "NO TRESPASSING" signs with 5-inch letters have been installed at no less than 500-feet spacing and at all corners to notice unauthorized access. The only point of access into the facility will be through the gate at the entrance. This gate will be locked during closed hours.

An 8-foot high landscape berm has been constructed along the site's frontage to Enterprise and Auton Roads, see Sheet C0.02 of the 2016 Plan Set provided in <u>Appendix ASection 4</u>.

3.6.4 Weighing or Measuring Incoming Waste

A scale system is used to keep records of materials received at the Facility. The scales are calibrated every six (6) months. Vehicles are weighed when they enter the Facility, and based upon the tare weight of the vehicle, the waste tonnage will be determined. Prior to unloading debris, the tonnage or volume of waste materials received will be determined and the appropriate fee assessed.

3.6.5 Vehicle Traffic Control and Unloading

Generally, truck traffic will be controlled on a first-in, first-out basis, as directed by the spotter at the working face. There is adequate space for truck staging at the site's entrance gate (7-8 trucks) to mitigate any queuing onto Enterprise Road. The Facility will discourage any truck staging prior to landfill opening. Signs will be posted at the entrance gate and on interior roads to guide truck traffic.

3.7 EXCAVATION OPERATIONS AND CELL CONSTRUCTION

On-site soils will be excavated according to the Pasco County Class I Mining Permit. The soils will be excavated and removed for various uses, including construction, roadways, and in landfilling operations. The County permit allows an excavation up to within a 200-foot setback from the property boundary and an excavation slope of 6H:1V. The Class I Mine will be "reclaimed" as a Class III landfill. The 6H:1V excavation slopes are associated with the mining

of the existing soil. Once the landfill is ready to accept waste, the mine side slopes will be excavated to 2H:1V side slopes (cell slopes). Waste will be placed against this excavated slope and then built above existing grade. Drawing Sheets C1.00 and C1.10 of the 2016 Plan Set (Appendix A Section 4) show the phasing of the cell construction and filling operation at the Facility.

Excavation slopes will not exceed 6H:1V pursuant to the Pasco County permit; however, once an excavation phase is complete and construction commences on a new cell, the slopes will be excavated to 2H:1V. A portion of the excavated soils from the mining operation will be used as landfill construction material. Excavated soils will be reserved to provide adequate cover material for the landfill operation. Cell construction will follow the sequence described in Section 3.8.

As new cells are excavated and constructed, the cells will be overexcavated to approximately three-feet below the approved excavation base grade to allow for the construction of a 3' clay <u>layer liner</u>. If limerock is encountered during construction, the following actions will be taken:

Where limerock is encountered at or below the elevation of the cell clay layer:

- In the event that limerock is encountered during clay layer excavation or construction activities, the excavation / construction activities shall cease and the Department shall be notified by email within 24 hours of discovery.
- Excavation / construction activities related to determining location, elevation, and extent of limestone or to remediation in accordance with these procedures will resume no sooner than 24 hours after notice, unless otherwise directed by the Department
- Written notification will be submitted within 7 days of discovery.
- The written notification shall include the location, elevation, and extent of limestone noted on a plan sheet, a description of the materials encountered, and a description of the completion of excavation / clay backfill in the identified area or the anticipated timeframe for completion of these activities.
- The limerock will be over-excavated (5-feet laterally beyond limerock boundary and 3-feet vertically below the bottom of the compacted clay layer) and the area backfilled with clay meeting the specifications in the FDEP Operation/Construction permit and Engineering Report.
- Excavation / construction activities will resume no sooner than 24 hours after notice, unless otherwise directed by the Department

Where limerock is encountered during mining operations at elevations above the elevation of the cell clay layer and do not extend into the clay layer:

- Document on the limerock observation log the location, elevation, and extent of limestone noted on a plan sheet, and a description of the materials encountered
- Submit limerock observation log to FDEP within 7 days of discovery
- Where limerock is encountered within 10-feet of the design elevation of the top of compacted clay layer, in addition to the procedures noted above, overexcavate 1-foot vertically and laterally around the exposed limerock and backfill with compacted clay to temporarily prevent infiltration during mining operations.

If limerock encountered during mining operations at elevations above the cell clay layer extends to or below the elevation of the cell clay layer, the procedures identified above under the heading "Where limerock is encountered at or below the elevation of the cell clay layer" shall be followed.

Stockpiled clay, obtained from on-site excavation, will be sampled for laboratory proctor testing for use as cell floor and cell side slope material to construct a three-foot thick clay barrier layer. Material with acceptable permeability and proctor test results will be placed onto the constructed

cell floor in lifts, and compacted by multiple passes with a 40,000 lb, D-6 Dozer, or equivalent.

A three-foot thick clay layer will also be placed on the 2H:1V side slopes of the exterior excavation side slopes of the perimeter cells Cell 7 to complete the continuous clay barrier layer. Due to the steepness of the slope, clay placement and compaction will require an iterative process consisting of several horizontal lifts, stepped up progressively until the base elevation of the landfill is reached. In order to achieve the required compaction and hydraulic conductivity, as well as to achieve a constant three feet of clay along the slope, each lift along the cell wall will need to exceed three feet wide and be wide enough for the compacting equipment. Construction of the clay side slopes is shown on Drawing C3.00 of the 2016 Plan Set provided in Appendix ASection 4. Soil in excess of three feet wide on the slopes may be removed after compaction and compliance testing have been approved. Acceptable test results means the results of the laboratory proctor and permeability tests indicate that the permeability of the material meets the requirements of the construction permit (1x10⁻⁷ cm/s), and the optimum moisture content is not too high for the equipment to manage. Optimum moisture content for the on-site stockpiles has been approximately 13 to 20 percent.

The dozer will compact the material in the bottom of the excavation and up the side slopes into the dozer track marks. After each lift is compacted with the dozer, a 12-ton, 84-inch vibratory sheeps-foot roller, or equivalent, will be used to roll the material. The daily activities will be recorded, including any tie-in locations, thickness of each compacted lift, verification of the compaction and moisture content testing, verification of equipment used for compaction, and verification of dozer tracks at the tie-in surfaces (no smooth surfaces). Field logs and photographs documenting the field work will be provided to the Department. A topographic survey will confirm the top of excavation and top of clay grades.

Excavation will be such that 2H:1V slopes will only be encountered on the outer edge boundaries of the Cells 7. A 3H:1V working face slope, beginning at the 2H:1V slope face, will be used for landfilling the waste.

A berm will be constructed along the northern outer edge boundaries of Cells 6B and 7 to account for mining excavation in this area. Stockpiled clay obtained from on-site excavation to be utilized for berm construction shall be sampled consistent with the procedures described for the clay barrier layer and demonstrate acceptable test results, as described above. A detail of the berm and tie-in is provided on sheet C-5 of the 2012 permit modification Plan Set provided by Kelner Engineering and on sheet C1.00 of the 2016 Plan Set in Section 4.

3.8 METHOD OF CELL SEQUENCE

Filling activities are currently (as of March 2016) occurring in Cells 6 and 6B of the Class III

Landfill. The cell construction and filling sequence operations will be as follows (see Drawing Sheets C 1.00 and C1.10 of the 2016 Plan Set provided in Appendix A):

Phasing Sequence 1	Fill Cells 6, 6B, 7, 1, 2, 3, 4, 5 and 15 in 10—12 foot lifts from base grade to elevation 150', including filling over Cells 1—5, and 15. Maximum side slope is 3H:1V. 10 ft wide stormwater benches are to be constructed at elevation 125' and 150'. Construction of Cell 16 will be ongoing during Phasing Sequence
	1
Phasing Sequence 2	Complete construction of Cell 16 per Sheet C1.00 of the drawing set in Appendix A. Continue filling Cell 7 and begin filling Cell 16 in 10 – 12 foot lifts from base grade to elevation 150', including filling over Cells
	1—6 and 15. Maximum side slope is 3H:1V. 10-ft wide stormwater benches are to be constructed at final cover elevations 125' and 150'.
Phasing Sequence 3	Continue filling Cells 1 through 7, and 16 in 10 – 12 foot lifts from base grade to elevation 150', including filling over Cells 1 – 6, and 15. Maximum side slope is 3H:1V and minimum 2 % grade from final cover elevation 170' to 175';
	10 ft wide stormwater benches are to be constructed at elevation 125' and 150'. Cover elevations noted include 18" intermediate cover and 18" top soil layer. Fill elevations shall be such that design cover elevations will be achieved on all external slopes.
	Sideslope berms and stormwater appurtenances are to be constructed at final closure. serials is currently (as of March 2016) filling in Cells 1 – 6 and 15 of the construction of Cell 7 is being completed. The cell construction and ns will be as follows:
Phasing Sequence 1	As shown in Drawing Sheets C1.00 and C1.01 Continue filling Cells 1, 2, 3, 4, 5, 6, 6B, 7 and 15 in 10 – 12 foot

	lifts to waste elevation of 172'
	Maximum slope is 3H:1V from base grade to waste elevation
	122'; 4H:1V from waste elevation 122' to 167'; 1% to 2% grade
	from waste elevation 167' to 172'
	10-ft wide stormwater benches are to be constructed at waste
	elevations 122' and 147'
	Sideslope berms and stormwater appurtenances are to be
	constructed at final closure.
	Construct Cell 16 in accordance with permitted design
Phasing Sequence 2	As shown in Drawing Sheets C1.10 and C1.11
	Begin filling $4-6$ feet lift north of the temporary berm until cell
	is floored out. Remove temporary berm and fill with $4-6$ feet lift.
	Continue filling Cell 16 in 10 – 12 foot lifts from base grade to
	waste elevation 147', including filling over Cell 15. Maximum
	slope is 3H:1V from base grade to waste elevation 122'; 4H:1V
	from waste elevation 122' to 147'.
	A 10-ft wide stormwater bench is to be constructed at elevation
	122'.
	Sideslope berms and stormwater appurtenances are to be
	constructed at final closure.
Phasing Sequence 3	As shown in Drawing Sheets C2.00 and C2.10
	Construct final closure cover system over Cells 1, 2, 3, 4, 5, 6, 6B,
	7, 15 and 16 in accordance with the permitted closure design
	Construct sideslope berms and stormwater appurtenances
	Construct landfill gas vents

Lift height includes cover material. Due to the landfill bottom elevation, some lifts may not be a full 10 feet in height.

As each sequence is active, the following procedures will be followed.

- The access road to the working face will be constructed and graded as necessary.
- Waste will be compacted as it is placed. General lift height will be 10 feet and will come within three (3) feet of the final elevation to provide for final cover.
- The working face will remain approximately 100 feet in length.

- Avoid channelizing stormwater flows
- Use mulch, grass, and maintain intermediate covers
- Use culverts, berms, or the best management practices based on actual weather and site conditions.
- Weekly cover of six (6) inches of soil will be placed on the working face.
- Intermediate cover of 12 inches of soil will be placed in areas that will not receive waste within 180 days. The cover may be removed immediately prior to placement of new waste.
- Stormwater runoff from the interior of the excavation and filling area will be diverted to the onsite temporary storage pond using a temporary interior swale and 6-foot berm. Perimeter berms will direct stormwater away from excavation and filling areas. The temporary stormwater pond will receive runoff until Pond 3 is developed.

3.8.1 <u>Vertical Expansion / Conceptual Closure</u>

The landfill is permitted to be completed to a maximum height of 175 feet, NGVD. The final grading plan is shown on Drawing C2.00 of the 2016 Plan Set provided in Appendix ASection 4 Appendix A. The Conceptual Closure Plan includes permitted Cells 1-7 and 15, and proposed Cell 16.

The Conceptual Closure Plan includes construction of berms on the stormwater benches that will direct stormwater to drop inlets and downcomer pipes spaced approximately every 400 – 500 feet along the benches. The downcomer pipes will discharge through an energy dissipater to the existing stormwater system. The facility's overall stormwater management system is governed by the mining operations and ERP Permits. Grades and elevation vary based on ongoing mining operations and topography. A detailed design that will tie the conceptual closure plan into the facility's stormwater management system will be submitted at the time of closure.

The top (1% to minimum 2% grade) and side slope (4H:1V and 3H:1V) designs provide for proper drainage and minimize rainfall infiltration into the landfill surface.

3.8.2 Erosion Control

The following engineering controls will be used to minimize erosion at the working face:

- Regrade a maximum of 100 linear feet of the outer edge slopes at a time to 2H:1V. The purpose of this recommendation is that a relatively small area will be subjected to surface erosion at any given time.
- Construct a berm along the top of the slope during the regrading to redirect any rainfall runoff away from the face of the slope. The area along the berm should be graded so as to allow rapid runoff along the top of the slope. Ponding of water near the top of the slope should not be allowed, since seepage through the slope may initiate slope erosion.
- As soon as possible following the construction of the clay <u>layerliner</u>, begin to fill against the <u>Cell 7</u> 2H:1V slope with the landfill material.
- For Cell 16 construction, filling shall begin immediately north of the east-west trending berm to be located near the southern boundary of Cell 16. The fill sequencing of Cell 16 is described in Section 3.8.
- Avoid channelizing stormwater flows
- Use mulch, grass, and maintain intermediate covers

Use culverts, berms, or the best management practices based on actual weather and site conditions.

3.8.3 Life Expectancy

The cell capacity and lifespan estimates for Cells 1 - 7, 15 and 16 have been estimated using the November 2013 topographic survey performed by Pickett and Associates (Sheets 1 and 2 of Appendix A Section 4); and recent and projected tonnages.

Using the November 2013 topographic survey as a base, a three-dimensional AutoCAD model of Cells 1-7, 15 and 16 at closure was generated, using the following assumptions:

- 3H:1V sideslopes between grades up to elevation 170'; minimum 2% grade from elevation 170' to elevation 175'.
- For all cells except Cell 16, 3H:1V side slopes from base grade to waste elevation 122'; 4H:1V from waste elevation 122' to 167'; 1% to 2% grade from waste elevation 167' to 172'
- For Cell 16, 3H:1V from base grade to waste elevation 122'; 4H:1V from waste elevation 122' to 147'.
- 10-foot inset for benches at waste elevations 122125-ft and 147150-ft NGVD

• 36 inches of cover over the 67.0 acre 2D surface was subtracted from the maximum volume

The airspace volume remaining as of March July 2016 was calculated to be approximately 2,443,034 2,535,047 yd³ after accounting for the final cover volume of 321,510 322,829 yd³.

The following design parameters were used to compute landfill design life remaining:

- **Density:** An in-place density of 1,350 lb/yd³ (0.675 tons/ yd³) was used for the design life estimate and is a typical density for Class III waste.
- Waste acceptance rate: a waste acceptance rate of 550 tons per day was used based on facility records.

The remaining life in Cells 1 - 7, 15 and 16 was calculated to be 13 years from the survey date, or 2026.

3.9 WASTE COMPACTION AND APPLICATION OF COVER

Waste received will be segregated based on compactibility. Bulky, incompressible items, such as concrete, asphalt, and tree debris, will be separated and stockpiled for future processing. Tree debris may be separated from the waste and periodically mulched on-site. The remaining debris is disposed of in designated cells using onsite equipment to place the debris and a Caterpillar 826 Compactor, or equivalent, to weekly compact the waste. Initial cover material is planned to be excavated from onsite areas and placed weekly in approximately 6-inch layers on the compacted lifts to control vectors, reduce rain infiltration and provide a more stable working face area. An intermediate cover of one (1) foot of compacted soil will be applied if final cover or an additional lift is not to be applied within 180 days of cell completion. Cell closure will occur when all permitted cells are filled. For final buildout grade and closure detail, see Drawing Sheets C2.00 and C2.10 of the 2016 Plan Set provided in Appendix A Section 4, respectively. The Conceptual Closure Plan includes permitted Cells 1-7 and 15, and proposed Cell 16. Fill grades shall be such that final cover elevations are not exceeded on all slopes.

Final cover consisting of 18 inches of compacted soil barrier layer and 18 inches of soil that will sustain vegetative growth, as specified in the Closure and Reclamation Plan provided in Appendix FSection 7. Cell closure shall generally conform to the lines and maximum grades specified on Drawing Sheet C2.00 (2016 Plan Set provided in Appendix ASection 4 and the requirements of Rule 62-701.600 F.A.C., Rule 62-701.400 (7), F.A.C., and Rule 62-701.400(8),F.A.C.. Pesticides when deemed necessary to control rodents, insects and other vectors shall be used as specified by the Florida Department of Agriculture and Consumer

Services. Uncontrolled and unauthorized scavenging shall not be permitted at the landfill site. Controlled recycling may be permitted by the Landfill Manager. Temporary storage of soil fill or recycling materials may occur within the inactive, or closed cell areas.

3.10 DESIGN OF GAS, LEACHATE AND STORMWATER CONTROLS

3.10.1 Gas Monitoring and Control

The type of materials to be disposed of in the Class III Landfill are not expected to generate significant amounts of methane or other gases since the landfill's design prevents groundwater contact. Therefore, no active gas control systems or venting is proposed. However, because some biodegradable waste may be accepted, a passive gas control system is proposed, see Section 3.10.1.5. The Landfill Manager will conduct daily and weekly inspections of the landfill and will check for objectionable odors or gas around the perimeter of the site. The Manager will notify the FDEP of any exceedances and immediately take corrective actions. Corrective actions will include placement of additional cover material or mulch, or lime containing materials such as crushed concrete that is documented to abate the odors. Quarterly gas point monitoring is currently conducted. The facility only accepts Class III debris for disposal and accepts no putrescible household wastes. Surface water and groundwater contact with the Class III wastes will be prevented by the approved facility design. Other best management practices to prevent odors include: 1) closure of each cell as it is completed; 2) weekly soil cover application; and, 3) immediate corrective actions to abate any detected onsite odors.

3.10.1.1 Gas Probe Locations

Gas monitoring points are spaced approximately 600 linear feet apart surrounding the landfill. Sheet C0.03 of the 2016 Plan Set provided in Appendix ASection 4 presents these locations of the gas probes surrounding the landfill. Gas Probes (GP) 6 through 15 are existing, GP 1 through 5 and 16 are proposed and will be installed as part of future cell construction completion certification at closure. The remaining gas probes are to be installed in accordance with the following schedule in Table 3.10:

Table 3.10 Gas Probe Installation Schedule	
Gas Probe	Cell Construction Completion
GP-1	Future Cell 10 or closure
GP-2	Future Cell 11 or closure
GP-3	Future Cell 12 or closure
GP-4	Future Cell 13 or closure
GP-5	Future Cell 14 or closure

GP-16	Future Cell 9 or closure
-------	--------------------------

Several existing gas probes on the southern and eastern portion of the property are currently located immediately adjacent to the disposal area rather than at the property boundary as required by Rule. Probes GP-6, -7, -8, -11, 12, 13, and -14 will be relocated to the property boundary as part of the construction activities for Cell 16. <u>Probes GP-12 and -13 were abandoned and replaced with GP-12R and -13R along the property boundary in 2013.</u>

3.10.1.2 Gas Probe Design

Figure 3-14 (provided in Appendix 3-C of the 2012 permit renewal application submitted by Kelner Engineering) presents the gas probe design for the subject landfill site. These gas probes are designed to be surface sealed and to provide a greater permeability than the surrounding sediments to act as collector points for any methane gas, if present. Based on the landfill design, all of the gas probes are designed to be approximately 20-foot in depth with an 18-foot open screen for the monitoring point, or to depth of adjacent waste. Table 3.10.1.2 presents supplemental information related to the anticipated total depths of gas monitoring probes GP-6R, GP-7R and GP-8R. This These depths will allow the screened interval to intercept the full cross-section of the landfilled waste that could potentially generate methane.

Table 3.10.1.2

Well	Elevation of the	Elevation at	Total Depth	Top of Perforated	Bottom of
	Bottom of Waste in the	Surface (ft.,	<u>(ft.)</u>	Section (ft.,	Perforated Section
	Adjacent Disposal Cell	NGVD)		NGVD)	<u>(ft., NGVD)</u>
	(ft., NGVD)				
<u>GP-6R</u>	<u>78</u>	<u>90</u>	<u>20</u>	<u>88</u>	<u>70</u>
<u>GP-7R</u>	<u>78</u>	<u>90</u>	<u>20</u>	<u>88</u>	<u>70</u>
<u>GP-8R</u>	<u>78</u>	<u>90</u>	<u>20</u>	<u>88</u>	<u>70</u>

The groundwater table may be encountered at depths of approximately 50-foot, or more below land surface (bls) across most of the site. Accordingly, gas probes are not designed to intercept the groundwater table. The gas probes are constructed of Schedule-40 polyvinyl chloride plastic pipe (PVC). The PVC casing and screen will be flush-threaded and have a screen slot size large enough to accommodate easy methane extraction from the monitoring point. The sand/bentonite slurry proposed for a surface seal will be a blend of 4 parts of sand to one part of granular bentonite. The sand and the bentonite will be mixed dry and hydrated immediately prior to placing it in the annular space of the borehole. The gas probe points are proposed to be installed by hollow-stem auger to construct an eight-inch borehole to be filled with pea gravel. The pea gravel will meet the requirements of FDOT standard size No. 10 aggregate washed pea gravel. Each gas probe will be protected by a surface mounted well protector and locked for security purposes. Each gas probe will terminate at the surface with a PVC ball valve to accommodate easy monitoring of methane levels, with a portable meter. The ball valve will remain closed between monitoring events and pre-purge measurements will be recorded. In the event of a positive gas measurement, the post-purge measurement will also be recorded.

3.10.1.3 Methane Gas Measurement

In accordance with the requirements of the current FDEP permits, methane gas levels are monitored at each of the active gas monitoring points quarterly, with results submitted to the FDEP. A lower explosive limit (LEL) meter will be used to measure methane levels from each of the gas probes. LEL meters, such as the MSA Model 260 or GEM 500 or equivalent, will be used to conduct this monitoring. These meters are capable of measuring percent volume of methane in air and the percent LEL level of the methane by volume. The meter will be calibrated in accordance with manufacturer's specifications prior to each methane monitoring event. Attachment 4 of the Operations Plan provided in Appendix H presents the proposed gas monitoring probe survey form to be used to conduct the quarterly monitoring at the subject site. This form will document at the time of each gas probe reading, air temperature in degrees Fahrenheit, methane levels in percent volume in air and percent LEL. The reporting action level for methane in air will be considered 5 percent by volume in air as measured by the lower explosive limit. The reporting action limit for methane in structures is 25% of the LEL, or

1.25% methane by volume. The results of each quarterly gas probe survey will be submitted to the Department on the presented form within two weeks of each monitoring event. These events are planned to be coordinated with the semi-annual groundwater monitoring at the subject site.

3.10.1.4 Gas Contingency Plan

The following Contingency Plan will be implemented if any of the measured gas monitoring points methane levels are detected above the 100% LEL of greater than 5 percent methane in air, or if 25% of the LEL or higher is measured in a structure. If this level of methane or greater is detected in any of the probes, the Facility operator will institute measurement of methane in nearby, at, or below grade structures, i.e., stormwater collection points, or any maintenance or office buildings within 100 feet of the subject gas probe on a weekly basis until these levels go below the 100% LEL at the subject probe. If methane levels measured in any on-site building exceed 25% of the LEL, building windows and/or doors will be opened for ventilation and all personnel evacuated until methane readings are maintained below 25% of the LEL for methane. The monitoring report for any event that detects methane above the LEL will also report methane levels from nearby structures, as indicated above, until the levels go below the methane LEL level or until corrective actions are conducted to reduce methane levels. The FDEP will be notified within seven days of any gas monitoring levels that exceed the reporting action levels.

3.10.1.5 Passive Gas Vents

Within 90 days of closure of each landfill cell, a passive landfill gas vent will be installed at the highest point of the cell to prevent explosions, fires and damages to vegetation from methane gas buildup. Sheet C2.00 shows the location of the 9_10 gas vents and Figure 3-16 (provided in Appendix 3-C of the 2012 permit renewal application submitted by Kelner Engineering) presents the design of a typical vent. The facility's gas emissions are expected to be far below the threshold of a Title V or an NSPS permit.

3.10.2 Leachate Control

Any leachate that may be produced at the landfill will be controlled with the use of a continuous 3-foot thick clay layer (1x10⁻⁷ cm/s) that will be placed on the bottom of the cells. The clay layer beneath each individual cell will form a continuous barrier layer that will be graded to direct leachate to the remaining portion of the temporary stormwater pond in future Cell 14 and/or Pond 3. During Cell 7 construction, leachate will continue to flow along the continuous bottom barrier layer towards the northern landfill boundary, and into the existing stormwater pond in future Cell 14 and proposed Cell 16. During excavation of proposed Cell 16, a 6-foot berm shall be constructed along the Cells 15 and Cell 16 boundary to divert leachate generated in Cells 1-7

and 15 to flow east through the permeable side berm and into the proposed stormwater Pond 3. In the occurrence of a heavy storm event, a pump will be kept onsite to prevent any overtopping of the berm. The remaining portion of the stormwater pond in future Cell 14 shall continue to collect the leachate currently flowing towards the northern boundary.

The controlled method of screening waste also supplements the leachate control. Because the Applicant privately owns the Enterprise Class III Landfill facility, most of the haulers, waste generators, and sources of waste are known to Angelo's and the scale house attendants. For those haulers that are unfamiliar to the Applicant, the scale house attendants question the haulers more intensely to determine the contents of their loads. The spotters and operators add additional monitoring at the active disposal location. The addition of video surveillance to the monitoring process of incoming wastes helps to identify fires or smoking loads. Combined methods of screening waste is an effective method to reduce any possible threat to public health or the environment.

3.10.3 Stormwater Controls

The approved Stormwater Management Plan for the landfill consists of berms, swales, and ponds constructed within the 200-foot landscape buffer zone to divert, collect and contain stormwater runoff from the completed site. These stormwater facilities are designated to retain the 100-year, 24-hour storm volume as required by Pasco County and the FDEP. During excavation, construction and waste disposal, stormwater will be controlled by a series of berms that direct stormwater to the temporary stormwater pond located in the northeast corner of the site. A 6-foot berm adjacent to active and filled cells retains stormwater from the filling area and diverts stormwater from the excavation area to the temporary stormwater pond. A portion of the temporary stormwater pond will be filled as part of the construction of Cell 16. A new stormwater Pond 3 is being proposed and submitted to be permitted as an Industrial Wastewater Pond through FDEP. Additional details concerning the stormwater management system are provided in Drawing Sheets C1.00, C1.10, C2.00 and C2.10.

3.11 EROSION CONTROL

The perimeter swales and ponds surrounding the landfill prevent stormwater from leaving the property. The series of berms described in Section 3.10.3 above will help prevent erosion.

Additionally, landfill side slopes will be constructed at 3H:1V (above elevation 125' NGVD) from base grade to elevation 125' NGVD and 4H:1V from 125' to 170' NGVD and will receive intermediate cover to be maintained until final landfill closure that will occur when all existing and proposed cells are filled. See the Reclamation and Closure Plan provided in Appendix F

Section 7 for further details.

3.12 FINAL GRADE PLAN

The filling sequence of the landfill is shown on Sheets C1.00 through C2.10 and C1.10 of the 2016 Plan Set provided in Appendix A Section 4. The excavated areas will be certified to the approved bottom grades prior to accepting any waste material. The finished elevation after all fill material has been placed and final cover provided is designed to reclaim excavated areas.

3.13 SETBACKS AND VISUAL BUFFERS

The following setbacks (buffers) shall be used:

- 1. Minimum of 200 feet from the property boundary to landfill footprint.
- 2. Minimum of 500 feet setback from surrounding potable residential wells to landfill footprint.

Buffer areas maintain visual screening of the landfill by the following methods.

- 1. 8-foot high berms along the frontage of Enterprise and Auton roads.
- 2. Landscaping and trees to provide visual buffers within setback areas
- 3. Existing trees within the setbacks will be maintained.

3.14 FOUNDATION ANALYSIS

A Geotechnical analysis was conducted on the landfill site to evaluate if the base and geologic setting are capable of providing structural support. Universal Engineering Sciences, Inc. completed the Geotechnical Report included as Section 4 to the September 2005 Enterprise Recycling and Disposal Facility Class III Landfill Permit Renewal Application, prepared by TetraTech HAI, and updated as the January 25, 2006. Universal Engineering Sciences Geotechnical Exploration – Update, provided as an appendix to the February 2006 letter from Jennifer Diehl, P.E. to Mr. Steve Morgan Subject: Angelo's Aggregate Materials, Ltd. Enterprise Recycling and Disposal Class III Landfill Pending Permit Nos.: 177982-007-SC and 177982-008-SO Pasco County. The report concludes that the landfill base will adequately support the Class III landfill wastes without excessive settlement. It also states that the potential for sinkhole development on the site is low. In the event a sinkhole is discovered on-site, or within 500-feet of the site, the Department will be notified within 24 hours. A reclamation plan

of action will be submitted to the Department within seven days. Please see Appendix <u>G-1-C</u>, Attachment 1 for Universal Engineering Sciences' Geotechnical Services / Documentation Review dated <u>May 31, 2016 January 29, 2016</u> for a signed and sealed review and evaluation of historical site related geotechnical records which includes a recent site reconnaissance visit.

An updated foundation bearing capacity analysis was performed by Civil Design Services, Inc. and is provided in Appendix E Section 2, Part I, I-2. The analysis demonstrates that the proposed Cell 16 has sufficient additional bearing capacity to accommodate the proposed design.

3.15 CERTIFICATION

Laboratory testing and observation of cell floor conditions during cell construction completion shall consist of the following:

- In-place density testing for each 12-inch thick soil lift, based on laboratory proctor test results for the construction material, will be recorded by a properly trained technician. These are to be conducted at the location of each permeability test.
- Thickness testing of each lift will be recorded at a minimum frequency of two tests per acre, per lift.
- Confirmation hydraulic conductivity testing of Shelby tube or drive cylinder samples of the compacted cell floor material will be performed at a minimum frequency of one test per lift, per acre.
- Observance for unstable areas such as limestone, sink holes and soft ground will be performed for each cell.

If the test data from a cell floor section does not meet the requirements of the anticipated conditions of the hydrologeological and geotechnical reports and the requirements of the facility construction permit, additional random samples may be tested from that cell section. If the additional testing demonstrates that the hydraulic conductivity meets the requirements, the cell will be considered acceptable. If not, that cell will be reworked or reconstructed so that it will meet these requirements.

Upon completion of construction of any cell within the disposal facility, the certification of construction completion will be provided to the FDEP on form 62-701.900(2), F.A.C.. The applicant will provide the completed form to the FDEP, along with the quality assurance test results described above, and arrange for an inspection prior to acceptance of Class III wastes

into the constructed disposal area.

3.16 OPERATIONS PLAN

The Landfill's Operations Plan is included as Appendix G3-AG.

3.17 CONTINGENCY PLAN

The Landfill's Contingency Plan is included as Appendix H 3-B H.

Appendix 3-A OPERATIONS PLAN

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY MAJOR PERMIT MODIFICATION LANDFILL OPERATIONS PLAN

Prepared for:

ANGELO'S AGGREGATE MATERIALS, LTD

855 28th Street South St. Petersburg, Florida 33712

Prepared by:

LOCKLEAR & ASSOCIATES, INC.

4140 NW 37th Place, Suite a Gainesville, Florida 32606

March 2016

Revised July 2016 (RAI 1 Response)

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ATTACHMENT 5 ATTACHMENT 6	LIST OF APPROVED COURSES TRAINING CERTIFICATES

1.0 DESIGNATION OF RESPONSIBLE PERSON(S) AND REFERENCES

Mr. John Arnold, P.E. is designated by Angelo's Aggregate Materials, LTD. (Applicant) as the individual responsible for operation and maintenance of the Enterprise Road Class III Recycling and Disposal Facility (Facility) in accordance with Rule 62-701.500, F.A.C. All correspondence and inquiries concerning the Facility permits and operation should be addressed to him at:

Mr. John Arnold, P.E. Angelo's Aggregate Materials, LTD. 855 28th Street South St. Petersburg, Florida 33712 Telephone: (813) 477-1719

Updated plan sheets and figures are provided in <u>Sections 4 and 3 respectively of the March 2016</u> permit modification application RAI 1 response dated July 2016. Appendices A and B of the <u>March 2016 Engineering Report, respectively.</u>

2.0 LANDFILL SITE IMPROVEMENTS

The 160 acre landfill site is also permitted by Pasco County to be a Class I mine (Pasco County Petition #CU04-26, approved 9/23/2004). The following site improvements have been installed to continue operation of the Class III Landfill.

2.1 Facilities

An office trailer (gate house) is located onsite for the gate attendant. This trailer has hand washing and toilet facilities. Bottled potable water is used to provide drinking water for the trailer. Electric and telephone services are available to the trailer office. Site entrance improvements also include an all-weather entrance roadway, scales and perimeter road as shown on the Sheet C0.02 of the 2016 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016.

2.2 Primary Haul Routes

The primary haul routes used to reach the Facility are U.S. 301, S.R. 52, C.R. 35A, U.S. 98, and Clinton Avenue. These routes lead to Enterprise Road, which is used to access the facility.

Enterprise Road was improved by the Applicant to an all-weather, paved access roadway from C.R. 35A to Auton Road. Enterprise Road is a Pasco county owned roadway that is maintained

by the county. The Facility has an all-weather, paved access roadway that will be maintained by the Applicant to provide adequate access at all times.

2.3 <u>Effective Barrier</u>

The existing Facility property previously had a five-foot high wire fence along the perimeter of the site. A 6-foot security fence has been constructed along the south and east boundaries. The security fence consists of a 6-foot high galvanized chain link fence, hereafter referred to as the "security fence." The five-foot wire fence still exists along the north and west property boundaries. The chain link fence has been installed in accordance with permit issuance in October, 2001. Three (3) foot square "NO TRESPASSING" signs with five-inch letters has been installed at no less than 500-feet spacing and at all corners to notice unauthorized access. The only point of access into the landfill site will be through the ticket gate at the entrance. This gate will be locked during closed hours.

An 8-foot high landscape berm has been constructed along the frontages of Enterprise and Auton roads as a visual and noise buffer.

3.0 OPERATING HOURS

The landfill will have the following operating hours:

Day	Hours of Operation	
Monday through Friday	7:00 am to 6:00 pm	
Saturday	7:00 am to 2:00 pm	

Operational hours may be extended periodically to meet special requests of customers, but at no time will normal operating hours extend beyond 7:00 A.M. to 7:00 P.M. Monday through Saturday. Waste will not be accepted during non-daylight hours.

4.0 CONTINGENCY OPERATIONS

If a natural disaster occurs at the facility rendering it unusable, the waste accepted at the Facility would be rerouted to another permitted landfill. If a storm occurs within the surrounding community, storm debris waste will also be accepted at the facility, providing additional staff if required. In terms of equipment breakdown, there will be two operating pieces of equipment for all stages of landfill operation. Currently, Angelo's has on-site two compactors [Cat 826 (2)], two loaders (Cat 950, Cat 980), two dozers (Cat D5, Cat D8), four excavators [John Deere 450 (2),

Komatsu PC1100, Komatsu PC300], and two articulated dump trucks (Volvo). If both should breakdown, replacements can be rented or substituted from onsite or offsite within 24 hours.

The site access roads will be constructed to allow passage of vehicles under all expected weather conditions. See Appendix 3-A H for the Contingency Plan.

5.0 WASTE STREAM QUALITY CONTROL PLAN

5.1 <u>Visual Inspection</u>

An estimated 550 tons of Class III waste material is currently received at the facility daily. Materials brought onto the Enterprise Road Class III RDF site will be inspected three times. The first inspection takes place at the site entrance. The site will only accept Class III debris (which includes construction and demolition debris by definition); therefore, any vehicles hauling unacceptable waste can be turned away by the attendant at the ticket gate. The gate attendant will question all waste carriers as to the character and origination of their wastes. A mirror is installed overhead and angled to allow gate inspection of all loads after they are untarped. A video camera has been installed over the scale location that allows the gate attendant to visually screen all carrier loads prior to disposal, mainly to identify fire or smoking loads. For loads that are not accepted, a Rejected Load Form will be completed.

The second inspection is a visual inspection that will occur at the working face by a certified, trained spotter. The spotter stationed at the working face will be responsible for spotting trucks bringing in disposal loads. The spotter will show the drivers where to unload, and will also inspect the trucks to make sure unacceptable materials are not unloaded. The spotter will have the authority to ensure that unacceptable materials are reloaded on the truck the material was brought in on.

The third inspection will occur as the waste is spread by the equipment operator. Any unacceptable wastes observed will be placed in the appropriate container located at the working face. The equipment operator may also serve as the spotter and will perform both visual inspections - as the waste is unloaded and as the waste is spread.

The facility will deploy and use spotters based on the volume of waste disposed at the working face. No more than two loads will be allowed to dump simultaneously per spotter at the working face.

5.2 Documentation of Waste Received

Documentation includes recording the name of the company disposing of the waste, driver's signature/information, all vehicle identification numbers, quantity of waste (tons), and type of waste (to meet FDEP and Pasco County's requirements). All vehicles entering the landfill will be weighed. The type of material and location from which the waste was generated will be recorded. This provides a record for tracing ownership of individual loads. See Landfill Operating Records, Section 19.2 for more details.

5.3 <u>Contingency for Unacceptable Materials</u>

If unacceptable waste materials are delivered to the landfill, the truck will be refused entry after inspection at the gate. If the unacceptable waste materials are observed by a spotter while unloading, they will be reloaded onto the delivery vehicle. Should the vehicle leave before the unacceptable waste has been discovered, Enterprise Road Class III RDF personnel will place the unacceptable material into an appropriate container located at the working face. A maximum of 20 cubic yards of covered dumpster storage for Class I waste will be provided near the active face of the landfill, as shown on Drawing C0.03 of the 2016 Plan Set provided in Section 4 Appendix A of the March 2016 permit modification application RAI 1 response dated July 2016. These containers are transported by Central Carting Disposal (or other qualified vendor) to a disposal facility permitted to accept Class I material. The covered storage containers will control vectors and odors and Class I waste will be removed within 30 days of discovery. If the storage containers cannot be secured to control vectors and odors, the putrescible waste will be stored no longer than 48-hours.

Unacceptable nonputrescible, non-hazardous wastes, such as batteries, paint, chemicals or similar items that are inadvertently accepted will be removed when observed and stored in a roll-off container or pile at the working face and removed daily to a lockable storage unit. A maximum of 40 cubic yards of stored unacceptable, nonputrescible, non-hazardous wastes may be provided near the active face of the landfill, as shown on Drawing C0.03 of the 2016 Plan Set provided in Section 4 Appendix A of the March 2016 permit modification application RAI 1 response dated July 2016. These materials will be removed from the site at least every 30 days (sooner if required) by City Environmental (or other qualified vendor) and taken to their facility for processing and proper disposal. This plan should meet the inspection needs for the site to prevent disposal of unacceptable wastes.

If suspect regulated hazardous wastes are identified by operators or spotters by random load inspection or discovered deposited at the landfill, the FDEP will be notified promptly, as well as the hauler and generator of the wastes, if known. The area where the hazardous wastes are stored will immediately be secured from public access. If the generator or hauler cannot be identified,

Enterprise Road Class III RDF will assume the cleanup, transportation and disposal of the waste at a permitted hazardous waste management facility.

5.4 Acceptable and Unacceptable Class III Landfill Waste Materials

The Enterprise Road Class III RDF will accept only those solid wastes as defined in Rule 62-701.200 (14), F.A.C. as Class III wastes, except as allowed otherwise by permit.

Acceptable Class III waste materials include the following:

- Land clearing debris
- Demolition debris
- Glass
- Carpet
- Cardboard
- Asbestos
- Plastic
- Automobiles and parts without visible contamination from petroleum products or other chemicals

- Construction debris
- Non-Treated Wood Pallets
- Unpainted, <u>painted</u> and untreated wood scraps from manufacturing
- Waste Tires (Processed)*
- Paper
- Furniture other than appliances
- Yard trash
- * Processed waste tires are acceptable for disposal in the Class III Landfill provided that they have been cut into sufficiently small parts. The processed waste tire parts may be disposed of or used as initial cover at a permitted landfill. For use as initial cover, a sufficiently small part means that 70 percent of the waste tire material is cut into pieces of 4 square inches or less and 100 percent of the waste tire material is 32 square inches or less. For purposes of disposal, a sufficiently small part means that the tire has been cut into at least eight substantially equal pieces. Any processed tire which is disposed of in a landfill and which does not meet the size requirement of subsection (a) above must receive initial cover, as defined in subsection 62-701.200(53), F.A.C., once every week.

The following is a compilation of unacceptable Class III waste materials:

- Putrescible Household Waste
- Paint (liquid)
- Any toxic or hazardous Materials (i.e., batteries, solvents, oils, etc.)
- Refrigerators, freezers, air conditioners (white goods)
- Biomedical waste
- Automobiles or parts that are contaminated with petroleum products or other chemicals.

- Contaminated soils
- Electronics

- Septic tanks and pumping
- Whole waste tires (except at the waste tire processing facility)
- CCA Treated wood

The site has a visible sign at the site entrance on Enterprise Road as provided in Attachment 1. The sign identifies the accepted wastes, hours of operation, landfill classification, and site's 24-hour emergency contact and telephone number. Industrial or excavated waste will be considered for acceptance on a case by case basis, only with prior consent of the Department.

5.5 Random Load Inspection

In accordance with Rule 62-701.500(6)a., F.A.C., the owner or operator will implement a load-checking program to detect and discourage attempts to dispose of unauthorized wastes at the landfill. The load checking program will consist of the following minimum requirements:

- 1. The landfill operator will examine at least three random loads of solid waste delivered to the landfill per week. The waste collection vehicle drivers selected by the inspector will be directed to discharge their loads at a designated location in the landfill. A detailed inspection of the discharged material will be made for any unauthorized wastes. The landfill operator will assure the random inspections will be distributed between both loads originating from the transfer facility and other private waste haulers delivering waste to the landfill.
- 2. If unauthorized wastes are found, the facility will contact the generator, hauler, or other party responsible for shipping the waste to the landfill to determine the identity of the waste sources.

The following procedures will be followed when inspecting the load:

- A. The load will be "broken apart" by both the spotter and equipment operator to allow for a thorough inspection.
- B. The inspectors will be searching and removing de minimis amounts of unauthorized waste contained in the load.
- C. If the load contains more than de minimis amounts of unauthorized materials, they will immediately be reloaded onto the customer's vehicle for removal from the site. In the event that the transporter will not remove the unacceptable materials, the materials will

be loaded into an appropriate container and removed from the site. The customer/generator will be contacted and notified of the site policies as well as charged for the off-site disposal services.

D. In all cases, if more than minimal unacceptable wastes are found during the inspection, the customer will be notified to assure the prevention of future occurrences.

All inspection will be documented on the site's "Random Load Inspection Form," signed by the inspector, and kept in a current Log Book, see Attachment 2. Log books will be maintained at the landfill for at least 3 years. Inspections will be performed by trained site personnel.

5.6 Asbestos Waste Disposal

Asbestos-containing materials (ACM's) will be accepted for disposal in accordance with 40 CFR Part 61.154. Arrangements for disposal of ACM's between the Facility and the waste generator/hauler will be recorded in the operations record as to the quantity and date of shipment to the landfill. The loads are accepted at pre-arranged times during operational hours.

To ensure that all waste deposited at the Facility meets state and local requirements, all facility personnel will receive training from their supervisor on the identification of unacceptable materials, which is any waste other than properly labeled and bagged ACM. Unregulated, non-friable asbestos containing materials are not required to be bagged, but all other requirements are unchanged.

Each load of ACM arriving at the facility must be accompanied by a completed Waste Shipment Record (WSR) in accordance with 40 CFR 61.150. Each load will be inspected to insure that it is properly bagged, that bags are intact and properly sealed, and that the required warning labels and generator labels are affixed. Bags will not be opened prior to disposal.

ACM arriving at the Facility for disposal will be visually screened by facility personnel a minimum of two times. The first screening will be at the scales, controlling access to the Facility, where the truck drivers will be questioned as to the contents of the load and the shipping documents will be reviewed. The gate attendant will direct the drivers to the appropriate disposal area.

The second screening will be at the working face where a trained inspector/spotter will again question the driver and make a visual examination of the load prior to dumping and as it is dumped. This examination will insure the ACM is properly bagged, the bags are intact and properly sealed, and that the warning labels and generator labels are affixed.

Facility personnel will direct the waste hauler to the designated ACM disposal location in each cell, to be determined by the Operator. The ACM will be covered with 6-inches of soil at the end of any day that ACM is accepted. This designated ACM location will be recorded and updated by the annual topographic survey in accordance with 40 CFR 61.154. ACM disposal records will be maintained for the life of the landfill and disposal locations documented in the Closure Report.

5.7 Incidental Recycling Operations

The Class III landfill does have a separate, dedicated materials recycling area. However, if recyclable wastes are incidentally received, such as metals, concrete rubble, asphalt, and wood wastes, the facility will separate them in stockpiles or in roll-off containers. Concrete and asphalt will be periodically transported to an appropriate location for crushing. Yard and wood wastes may be chipped for use onsite or be placed in roll-off containers for shipment to a wood recycler. These materials will be removed from the site approximately every 6 months. However, if the storage capacity is exceeded, the materials will be removed sooner. Incidental recyclable materials that are identified at the disposal area will be placed in containers located near the working face, as follows and as shown on Drawing C0.03 of the 2016 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016 Appendix A of the Engineering Report.

TYPE	MAX. QTY	STORAGE	
Ferrous Metal	500 CY	Roll-off or pile	
Aluminum	300 CY	Roll-off or pile	
Stainless Steel	300 CY	Roll-off or pile	
Copper	25 CY	Trash pail, roll-off or pile	
Asphalt	300 CY	Roll-off or pile	
Concrete / Rubble	300 CY	Roll-off or pile	
Recyclable electronics	8 CY	Covered dumpster	

Trucks identified at the entrance as carrying primarily recyclable products, (i.e., concrete, metal, wood, paper) will be refused entrance into the landfill.

5.7.1 Reports

A Recovered Materials report will be submitted by type of waste recovered and tonnage to the FDEP and Pasco County Solid Waste Department. These reports will also be compiled into an annual report to the FDEP.

5.8 Wood Acceptance Area

Initial inspection will be performed at the scalehouse by the attendant. Wood wastes are stockpiled until processing takes place every 180 days. Personnel trained to identify and remove any unacceptable wastes will be present during processing. Unacceptable wastes, if found, will be removed prior to wood processing.

5.9 CCA Treated Wood Management Plan

The following serves as the CCA-treated wood management plan required by 62-701.730(20), F.A.C. Employees will be trained in the proper management of CCA-treated wood. CCA-treated (chromate-copper arsenate) wood must be stored in the temporary storage container for waste destined to go to a lined facility. CCA-treated wood is not allowed to be disposed of in the Enterprise Class III Recycling and Disposal Facility.

The following is strictly prohibited:

- Disposal of CCA-treated wood in any unlined landfill or disposal facility
- Burning of CCA-treated wood in an open burn or an air curtain incinerator
- Mulching of CCA-treated wood or use of CCA-treated wood in other soil amendment products

There are several ways for employees to identify CCA-treated wood: 1) determining the place of origin, 2) identification by shape – typically large, dimensioned pieces of wood and 3) identification by color. CCA-treated wood has been used in a variety of applications including fencing, docks, outdoor decks and stairs, playground equipment and landscaping. The wood is typically large – dimensioned 4-inches or larger.

The most common method for visually identifying treated wood among lumber, timber and plywood is to look at the color of the wood. Untreated wood and borate-treated wood typically have a light yellow color. Wood treated with copper varies in color from a very light green to an intense green color depending on the degree of treatment. A higher degree of treatment is typical for marine applications and for structure with a high load-bearing support. Once the wood treated with copper has been in-service and has weathered, the green color is generally converted to a silver color. It still may be difficult to visually distinguish weathered treated wood from weathered untreated wood.

Employees are cautioned against handling CCA-treated wood. Workers handling wood preserved with CCA should be sure to wash their hands before eating or smoking. CCA-treated wood splinters in the hands and fingers of workers are reported to be very problematic and should be removed as soon as possible. It is important to make sure that the entire splinter is removed. Removal may require medical attention.

The most efficient way to minimize CCA-treated wood disposal in the facility is to communicate with landfill customers. Dedicated, separate suitable temporary container for CCA-treated wood at demolition and construction job sites can be used. At the scale house, personnel will question transporters on the type of wood and direct customers to dispose CCA-treated wood at a Class I landfill. Personnel will also perform a visual inspection at the scale house if necessary especially for loads originating from the construction and demolition of fences and decks.

The facility shall incorporate CCA-treated wood into its spot-checking program. Spotters visually inspect and determine if any dimensioned wood is in the load, such as railroad ties and fence posts or building materials. If CCA-treated wood is found, the load will be diverted to a Class I landfill for disposal. Tipped loads will be spread and inspected for the presence of CCA-treated wood. CCA-treated wood will be adequately protected from rain to prevent leaching of contaminants.

The landfill operations are intended to minimize the amount of CCA treated wood that is delivered to the facility. Written notice will be posted at the scalehouse notifying incoming customers that CCA wood is not suitable for disposal. All reasonable efforts will be made to separate any CCA treated wood from other wastes during spotting operations. If any tipped load has excessive amounts of CCA, they will be rejected. CCA wood that is separated from other wastes at the Facility will not be disposed of at an unlined solid waste disposal facility.

6.0 WEIGHING OR MEASURING INCOMING WASTE

A scale system is used to weigh incoming waste. The scales will be calibrated every six (6) months. Vehicles will be weighed when they enter the disposal site, and based upon the tare weight of the vehicle, the waste tonnage will be determined. Prior to unloading debris, the tonnage or volume of the waste material disposed will be determined and the appropriate fee assessed. Weigh tickets will be kept on-site for a minimum of 5 years.

6.1 Fee Schedule

The fee schedule for disposal varies depending on the client, type of waste and volume received.

Waste Type	Unit	Fee per Unit	
Class III	CY	Variable	

This fee schedule will be periodically revised according to the prevailing market for waste disposal. The Operator will notify clients immediately in writing of all fee schedule changes.

7.0 VEHICLE TRAFFIC CONTROL AND UNLOADING

Generally, truck traffic will be controlled by first-in, first-out, as directed by the spotter located at the working. There will be adequate space for truck staging at the site's entrance (7-8 trucks) to mitigate any queuing onto Enterprise Road. Enterprise Road Class III RDF will discourage any truck staging prior to landfill opening. Signs will be posted at the entrance gate and on interior roads to guide mining truck traffic vs. landfill truck traffic to their appropriate areas of the site.

8.0 METHOD OF CELL SEQUENCE AND LIFE EXPECTANCY

8.1 <u>Cell Sequence</u>

Filling activities are currently (as of March 2016) occurring in Cells 6 and 6B of the Class III Landfill. The cell construction and filling sequence operations will be as follows (see Drawing Sheets C 1.00 and C1.10 of the 2016 Plan Set provided in Appendix A):

Phasing Sequence 1	Fill Cells 6, 6B, 7, 1, 2, 3, 4, 5 and 15 in 10 12 foot lifts from			
	base grade to elevation 150', including filling over Cells 1 - 5,			
	and 15. Maximum side slope is 3H:1V.			
-	10-ft wide stormwater benches are to be constructed at elevation			
	125' and 150'.			
	——————————————————————————————————————			
	1			
Phasing Sequence 2	Complete construction of Cell 16 per Sheet C1.00 of the drawing			
	set in Appendix A.			
	Continue filling Cell 7 and begin filling Cell 16 in 10 12 foot			
	lifts from base grade to elevation 150', including filling over Cells			
	1 - 6 and 15. Maximum side slope is 3H:1V.			
	10-ft wide stormwater benches are to be constructed at final cover			
	elevations 125' and 150'.			
Phasing Sequence 3	Continue filling Cells 1 through 7, and 16 in 10 – 12 foot lifts			
	from base grade to elevation 150', including filling over Cells 1			
	6, and 15.			
	Maximum side slope is 3H:1V and minimum 2 % grade from final			
	cover elevation 170' to 175';			
	10 ft wide stormwater benches are to be constructed at elevation			

	125' and 150'.			
	Cover elevations noted include 18" intermediate cover and 18" top			
	soil layer. Fill elevations shall be such that design cover elevations			
	will be achieved on all external slopes.			
	Sideslope berms and stormwater appurtenances are to be			
	constructed at final closure.			
Angelo's Aggregate Mate	erials is currently (as of March 2016) filling in Cells 1 – 6 and 15 of the			
	construction of Cell 7 is being completed. The cell construction and			
filling sequence operation				
Phasing Sequence 1	As shown in Drawing Sheets C1.00 and C1.01			
	Continue filling Cells 1, 2, 3, 4, 5, 6, 6B, 7 and 15 in 10 – 12 foot			
	lifts to waste elevation of 172'			
	Maximum slope is 3H:1V from base grade to waste elevation			
	122'; 4H:1V from waste elevation 122' to 167'; 1% to 2% grade			
	from waste elevation 167' to 172'			
	10-ft wide stormwater benches are to be constructed at waste			
	elevations 122' and 147'			
	Sideslope berms and stormwater appurtenances are to be			
	constructed at final closure.			
	Construct Cell 16 in accordance with permitted design			
Phasing Sequence 2	As shown in Drawing Sheets C1.10 and C1.11			
	Begin filling 4 – 6 feet lift north of the temporary berm until cell			
	is floored out. Remove temporary berm and fill with 4 – 6 feet lift.			
	Continue filling Cell 16 in 10 – 12 foot lifts from base grade to			
	waste elevation 147', including filling over Cell 15. Maximum			
	slope is 3H:1V from base grade to waste elevation 122'; 4H:1V			
	from waste elevation 122' to 147'.			
	A 10-ft wide stormwater bench is to be constructed at elevation			
	122'. Sidesland harms and starmywater appurtaneous are to be			
	Sideslope berms and stormwater appurtenances are to be			
	constructed at final closure.			
Phasing Sequence 3	As shown in Drawing Sheets C2.00 and C2.10			
Thusing sequence s	Construct final closure cover system over Cells 1, 2, 3, 4, 5, 6, 6B,			
	7, 15 and 16 in accordance with the permitted closure design			
	Construct sideslope berms and stormwater appurtenances			
	Construct landfill gas vents			
				

Lift height includes cover material. Due to the landfill bottom elevation, some lifts may not be a full 10 feet in height.

As each sequence is active, the following procedures will be followed.

- The access road to the working face will be constructed and graded as necessary.
- Waste will be compacted as it is placed. General lift height will be 10 feet and will come within three (3) feet of the final elevation to provide for final cover.
- The working face will remain approximately 100 feet in length.
- Avoid channelizing stormwater flows
- Use mulch, grass, and maintain intermediate covers
- Use culverts, berms, or the best management practices based on actual weather and site conditions.
- Weekly cover of six (6) inches of soil will be placed on the working face.
- Intermediate cover of 12 inches of soil will be placed in areas that will not receive waste within 180 days. The cover may be removed immediately prior to placement of new waste.

Stormwater runoff from the interior of the excavation and filling area will be diverted to the onsite temporary storage pond using a temporary interior swale and 6-foot berm. Perimeter berms will direct stormwater away from excavation and filling areas. The temporary stormwater pond will receive runoff until Pond 3 is developed.

8.2 Erosion Control

The following engineering controls will be used to minimize erosion at the working face:

- Regrade a maximum of 100 linear feet of the outer edge slopes at a time to 2H:1V. The purpose of this recommendation is that a relatively small area will be subjected to surface erosion at any given time.
- Construct a berm along the top of the slope during the regrading to redirect any rainfall runoff away from the face of the slope. The area along the berm should be graded so as to

allow rapid runoff along the top of the slope. Ponding of water near the top of the slope should not be allowed, since seepage through the slope may initiate slope erosion.

- As soon as possible following the construction of the clay <u>layerliner</u>, begin to fill against the 2H:1V slope with the landfill material.
- Avoid channelizing stormwater flows
- Use mulch, grass, and maintain intermediate covers

Use culverts, berms, or the best management practices based on actual weather and site conditions.

8.3 <u>Life Expectancy.</u>

The capacity and lifespan estimates are provided in Section 3.8.3 of the Engineering Report.

9.0 WASTE COMPACTION AND APPLICATION OF COVER

Waste received will be segregated based on compatibility. Bulky, incompressible items, such as concrete and tree debris, will be separated and stockpiled for future processing. Tree debris is separated from the waste and periodically mulched for on-site uses. The remaining debris is disposed of in designated "cells" using a CAT 826G Compactor, or equivalent to place, spread the waste daily and compact the debris weekly. Initial cover material is planned to be excavated from onsite areas and placed weekly in approximately 6-inch layers on the compacted lifts to control vectors, reduce rain infiltration and provide a more stable working face area. The facility may also use a 50/50 mixture of mulch and soil as cover in accordance with Policy Memo # SWM-05.4 dated April 25, 2001. An intermediate cover of one (1) foot of compacted soil will be applied if final cover or an additional lift is not to be applied within 180 days of cell completion. Cell closure will occur when all permitted cells are filled. For final buildout grade and closure details, see Drawing Sheets C2.00 and C2.10 of the 2016 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016. Appendix A of the Engineering Report, respectively. The Conceptual Closure Plan includes permitted Cells 1-7 and 15, and proposed Cell 16.

Cell closure will generally conform to the lines and grades specified in the Landfill Conceptual Closure Plan. The grading plan will conform to the rules and regulation specified in 62-701.600, as well as 62-701.400(7) and 62-701.400(8), Florida Administrative Code. Pesticides when deemed necessary to control rodents, insects and other vectors will be used as specified by the Florida Department of Agriculture and Consumer Services. Uncontrolled and unauthorized

scavenging will not be permitted at the landfill site. Controlled recycling may be permitted by the Site Manager responsible for the operation of the landfill facility. Temporary storage of soil fill or recycling materials may occur in the closed cell areas.

10.0 OPERATION OF GAS, LEACHATE AND STORMWATER CONTROLS

10.1 Gas Monitoring and Control

The type of materials to be disposed in the Class III Landfill are not expected to generate significant amounts of methane or other toxic gases since the landfill's design prevents groundwater contact therefore, a passive gas control system is proposed. The Landfill Manager will conduct daily and weekly inspections of the landfill and will check for objectionable odors or gas by driving around the perimeter of the site, record the results, and notify the FDEP and County of any positive detection and immediately take corrective actions. Corrective actions will include placement of additional soil cover, or mulch, or lime containing materials such as crushed concrete that is documented to abate the odors. Quarterly gas monitoring is currently conducted.

Within 30 days of being notified by the Department that objectionable odors per Rule 62-701.200(77), F.A.C. have been confirmed off-site, the Facility will submit to the Department for approval an odor remediation plan. The plan will describe the nature and extent of the problem and the proposed long-term solution, which will be implemented within 30 days of approval. The plan will include procedures to implement a routine odor monitoring program to determine the timing and extent of objectionable odors and a means of evaluating the effectiveness of the remedy.

The facility only accepts Class III debris for disposal and accepts no putrescible household wastes. Surface water and groundwater contact with the Class III wastes will be prevented by the approved facility design thus preventing possible odor operation. Other best management practices to prevent odors include: 1) closure of each cell as it is completed; 2) weekly soil cover application; and, 3) immediate corrective actions to abate odors.

A system of passive gas vents will be installed to manage landfill gas. The location of the gas vents is shown on Sheet C2.00 of the 2016 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016. Appendix A of the Engineering Report. The construction details of the vents are shown on Figure 3-14 (provided in Appendix 3-C of the 2012 permit renewal application submitted by Kelner Engineering) Figure 1 provided in Appendix B of the Engineering Report. The vents will be installed during the final closure and installation of the final cover over each landfill cell.

A system of 16 gas monitoring points will be installed to monitor gas at the site, see Sheet C0.03 of the 20165 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016. Appendix A of the Engineering Report. The construction details of a typical gas probe are shown on Figure 3-14 (provided in Appendix 3-C of the 2012 permit renewal application submitted by Kelner Engineering) Figure 1 in Appendix B of the Engineering Report.

10.1.1 Methane Gas Measurement

In accordance with the requirements of the current FDEP permits, methane gas levels are monitored at each of the active gas monitoring points quarterly, with results submitted to the FDEP. A lower explosive limit (LEL) meter will be used to measure methane levels from each of the gas probes. LEL meters, such as the MSA Model 260 or GEM 500 or equivalent, will be used to conduct this monitoring. These meters are capable of measuring percent volume of methane in air and the percent LEL level of the methane by volume. The meter shall be calibrated in accordance with manufacturer's specifications prior to each methane monitoring event. Attachment 4 of the Operations Plan provided in Appendix 3A-G of the Engineering Report presents the proposed gas monitoring probe survey form to be used to conduct the quarterly monitoring at the subject site. This form will document at the time of each gas probe reading, air temperature in degrees Fahrenheit, methane levels in percent volume in air and percent LEL. The reporting action level for methane in air will be considered 5 percent by volume in air as measured by the lower explosive limit. The reporting action limit for methane in structures is 25% of the LEL, or 1.25% methane by volume. The results of each quarterly gas probe survey will be submitted to the Department on the presented form within two weeks of each monitoring event. These events are planned to be coordinated with the semi-annual groundwater monitoring at the subject site.

10.1.2 Gas Contingency Plan

The following Contingency Plan will be implemented if any of the measured gas monitoring points methane levels are detected above the 100% LEL of greater than 5 percent methane in air, or if 25% of the LEL or higher is measured in a structure. If this level of methane or greater is detected in any of the probes, the Facility operator will institute measurement of methane in nearby, at, or below grade structures, i.e., stormwater collection points, or any maintenance or office buildings within 100 feet of the subject gas probe on a weekly basis until these levels go below the 100% LEL at the subject probe. If methane levels measured in any on-site building exceed 25% of the LEL, building windows and/or doors will be opened for ventilation and all personnel evacuated until methane readings are maintained below 25% of the LEL for methane. The monitoring report for any event that detects methane above the LEL will also report methane levels from nearby structures, as indicated above, until the levels go below the methane

LEL level or until corrective actions are conducted to reduce methane levels. The FDEP will be notified within seven days of any gas monitoring levels that exceed the reporting action levels.

10.2 <u>Leachate Control</u>

Any leachate that may be produced at the landfill will be controlled with the use of a continuous 3-foot thick clay layer (1×10^{-7}) that will be placed on the bottom of the cells. The clay layer beneath each individual cell will form a continuous barrier layer that will be graded to direct leachate to the remaining portion of the temporary stormwater pond in future Cell 14 and/or the proposed stormwater Pond 3. During Cell 7 construction, leachate will continue to flow along the continuous bottom barrier layer towards the northern landfill boundary, and into the existing stormwater pond in future Cell 14 and proposed Cell 16. Prior to starting construction in Cell 16, a berm will be constructed immediately north of Cell 15. The berm will extend east to west the full width of Cell 16. A portion of the leachate generated in existing cells 1-7 and 15 will move to the remaining temporary stormwater pond in the future Cell 14 area. The remainder of the leachate generated in existing cells 1-7 and 15 will move to Pond 3 via the berm located immediately north of Cell 15. Once Cell 16 construction is complete, the berm will remain in place while the initial lift of waste is placed across the entire floor of Cell 16. Once Cell 16 is "floored out", the berm will be removed for the remainder of operations. Leachate generated in existing cells 1-7 and 15 will then move to temporary stormwater pond in the future Cell 14 area as it did prior to removal of the berms. The remainder of the leachate generated in cells 1-7, 15 and all leachate generated in Cell 16 will move to Pond 3 via the clay barrier layer beneath Cell 16. Under no circumstances will waste be placed in water. In the event that water is present above the clay barrier layer at the time waste is to be placed, the operator will utilize pumps to remove the water to Pond 3.

The controlled method of screening waste also supplements the leachate control. Because the Applicant privately owns the Enterprise Class III Landfill facility, most of the haulers, waste generators, and sources of waste are known to Angelo's and the scale house attendants. For those haulers that are unfamiliar to the Applicant, the scale house attendants question the haulers more intensely to determine the contents of their loads. The spotters and operators add additional monitoring at the active disposal location. The addition of video surveillance to the monitoring process of incoming wastes helps to identify fires or smoking loads. Combined methods of screening waste is an effective method to reduce any possible threat to public health or the environment.

10.3 Stormwater Control

The approved Stormwater Management Plan for the landfill consists of berms, swales, and ponds constructed within the 200-foot landscape buffer zone to divert, collect and contain

stormwater runoff from the completed site. These stormwater facilities are designated to retain the 100-year, 24-hour storm volume as required by Pasco County and the FDEP. During excavation, construction and waste disposal, stormwater will be controlled by a series of berms that direct stormwater to the temporary stormwater pond located in the northeast corner of the site. A 6-foot berm adjacent to active and filled cells retains stormwater from the filling area and diverts stormwater from the excavation area to the temporary stormwater pond. A new stormwater Pond 3 is being proposed and submitted to be permitted as an Industrial Wastewater Pond through FDEP. Additional details concerning the stormwater management system are provided in Drawing Sheets C1.00, C1.10, C2.00 and C2.10.

The site manager will perform weekly inspections of the storm water management system. Any areas in need of maintenance will be repaired within seven days.

11.0 **SIGNS**

Signs will be posted at the entrance to the Facility site which will list the following information:

The operating entity;

Hours of operation;

No scavenging allowed;

No hazardous waste accepted;

List of acceptable and unacceptable waste; and,

24-hour phone number of emergency contact.

The scalehouse attendant will direct each driver to the area appropriate to unload wastes. Signs will also be posted to direct trucks to either the borrow pit or the landfill working face.

12.0 DUST ABATEMENT PLAN

The Facility will provide a water tanker to water the landfill access roads if and when dust becomes a problem. This will also be done whenever the County receives complaints about dust or when a dust problem is observed during a County or State inspection.

13.0 DUST, LITTER, AND VECTOR CONTROL PLAN

The nature of the waste to be disposed in the landfill does not typically create litter and vector problems. Daily placement of waste and/or compaction will be the primary means utilized to control litter and vectors. The facility personnel will perform daily inspections of the facility and the access road to assure litter is controlled. As needed, laborers will pick up blowing debris and dispose of it in appropriate containers and/or on site. Temporary fencing to contain litter at the

working face of the landfill may be used as needed. These litter controls will also be implemented whenever the County or State receives a complaint from adjacent landowners or a litter problem is observed during an inspection.

If vectors (rodents, insects, and domestic animals) become a nuisance at the Facility, the Operator may obtain the services of a licensed pest management company to review the operations and recommend control measures.

14.0 FIRE PROTECTION AND FIRE FIGHTING FACILITIES

Fires that originate in landfills are primarily extinguished by soil application. Supplemental fire protection will be furnished by the Dade City Fire Department (Station No. 1). The Fire Department will be notified immediately of all landfill fires. An emergency contact list will be posted at the scalehouse with contact phone numbers.

During a fire, incoming trucks will be directed toward another area of the landfill so that a temporary active face can be established. Once the fire is extinguished, appropriate cover will be applied to the waste and operations will continue at the original active face. If the fire is extensive and a temporary active face cannot be established, incoming trucks will be redirected to another landfill.

Onsite fire prevention facilities will include:

- Fire extinguishers mounted in the cab of all heavy equipment and in the office/scalehouse;
- Telephones to notify personnel of a fire;
- Onsite equipment (dozer) and fill dirt to extinguish fires on working face; and
- Site water truck

Soil for firefighting purposes will be borrowed from the closest unexcavated area of the site to the fire. Details of all firefighting episodes will be recorded in the landfill operating record.

14.1 Hot Loads and Spills

Any hot load (of authorized material) found will be dumped on an area at least 500 feet away from the active working face. The load will immediately be covered with soil if a fire is imminent. Once the fire is extinguished, the load will be pushed and spread using a dozer,

allowing for the load to be inspected by a spotter. The waste will not be disposed of until it has cooled completely, and the fire hazard has been mitigated.

In the event of a fire at the working face, waste acceptance will cease until the fire has been completely extinguished and additional cover material compacted in the area of the fire. If the fire is located elsewhere in the landfill, waste acceptance operations may continue at the manager's discretion.

Since liquid disposal is prohibited in a Class III landfill, spills from waste vehicles are not anticipated. In the case of a fuel spill or leak, the contaminated soil will be collected to the extent possible, contained in a drum or roll off container, and taken offsite within thirty (30) days for proper disposal or treatment.

15.0 LANDFILL PERSONNEL

The scalehouse attendant and certified landfill operator will be onsite during all operating hours. In addition, there will be a minimum of one (1) other person (spotter) onsite, for a total of three (3). The state certified landfill operator will be assigned to manage the daily landfill operations. The personnel will be stationed at the landfill ticket gate and active disposal face. Additional personnel will be assigned to the landfill operation as the demand necessitates. Two spotters are generally located at the working face at all times that waste is accepted. However, there are up to eight spotter-trained or in-house trained spotter employees on-site each day and therefore; additional trained employees can be relocated to the working face as necessary to inspect the incoming waste. Certificates for current trained personnel are attached as Attachment 6 to this plan.

At least one (1) spotter will be at the working face at all times the facility is accepting waste. The spotter will direct vehicle traffic around the working face and will direct drivers where to empty their vehicles. The loads will be inspected as described in Section 5.0. If the load is acceptable, the waste will be spread and compacted as necessary. If the load is unacceptable, the spotter will direct the driver to reload the waste into the vehicle, if possible. If the driver is unable to reload the material, on-site personnel will reload the material for the driver using onsite equipment. The spotter will also discourage scavenging by the public.

The equipment operator spreading waste at the working face may also act as a spotter in accordance with the following:

- 1. The heavy equipment operator must be trained as a spotter;
- 2. When unauthorized waste is discovered, the heavy equipment operator must either move the unauthorized waste away from the active area for later removal and proper

- management, or must stop operation and notify another person on the ground or on other equipment who will come to the active area and remove the unauthorized waste before operations are resumed;
- 3. Each load of waste must be visually inspected for unauthorized waste prior to being compacted or loaded into a transfer vehicle.

A typical work schedule is as follows:

Dov	Operating	ng Scalehouse Certified Spotter(c)	Equipment		
Day	Hours	Attendant	Operator	Spotter(s)	Operator*
M-F	7 am – 6 pm	1 (7 am – 6 pm)	1 (7 am – 6 pm)	Min. 1 (7 am – 6 pm)	Min. 1
				For 2 or more	(7 am – 6 pm)
				(7 am - 4 pm),	
				(12 pm - 6 pm)	
S	7 am – 2 pm	1 (7 am – 3pm)	1 (7 am – 3 pm)		Min. 1
					(7 am - 2 pm)

^{* -} Equipment Operator may also serve as a spotter

15.1 <u>Training Plan</u>

The Facility will implement an employee training plan to properly train their landfill operators and spotters to operate the landfill in accordance with this Operations Plan, state and local regulations, and accepted disposal practices and to properly manage any hazardous or prohibited materials which are received at the landfill.

A trained operator will be at the site during all times that the landfill receives waste. All facility operators will be trained at an approved FDEP training course. Each operator will submit proof of training and documentation to the FDEP upon receipt of their certificates.

Landfill operators must have at least one year of work experience in landfill operation and a high school diploma; or have at least two (2) years' experience at a Class I, II, or III landfill. Each operator will complete at least 24 hours of initial training in an FDEP-approved training course, and will pass an examination as part of that training. Sixteen (16) hours of continuing training will be completed within three (3) years of each operator's initial training from an approved course documented by the form in Attachment 3. A list of FDEP approved training courses for operators and spotters are included in Attachment 5.

The Facility spotters will complete an initial eight (8) hour FDEP-approved course and four (4) hours of continuing training every three (3) years. Records documenting each employee's training course completion and schedule will be maintained and kept at the landfill office at all times.

Interim operators must become trained operators within one year of employment as an interim

operator and interim spotters must become trained spotters within 3 months of employment as an

interim spotter

16.0 COMMUNICATIONS FACILITIES

The landfill scalehouse will have both telephone and facsimile facilities. In addition, all landfill

operating areas (gate house, working face etc.) will have radio communication or cell phones

with the base station at the gate house.

17.0 **EQUIPMENT INVENTORY**

Equipment currently planned for use at the landfill site includes:

A. D-8 Caterpillar bulldozer, CAT 826 G Compactor; two 2.5 cud loaders, water truck, 590

John Deer backhoe, or equivalent are sufficient for adequate operation of the facility. A wood chipper/grinding machine (Hogzilla), or equivalent, will be moved to the site

periodically (approximately once every six months) to process wood wastes as needed.

Additional equipment, such as a grader may be rented as needed.

B. Arrangements will be made to provide alternate equipment within 24 hours following an

equipment breakdown.

Equipment rental companies that may be used to obtain reserve equipment include the

following:

Ring Power - Brooksville, Florida

Contact: 352-796-4978

Flagler Equipment - Tampa, Florida

Contact: 813-630-0077

C. There will be safety devices present on equipment to shield and protect the operators

from potential hazards during operation.

ENTERPRISE CLASS III RECYCLING AND DISPOSAL FACILITY

OPERATIONS PLAN

17.1 Equipment Maintenance

The Facility will conduct routine heavy equipment and vehicle maintenance onsite. Maintenance includes fueling of heavy equipment with diesel fuel, lubrication, oil changes and, antifreeze changes. Tire repairs will be handled by an outside service company.

A permanent equipment fueling facility will be installed and registered in accordance with F.A.C. 62-761. Pasco County will be copied on the registration.

Oil and antifreeze changes will be contained by large drip pans to catch the waste oils. These wastes will then be transferred either to a 250-gallon waste oil skid tank or to a 55-gallon drum for waste antifreeze, which will be located in a containment area. The containment area is a covered metal storage shed. Enterprise RDF plans to enter into contracts with licensed recyclers to periodically pick up the waste oil and antifreeze. Records of these pickups will be maintained by Enterprise RDF. All virgin lubricants will be stored undercover within the gate house building or suitable enclosure.

18.0 SAFETY DEVICES

All operating equipment which will be utilized at the landfill site will be fitted with rollover protection and fire extinguishers. All landfill personnel will be required to wear safety helmets, safety shoes, eye protective glasses, gloves, and safety vests. The onsite heavy equipment will meet OSHA safety requirements. First aid equipment will be kept in the office trailer and in the operating equipment.

19.0 RECORDS, PERMITS AND REPORTS

A copy of any Florida Department of Environmental Protection (FDEP) and Pasco County approved engineering drawings, permits and supporting information will be kept at the facility for reference and inspections. Permits will be posted at site per ordinance. A waste type and quantity intake (in tons) log will be kept daily, compiled monthly and a report will be submitted annually to Pasco County and the FDEP.

An annual estimate of the remaining life and capacity in cubic yards of the landfill will be reported annually to the FDEP.

19.1 Water Quality Monitoring

The Facility will conduct the required initial and semi-annual groundwater monitoring at the sites' monitoring wells as described in the Facility's Groundwater Monitoring Plan. Semi-annual

reports of this monitoring will be submitted to Pasco County and FDEP in accordance with this plan. Quarterly monitoring will also be conducted and reported at specific wells per Pasco County conditions.

19.2 Landfill Operating Records

The operating record for the landfill will document daily as a minimum the following activities:

- Self-inspections of landfill conditions, safety equipment and unacceptable waste received, any odor detected;
- Records used to develop permit applications;
- Change in construction, operation or closure permits and supporting designs;
- Water quality sampling events, analytical reports, well installation or repair;
- Employee training;
- Random load checks;
- Facility construction, major maintenance, or demolition;
- Other activities that significantly affect facility operations.

Self-inspections of the landfill conditions are conducted daily, and more extensive inspections are included weekly. Daily inspections include general inspection of site access, site security, and conditions of intermediate cover. Weekly inspections include more detailed inspections of the conditions of the surface water and stormwater management systems and groundwater monitoring wells.

The Operating Record will be kept at the landfill and be accessible to the landfill operators to maintain and for FDEP or Pasco County inspection at reasonable times.

Operational records will be maintained for the design life of the landfill, with the exception of weigh tickets which will be kept at least 5 years. Water quality monitoring information, maintenance records, and permit reports will be maintained for a minimum of 10 years. Background water quality records will be maintained for the design period of the landfill.

20.0 EROSION CONTROL

The site's inherent design as an excavation pit will prevent stormwater from leaving the property. Stabilization by seeding and mulching of the final fill areas will occur as the fill operations progress from cell to cell.

21.0 FINAL GRADE PLAN

Interim grades of the cells are shown on the plans (Drawings C1.00 and C2.00 of the 2016 Plan Set provided in Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016, Appendix A of the Engineering Report) and in the cross-sections (Drawings C1.10 and C2.10). Permitted mining activities will continue in accordance with the site's Class I mining permit. The final elevations after construction of future cells is planned to reclaim excavated areas back to the grade which existed prior to the site being opened as a mine with allowance for positive drainage. The Landfill Conceptual Closure Plan is provided in Drawing C2.00 (Section 4 of the March 2016 permit modification application RAI 1 response dated July 2016. Appendix A of the Engineering Report).

22.0 CLOSURE AND LONG TERM CARE

The site's Reclamation and Closure Plan details the procedures to properly close and maintain the landfill during the 30-year post-closure period. A Closure Report will be prepared for the landfill that details the site-specific limitations for land use based on geotechnical stability (settlement), potential gas migration, and site access. Long-term maintenance of erosion controls, storm water controls and monitoring devices is discussed in the Closure Plan (Section 7 of the March 2016 permit modification application RAI 1 response dated July 2016.—Appendix F of the Engineering Report).

23.0 CERTIFICATION

Laboratory testing and observation of cell floor conditions during cell construction completion will consist of the following:

- In-place density testing for each 12-inch thick soil lift, based on laboratory proctor test results for the construction material, will be recorded by a properly trained technician. These tests will be conducted in the location of each permeability test.
- Thickness testing of each lift will be recorded at a minimum frequency of two tests per acre, per lift.

- Confirmation hydraulic conductivity testing of Shelby tube or drive cylinder samples of the compacted cell floor material will be performed at a minimum frequency of one test per lift, per acre.
- Observance for unstable areas such as limestone, sink holes and soft ground will be performed for each cell.

If the test data from a cell floor section does not meet the requirements of the anticipated conditions of the hydrogeological and geotechnical reports and the requirements of the facility construction permit, additional random samples may be tested from that cell section. If the additional testing demonstrates that the hydraulic conductivity meets the requirements, the cell will be considered acceptable. If not, that cell will be reworked or reconstructed so that it will meet these requirements.

Upon completion of construction of any cell (or cell increment) within the disposal facility, the Applicant will provide the FDEP with the necessary reports, documents, and form 62-701.900(2), F.A.C. demonstrating that the approved construction is complete and in accordance with the submitted plans. The operator will provide the completed form to the FDEP in accordance with Rule 62-701.320(9)a., F.A.C., along with the quality assurance test results described above.

24.0 HISTORY OF ENFORCEMENT ACTION

In 2000, OGC Case No. 00-0009 was opened against the applicant for the Frontier Recycling facility (now Angelo's Recycling Facility) in Largo, Florida. A model consent order was used to resolve the issues of the case. The DEP's database did not include information regarding the subject of the enforcement.

In 2004, OGC Case No. 04-0887 (solid waste) and No. 04-0426 (stormwater) were opened against the applicant for Angelo's Recycling facility in Largo, Florida. ARM requested a minor permit modification to resolve the solid waste enforcement case. Formal enforcement was not taken to resolve the stormwater case. Instead, it was handled through submittal of a new permit application.

In 2006, OGC Case No. 06-0783 was opened against the applicant for the Enterprise Class III Landfill and Recycling Facility in Pasco County, Florida. ARM performed the corrective actions that were required to bring the facility into compliance and the assessed civil penalties were paid.

In 2007, OGC Case No. 07-1985 was opened against the applicant for the Angelo's C&D Recycling Waste Processing Facility in Apopka, Florida. ARM performed the corrective actions that were required to bring the facility into compliance and the assessed civil penalties were paid.

In 2007, Warning Letter #WL07-0019SW51SWD was issued to Angelo's Aggregate Materials, Ltd. for the Enterprise Class III Landfill. The Warning Letter was settled June 5, 2008 for total fines of \$18,397. In the "Proposed Settlement of Warning Letter WL07-0019SW51SWD", the Department acknowledged that Angelo's would not be considered "irresponsible" under FDEP Rule 62-701.320, FAC, as a result of the enforcement action.

In 2007, Warning Letter # WL07-0008SW52SWD was issued to Angelo's Aggregate Materials, Ltd. for the Recycling Waste Processing Facility in Largo, FL. The Warning Letter was settled April, 2009 for total fines of \$24,986. In the "Proposed Settlement of Amended Warning Letter WL07-0008SW52SWD", the Department acknowledged that Angelo's would not be considered "irresponsible" under FDEP Rule 62-701.320, FAC, as a result of the enforcement action.

ATTACHMENT 1 FACILITY ENTRANCE SIGN



PERATING HOURS: MONDAY - FRIDAY 7:00 am 5:00 pm

24 Hour Emergency Contacts:

Manager (352) 302-8934

ALL CUSTOMERS MUST CHECK IN AT GATE HOUSE

ACCEPTABLE WASTE:

Construction and demolition debris, yard waste, land clearing, glass, carpet, cardboard, plastic,

asbestos, paper, furniture, wood pallets, scrap and

shredded tires.

UNACCEPTABLE WASTE: Household garbage, toxic and hazardous waste, batteries, appliances, automobile, paint, solvents,

drums, septic tanks and pumping, whole tires.

WARNING:

We will be sorting all loads for prohibited waste. Any unacceptable waste/loads may be reloaded onto a vehicle to be taken to an

appropriate disposal facility at your expense.

FDEP/SWN PERMIT NUMBER: 177982-002-SO

ERP PERMIT NUMBER: 51-0172489-001

NO SCAVENGING



ATTACHMENT 2 RANDOM LOAD INSPECTION FORM

ENTERPRISE RECYCLING AND DISPOSAL FACILITY

RANDOM LOAD INSPECTION FORM

TIME:	
HAULING COMPANY:	
VEHICLE INFORMATION:	A) TRUCK #B) LICENSE PLATE #
NAME OF DRIVER:	
SOURCE OF WASTE MATERI	<u>^L:</u>
DESCRIPTION OF WASTE MA	TERIAL:
IF YES, WHAT MATERIALS W	ERE FOUND, AND WHAT PROCEDURES WERE
IF YES, WHAT MATERIALS W FOLLOWED?	VERE FOUND, AND WHAT PROCEDURES WERE
IF YES, WHAT MATERIALS W FOLLOWED?	VERE FOUND, AND WHAT PROCEDURES WERE
OTHER OBSERVATIONS:	

Note: Forms must be maintained in Inspection Log Book

ENTERPRISE CLASS II	ILANDFILL	Load Rejection Form
Date:	Time:	am/pm
CUSTOMER/GENERAT	OR	
Name	,	
Address		
City/State/Zip		
TRANSPORTER/HAULE	ER	
Name	****	
Address		
City/State/Zip		
Vehicle License and State		
REASON FOR REJECTION		
Suspected Special Waste Suspected Hazardous Waste	Suspected Medical Waste Suspected Asbestos	☐ Non-Processable ☐ Other (Explain below)
Explanation		
ACKNOWLEDGEMENT		
Rejected prior to dumping	Rejected	d After Load was Dumped
Comments		
Driver's Signature	Operator's Sign	nature
Customer/Generator Notified?		/Hauler Notified? YES NO
If yes, name of person contacted	If yes, name o	of person contacted

ATTACHMENT 3 FACILITY TRAINING LOG

ENTERPRISE RECYCLING AND DISPOSAL FACILITY

TRAINING LOG

COURSE	TRAINED OPERATOR INSTRUCTOR	HRS. ATTENDED	SIGNATURES/ DATE
			,

ATTACHMENT 4 GAS MONITORING SURVEY FORM

ENTERPRISE RECYCLING & DISPOSAL FACILITY CLASS III LANDFILL GAS MONITORING SURVEY FORM

Instrumen	t:									
GAS PROBE	TIME OF READING	AMBIENT AIR TEMP	AMBIENT AIR	AMBIENT AIR		HANE LI		. F	HANE LI Post-Purg easureme	e
NO.		°F	OXYGEN CONTENT %	METHANE % of LEL	% O ₂	% by Vol.	% of LEL	% O ₂	% by Vol.	% of LEL
11	Not installed									
2	Not installed									
3	Not installed				·					
4	Not installed									
5	Not installed									
6										
7										
8							<u> </u>			
9-R**			·					· · · · · · · · · · · · · · · · · · ·		
10 _{-R**}		· · · · · · · · · · · · · · · · · · ·								
11					i					
12										
13										
14			·							
15 *							<u>-</u> ,			
16	Not installed									
Scale house					N/A	N/A	N/A	N/A	N/A	N/A

NR - Not required, no methane indicated in pre-purge measurement

Notes: (Wind direction, weather conditions, damage to gas probes, adjacent off-site activity observed, etc.)

^{**} Revised December 2012 by Kelner Engineering (RAI #1)

^{*}Revised March 2012 by Kelner Engineering to reflect installation of GW-15

ATTACHMENT 5 LIST OF APPROVED COURSES

Florida's Solid Waste Operators & Spotters University of Florida

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Track Detail

Class I, III Landfill Operator

Is a solid waste facility that accepts Class I waste that is not hazardous waste and can be disposed in a lined landfill. The landfill may also accept yard trash, construction and demolition debris, processed tires, asbestos, carpet, cardboard, paper, glass, plastic, furniture other than appliances, or other materials approved by the FDEP that are not expected to produce leachate which poses a threat to public health or the environment. Operators required 24 hours initial course and pass exam with 70% proficiency, then 16 hours of continuing education every 3-year period.

Requirements

Initial Courses

- 24-Hour Initial Training Course for Landfill Operators (Class I, II, III and C&D Sites)
- · Initial Training Course for Landfill Operators and C&D Sites 24 Hour
- SWANA Manager of Landfill Operations [MOLO] & Exam
- · SWANA-Management of Landfill Operations
- SWANA-Manager of Landfill Operations (MOLO) Course and Exam

Hours

Hours Required	Effective Date
15	01/01/1800
16	05/27/2001

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Track Detail

Spotter / Waste Screener

Is a person employed at a solid waste management facility whose job it is to inspect incoming waste and to identify and properly manage any hazardous or prohibited materials, which are received at the facility. Spotter required 8 hours initial course, then 4 hours of continuing education every 3-year period.

Requirements

Initial Courses

- · 8-Hour Initial Training Course for Spotters at Class I, II, III Facilities, Waste Processing Facilities and C&D Facilities
- · 8-hour Initial Training for Spotters
- 8-Hour Spotter Training for Class I II III Landfill C&D Sites and Transfer Facilities
- 8-Hour Training Course for Spotters at Landfills, C&D Sites and Transfer Stations
- Environmental Management Systems: An Introduction
- · Spotter Training
- · Spotter Training for Solid Waste Facilities
- · Spotter Training for Solid Waste Facilities Spanish
- · Spotter Training for Solid Waste Management Staff with Elements of a Solid Waste Operations Plan
- · Waste Screening and Identification for Landfill Operators and Spotters
- Waste Screening at MSW Mgmt Facilities [Onsite Delivery]

Hours

Hours Required	Effective Date
4	01/01/1800

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Course Information

Course #	Name /	Status
582	16-Hour Initial Training Course for Transfer Station and MRF Operators	Active
575	2010 North American Environmental Field Conference and Expo	Active
516	24 Hour HazMat Techician Level	Active
608	24-Hour Initial Training Course for Landfill Operators (Class I, II, III and C&D Sites)	Active
478	40 Hour HazWoper	Active
507	40-Hour HazWoper	Active
626	40-Hour HazWoper Course in Accordance to 29 CFR 1910.120	Active
646	40-Hour OSHA HazWoper	Active
69	40-hour OSHA HAZWOPER Training Course	Active
450	40hr General Site Worker Hazardous Waste Operations	Active
463	4-Hour Refresher Course for Spotters at Landfills, C&D Sites and Transfer Stations	Active
616	6-Hour DOT Regulations	Active
601	8 Hour General Site Worker Refresher Training	Active
623	8 Hour HazWoper Refresher Training	Active
203	8-Hour Initial Training Course for Spotters at Class I, II, III Facilities, Waste Processing Facilities and C&D Facilities	Active
219	8-hour Initial Training for Spotters	Active
62	8-Hour OSHA HazWoper Annual Refresher	Active
644	8-Hour OSHA HazWoper Refresher	Active
488	8-Hour Spotter Training for Class I II III Landfill C&D Sites and Transfer Facilities	Active
462	8-Hour Training Course for Spotters at Landfills, C&D Sites and Transfer Stations	Active
410	Adult CPR	Active
0	Adult CPR	Active
675	Air Regulations and How They Impact MSW Facilities	Active
624	ANSI/AIHA Z10-2006 Occupational Safety and Health Management Systems Training Course Construction Standard	Active
652	Asbestos: Awareness (Class IV)	Active
630	Basic Life Support	Active
639	Bird and Wildlife Management for Utilities	Active
550	Bloodborne Pathogens	Active
618	Carbon Markets, Offsets & Project Level GHG Accounting	Active
614	Chemical Spill Response Training for Hazardous Materials Operations/OSHA Level II	Active
386	Community Hurricane Preparedness - online	Active
525	Composting Wastewater Residuals (Biosolids) in Charlotte County	Active
656	Confined Space Awareness	Active
657	Confined Space Competent Person Training	Active
436	Confined Space Entry Safety Course	Active
440	Construction and Demolition Debris Workshop	Active
485	Contemporary Techniques of Supervision/Management	Active
357	CPR and First Aid	Active

	Design of Waste Containment Liners and Closure Systems	Active
457	<u>Disaster Debris Management</u>	Active
544	EIA/NSWMA Safety Seminar	Active
542	Electrical Troubleshooting & Preventive Maintenance	Active
596	Emergency Response and Recovery Training	Active
557	Environmental Quality Training Workshop	Active
563	Environmental Safety Occupational Health [EOSH] 2009 Training Symposium	Active
568	Environmental Sampling Field Course	Active
679	Environmental Studies	Active
500	Excavation and Trenching Safety Procedures	Active
100	Excavation and Trenching: Competent Person Training	Active
228	FDEP 8 Hour HazWoper OSHA Refresher	Active
435	FDEP 8 Hour HazWoper OSHA Refresher [DeHate]	Active
433	FDEP Annuals SQG Workshop [5/3-5/06]	Active
434	FDEP Household Hazardous Waste Workshop [5/1-3/06]	Active
445	FEMA Debris Management Course	Active
678	FEMA Debris Management Course - G202	Active
484	Fires at Landfills and Other Solid Waste Management Facilities	Active
411	First Aid (Standard) Workplace Training	Active
634	Florida Composting Facility Operator Training Course: Introduction to Handling Source Seperated	Active
	Organics	7 101110
491	Florida Construction & Demolition Debris & Management Workshop - May 2008	Active
451	Florida Water & Pollution Control Operators Association Short School - Stormwater Section	Active
579	Food Recycling and Composting Workshop	Active
521	Foundations of Project Management	Active
156	Four Hour Spotter Refresher for Class I, II and III Landfills, Waste Processing Facilities and C&D Facilities	Active
591	Fundamentals of Emergency Management	Active
638	General Site Worker 8-hour Refresher Course Hazardous Waste Operations & Emergency Response	Active
423	Geosynthetic Testing and Landfill Design Issues Short Course	Active
629	Getting Back to Basics With Landfill Gas	Active
545	GHG Reporting for Landfill & Wastewater Treatment - Webinar	Active
558	Greenhouse Gas Accounting	Active
0	Greenhouse Gas Accounting- Measuring an Organization's Carbon Footprint	Active
	Greenhouse Gas Recovery at Solid Waste Landfills	Active
004	Crostiniodos Galeritosofor, al Cona Tracto Editamo	
604 224	Hazardous Materials in Construction and Demolition Waste Online	
224	Hazardous Materials in Construction and Demolition Waste OnLine Hazardous Materials Incident & Waste Training - 24 Hours	Active
224 503	Hazardous Materials Incident & Waste Training - 24 Hours	
224 503 356	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr	Active Active
224 503 356 469	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II	Active Active Active Active
224 503 356 469 439	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training	Active Active Active Active Active
224 503 356 469 439 510	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course	Active Active Active Active Active Active
224 503 356 469 439 510	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour	Active Active Active Active Active Active Active Active
224 503 356 469 439 510 535	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour	Active
224 503 356 469 439 510 535 541	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour Hazardous Waste Operations with Emergency Response	Active
224 503 356 469 439 510 535 541 540	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour Hazardous Waste Operations with Emergency Response Hazardous Waste Regulations for Generators	Active
224 503 356 469 439 510 535 541 540 63 514	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour Hazardous Waste Operations with Emergency Response Hazardous Waste Regulations for Generators Hazardous/Chemical Safety Training	Active
224 503 356 469 439 510 535 541 540 63 514	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour Hazardous Waste Operations with Emergency Response Hazardous Waste Regulations for Generators Hazardous/Chemical Safety Training HazMat IQ	Active
224 503 356 469 439 510 535 541 540 63 514	Hazardous Materials Incident & Waste Training - 24 Hours Hazardous Materials Incident Response Operations-40hr Hazardous Materials Operations / OSHA Level II Hazardous Materials Training Hazardous Waste Management Course Hazardous Waste Management: The Complete Course - 16 hour Hazardous Waste Management: The Complete Course - 8 hour Hazardous Waste Operations with Emergency Response Hazardous Waste Regulations for Generators Hazardous/Chemical Safety Training	Active

218	HazWoper 8-Hour Refresher Online	Active
422	HazWoper 8-Hour Refresher OSHA Course	Active
659	HazWoper Refresher	Active
617	HazWoper Training for Escambia County	Active
170	Health & Safety Issues for Solid Waste Management Facilities	Active
498	Health and Safety for Solid Waste Workers-4 Hours	Active
281	Health and Safety for Solid Waste Workers-8 Hours	Active
149	Health and Safety Training for Landfill Operations	Active
495	Heavy Equipment Safety	Active
492	Hurricane Debris Management Workshop	Active
683	Hydraulic Excavator Operator Training	Active
613	Identification of Unknowns	Active
476	Improving Landfill Operations	Active
517	Improving Transfer Station Efficiency	Active
442	Initial Training Course for Landfill Operators and C&D Sites - 24 Hour	Active
443	Initial Training Course for Transfer Station Operators and Material Recovery Facilities - 16 Hour	Active
628	Innovative Recycling Grant Workshop at Polk County Landfill	Active
574	Integrated Waste Management Workshop	Active
645	Introduction to Debris Operations in FEMA Public Assistance Program IS-632	Active
212	Introduction to Electrical Maintenance	Active
527	Introduction to Heavy Equipment and Skill Testing	Active
0	Introduction to Wastescreening for Spotters-Spanish	Active
546	IS-700.a NIMS An Introduction	Active
472	Landfill and Transfer Station Operators: Waste Acceptability and Safety Issues Review	Active
676	Landfill Design and Construction	Active
518	Landfill Gas Collection and Re-Use	Active
686	Landfill Gas Collection System Operations and Compliance Training Course	Active
511	Landfill Gas Control and Compliance Seminar	Active
650	Landfill Operations	Active
399	Landfill Operator and MRF Operator Training	Active
589	Landfill Operator Training - 2007 Certified Operators Class	Active
588	Landfill Operator Training 2008 - Certified Operators Class	Active
553	Landfills and Transfer Stations: Past, Present and Future	Active
552	Landfills: Past, Present and Future	Active
441	Laws and Rules	Active
277	Laws and Rules for Florida Engineers	Active
677	Leachate and Landfill Gas Management System Design	Active
684	Linear Construction - Stormwater Compliance for Road and Utility Construction	Active
538	Maintenance of Traffic Training	Active
654	Mathematics for Landfill Operators	Active
523	Maximizing Beneficial Use of Disaster Debris	Active
674	Measurement and Improvement of Performance at Solid Waste Management Facilities ("If you Can't Measure it, You Can't Manage It")	Active
3	Military Service Active Duty	Active
528	NAHAMMA Conf HHW / SQG Workshop - 2009 - HazMat IQ Training	Active
528	NAHAMMA Conference HHW / SQG Workshop - 2009 - General Session	Active
609	NAHMMA 2010 Annual Conference	Active
653	NAHMMA 2011 Florida Chapter Annual Conference	Active
424	National Incident Management System [NIMS] and Introduction IS-00700	Active

454	North American Hazardous Materials Management Association Conference 2007 - FL Chapter	Active
489	North American Hazardous Materials Management Association Conference 2008- FL Chapter	Active
670	North Carolina Landfill Manager Course	Active
1001	OK per "Current" Class I II III Transcript	Active
621	Online Laws and Rules	Active
438	Operating Considerations for Transfer Stations	Active
655	Operational Techniques and Compliance Inspections for Landfills	Active
412	Operator Certification for Caterpillar Landfill Equipment	Active
0	OSHA 10-Hour General Industry Course	Active
547	OSHA 10-Hour General Industry Outreach Course	Active
619	OSHA 10-Hour Industrial Outreach Safety Training Program	Active
592	OSHA 1910 General Industry 10-Hour Course	Active
0	OSHA 24 Hour Emergency Response Course (Technician Level)	Active
0	OSHA 8-hour HazWoper Refresher Training	Active
561	OSHA Annual Refresher at KSC	Active
515	OSHA Operations Level Course	Active
532	Paint Filter Test - 1 Hour	Active
192	Pedestrian, Vehicles and Equipment Safety at Transfer Stations	Active
494	Permit Required Confined Space Awareness	Active
104	Permit Required Confined Space Entry	Active
0	Permit Required Confined Space Entry Supervisor	Active
497	Personal Protection Equipment (PPE) and Safety Procedures	Active
602	Personal Radiation Detector Course [PRD] PER-243	Active
533	Principles of Landfill Fires E-Course	Active
468	Project Risk Management	Active
603	Recycle Florida Today - 2010 Annual Conference	Active
651	Recycle Florida Today - 2011 Annual Conference	Active
432	Recycle Florida Today 2006 Annual Conf	Active
431	Recycle Florida Today 2006 Issues Forum 1/2006	Active
414	Recycle Florida Today 2006 Issues Forum 1/23-24/06	Active
460	Recycle Florida Today 2007 Annual Confrence - 6/4-7/2007	Active
512	Recycle Florida Today 2008 Annual Conference	Active
554	Recycle Florida Today Conference [June 2009]	Active
479	Recycled Florida Today 2007 Issues Forum 1/2007	Active
0	Recycled Florida Today 2007 Issues Forum 1/2007	Active
661	Refresher Training Course for Experienced Solid Waste Operators-16 Hours	Active
663	Refresher Training Course for Experienced Solid Waste Operators-4 Hours	Active
662	Refresher Training Course for Experienced Solid Waste Operators-8 Hours	Active
627	RFT / SWANA FL Winter Meeting & Issues Forum 2011	Active
687	RFT / SWANA FL Winter Meeting & Issues Forum 2012	Active
581	RFT/SWANA-FL Winter Wonderland in Waste - 2010 Issues Forum	Active
565	Sanitary Landfill Design	Active
690	Sector L: Landfills & Land Application Sites	Active
4811	Solid Waste Operator & Spotter Refresher Training - Spring 2008 a	Active
584	Southeast Recycling 2010 Conference & Trade Show	Active
640	Southeast Recycling 2011 Conference & Trade Show	Active
692	Southeast Recycling 2012 Conference & Trade Show	Active
580	Southwest Partners Meeting	Active

605	SPCC - Spill Prevention Control Act - online	Active
526	Spill Prevention, Control, and Countermeasure Regulation Seminar	Active
400	Spotter Training	Active
0	Spotter Training	Active
214	Spotter Training	Active
437	Spotter Training Course for Waste Processing and Transfer Stations	Active
248	Spotter Training for Solid Waste Facilities	Active
378	Spotter Training for Solid Waste Facilities - Spanish	Active
474	Spotter Training for Solid Waste Management Staff with Elements of a Solid Waste Operations Plan	Active
471	Spotters at Landfills and Transfer Stations: Safety Awareness Review	Active
506	Storage Tank Conference - Central Florida 18th Annual	Active
505	Storage Tank Conference - North Florida 14th Annual	Active
578	Storage Tank Conference -16th Annual Central Florida State Conference	Active
453	Storage Tank Conference 17th Annual	Active
475	Storage Tank Conference Central Florida State 13th Annual	Active
647	Stormwater Erosion And Sedimentation Control Inspector Training Program	Active
202	Stormwater Inspector Certification Course	Active
594	Stormwater Matters	Active
632	Supervisor Safety Training for Solid Waste Operations Staff	Active
586	Sustainability and Recycling	Active
429	SWANA - Compost on Subtitile D Landfills - Webinar	Active
416	SWANA - eCourse - Litter Management at Landfills	Active
567	SWANA – Groundwater Monitoring, Sampling, Analysis and Well Construction	Active
636	SWANA - Integrated Solid Waste Management	Active
693	SWANA - Landfill Gas Basics 1-Day Course	Active
635	SWANA - Landfill Gas Systems Operation and Maintenance	Active
694	SWANA - Landfill Gas Systems Operation and Maintenance - 1 day	Active
537	SWANA - Landfill Operations E- Course	Active
543	SWANA - Landfill Symposium 14th Annual (June 2009)	Active
597	SWANA - Manager of Landfill Operations [MOLO]	Active
598	SWANA - Manager of Landfill Operations [MOLO] & Exam	Active
560	SWANA - Manager of Recycling Course	Active
413	SWANA 2006 Recycling and Special Waste Conference	Active
562	SWANA E-Course Just the Math	Active
556	SWANA e-Course Operation Efficiency at Landfills	Active
599	SWANA e-course: Bioreactor Landfill Research & Development Agencies	Active
577	SWANA e-course: Carbon Credit and Production Tax Credits for LFG Projects	Active
576	SWANA e-course: Financing Solid Waste Facilities: The Roller Coaster to Oblivion?	Active
691	SWANA e-course: Traumatic Injury and Fatality Risks in Solid Waste	Active
564	SWANA- Health & Safety E-Study (Home Study Course)	Active
566	SWANA- Managing Landfill Gas at MSW Landfills	Active
297	SWANA Online - Health & Safety at MSW Landfills	Active
296	SWANA Online - Training Sanitary Landfill Operation Personnel	Active
298	SWANA Online - Wastescreening at MSWS Facilities	Active
345	SWANA-Bioreactor Landfill Course	Active
404	SWANA-Bioreactor Landfill Course SWANA-Bioreactor Landfill Manager	Active
250	SWANA-Construction and Demolition Debris Course	
		Active
685	SWANA-e Course: Groundwater Monitoring	Active

643	SWANA-e Course: Landfill Gas & Solid Waste Air Contaminant Hazards	Active
252	SWANA-FEMA's Debris Management	Active
425	SWANA-FL 2006 Spring Tri-State Conference [4/2-5/06]	Active
426	SWANA-FL 2006 Summer Conference [7/23-26/06]	Active
447	SWANA-FL 2007 Summer Conference [7/15-18/07]	Active
480	SWANA-FL 2008 Senior Managers Conference [1/2008]	Active
551	SWANA-FL 2009 Summer Symposium	Active
607	SWANA-FL 2010 Summer Conference	Active
658	SWANA-FL 2011 Summer Conference	Active
534	SWANA-FL Managers Meeting - 2009 Winter	Active
606	SWANA-FL Road-e-o: Heavy Equipment Safety Training	Active
94	SWANA-Health & Safety at MSW Landfills	Active
244	SWANA-Landfill Gas Basics	Active
428	SWANA-Landfill Gas Symposium 29th Annual [3/27-30/06]	Active
446	SWANA-Landfill Gas Symposium 30th Annual [3/4-8/07]	Active
483	SWANA-Landfill Gas Symposium 31st Annual [3/2008]	Active
536	SWANA-Landfill Gas Symposium 32nd	Active
689	SWANA-Landfill Gas Symposium 35th Annual - 2012	Active
231	SWANA-Landfill Gas System Operation and Maintenance	Active
539	SWANA-Landfill Gas System Operations Workshop	Active
93	SWANA-Landfill Operational Issues	Active
681	SWANA-Landfill Symposium (16th Annual - 2011)	Active
427	SWANA-Landfill Symposium 11th Annual [6/5-7/06]	Active
465	SWANA-Landfill Symposium 12th Annual [6/25-28/07]	Active
30	SWANA-Management of Landfill Operations	Active
1	SWANA-Manager of Landfill Operations (MOLO) - Exam Only	Active
1600	SWANA-Manager of Landfill Operations (MOLO) Course	Active
160	SWANA-Manager of Landfill Operations (MOLO) Course and Exam	Active
243	SWANA-Managing Composting Programs	Active
251	SWANA-Managing MSW Collection Systems	Active
234	SWANA-Managing MSW Recycling Systems	Active
222	SWANA-Managing Transfer Station Systems	Active
444	SWANA-Transfer Station Design & Operations	Active
42	SWANA-Transfer Station Design & Operations	Active
448	SWANA-WasteCon 2006 [9/19-21/06]	Active
455	SWANA-WasteCon 2007 [10/16-18/07]	Active
509	SWANA-WasteCon 2008	Active
559	SWANA-WasteCon 2009	Active
660	SWANA-WasteCon 2011	Active
570	The Complete Ground Water Monitoring Field Course	Active
572	The Complete Ground Water Monitoring Well Design, Construction and Development Course	Active
569	The Complete Ground Water Monitoring View Design, Construction and Development Course The Complete Ground Water Sampling Field Course	Active
116	The Complete Ground-Water Monitoring Course	Active
571	The Complete Strace Water and Sediment Field Course	Active
573	The Florida Stormwater Construction Permit-Contractor's Short Course	Active
530	The Original Environmental Bootcamp	Active
406	The Sense of Smell, Odor, Theory and Odor Control	Active
612	Things That Go Boom	Active

Topics in Solid Waste Management for Landfill Operators, MRF Operators and Transfer Station	Active
<u>Operators</u>	
<u>Tractor/Mower Operator Safety Training Program</u>	Active
Traffic and Equipment Safety at Landfills	Active
Train the Trainer: How to Design & Deliver Effective Training	Active
Train-the-Trainer for Operator of Heavy Equipment	Active
Trenching Shoring Services Safety in Excavation Course	Active
U.S. DOT Hazardous Materials/Waste Transportation	Active
<u>Understanding Hazardous Waste in Solid Waste Operations</u>	Active
Waste Expo [4/4-6/06]	Active
Waste Expo 2007	Active
Waste Expo 2010	Active
Waste Screening and Identification for Landfill Operators and Spotters	Active
Waste Screening at MSW Mgmt Facilities [Onsite Delivery]	Active
Waste Screening at Municipal Solid Waste [5/23/94, 12/5/01]	Active
Waste Screening Introduction-Spanish	Active
Waste Screening Refresher for Supervisors and Managers	Active
Waste Tech 2006 [2/27-28/06]	Active
Waste Tech 2007	Active
Waste-to-Fuels 2010 Conference	Active
Wet Weather Operations	Active
Wetlands Variance Training	Active
Wildlife and Plants at Florida Solid Waste Management Facilities	Active
Workzone Safety Training	Active
	Operators Tractor/Mower Operator Safety Training Program Traffic and Equipment Safety at Landfills Train the Trainer: How to Design & Deliver Effective Training Train-the-Trainer for Operator of Heavy Equipment Trenching Shoring Services Safety in Excavation Course U.S. DOT Hazardous Materials/Waste Transportation Understanding Hazardous Waste in Solid Waste Operations Waste Expo [4/4-6/06] Waste Expo 2007 Waste Expo 2010 Waste Screening and Identification for Landfill Operators and Spotters Waste Screening at MSW Mgmt Facilities [Onsite Delivery] Waste Screening at Municipal Solid Waste [5/23/94, 12/5/01] Waste Screening Introduction-Spanish Waste Screening Refresher for Supervisors and Managers Waste Tech 2006 [2/27-28/06] Waste Tech 2007 Waste-to-Fuels 2010 Conference Wet Weather Operations Wetlands Variance Training Wildlife and Plants at Florida Solid Waste Management Facilities

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3900 SW 63rd Blvd. tel: (352) 392-9570 <u>train@treeo.ufl.edu</u> Gainesville, FL 32608 fax: (352) 392-6910 <u>train@treeo.ufl.edu</u>



ATTACHMENT 6 TRAINING CERTIFICATES





Has Successfully Completed the 16 Hour Continuing Training Course for Landfill Operators Entitled:

16-Hour Landfill Operator Refresher Course #703 August 31 and September 2, 2015

And Has Successfully Completed 16 hours of Continuing Training for Landfill Operators in Florida

Signed this 15th day of September, 2015 Melody tohl

MSW

Melody Kohl President



Has Successfully Completed the 16 Hour Continuing Training Course for Landfill Operators Entitled:

16-Hour Landfill Operator Refresher Course #703 August 31 and September 2, 2015

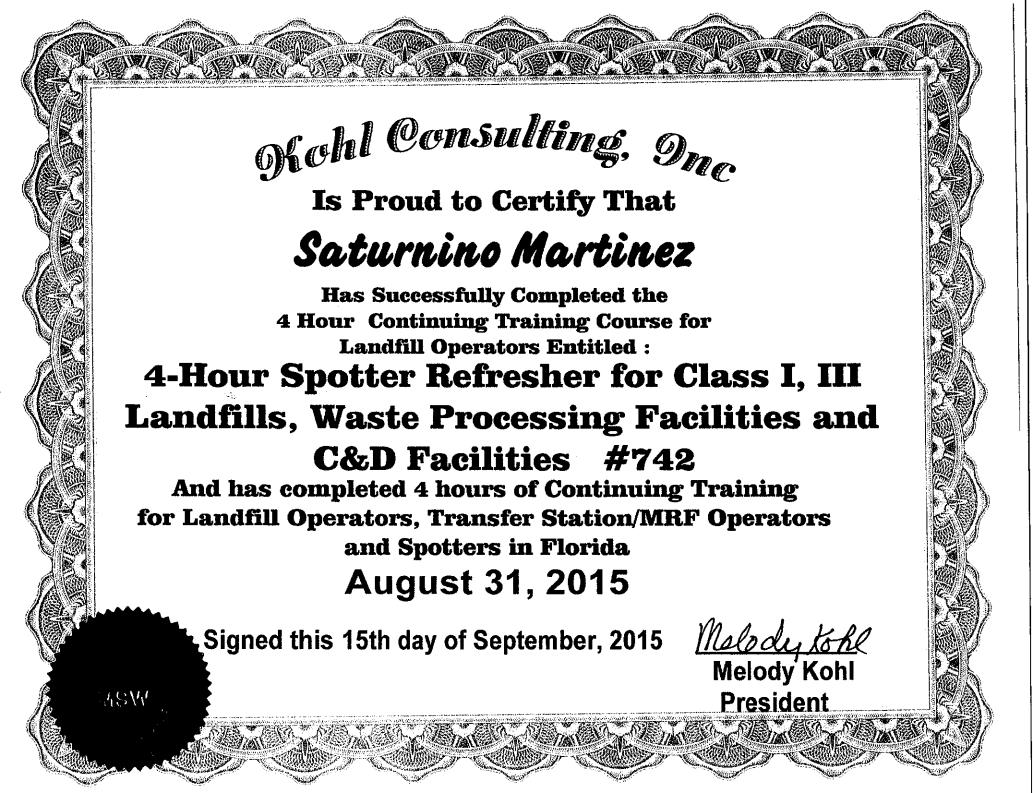
48W

And Has Successfully Completed 16 hours of Continuing Training for Landfill Operators in Florida

Signed this 15th day of September, 2015 <u>Melody Kohl</u> Melody Kohl

CONTRACTOR OF THE PROPERTY OF

President



of chi Consulting 9nc.

Is Proud to Certify That

David Cooner

Has Successfully Completed the Initial Training Course for Transfer Station and MRF Operators Entitled :

16-hour Initial Training for Transfer Station and Materials Recovery Facility Operators (with Exam) #582 November 14 and 15, 2013

> And Has Successfully Completed the Required Examination in Accordance with the Initial Training Requirements for both Transfer Station and MRF Operators in Florida

Signed the 18th day of November, 2013 Melody Kokl

Melody Kohl
Melody Kohl

ATTACHMENT 7 SOURCE-SEPARATED ORGANICS PROCESSING FACILITY REGISTRATION



Florida Department of Environmental Protection

Carlos Lopez-Cantera Lt. Governor

Rick Scott

Governor

Bob Martinez Center 2600 Blair Stone Road Tallahassee, Florida 32399-2400

Jonathan P. Steverson Secretary

July 10, 2016

John Arnold Angelo's Aggregate Materials, LTD. 855 28th Street, S. St. Petersburg, FL 33712

Dear John Arnold:

Your registration application for Angelo's Recycled Materials - Dade City, located at 41111 Enterprise Road, Dade City, in Pasco County has been received. The application indicated this facility is operating as a:

X Yard Trash Transfer Station
X Yard Trash Recycling Facility
Manure Blending Operation
Vegetative, Animal Byproducts or Manure Composting Facility
And processing the following:
X Yard trash (including clean wood)
Manure
Animal byproducts (composting)
Vegetative wastes (composting)
Pre-consumer vegetative (composting)

The registration application is complete, and is valid until August 1, 2017. The WACS identification number for this facility is 00087895. The receipt number for the registration fee you paid is 911551.

You must comply with the requirements specified in Rule 62-709.320, and Rules 62-709.330 or 62-709.350, Florida Administrative Code (F.A.C.), in order to maintain qualification for the registration program. A summary of the operating requirements is enclosed.

July 10, 2016 John Arnold Page 2 of 2

If you need further information, please contact the Division of Waste Management, Waste Registration Section at the above address, Mail Station 4550, telephone (850) 245-8707, or email Lauren.OConnor@dep.state.fl.us.

Sincerely,

Planner I

Waste Registration Section

Lawren O'Connod

Enclosure

cc: Melissa Madden, Southwest District Steven Tafuni, Southwest District

Rule/Referenced Rule	Provision			
Specific to all				
62-709.300(7)(a)	No person shall cause or allow objectionable odor in violation of Chapter 62-296, F.A.C.			
62-709.300(7)(b)	Rule 62-701.300, and subsection 62-701.320(13) apply to facilities regulated under 62-709.			
62-701.300(1)(b)	Stored or processed in a way or location that does not violate air quality or water quality standards.			
62-701.300(2)(a)	Geological formations or subsurface features must provide support for the facility			
62-701.300(2)(c)	Not in a dewatered pit unless permanent leachate containment and special design techniques used.			
62-701.300(2)(d)	Not in any natural or artificial water body(e.g., ground water and wetlands within DEP jurisdiction).			
62-701.300(2)(f)	Not be placed on the right of way of any public highway, road, or alley.			
62-701.300(3)	No open burning in the recycling area of the facility and controlled burning complies with DEP rules.			
62-701.300(14)	No CCA treated wood in material applied as a ground cover, soil or soil amendment.			
62-701.300(15)	No unconfined emissions of particulate matter in violation of paragraph 62-296.320(4)(c), F.A.C.			
62-709.320(2)(a)	Have the necessary operational features and equipment - unless otherwise specified, including			
62-709.320(2)(a)1.	effective barrier to prevent unauthorized entry and dumping			
62-709.320(2)(a)2.	Dust and litter control methods			
62-709.320(2)(a)3.	Fire protection and control provisions to deal with accidental burning of solid waste, including			
62-709.320(2)(a)3.a.	20-foot all-weather access road all around the perimeter			
62-709.320(2)(a)3.b.	No material shall be mechanically compacted			
62-709.320(2)(a)3.c.	No material shall be more than 50 feet from access by motorized firefighting equipment			
62-709.320(2)(b)	Operate in a manner to control vectors			
62-709.320(2)(c)	Operate in a manner to control objectionable odors per with Rule 62-296.320(2), F.A.C.			
62-709.320(2)(d)	Keep any installed drains and leachate or condensate conveyances cleaned			
62-709.320(2)(e)	Process received solid waste timely as follows			
62-709.320(2)(e)1.	Size-reduce or remove yard trash within 6 months or time needed to receive 3,000 tons or 12,000			
	cubic yards, whichever is greater. Separated logs with 6 inch diameter or greater can be stored for			
	up to 12 months before being size-reduced or removed.			
62-709.320(2)(e)2.	Putrescible waste (e.g., vegetative wastes, animal byproducts or manure) shall be processed and			
	incorporated into the composting material, or removed from the facility, within 48 hours.			
62-709.320(2)(f)	Containerized and removed immediately any treated or untreated biomedical waste; hazardous			
	waste; or any materials having (PCB) concentration of 50 ppm or greater.			
62-709.320(2)(g)	All residuals, solid waste and recyclable materials removed and recycled or disposed upon ceasing			
00.700.000(4)()	operations. Any remaining processed material shall be properly used or disposed.			
62-709.320(4)(a)	Keep monthly records of incoming and outgoing material for at least three years			
62-709.320(4)(b)	If temperature used to show disinfection or vector attraction achieved, keep records for 3 years.			

Specific to yard trash only facilities		
62-709.300(7)(b)	Rule 62-701.300, and subsection 62-701.320(13) apply to facilities regulated under 62-709.	
62-701.300(12)(a)	At least 100 feet from off-site potable water well that existed before facility registered.	
62-701.300(12)(b)	At least 50 feet from any body of water, including wetlands. Not including parts of permitted	
	stormwater system, or water bodies totally within facility with no discharge to surface waters.	
62-709.330(2)	Processed material gone from facility within 18 months, unless longer storage authorized by permit.	
62-709.330(3)	Accept only yard trash, and bags used to collect yard trash. Containerized any other material	

Specific to composting of vegetative wastes, animal byproducts or manure, or blending manure		
62-709.300(7)(b)	Rule 62-701.300, and subsection 62-701.320(13) apply to facilities regulated under 62-709.	
62-701.300(2)(b)	Be more than 500 feet off-site potable water well that existed before facility registered	
62-701.300(2)(e)	Within 200 feet from any body of water, including wetlands. Not including parts of permitted stormwater system, or water bodies totally within facility with no discharge to surface waters.	
62-701.320(13)(b)	Not within 10,000 feet of any licensed and operating airport runway used by turbine powered aircraft, or within 5,000 feet of any licensed and operating airport runway used only by piston engine aircraft, unless applicant demonstrates that the facility is designed and will be operated so that it does not pose a bird hazard to aircraft.	
62-709.350(2)	Carbon:nitrogen ratio of the blended feedstocks shall be greater than 20.	
62-709.350(3)	Piles do not exceed 12 feet in height.	
62-709.350(5)	All material removed within 18 months, unless longer storage authorized by permit.	
62-709.350(6)	Show that disinfection achieved. not required if made from only pre-consumer vegetative waste	
62-709.350(7)	Vector attraction reduction controls shall include either (a) or (b) below:	
62-709.350(7)(a)	Composted for at least 14 days, with temperature no lower than 40 degrees Celsius and average temperature of the material being composted higher than 45 degrees Celsius; or	
62-709.350(7)(b)	Specific oxygen uptake rate (SOUR) for material being composted or blended shall be equal to or less than 1.5 milligrams of oxygen per hour per gram of total solids (dry weight basis) at a temperature of 20 degrees Celsius	

Appendix 3-B CONTINGENCY PLAN

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY MAJOR PERMIT MODIFICATION EMERGENCY AND CONTINGENCY OPERATIONS

Prepared for:

ANGELO'S AGGREGATE MATERIALS, LTD

855 28th Street South St. Petersburg, Florida 33712

Presented to:

FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION SOUTHWEST DISTRICT – SOLID WASTE DIVISION

13051 N. Telecom Parkway Temple Terrace, Florida 33637

Prepared by:

LOCKLEAR & ASSOCIATES, INC.

4140 NW 37 Place, Suite A Gainesville, Florida 32606 Certificate of Authorization #30066

Project No.: 02000-144-15

March 2016

Revised July 2016 RAI 1 Response

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1.7	Landfill Shutdown	4

1.0 EMERGENCY AND CONTIGENCY OPERATIONS

Angelo's Aggregate Materials, LTD (Applicant) is the Owner and Operator of the Enterprise Road Class III Recycling and Disposal Facility (Facility). Emergency conditions that may require a contingency operation plan may be created by a natural disaster (i.e., hurricane, tornado, and/or flooding), or fire. During emergency conditions normal waste acceptance procedures will continue, as feasible. The following procedures are to be initiated at the onset of a site emergency or major storm:

1.1 Communications

The designated emergency coordinator for the Facility is Mr. Fred Martinez, who may be reached at (352) 303-5618. Mr. Martinez is responsible for implementing emergency and contingency operations or designating an alternate coordinator.

As necessary the emergency coordinator will notify the appropriate emergency response personnel including:

- 911 Fire/Police/Medical
- Dade City Fire Department- (352) 521-1492
- Dade City Police Department- (352) 521-1493
- Pasco County Hospital Dade City (352) 521-1100
- Florida Department of Environmental Protection (813) 470-5700 632-7600
- Pasco County (727) 847-2411

If needed, the Operator will coordinate with emergency response and Pasco County personnel to notify neighbors and / or local government officials of emergency and contingency conditions that may affect them.

1.2 Major Storm or Disaster

- 1. All personnel understand their role in an emergency situation. At least one office employee will monitor the telephone. Radio or telephone communication is provided between the office and all operating areas of the landfill at all times.
- 2. All lightweight signs and equipment are to be collected and stored in a secure area.
- 3. All depressed and eroded areas are to be protected and the stormwater management system is to be inspected and maintained, as necessary.

- 4. Work is to begin in dry areas only when operations are resumed; waste materials are not to be deposited in standing water.
- 5. On-site emergency equipment locations, such as first aid and eye wash stations, are shown on Site Plan.

1.3 Fire

Although open burning is strictly prohibited, several types of fires could occur at the Facility including equipment fires, structure fires, waste fires, buffer zone fires, and receipt of hot loads. The Operator will provide a truck mounted water tank on-site for use in firefighting purposes. A stockpile of soil will be located near the active disposal area at all times for use in smothering waste fires and hot loads. During a fire, incoming trucks will be directed toward another area of the landfill so that a temporary active face can be established. Once the fire is extinguished, appropriate cover will be applied to the waste and operations will continue at the original active face. If the fire is extensive and a temporary active face cannot be established, incoming trucks will be redirected to another landfill.

For all fires, the Florida Department of Environmental Protection (FDEP) and Pasco County will be notified of the fire control plan being implemented if the fire cannot be extinguished or controlled within an hour. If the fire cannot be extinguished or controlled within 48 hours, the emergency coordinator will notify the local Fire Department listed above for assistance and will also notify Pasco County and any neighbors likely to be affected by the fire.

The Operator will take the following procedures if a fire occurs at the Facility:

1.3.1 Equipment and Structural Fires

If the fire is minor in nature, site personnel will attempt to extinguish the fire using available onsite fire fighting equipment. The local Fire Department listed above will be summoned for assistance if site personnel and equipment cannot extinguish the fire.

1.3.2 Waste Fires

Burning waste will be separated from the fill area and immediately covered with soil stockpiled near the disposal area. If necessary, water will also be applied to the burning waste using the on-site truck mounted water tank. The local Fire Department listed above will be summoned for assistance if the site personnel and equipment cannot extinguish the fire.

1.3.3 Buffer Zone Fires

The local Fire Department listed above will be immediately summoned to control and extinguish the fire. Available site personnel will create and maintain fire breaks between the active disposal area and the oncoming fire, and water down areas between the fire and the disposal area using the water tank. Available site personnel will assist the Fire Department as requested.

1.3.4 Hot Load Fires

If a hot load has not been unloaded, the driver will be directed to an isolated area of the Facility and site personnel will use available fire fighting equipment in an attempt to extinguish the load. If a hot load has been unloaded, the load will be spread out and separated from the active disposal area and immediately covered with soil stockpiled near the area. If necessary, water will also be applied to the load using the on-site water tank.

The local Fire Department listed above will be summoned for assistance if site personnel and equipment cannot extinguish the load.

1.3.5 Fire-Fighting Equipment

Fire extinguishers are located in locations indicated below.

- Office / Scale House
- Heavy Equipment Cabs

1.4 Spills

In the event of a spill, the site manager will determine whether on site personnel are capable of the cleanup. For example, if oil is spilled while performing vehicle maintenance, the site manager will direct landfill personnel to use a sorbent material to clean up the spill if spill occurred on an impervious surface. For spills on unpaved areas of the facility, the contaminated soil will be removed and placed in an appropriate container. All cleanup materials will be placed in a drum, stored in the shipping/storage container on-site for proper disposal. If unknown or hazardous chemicals are spilled, the site manager will contact the Department (813-470-5700 632 7600) and Pasco County (727-847-2411) for direction.

1.5 Discovery of Hazardous Wastes

The operator will take the following steps if hazardous wastes are discovered at the active

disposal area that may pose a serious health and safety risk to site personnel, the public, or the environment. Site personnel will establish a minimum 50-foot perimeter around the suspect

waste using pylons and "Caution" and/or "Do Not Enter" tape. The driver and other customers

will not be allowed closer than 50 feet to the suspect waste. Site personnel will immediately

contact their supervisor. The supervisor will contact a hazardous waste materials response team

to coordinate cleanup and disposal of the hazardous materials.

1.6 **Equipment Failure**

Arrangements with equipment rental companies will be maintained in order to provide for

additional equipment during unanticipated breakdowns.

Equipment rental companies that may be used to obtain reserve equipment include the

following:

Ring Power - Brooksville, Florida

Contact: 352-796-4978

Flagler Equipment - Tampa, Florida

Contact: 813-630-0077

1.7 Landfill Shutdown

1. If the landfill should need to be shut down, the Department will be notified and haulers

will be directed to another properly permitted facility.

2. Initial cover of six (6) inches will be placed on all waste exposed areas.

The stormwater management system will allow for disposal operations to continue during

periods of inclement weather. Temporary berms, ditches, and grading are to be used to drain stormwater away from the active face of the landfill. The following actions should be taken at

the landfill following a severe storm, hurricane, or other natural disaster:

FDEP and Pasco County are to be notified by telephone immediately should any need for

emergency and contingency operations arise. The phone number for the Department's Solid Waste Section is (813) 470-5700. The phone number for Pasco County is (727)

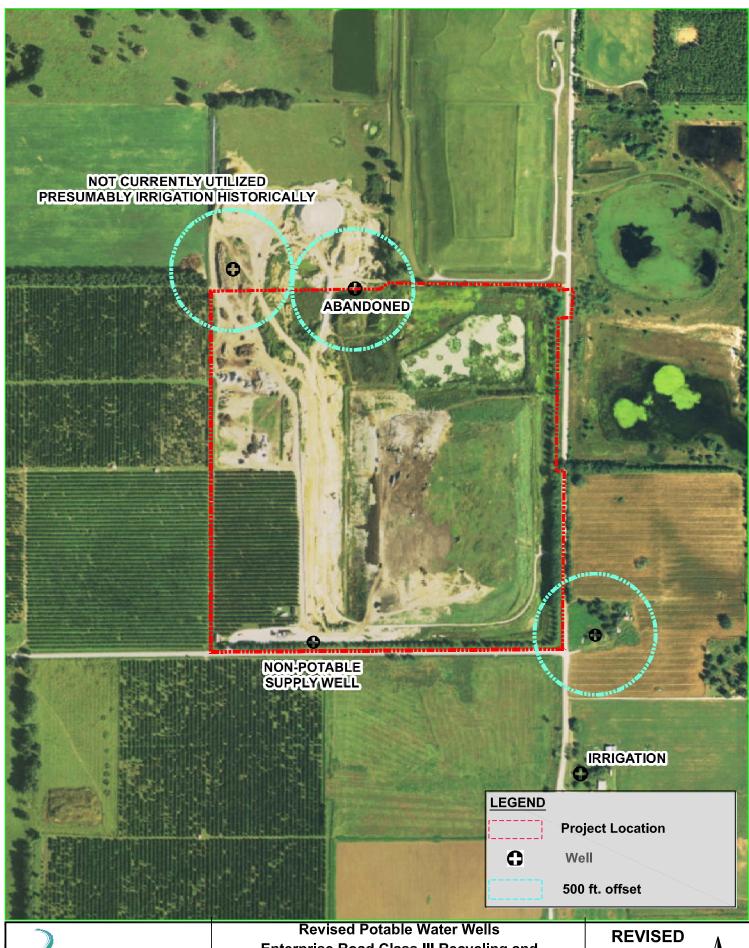
847-2411. The calls are to be confirmed by letter.

- Operational hours of the landfill may be extended at the landfill to meet the needs of the community. Pasco County and the Department will be consulted prior to changes in the hours of operation of the landfill.
- Necessary additional equipment, if required, will be rented. Arrangements are in place between the operator of the Landfill and equipment rental companies to facilitate this activity.
- If required, additional equipment operators and/or other personnel will be contracted. Arrangements are in place between the operator of the Landfill and temporary staffing companies to facilitate this activity.
- Appropriate public notices will be issued, including notification of the landfill's customer's by telephone and other media
- Contacts with local governmental bodies and local emergency agencies such as fire and
 rescue have been established in order to coordinate emergency activities. Fire and rescue
 personnel responsible for this district have visited the site in order to discuss emergency
 procedures.
- Site personnel may be trained in CPR and First Aid.

Appendix 3-C

FIGURES

(with the exception of revised Figure S-1, Potable Water Wells, please refer to the current permitted facility figures)





Revised Potable Water Wells Enterprise Road Class III Recycling and Disposal Facility Permit Modification Dade City, Pasco County, Florida REVISED FIGURE



SOURCE: FDEP

Appendix 3-D WELL ABANDONMENT DOCUMENTATION

STATE OF FLORIDA WELL COMPLETION REPORT



X Southwest

☐ Delegated Authority (If Applicable)

PLEASE, FILL OUT ALL APPLICABLE FIELDS (*Denotes Required Fields Where Applicable)

Received:

Nov 20, 2015 11:19 am

Date Stamp

□ Northwest
□ St. Johns River ☐ South Florida ☐ Suwannee River DEP

Official Use Only

1.*Permit Number_843536
2.*Number of permitted wells constructed, repaired, or abandoned1
3.*Owner's Name Angelo's Recycled Materials 4.*Completion Date 06/16/2015 5. Florida Unique ID
6. 41111 Enterprise Rd Dade City 33525 *Well Location - Address, Road Name or Number, City, ZIP
7. *County_PASCO *Section5 Land Grant*Township25 *Range22
8. Latitude 28 20 12.50 Longitude 82 08 08.20
9. Data Obtained From:GPSX_MapSurvey Datum:NAD 27X_NAD 83WGS 84
10.*Type of Work:ConstructionRepairModification _XAbandonment 11.*Specify Intended Use(s) of Well(s):DomesticLandscape IrrigationLivestockMonitoringSte InvestigationLivestockMonitoringTestPublic Water Supply (Limited Use/DOH)Public Water Supply (Community or Non-Community/DEP)Golf Course IrrigationHVAC SupplyHVAC SupplyHVAC Return
Class V Injection:Recharge Commercial/Industrial DisposalAquifer Storage and RecoveryDrainage
Remediation:RecoveryAir SpargeOther (Describe)
X Other (Describe) PLUGGED
12.*Drill Method:AugerCable ToolRotaryCombination (Two or More Methods)JettedSonic
Horizontal Drilling Hydraulic Point (Direct Push) X Other PLUGGED BY APPROVED METHOD 13.*Measured Static Water Level 0.0 ft. Measured Pumping Water Level ft. After Hours at GPM 14.*Measuring Point (Describe) Which is ft. Above Below Land Surface *Flowing: Yes No. 15.*Casing Material: X Black Steel Galvanized PVC Stainless Steel Not Cased Other
16.*Total Well Depth <u>260.0</u> ft. Cased Depth <u>149.0</u> ft. *Open Hole: FromToft. *Screen: FromToft. Slot Size
17.*Abandonment:
18.*Surface Casing Diameter and Depth: Dia 12.10 in. Fron149.00 ft. To 153.00 ft. No. of Bag\$24.00 Seal Material (Check One): X Neat Cement Bentonite Other Dia 12.10 in. Fron153.00 ft. To 260.00 ft. No. of Bag\$51.00 Seal Material (Check One): Neat Cement Bentonite Other Seal Material (Check One): Neat Cement Bentonite Other Other
19.*Primary Casing Diameter and Depth: Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other Dia in. From ft. To ft. No. of Bags Seal Material (Check One): Neat Cement Bentonite Other
20.*Liner Casing Diameter and Depth: Diain. Fromft. Toft. No. of Bags Seal Material (Check One):Neat CementBentoniteOther Diain. Fromft. Toft. No. of Bags Seal Material (Check One):Neat CementBentoniteOther Diain. Fromft. Toft. No. of Bags Seal Material (Check One):Neat CementBentoniteOther
21.*Telescope Casing Diameter and Depth: Diain. Fromft. Toft. No. of BagsSeal Material (Check One):Neat CementBentoniteOther Diain. Fromft. Toft. No. of BagsSeal Material (Check One):Neat CementBentoniteOther Diain. Fromft. Toft. No. of BagsSeal Material (Check One):Neat CementBentoniteOther
22. Pump Type (If Known): 23. Chemical Analysis (When Required):
CentrifugalJetSubmersibleTurbine
Pump Depthft. Intake DepthftLaboratory TestField Test Kit
24. Water Well Contractor:
*Contractor Name Charles S Diehl *License Number 9415 E-mail Address cdiehl@wellwater.com
*Contractor's Signature Digitally Signed (I certify that the information provided in this report is accurate and true.) *Driller's Name (Print or Type)

SOUTHWEST FLORIDA WATER MANAGEMENT DISTRICT WELL GROUTING/ABANDONMENT FORM

GRO	UTING	the range of the state of	ABANDONMENT	X	PHOL
Permit No. 843536 Drill					9415
1/41/4 SEC5 T	ng Contractor	27	18 1012 60	License No	7713
Data obtained from: GPS or N	ap or Surv	ey: D	oatum NAD 27	NAD 83	
Property Owner Malls Re Address of Welly 41111 Exxe	system //	Mercals	1.		
Address of Welly 7/11/ Zaxw	prise ex	· , Xlack	ary		
County Pasco	QWI	P No		UP No	
			D	ID No	
	WELL S	SPECIFICATIONS			
T.D. of Well (to be verified by inspector)	260			Notor Lovel 16	_
T.D. of Well (to be verified by inspector) Casing: Double or Single;	Diameters /2	' Denth	· Measured V	Fetimated	Logged I
Material: (check) Black Steel , Galv.	. PVC . Othe	er ,boptii	. Wicasarca -	, Louinated,	Logged <u>-</u>
Drill Method (check) Rotary,	Cable Tool, Con	nbination, Other	er	3.5	
Was well information verified from driller's					
Special Construction Stipulation? No					
Old Permit? No Yes Permit No.				th Diamete	er
(For public supply) Approved Public Supply					
(For 62-524) Yes No Well loca	ation same as surveye	ed location? Yes	No		
3.1	GROUT SPECIFIC	ATIONS AND INS	DECTION		
Date:	GROUT SPECIFIC	ATIONS AND INS	/ /	15 61	12/5
Date	0/4/15	6/10/15	_ 6/11/	14	1/2/10/
BENTONITE INTERVAL					6-106
Type (check): chips, pellets/tablets	: Size: 3/-	4 🛂 , 1/2 ,	3/8;	Bentonite Slurry	_
Estimated Bags of Bentonite		· · · · · · · · · · · · · · · · · · ·			
Actual Bags of Bentonite	A	10 10 12 11 1	-	<i></i>	0
** Special additives	funy	-	_		
% of water with slurry	NOKE	-			
heap =		100-11/0	-	land Halin	See a
CEMENT INTERVAL	-	150 -190	_ MINE	www will	war.
Cement Type (check):	Type I	Type II	Type I / II		
* Estimated No. of sacks/yards _/	1000				
Actual No. of sacks/yards/					
% Bentonite added					
Gallons water per sack /yard	1	-			
Grout Method (types)	arulpod	drellan	L drye	LAOR _	
Total Time on Site	4hrs.	This		M. 5	,5 M.
with the communities (golfarourly way inter-	,	OMMENTS	Suggest with the	.6/1	
Kock Variance grante	from 200 1	0150 - KO	CK interva	1 15/15 54	ploto 199
+5 yrs to 189	6/8/15 3.5	yars grock	added to	150: 6/6	7115
fump bake, no growt four	mped.	1171 17 19 19 19 19 19 19 19 19 19 19 19 19 19 			
Driller or Contractor/Signature _	1			Date 6	15/16
Observer Signature	1200 1	1		Date Date	PICTIC
Work was satisfactorily completed in acc	ordance with 40D-3.	F.A.C.? Yes No	Water sa	mples taken? Yes	No 1/
Compliance Tracking No.					
	//				
Production of the second of th	4/1	4		ing about the second	LIDIK
Authorized Signature	Surparadear and action	ated representative	`	Date9	(06/01)
(Not official unless signed by SWFWMD)	Supervisor or design	aleu representative	,	41.10-410	(00/01)

The following grouting techniques and procedures shall be adhered to. Failure to do so could jeopardize the approval of the well abandonment due to the grouting technique used.

- The field representative should measure the annulus to insure that the 20 ft. (for top grouting) or the total depth of the casing is exact. If a tremie is introduced, then the annulus should be checked by rotating the tremie pipe clockwise around the casing.
- The District representative must calculate a theoretical amount of cement needed prior to the beginning of the grouting operation.
- The cement and water shall be mixed at a ratio of 5.2 to 5.5. gallons of water to one 94 lb. bag of Portland cement. No other mix will be accepted unless approved by the Well Permitting Manager.
- Should the cement return to the surface with less than the acceptable amount, then the tremie pipe should be moved to clear the annulus.

The following table is the minimum acceptable amount of cement per ft. at 5.2 gallons of water per 94 lb. sack of cement (yields 8.82 gallons of slurry/sack) for neat cement slurry to be used in grouting wells. Table assumes no formation loss. Quantity actually used may be rounded up to the nearest 1/4 sack.

CEMENT ONLY (No Bentonite) TABLE ANNULUS / ONE FT. INTERVAL Hole Volume Hole Gallons/ Bags/ Casing Hole Hole Bags/ Diameter one ft. one ft. Diameter Diameter Volume one ft. 2" .16 .02 2" 4" .42 .05 3" .37 .04 2" 5" .79 .09 4" 2" .65 .07 6" 1.24 .14 5" .12 3" 1.02 5" .52 .06 6" 1.47 3" .17 6" .97 .11 8" 2.61 .30 4" 8" 1.79 .20 10" 4.08 .46 4" 10" 3.25 .37 12" 5.87 .67 5" 10" 2.85 .32 14" 8.00 .91 6" 10" .26 2.29 16" 10.44 1.18 8" 12" 2.84 .32 18" 13.22 1.50 10" 14" 3.28 .37 20" 16.32 1.85 10" 16" 5.73 .65 12" 16" 3.81 .43 12" 18" 6.59 .75 16" (O.D.) 20" 5.88 .67

BENTONITE ADDITIVE TO CEMENT TABLE ** Multiply for ** Multiply for * Gallons of Slurry Yield sacks of sacks of Percent water/sack gallons/sack **Bentonite** cement **Bentonite** of cement of cement required required 10 11.7 15.78 0.103 .56 8 10.4 14.36 0.092 .61 6 9.1 12.94 0.077 .68 4 7.8 11.59 0.057 .76 2 6.5 10.17 0.032 .87 0 5.2 8.82 0.000 1.00

DRY BENTONITE

One 50 lb. bag (granular/chips) is equivalent to approximately 5.5 gal. (±10%). In order to determine a theoretical estimate of number of bags required, determine total hole volume in gallons from the "Cement Only Table" and divide by 5.5 gal./bag to obtain the number of bags of dry (granular/chips) Bentonite.

EXAMPLE: 100 ft., 4 in		x .65 = 65. gal, 65÷5. T METHOD TYPES	.5 = 12 bags dry Bentonite.	
Grout Methods (please check one): (Explain other)	Tremie	Dump Bailer _	Other	10:1 J. O. (6:14)
e/c/J	HAN MIN	W. V.J.A. T. S. G04 o	The posterior and the control of	Black to the service

^{*} Gallons of water required per 94 lb. sack of cement when dry mixed with Bentonite.

^{**} Multiply the theoretical number of (Cement Only Table) sacks required by the corresponding decimal values for the sacks of cement and Bentonite mixture desired. A dispersant may be added if slurry becomes difficult to pump.

SOUTHWEST FLORIDA WATER MANAGEMENT DISTRICT WELL GROUTING/ABANDONMENT FORM

	WELL GROUTING/ABANDON	MENT FORM	04/57
GROU	UTING	ABANDONMENT	PAGEZ
Permit No. 843536 Drilli	ing Contractor	10:11 Line	9415
1/4 1/4 SEC. 5 TV	WP. 25 RGE. 22 Latitud	do 1830 1250 Longitu	1do 8 2 08 08 20
···	ap or Survey:	do Longito	
Property Owner or M	1	uali NAD 27 N	AD 63
Address of Well	1	De la Carta	
11 1	QWIP No.	WIID No.	
County Pasco	QWIF NO		
	WELL SPECIFICATIO		
	4 P 14		11/
T.D. of Well (to be verified by inspector) _ Casing: Doubleor Single;	160	Water Lev	vel
Casing: Doubleor Single; Material: (check) Black Steel, Galv.	Diameters;Depth	: Measured, Estimate	ed, Logged
Drill Method (check) Rotary, Calv.		Other	
Was well information verified from driller's			
Special Construction Stipulation? No			met? Yes No
Old Permit? No Yes Permit No.			
(For public supply) Approved Public Supp	ly Plan match location? Yes N	lo	
(For 62-524) Yes No Well loca	tion same as surveyed location? Ye	es No	
	GROUT SPECIFICATIONS AND		
Date	6/15/15, 6/16/	15	
BENTONITE INTERVAL	106'-68		
Type (check): chips, pellets/tablets	: Size: 3/4 🔀 , 1/2	, 3/8; Bentonite	Slurry
Estimated Bags of Bentonite	38		
Actual Bags of Bentonite	40		
** Special additives	of Alexander		
% of water with slurry	Viga-	La Partie	
- Contraction		7,000	
CEMENT INTERVAL	68 -	0	
Cement Type (check):	Type I Type II	Type I / II	
* Estimated No. of sacks/yards	7,750 i	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
Actual No. of sacks/yards	43		
% Bentonite added			
Gallons water per sack /yard			
	diam'		
Grout Method (types)	3hrs. / h.		
Total Time on Site	Jus. Ih		
ayes to easily the growth care than	COMMENTS		
Witnessel grant re	turn to the surga	u	100
1800 NO. 1	U		
	0.		
Driller or Contractor Signature	5/	(SUC) - C	Date 6/15/15
Observer Signature	Person 11		Date 10/16/15
Work was satisfactorily completed in acco	ordance with 40D-3, F.A.C.? Yes		41131
Compliance Tracking No.	———		
, A. (2/L/11/15 C	They has	12 2 1 2 2 1 1 1 0 1 1 0 1 1 1 2 1 1 1 1	WINK
Authorized Signature	Supportion or designated assessment		Date
(Not official unless signed by SWFWMD 5	supervisor or designated representa	2 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	11.10-410(06/01)

The following grouting techniques and procedures shall be adhered to. Failure to do so could jeopardize the approval of the well abandonment due to the grouting technique used.

- The field representative should measure the annulus to insure that the 20 ft. (for top grouting) or the total depth of the casing
 is exact. If a tremie is introduced, then the annulus should be checked by rotating the tremie pipe clockwise around the
 casing.
- The District representative must calculate a theoretical amount of cement needed prior to the beginning of the grouting operation.
- The cement and water shall be mixed at a ratio of 5.2 to 5.5. gallons of water to one 94 lb. bag of Portland cement. No other mix will be accepted unless approved by the Well Permitting Manager.
- Should the cement return to the surface with less than the acceptable amount, then the tremie pipe should be moved to clear the annulus.

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BENTONITE ADDITIVE TO CEMENT TABLE

	* 0 - 11 4	01	** Multiply for	** Multiply for
_	* Gallons of	Slurry Yield	sacks of	sacks of
Percent	water/sack	gallons/sack	Bentonite	cement
Bentonite	of cement	of cement	required	required
10	11.7	15.78	0.103	.56
8	10.4	14.36	0.092	.61
6	9.1	12.94	0.077	.68
4	7.8	11.59	0.057	.76
2	6.5	10.17	0.032	.87
0	5.2	8.82	0.000	1.00

^{*} Gallons of water required per 94 lb. sack of cement when dry mixed with Bentonite.

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EXAMPLE:	100 ft., 4 inch		x .65 = 65. gal, 65÷5. Г МЕТНОD TYPES	.5 = 12 bags dry Bento	nite.	
Grout Methods (please (Explain other)	check one):	Tremie	Dump Bailer _	Other	e spreading	0 0.00
30.47	forte assurer e.	W				- 1.0
a marine de la companya de la compa				1		

^{**} Multiply the theoretical number of (Cement Only Table) sacks required by the corresponding decimal values for the sacks of cement and Bentonite mixture desired. A dispersant may be added if slurry becomes difficult to pump.

SOUTHWEST FLORIDA WATER MANAGEMENT DISTRICT

2379 BROAD STREET, BROOKSVILLE, FL 34604-6899

PHONE: (352) 796-7211 or (800) 423-1476

WWW.SWFWMD.STATE.FL.US

ST. JOHNS RIVER WATER MANAGEMENT DISTRICT

4049 REID STREET, PALATKA, FL 32178-1429

PHONE: (386) 329-4500 WWW.SJRWMD.COM

NORTHWEST FLORIDA WATER MANAGEMENT DISTRICT

152 WATER MANAGEMENT DR., HAVANA, FL 32333-4712

(U.S. Highway 90, 10 miles west of Tallahassee)

PHONE: (850) 539-5999

WWW.NWFWMD.STATE.FL.US

SOUTH FLORIDA WATER MANAGEMENT DISTRICT

P.O. BOX 24680 3301 GUN CLUB ROAD WEST PALM BEACH, FL 33416-4680 PHONE: (561) 686-8800 WWW.SFWMD.GOV

SUWANNEE RIVER WATER MANAGEMENT DISTRICT

9225 CR 49

LIVE OAK, FL 32060

PHONE: (386) 362-1001 or (800) 226-1066 (Florida only)

WWW.MYSUWANNEERIVER.COM

From	ft.	To	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	To	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	To	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	To	ft.	Color	Grain Size (F, M, C)	
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	
From	ft.	То	ft.	Color	Grain Size (F, M, C)	
From	ft.	То	ft.	Color	Grain Size (F, M, C)	
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	To	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	To	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
rom	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material
From	ft.	То	ft.	Color	Grain Size (F, M, C)	Material

Comments:

Finish: PLUGGED

*Detailed Site Map of Well Location

Z

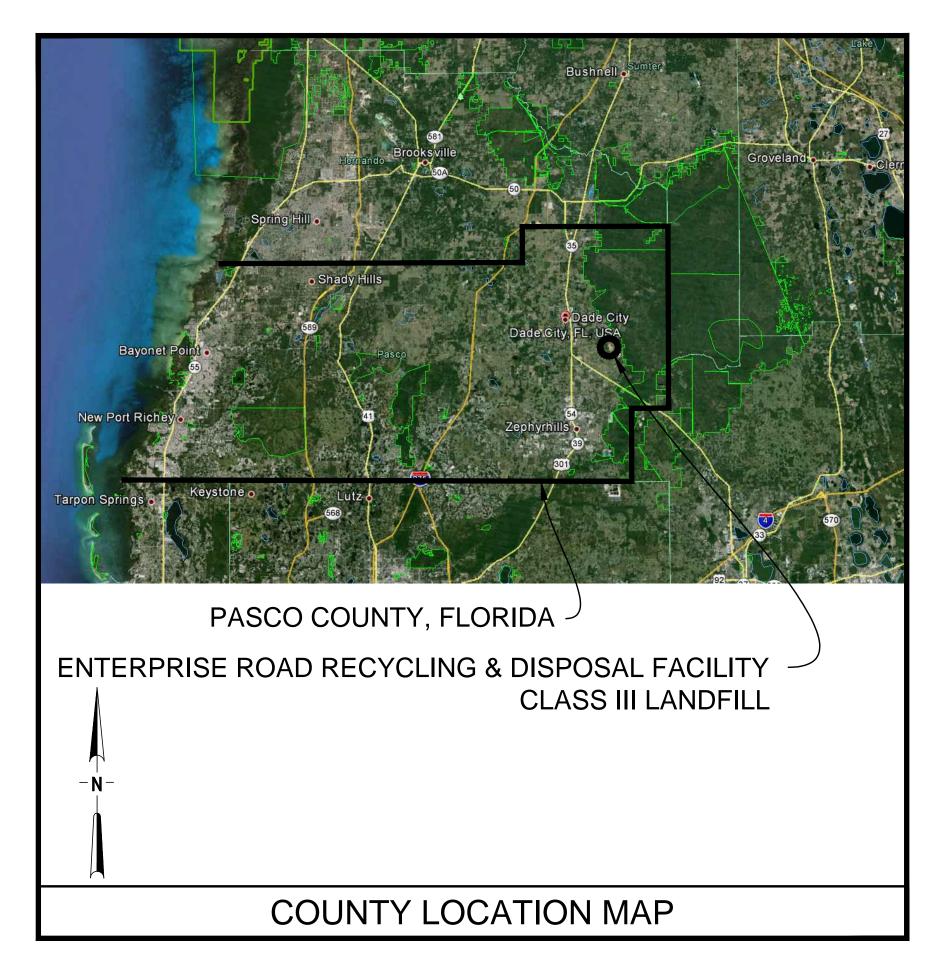
Give distances from all reference points or structures, septic systems, sanitary hazards, and contamination sources within 500 ft. of well.

SECTION 4 2016 PLAN SET

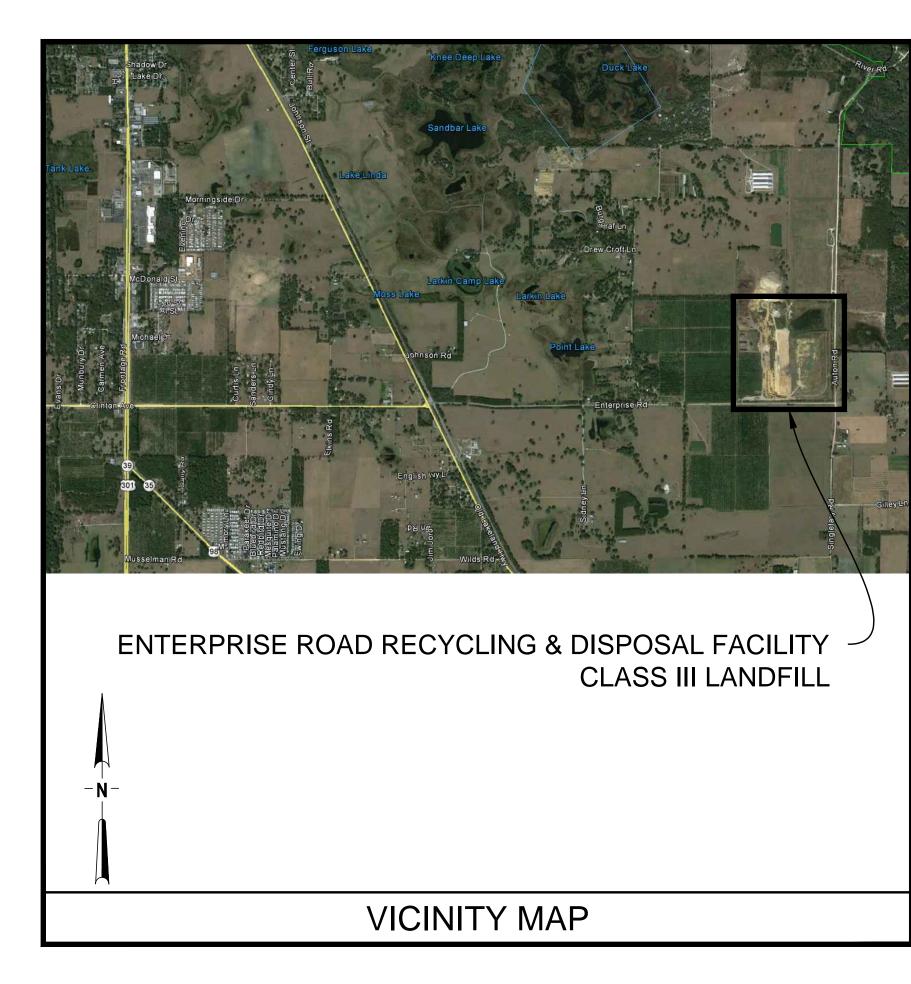
ENTERPRISE ROAD CLASS III LANDFILL RECYCLING & DISPOSAL FACILITY LANDFILL PERMIT MODIFICATION

LOCATED: DADE CITY, PASCO COUNTY, FLORIDA

SUBMITTED TO: FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION



Sheet Number	Sheet Title
C0.00	COVER SHEET
C0.01	GENERAL NOTES AND ABBREVIATIONS
C0.02	AERIAL SITE PLAN
C0.03	SITE PLAN
C0.04	CELL FLOOR GRADING PLAN
C1.00	PHASING PLAN SEQUENCE NO. 1
C1.01	PHASING PLAN SEQUENCE NO. 1 SECTIONS
C1.10	PHASING PLAN SEQUENCE NO. 2
C1.11	PHASING PLAN SEQUENCE NO. 2 SECTIONS
C2.00	PHASING PLAN SEQUENCE NO. 3 CONCEPTUAL CLOSURE
C2.10	PHASING PLAN SEQUENCE NO. 3 CONCEPTUAL CLOSURE SECTIONS
C3.00	CLOSURE DETAILS
SHEET 1	TOPOGRAPHIC SURVEY (BY PICKETT SURVEYING & PHOTOGRAMMETRY)
SHEET 2	TOPOGRAPHIC SURVEY (BY PICKETT SURVEYING & PHOTOGRAMMETRY)



NO.	DATE	REVISION DESCRIPTION	BY
1	7/31/16	FDEP R.A.I. NO. 1 RESPONSE	LJB
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4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

PERMIT PLANS
ENTERPRISE ROAD CLASS III
RECYCLING & DISPOSAL FACILITY
2016 PERMIT MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

PROJECT TITLE:

LISA J. BAKER

DESIGNED BY

LJB

DRAWN BY

MAF

CHECKED BY

JDL

FL PE NO. 74652

APPROVED BY

LJB

COVER SHEET

SHEET TITLE:

PROJECT NO.:
02000-144-14

SCALE:
AS SHOWN

DATE:
MARCH 2016

C0.00

- 3. CONTRACTOR SHALL CERTIFY IN WRITING TO THE ENGINEER OF RECORD THE ACCURACY OF ALL SURVEY AND OTHER GRADING DATA PRIOR TO BEGINNING WORK.
- 4. LOCATIONS, ELEVATIONS, AND DIMENSIONS OF EXISTING UTILITIES, STRUCTURES, AND OTHER FEATURES ARE SHOWN TO THE BEST INFORMATION AVAILABLE AT THE TIME OF PREPARATION OF THESE PLANS BUT DO NOT PURPORT TO BE ABSOLUTELY CORRECT. THERE MAY BE OTHER IMPROVEMENTS, UTILITIES, ETC. WHICH ARE WITHIN THE PROJECT AREA. THE CONTRACTOR SHALL VERIFY, PRIOR TO CONSTRUCTION, THE LOCATIONS, ELEVATIONS, AND DIMENSIONS OF ALL EXISTING UTILITIES, STRUCTURES, AND OTHER FEATURES (WHETHER OR NOT SHOWN ON THE PLANS) AFFECTING THE WORK.
- 5. CONTRACTOR SHALL TAKE WHATEVER MEANS NECESSARY TO PROTECT EXISTING PIPING, MONITORING WELLS/PIEZOMETERS FROM DAMAGE DURING CONSTRUCTION. CONTRACTOR SHALL REPAIR OR REPLACE PIPING, MONITORING WELLS/PIEZOMETERS DAMAGED DURING CONSTRUCTION WITH EQUIVALENT MATERIALS AND CONSTRUCTION METHODS AS APPROVED BY FACILITY OWNER AT NO ADDITIONAL COST TO THE OWNER.
- FIELD CONDITIONS MAY NECESSITATE SLIGHT ALIGNMENT AND GRADE DEVIATION OF THE PROPOSED CONSTRUCTION TO AVOID OBSTACLES, AS ORDERED BY THE ENGINEER AT NO ADDITIONAL COST TO THE OWNER.
- 7. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH EXISTING PASCO COUNTY DESIGN AND CONSTRUCTION STANDARDS UNLESS THOSE STANDARDS CONFLICT WITH THESE CONTRACT DOCUMENTS IN WHICH CASE THESE CONTRACT DOCUMENTS SHALL GOVERN. SUCH CONFLICTS SHALL BE BROUGHT TO THE PROFESSIONAL'S ATTENTION IMMEDIATELY.
- 8. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH PREVAILING FEDERAL, STATE, LOCAL AND OTHER APPLICABLE REGULATIONS.
- 9. CONSTRUCTION MONUMENTS FOR VERTICAL AND HORIZONTAL CONTROL HAVE BEEN PROVIDED AT THE PROJECT SITE.
- 10. PRIOR TO BEGINNING EARTHWORK, THE CONTRACTOR SHALL PROVIDE STORMWATER AND EROSION CONTROL PLANS TO PREVENT PONDING AND CONTROL EROSION AND RUNOFF. NO PONDING OF WATER SHALL BE ALLOWED. THE CONTRACTOR SHALL USE WHATEVER MEANS NECESSARY TO PREVENT EROSION AND SHALL BE RESPONSIBLE FOR ALL WORK, INCLUDING PROVIDING EQUIPMENT, LABOR, FILL, ETC NECESSARY TO REMEDIATE AND/OR RESTORE ALL AREAS IMPACTED BY EROSION.
- 11. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO BECOME FAMILIAR WITH THE OSHA EXCAVATION SAFETY STANDARDS AND TO ABIDE BY THEM.
- 12. THE CONTRACTOR SHALL PROVIDE ALL WARNING SIGNALS, SIGNS, LIGHTS, AND FLAG PERSON AS REQUIRED BY DOT IN THE "MANUAL ON TRAFFIC CONTROL & SAFE PRACTICES."
- 13. ALL PIPING SHALL HAVE MINIMUM COVER OF 24" UNLESS OTHERWISE NOTED.
- 14. WHERE IT IS NECESSARY TO DEFLECT PIPE EITHER HORIZONTALLY OR VERTICALLY, PIPE DEFLECTION SHALL NOT EXCEED 75% OF THE MANUFACTURER'S RECOMMENDED DEFLECTION ANGLE. MINIMUM PIPE RADIUS SHALL BE A MINIMUM OF 25% GREATER THAN THE MANUFACTURER'S RECOMMENDED MINIMUM RADIUS.
- 15. CONTAMINATED STORMWATER, DEWATERING DISCHARGE, LEACHATE, CONTAMINATED SOILS, OR EXCAVATED WASTE SHALL BE CONTAINED AND DISPOSED OF IN ACCORDANCE WITH THE LANDFILL OPERATIONS.
- 16. CONTRACTOR SHALL VERIFY ALL CLEARANCES PRIOR TO CONSTRUCTION.
- 17. THE CONTRACTOR SHALL MAINTAIN A CLEAR PATH FOR ALL SURFACE WATER DRAINAGE STRUCTURES AND DITCHES DURING ALL PHASES OF CONSTRUCTION AND SHALL UTILIZE WHATEVER MEANS NECESSARY TO MANAGE STORMWATER SUCH THAT IMPACT TO CONSTRUCTION IS MINIMIZED. CONTRACTOR SHALL BE RESPONSIBLE FOR REPAIR OF DAMAGE DUE TO STORMWATER.
- 18. NO DISTURBANCE SHALL BE ALLOWED OUTSIDE OF THE AREAS SHOWN ON THE FINAL GRADING PLAN UNLESS APPROVED BY THE ENGINEER, OR SPECIFICALLY NOTED ON THE PLANS.
- THE CONTRACTOR SHALL PROVIDE AND MAINTAIN ENVIRONMENTAL PROTECTION DURING THE LIFE OF THE CONTRACT. THE CONTRACTOR'S OPERATIONS SHALL COMPLY WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS PERTAINING TO WATER, AIR, SOLID WASTE, HAZARDOUS WASTE MATERIALS, OILY SUBSTANCES, AND NOISE POLLUTION. THE CONTRACTOR SHALL IMPLEMENT EROSION AND SEDIMENTATION CONTROL MEASURES AS NECESSARY TO COMPLY WITH THESE REGULATIONS FOR BOTH TEMPORARY AND PERMANENT CONSTRUCTION.
- 23. THE CONTRACTOR SHALL COMPLY WITH ALL TERMS, CONDITIONS, AND REQUIREMENTS OF ALL APPLICABLE PERMITS, INCLUDING FDEP PERMITS FOR THE SITE.
- 24. THE CONTRACTOR SHALL REPLACE ALL EXISTING PAVING, LANDFILL COVER MATERIAL, ACCESS ROADS, PIPES, STABILIZED EARTH, FENCES, SIGNS AND OTHER IMPROVEMENTS WITH THE SAME TYPE OF MATERIAL THAT WAS REMOVED OR DAMAGED DURING CONSTRUCTION, AS A RESULT OF CONSTRUCTION, OR AS DIRECTED BY THE ENGINEER WITHOUT INCREASE IN THE CONTRACT PRICE OR TIME.
- 25. THE CONTRACTOR SHALL BE AWARE THAT THERE MAY BE SOME UTILITY CONFLICTS. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO LOCATE AND PROTECT ANY AND ALL EXISTING UTILITIES ON THIS PROJECT WITHOUT INCREASE IN THE CONTRACT PRICE OR TIME.
- 26. THE CONTRACTOR SHALL NOTIFY THE ENGINEER IMMEDIATELY WHEN CONFLICTS BETWEEN DRAWINGS AND ACTUAL CONDITIONS ARE DISCOVERED.
- 27. THE CONTRACTOR SHALL COMPLY WITH ALL TERMS, CONDITIONS, AND REQUIREMENTS OF ALL APPLICABLE PERMITS, INCLUDING FDEP AND WATER MANAGEMENT DISTRICT PERMITS FOR THE SITE.

GRADING NOTES

- 1. ALL AREAS WITHIN AND AROUND THE LIMITS OF CONSTRUCTION SHALL BE MAINTAINED AS NEEDED TO CONTROL EROSION DURING THE LENGTH OF THE PROJECT.
- 2. FILL ELEVATIONS SHALL BE SUCH THAT INTERMEDIATE AND FINAL COVER DESIGN ELEVATIONS SHALL BE ACHIEVED ON ALL SLOPES.

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4140 NW 37th Place, Suite A
Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

PROJECT TITLE:

PERMIT PLANS

ENTERPRISE ROAD CLASS III

RECYCLING & DISPOSAL FACILITY

2016 PERMIT MODIFICATION

DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER

DESIGNED BY

LJB

DRAWN BY

MAF

CHECKED BY

JDL

FL PE NO. 74652

APPROVED BY

LJB

GENERAL NOTES AND ABBREVIATIONS

SHEET TITLE:

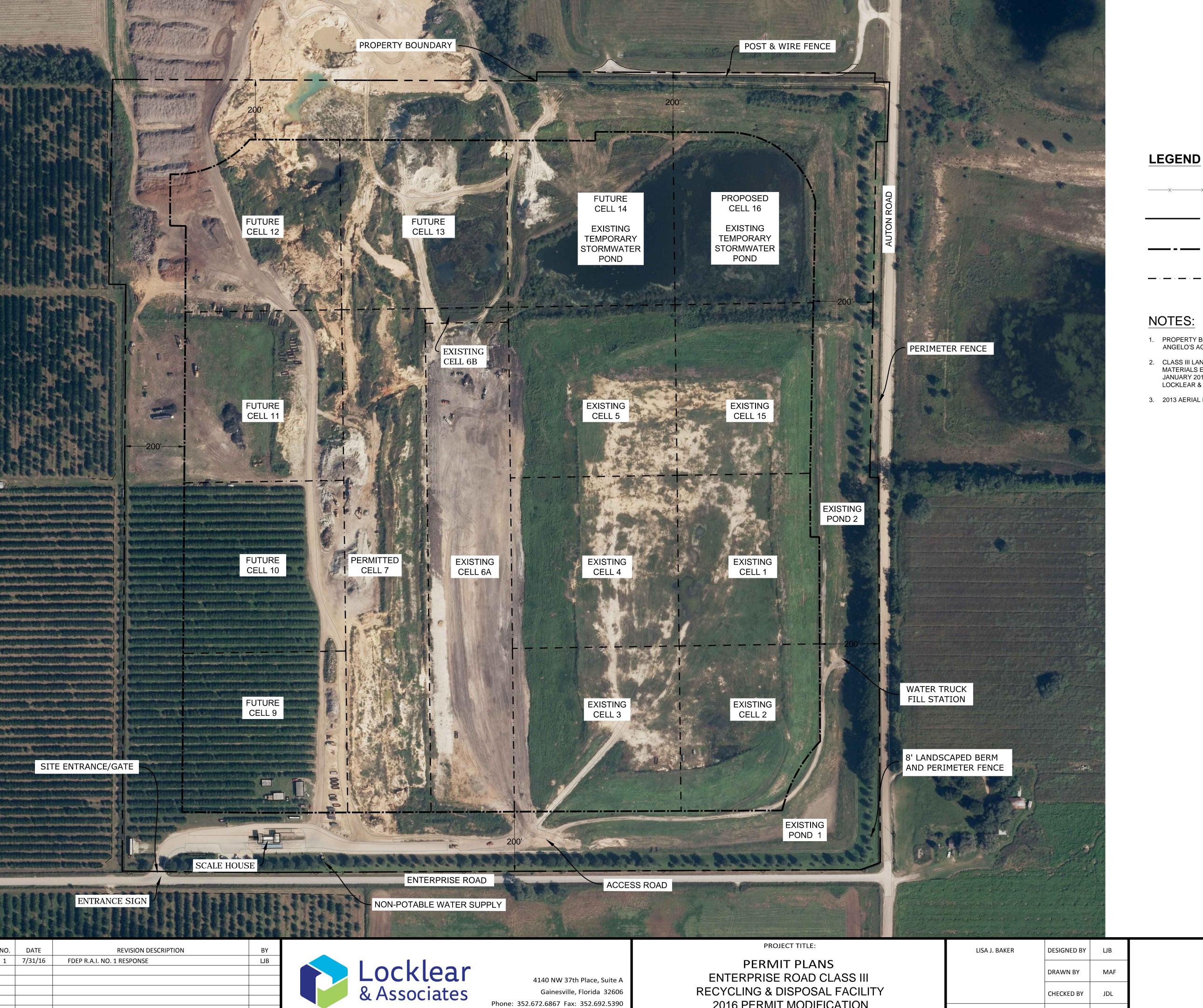
PROJECT NO.:
02000-144-14

SCALE:
AS SHOWN

DATE:
MARCH 2016

C0.01

REVIEW ONLY-NOT FOR CONSTRUCTION



Phone: 352.672.6867 Fax: 352.692.5390

Certificate of Authorization No. 30066

2016 PERMIT MODIFICATION

DADE CITY, PASCO COUNTY, FLORIDA



GRAPHIC SCALE

PERIMETER FENCE PROPERTY BOUNDARY

LANDFILL FOOTPRINT (AT BUILD OUT)

LANDFILL CELLS

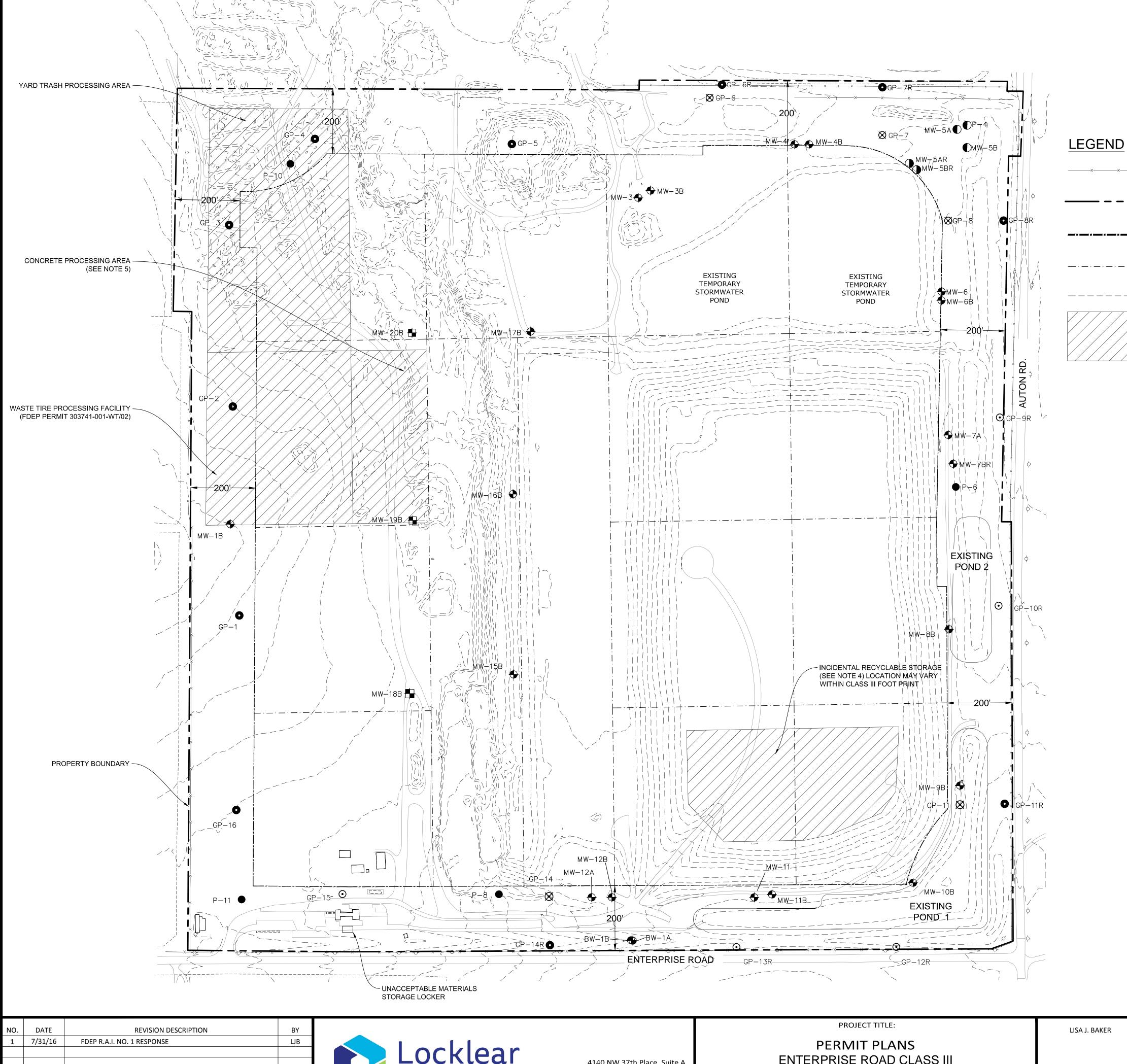
NOTES:

APPROVED BY

FL PE NO. 74652

- 1. PROPERTY BOUNDARY SURVEY CONDUCTED BY SIMMONS & BEALL, INC. 3-30-2001, PROVIDED BY ANGELO'S AGGREGATE MATERIALS.
- CLASS III LANDFILL PERMITTED AND FUTURE CELL LAYOUT PER NOVEMBER 2006 ANGELO'S RECYCLED MATERIALS ENTERPRISE RECYCLING & DISPOSAL FACILITY (AS AMENDED FEBRUARY 2008 AND JANUARY 2010 BY JONES EDMUNDS, AS AMENDED MARCH 2013 BY KELNER ENGINEERING AND 2015 BY LOCKLEAR & ASSOCIATES).
- 3. 2013 AERIAL PHOTOGRAPHY PER FLORIDA DEPARTMENT OF TRANSPORTATION WEBSITE.

PROJECT NO.: 02000-144-14 SHEET TITLE: **AS SHOWN AERIAL SITE PLAN** MARCH 2016 DRAWING: C0.02





LEGEND

- → MW−4B MONITORING WELL LOCATION
- MW-5BR MONITORING WELL TO BE INSTALLED
- GP-1 GAS PROBE LOCATION
- GAS PROBE TO BE ABANDONED
- GP−8R FUTURE GAS PROBE LOCATION
- ₩−18B FUTURE MONITOR WELL LOCATION*

PIEZOMETER WELL LOCATION

NOTES:

1. PROPERTY BOUNDARY SURVEY CONDUCTED BY SIMMONS & BEALL, INC. 3-30-2001, PROVIDED BY ANGELO'S AGGREGATE MATERIALS.

PERIMETER FENCE

LANDFILL CELLS

EXISTING CONTOURS

PROPERTY BOUNDARY

LANDFILL FOOTPRINT (AT BUILD OUT)

SPECIAL WASTE MANAGEMENT AREA

- 2. CLASS III LANDFILL PERMITTED AND FUTURE CELL LAYOUT PER NOVEMBER 2006 ANGELO'S RECYCLED MATERIALS ENTERPRISE RECYCLING & DISPOSAL FACILITY (AS AMENDED FEBRUARY 2008 AND JANUARY 2010 BY JONES EDMUNDS AND AMENDED MARCH 2013 BY KELNER ENGINEERING).
- 3. TOPOGRAPHIC SURVEY BY PICKETT SURVEYING & PHOTOGRAMMETRY, DATED 11/11/13, UPDATED ON 12/31/13.
- 4. TEMPORARY STORAGE OF UNACCEPTABLE MATERIALS AND INCIDENTAL RECYCLABLES WITHIN THE LANDFILL FOOTPRINT AND NEAR WORKING FACE MAY BE PROVIDED AS FOLLOWS:

TYPE	MAX. QTY	STORAGE
INCII	ABLES	
FERROUS METAL	500 CY	ROLL-OFF OR PILE
ALUMINUM	300 CY	ROLL-OFF OR PILE
STAINLESS STEEL	300 CY	ROLL-OFF OR PILE
COPPER	25 CY	TRASH PAIL, ROLL-OFF OR PILE
ASPHALT	300 CY	ROLL-OFF OR PILE
CONCRETE / RUBBLE	300 CY	ROLL-OFF OR PILE
ELECTRONICS	8 CY	COVERED DUMPSTER
	UNACCEPTABLE MATERIALS	
PAINT, BATTERIES, SOLVENTS, ELECTRONICS, OILS, ETC.	40 CY	ROLL-OFF OR PILE AT WORKING FACE, REMOVED DAILY TO STORAGE LOCKER
CLASS I WASTE	20 CY	COVERED DUMPSTERS

5. CONCRETE PROCESSING AREA WILL BE RELOCATED WHEN EXCAVATION OPERATIONS MOVE TO THIS AREA.

NO.	DATE	REVISION DESCRIPTION	BY
1	7/31/16	FDEP R.A.I. NO. 1 RESPONSE	LJB



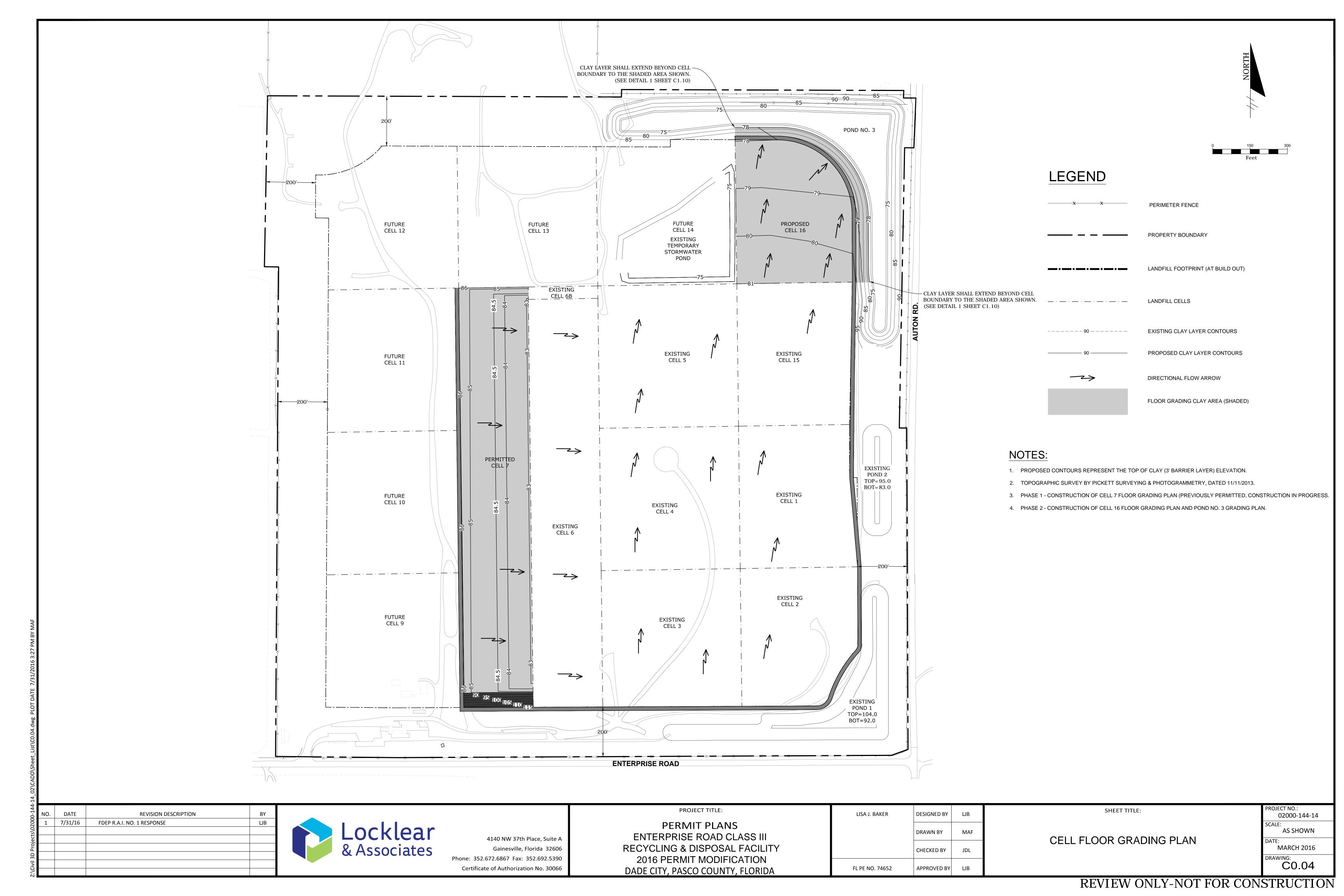
4140 NW 37th Place, Suite A Gainesville, Florida 32606 Phone: 352.672.6867 Fax: 352.692.5390 Certificate of Authorization No. 30066

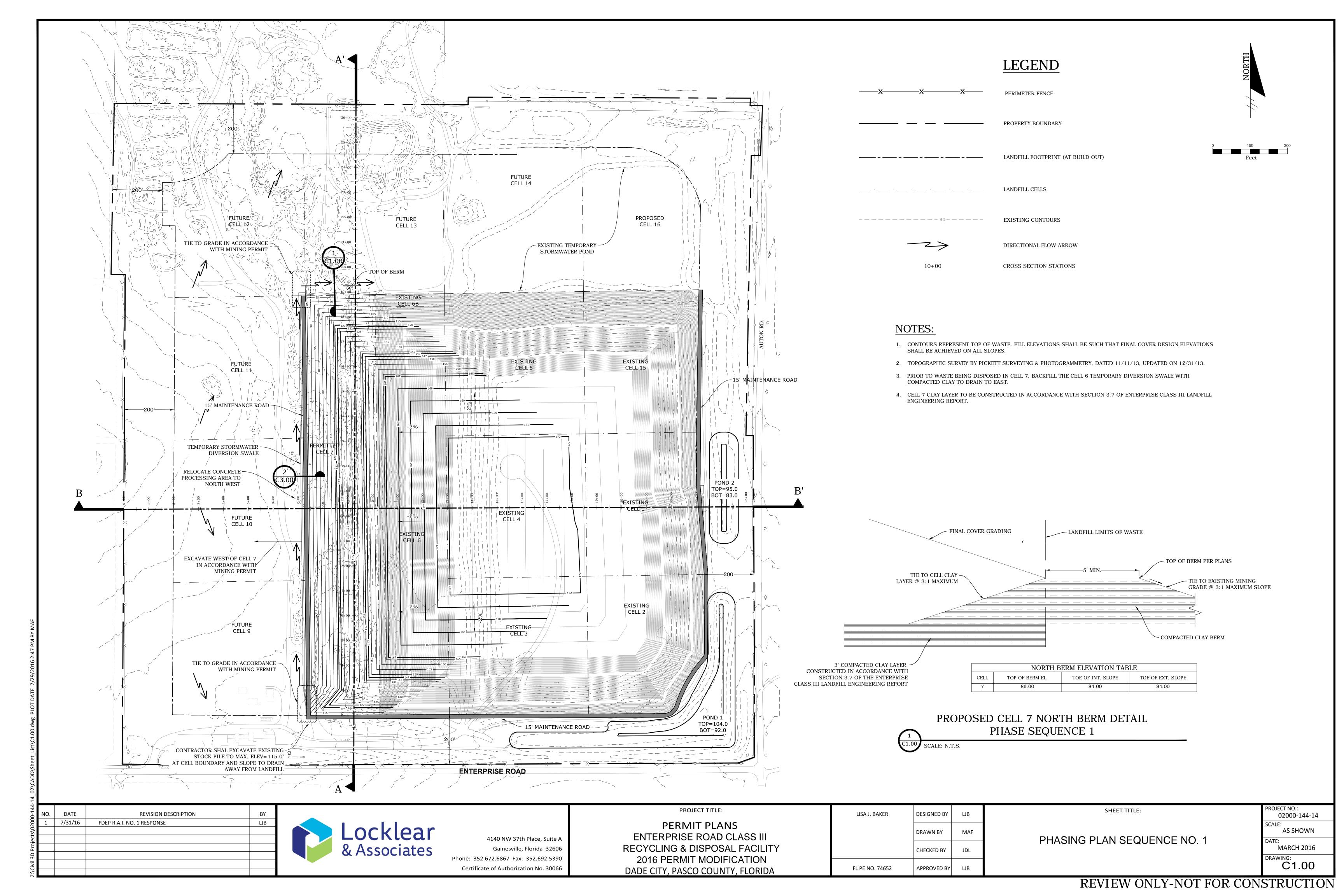
ENTERPRISE ROAD CLASS III RECYCLING & DISPOSAL FACILITY 2016 PERMIT MODIFICATION DADE CITY, PASCO COUNTY, FLORIDA

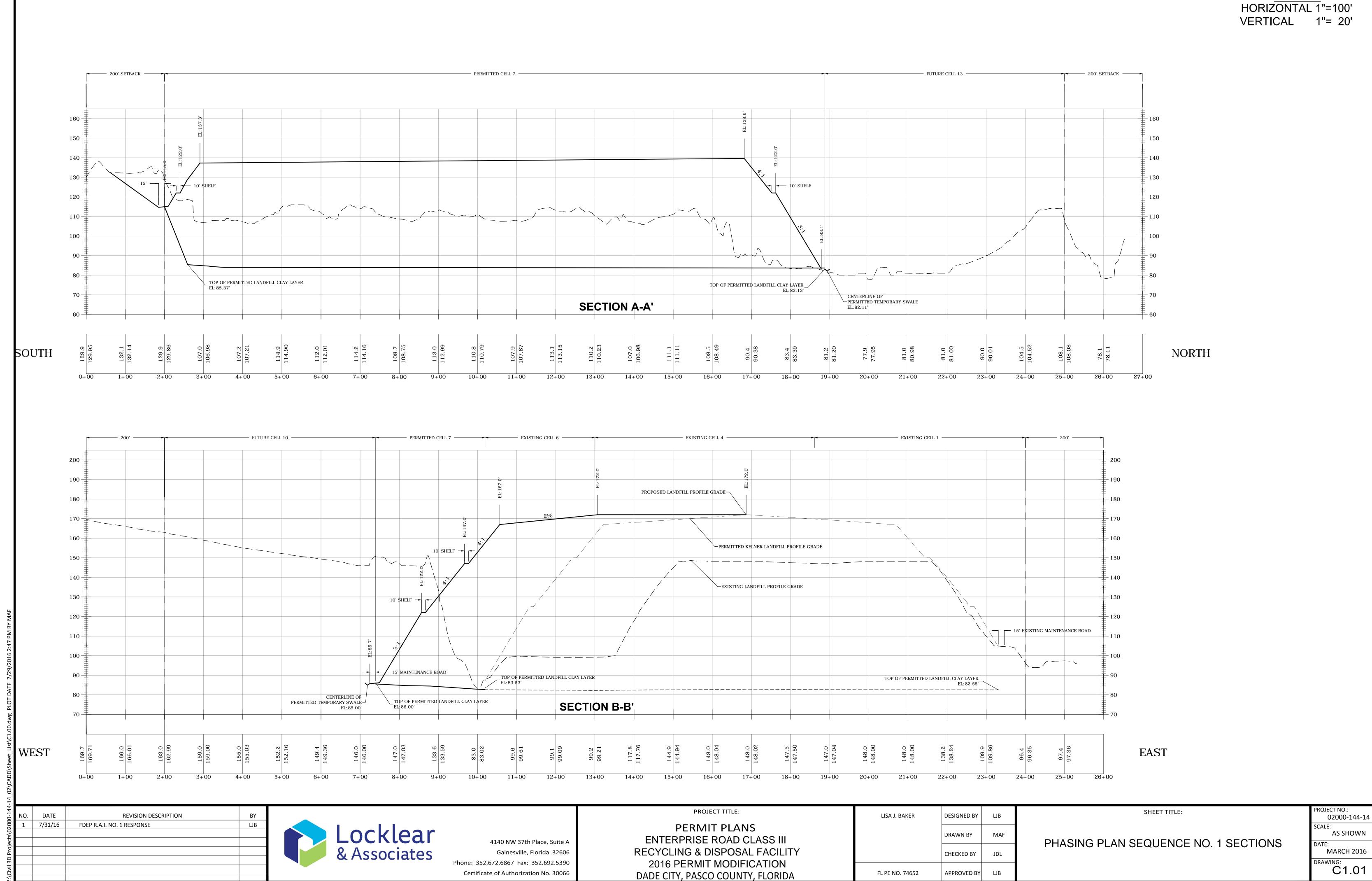
LISA J. BAKER DESIGNED BY DRAWN BY CHECKED BY JDL APPROVED BY FL PE NO. 74652

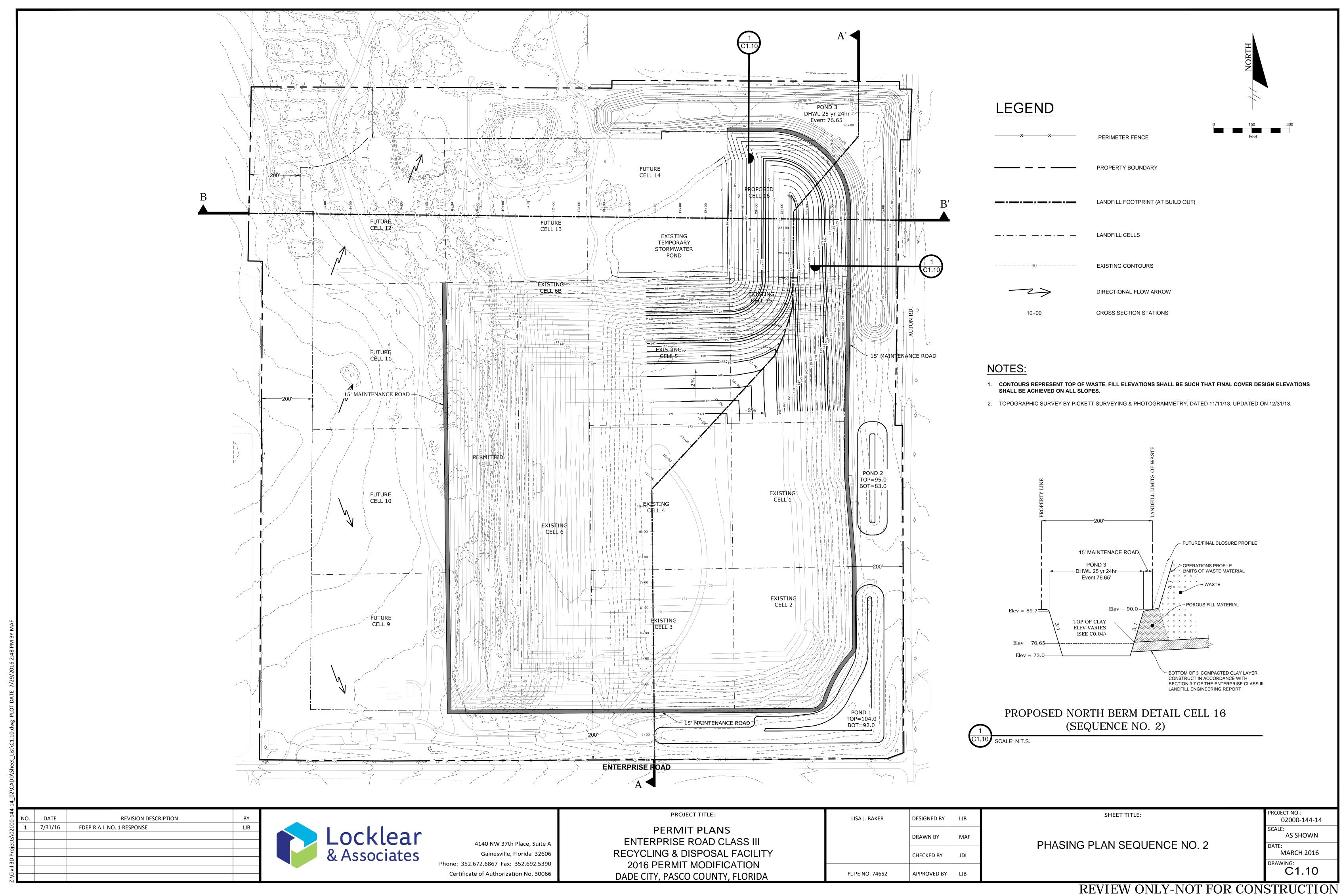
SHEET TITLE: 02000-144-14 **AS SHOWN** SITE PLAN MARCH 2016

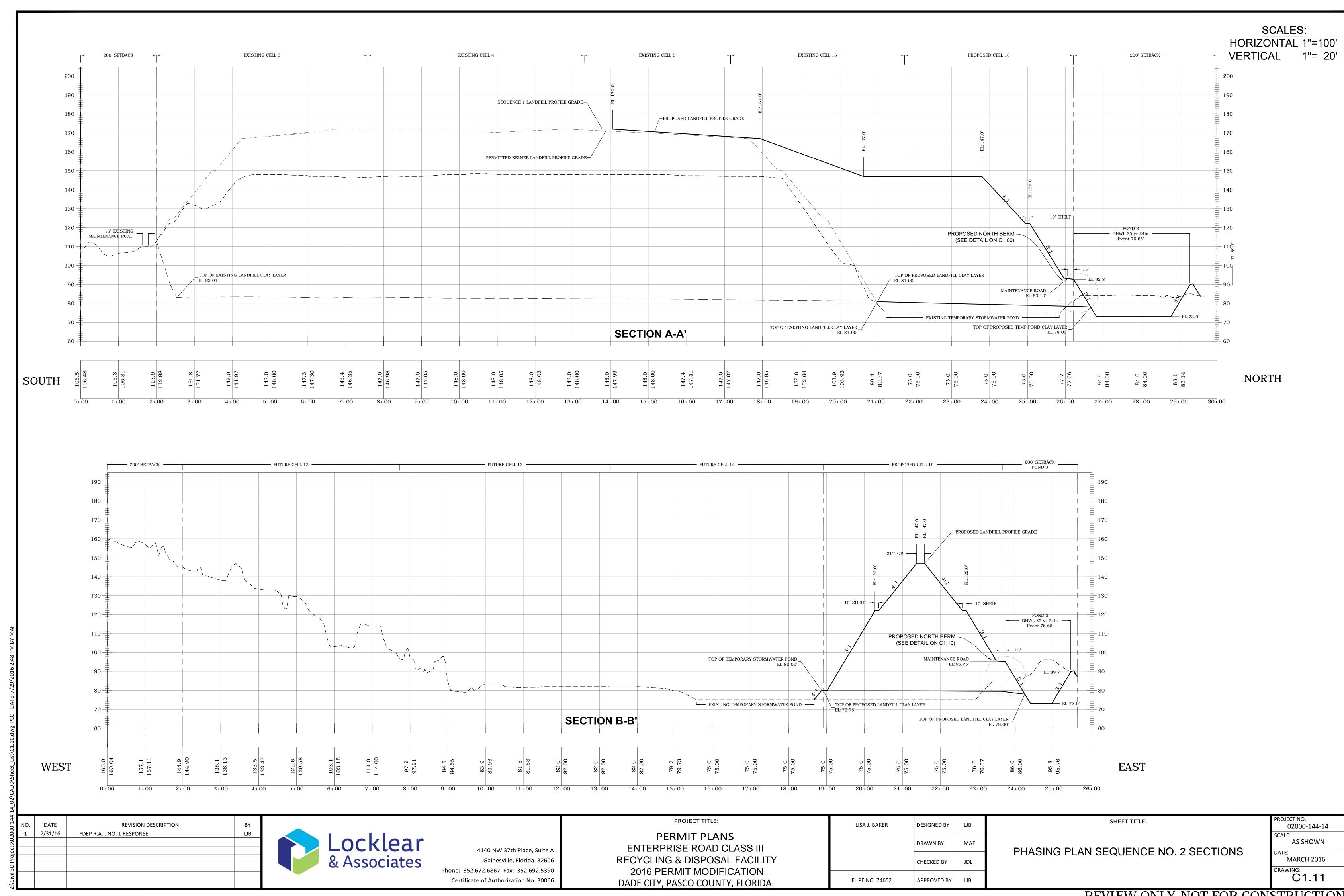
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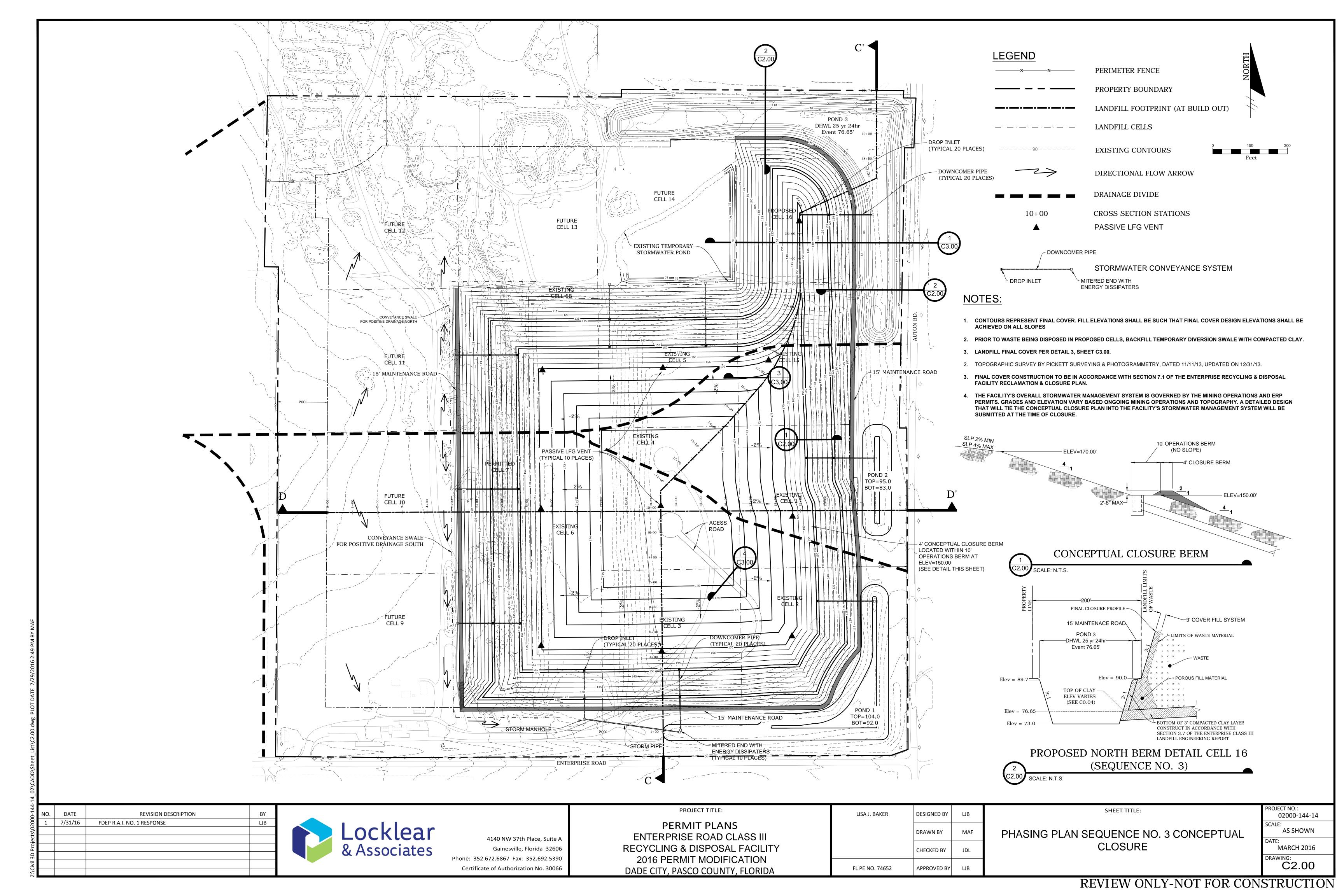


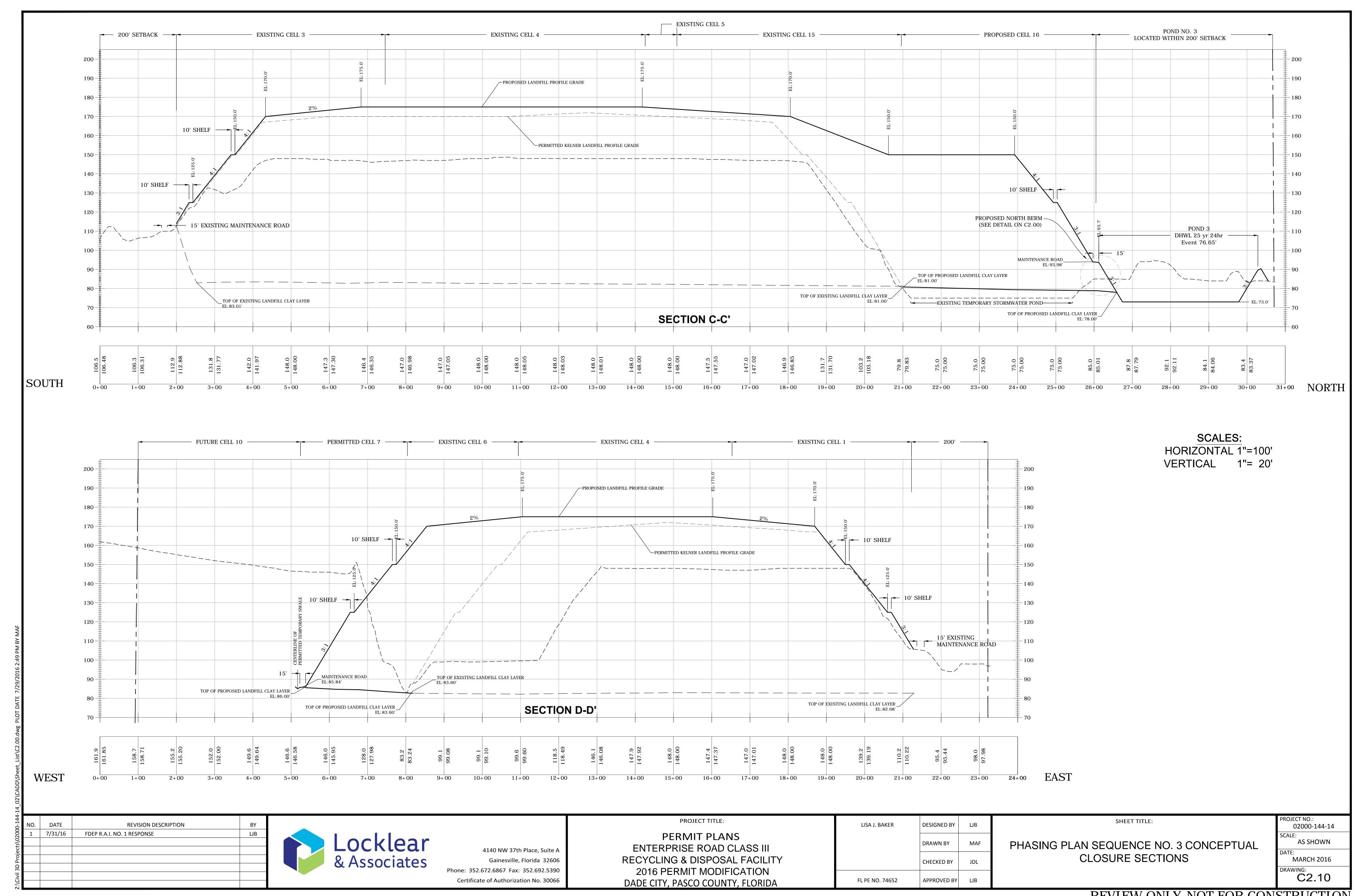


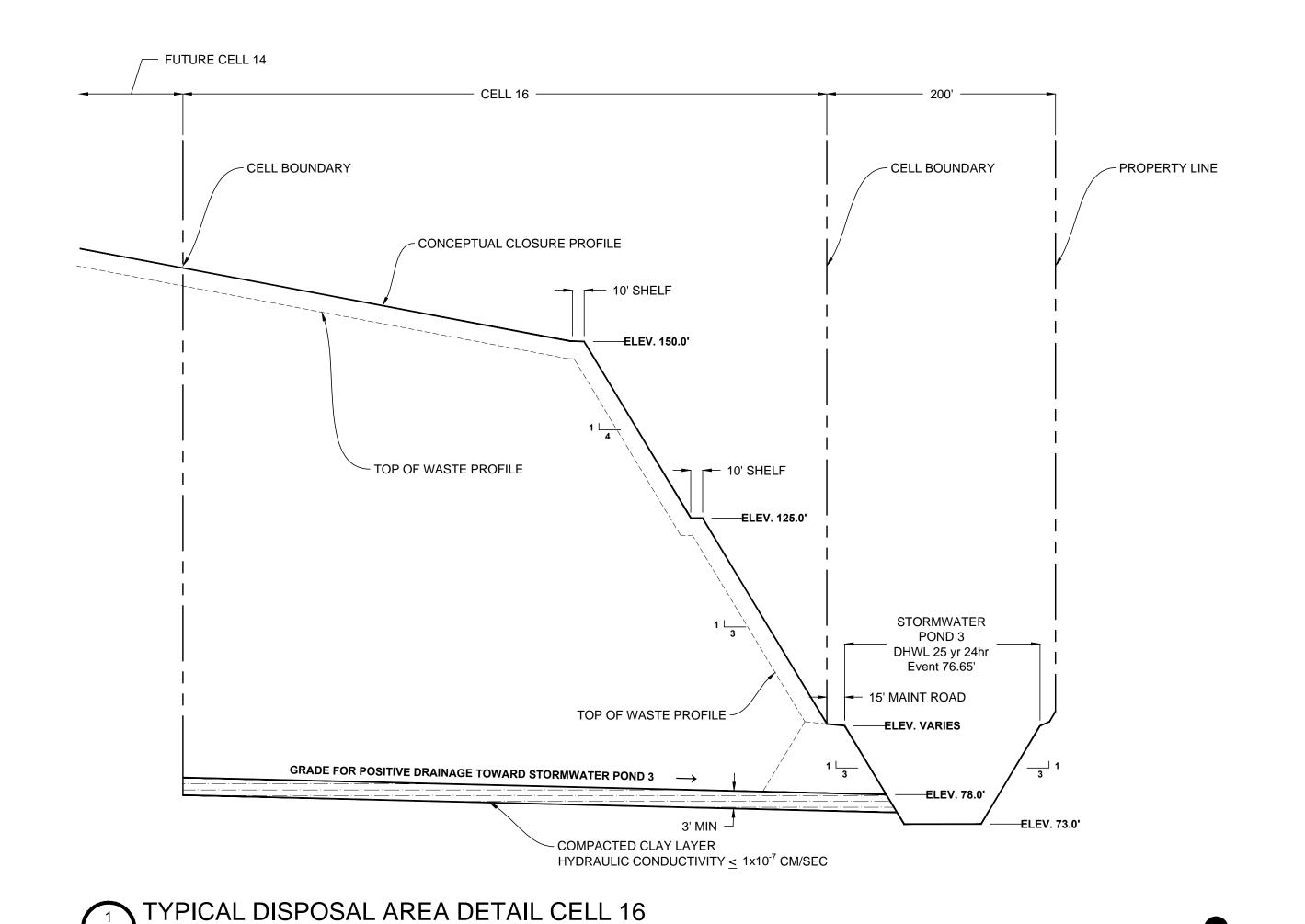












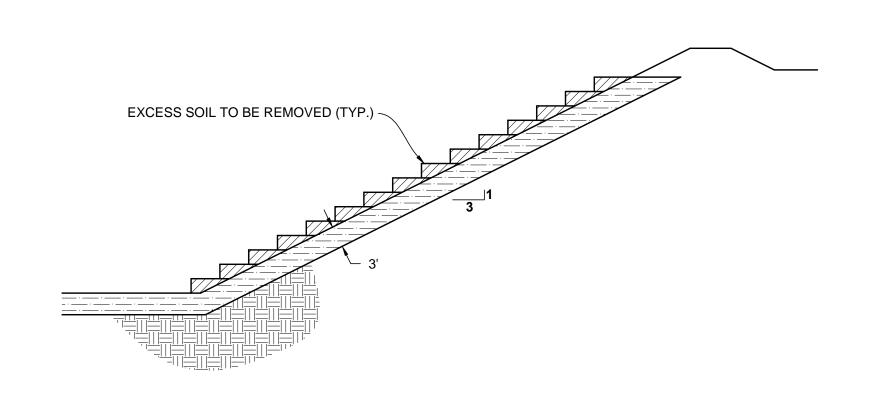
2' (TYP.)

2' (TYP.)

COMPACTED CLAY LAYER

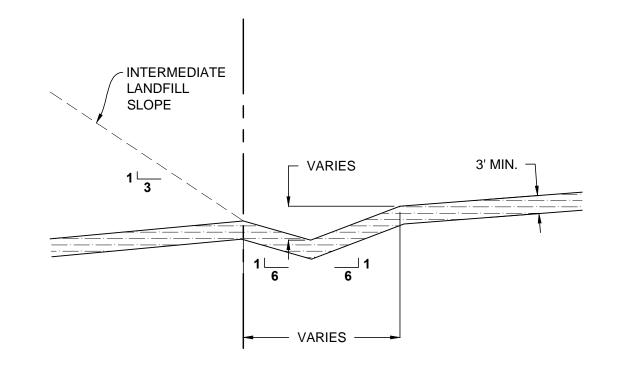
HYDRAULIC CONDUCTIVITY ≤ 1x10⁻⁷ CM/SEC

6 CELL 7 SOUTH CLAY SIDE SLOPE CONSTRUCTION DETAIL
C3.00 SCALE: N.T.S.



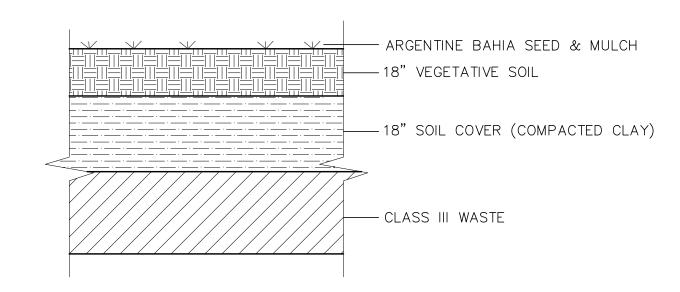
CELL 7 SOUTH CLAY SIDE SLOPE CONSTRUCTION DETAIL

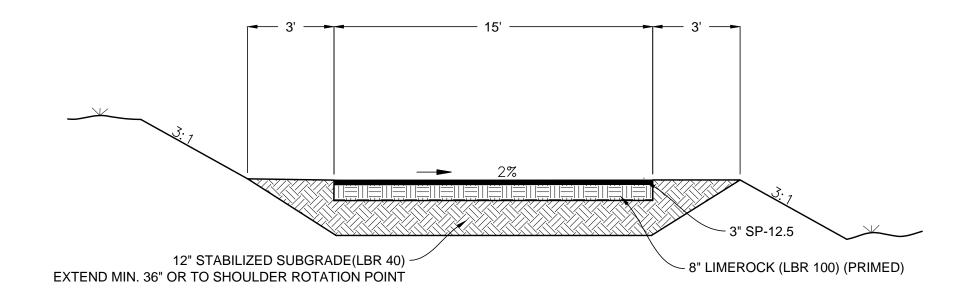
SCALE: N.T.S.



NOTES:

- 1. FOR CELL 7 THE TEMPORARY DIVERSION SWALE IS CONSTRUCTED PRIOR TO WASTE ACCEPTANCE WITHIN CELL.
- 2. PRIOR TO WASTE BEING DISPOSED OF ON THE PREVIOUS INTERMEDIATE SLOPE THE TEMPORARY SWALE IS BACKFILLED AND COMPACTED WITH CLAY TO PROVIDE A CONTINUOUS CLAY BARRIER LAYER THAT DRAINS TO THE STORMWATER POND 3.
- 3. CLAY BARRIER LAYER TO BE CONSTRUCTED IN ACCORDANCE WITH SECTION 3.7 OF THE ENTERPRISE CLASS III LANDFILL ENGINEERING REPORT.
- 4. STEP BACK AND SCARIFY EXISTING CLAY LAYER IN 12" LIFTS PRIOR TO CONSTRUCTION NEW CLAY LAYER ADJACENT TO EXISTING.
- FINAL COVER CONSTRUCTION TO BE IN ACCORDANCE WITH SECTION 7.1
 OF THE ENTERPRISE RECYCLING & DISPOSAL FACILITY RECLAMATION &
 CLOSURE PLAN.











2000-144-	NO.	DATE	REVISION DESCRIPTION	BY		
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Gainesville, Florida 32606
Phone: 352.672.6867 Fax: 352.692.5390
Certificate of Authorization No. 30066

PERMIT PLANS
ENTERPRISE ROAD CLASS III
RECYCLING & DISPOSAL FACILITY
2016 PERMIT MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB
	DRAWN BY	LJB
	CHECKED BY	JDL

APPROVED BY LJB

FL PE NO. 74652

CLOSURE DETAILS

SHEET TITLE:

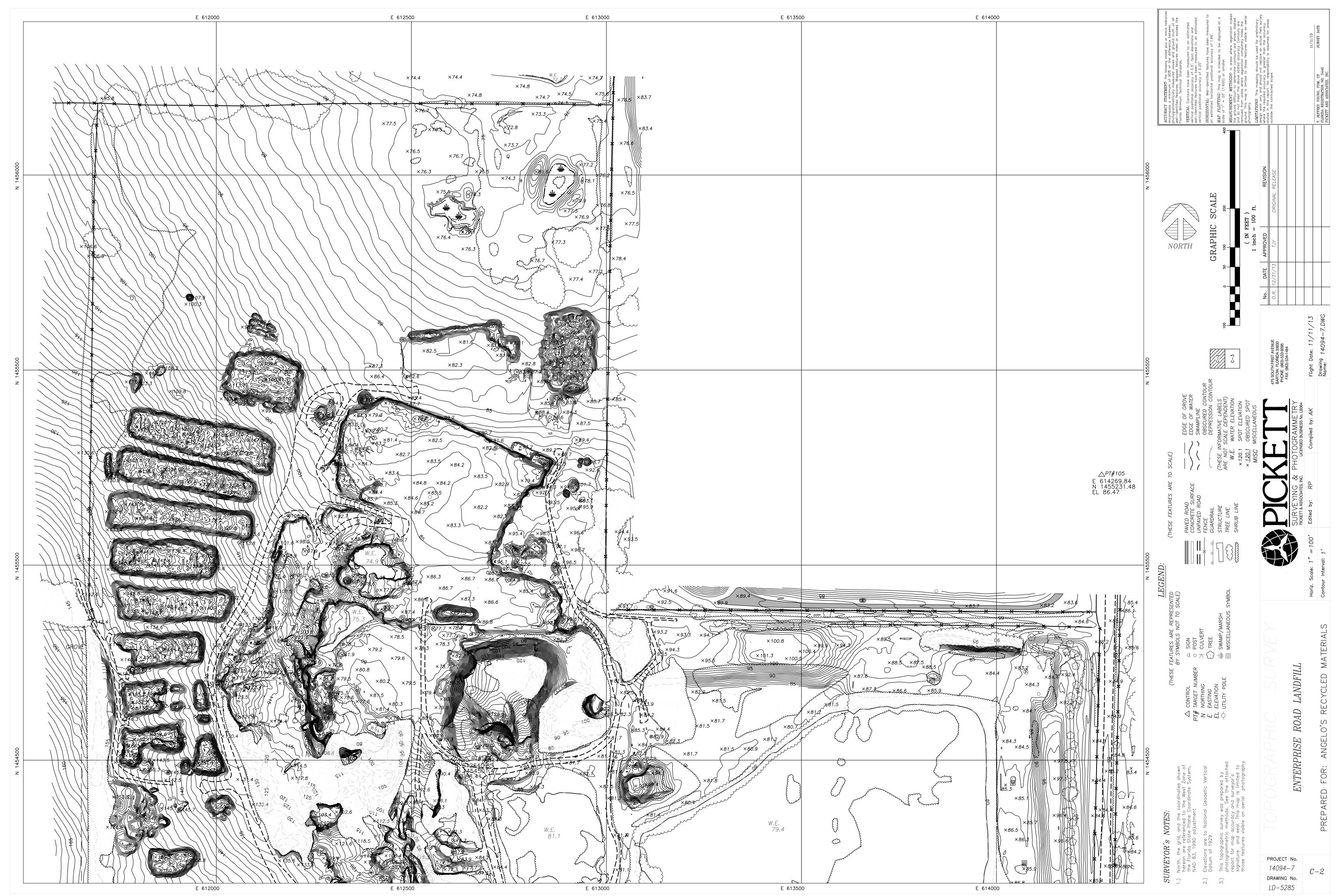
PROJECT NO.:

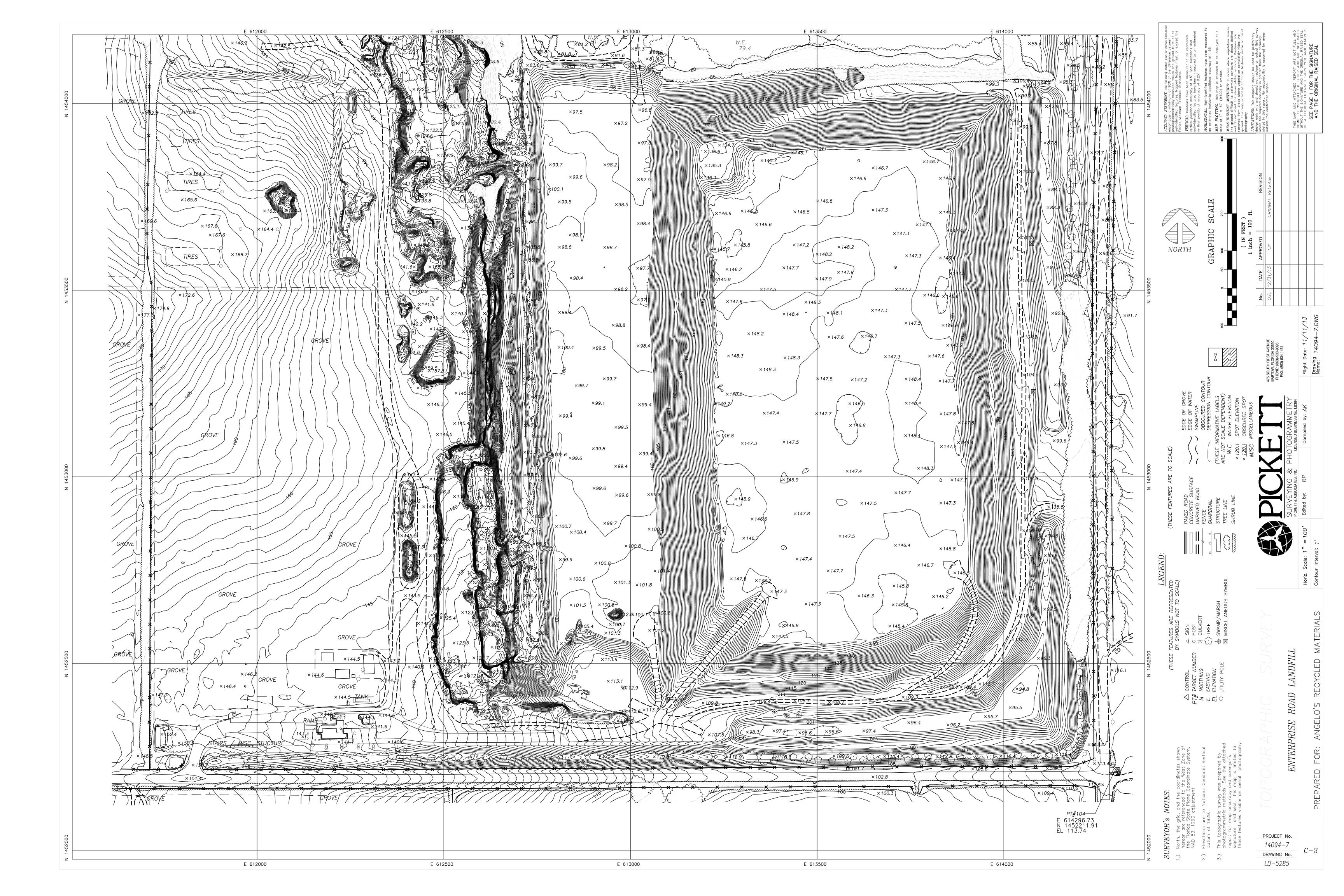
02000-144-14
SCALE:

AS SHOWN
DATE:

MARCH 2016
DRAWING:

C3.00





SECTION 5 GROUNDWATER MONITORING PLAN

Enterprise Class III Landfill Groundwater Monitoring Plan

March 2016
Revised July 2016 (RAI 1 Response)

Prepared for:

ANGELO'S RECYCLED MATERIALS, LTD.

41111 Enterprise Road Dade City, Florida 33525

Prepared by:

LOCKLEAR & ASSOCIATES, INC.

4140 NW 37th Place, Suite A Gainesville, FL 32606



This Groundwater Monitoring Plan (GWMP) has been prepared in accordance with the provisions of Rule 62-701.510, F.A.C., and any non-conflicting provisions of Chapter 62-520, F.A.C. The GWMP was developed based upon an extensive evaluation of site data provided in the March 2012 (Revised March 2013) Water Quality Monitoring Plan Evaluation Report prepared by Locklear & Associates, Inc. The Water Quality Monitoring Plan Evaluation Report is provided in Section 6 of the March 2012 Operations Permit Renewal Application. Analytical data tables and graphs as well as groundwater contour maps updated since 2012 were recently provided to the Department in the December 2015 Groundwater Technical Report (formerly referred to as a Biennial Report).

1. Water Quality Monitoring Plan

The groundwater monitoring network is shown in Table 1 and in Figure 1.

a. All groundwater monitoring well installations and abandonments shall be performed in accordance with ASTM D 5092-04, Rule 62-532.500(5) 62-701.500(5), F.A.C. and the rules of Southwest Florida Water Management District.

b. Sign and Seal

The reports shall be signed and sealed in accordance with Chapter 471, Florida Statutes and Chapter 61G15, FAC for engineers or with Chapter 492 for professional geologists.

c. Sampling and Analysis

All sampling and analysis shall be performed in accordance with Chapter 62-160, FAC; 62-701.510(2)(b), FAC; the DEP Standard Operating Procedures for Field Activities (DEP-SOP-001/01); and the DEP Standard Operating Procedures for Laboratory Activities (DEP-SOP-002/01).

d. Groundwater Monitoring Requirements

The groundwater monitoring network consists of detection monitoring wells located downgradient from and within 50 feet of the disposal units. The detection wells are located no more than 500 feet apart. The network also includes background monitoring wells BW-1A and BW-1B screened within the surficial and Floridan aquifers, respectively. Downgradient compliance

1

Enterprise Class III Landfill Groundwater Monitoring Plan July 2016 RAI March 2016

monitoring wells will be installed if warranted based on the results of detection monitoring results and Evaluation Monitoring as discussed in Section 1.h. Compliance wells will be located at or immediately adjacent to the compliance line of the zone of discharge.

Monitoring wells shall be constructed to provide representative groundwater samples from the surficial aquifer, where present, and the Floridan aquifer system. Well screen placement will be determined from lithologic information collected at the time of well installation and historic water level elevations as discussed-below-in-Section III of the March 2012 Water Quality Monitoring Plan Evaluation Report.

The top and bottom of the screen elevations for proposed surficial aguifer monitoring wells MW-18A, -19A and -20A are based on the top of clay confining unit elevations encountered during the installation of adjacent monitoring wells MW-15B, -16B and -17B. The clay confining layer was encountered at the surface during the installation of these wells, and therefore, we do not anticipate water bearing soils above the clay confining layer at the locations of the proposed surficial aguifer monitoring wells MW-18A, -19A and -20A. However, the lithology will be assessed at the location of each new well and surficial aquifer wells will be installed if water bearing soils exist above the clay confining layer. The historic range of surficial aquifer water elevations in this area is not available. The top and bottom of the screen elevations for proposed surficial aguifer well MW-5AR are based on the characteristics of existing surficial aquifer well MW-5A. The historical range of surficial aguifer water elevations in MW-5A is 78.45 to 68.99 ft. NGVD (previous ten sampling events). Proposed top and bottom screen elevations for MW-5AR are 82 ft. and 62 ft. NGVD, respectively.

The top and bottom of the screen elevations for proposed Floridan aquifer monitoring wells MW-18B, -19B and -20B are based on the top of limestone elevations encountered during the installation of adjacent monitoring wells MW-15B, -16B and -17B. The top of limestone elevation encountered during the installation of MW-15B was observed at 119 ft. NGVD, however the limestone in this boring was dry down to an elevation of 83 ft. NGVD. Moisture was not described below this elevation. The historical range of Floridan aquifer water elevations in MW-15B is 66.1 to 74.17 ft. NGVD (previous ten sampling events). Proposed top and bottom screen elevations for MW-18B are 65 ft. and 45 ft. NGVD, respectively. The bottom of the clay confining layer elevations encountered during the installation of MW-16B and -17B were observed at 64.5ft. and 43.5 ft. NGVD, respectively. The historical range of Floridan aquifer water elevations in MW-16B and -17B is 66.2 to 74.3 ft. NGVD (previous ten sampling events), indicating the clay

Enterprise Class III Landfill Groundwater Monitoring Plan July 2016 RAI March 2016

confining layer in these locations is creating artesian conditions. Proposed top and bottom screen elevations for MW-19B are 58 ft. and 38 ft. NGVD, respectively. Proposed top and bottom screen elevations for MW-20B are 35 ft. and 15 ft. NGVD, respectively. The top of limestone elevation encountered during the installation of MW-5B was observed at 60 ft. NGVD. The historical range of Floridan aquifer water elevations in MW-5B is 74.66 to 66.01 ft. NGVD (previous ten sampling events), indicating the clay confining layer in these locations is creating artesian conditions. Proposed top and bottom screen elevations for MW-5BR are 55 ft. and 35 ft. NGVD, respectively. Screen elevations for all proposed Floridan aquifer wells will be placed to encounter the upper-most saturated limestone layer beneath the bottom of the clay confining layer. Screen elevations will be determined based on field findings during well installation.

Figure 4 presents sections through Cell 16, the three sets of monitoring well pairs (MW-4/-4B, -5/AR/-5BR and -6/-6B), and Pond 3. The sections include the lateral distance from the edge of waste in Cell 16 to the monitoring well pairs and the lateral distance from the monitoring well pairs to the top of the bank of Pond 3.

Wells shall be constructed in accordance with the details provided in <u>REV</u> Figures 2 and 3. Documentation of well construction shall be submitted within 30 days of installation using Department Form #62-701.900(30).

Wells scheduled to be abandoned during construction of Cell 16 and Pond 3, (MW-5A, MW-5B and P-4), and wells which become damaged, shall be plugged and abandoned in accordance with Rule 62-532.500(5), F.A.C. and the rules of the Southwest Florida Water Management District. Documentation of abandonment shall be submitted to the Department within 30 days of abandonment.

Replacement wells associated with those abandoned as part of construction of Cell 16 and Pond 3 (MW-5AR and MW-5BR) will be constructed in accordance with the details provided in Figures 2 and 3.

The location(s) of all new or replacement monitoring wells, in degrees, minutes and seconds of latitude and longitude, and the elevation of the top of the well casing to the nearest 0.01 foot, using a consistent, nationally recognized datum, shall be determined by a Florida Licensed Professional Surveyor and Mapper. Wells will be marked with their identification label in the field.

e. Surface Water Monitoring Requirements

Ponds 1, 2 and 3 do not have off-site discharge associated with the 100-year flood event. Therefore, surface water sampling is not required as part of the solid waste operating permit. In the unexpected event of a surface water discharge event, surface water monitoring will occur per Appendix 3, Para. 8.a. and Para. 8.b. of #177982-020-SO/T3. However, surface water in Pond 3 will be sampled in accordance with the Industrial Wastewater pond permit being applied for concurrent with the solid waste permit modification application.

f. Leachate Monitoring Requirements

(1) Leachate monitoring is not applicable to this facility.

g. Sampling Frequency and Requirements

(1) Water samples from all newly installed monitoring wells (including replacement wells associated with those abandoned as part of construction of Cell 16 and Pond 3) will be collected to determine background groundwater quality. Groundwater samples from the initial sampling of any new wells will be analyzed for parameters listed in Rule 62-701.510(7)(a) and (7)(c), F.A.C. (Table 2).

Table 2				
Initial Groundwater Sampling Parameters				
Field Parameters	Laboratory Parameters			
Static Water Levels	Total Ammonia – N			
Specific Conductivity	Chlorides			
pН	Iron			
Dissolved Oxygen	Mercury			
Turbidity	Nitrate			
Temperature	Sodium			
Colors and Sheens	Total Dissolved Solids (TDS)			
	Those Parameters listed in 40 CFR Part 258,			
	Appendices I and II			

(2) Groundwater samples from all monitoring wells (background and detection) and the on-site supply well shall be sampled and analyzed semiannually for the parameters listed in Table 3. A semiannual sampling frequency is adequate to detect potential groundwater

quality standard exceedances based upon the flow velocities provided in Section III of the 2012 WQMPE. Maximum groundwater flow velocities were less than 50 feet per six months within both the surficial and Floridan aquifers. The first semiannual sampling event shall be performed between January 1 and June 30. The second semiannual sampling event shall be performed between July 1 and December 31.

Table 3				
Routine Groundwater Sampling Parameters				
Field Parameters	Laboratory Parameters			
Static Water Level	Total Ammonia – N			
Specific	Chlorides			
Conductivity	Iron			
pН	Mercury			
Dissolved Oxygen	Nitrate			
Turbidity	Sodium			
Temperature	Total Dissolved Solids (TDS)			
Colors, Sheens	Those Parameters listed in 40			
	CFR Part 258, Appendix I			

- (3) Surface water sampling shall be conducted at Pond 3 in accordance with the requirements of the separate Industrial Wastewater pond permit.
- (4) Leachate sampling is not applicable to this facility.
- h. Evaluation Monitoring, Prevention Measures, and Corrective Action

If parameters are detected in detection wells at concentrations that are significantly above background water quality, or that are at concentrations above the FDEP's water quality standards or criteria specified in 62-520, F.A.C., the well will be resampled within 30 days after the initial analytical data are received to confirm the data. If the data are confirmed or the well is not resampled, the FDEP will be notified in writing within 14 days of detection. Evaluation monitoring shall be initiated as follows:

• Routine monitoring of all monitoring wells will continue according to the GWMP.

- Within 90 days of initiating evaluation monitoring and annually thereafter, the background wells and all affected detection wells will be sampled for the parameters listed in 62-701.510(7)(c), F.A.C. Any new parameter detected and confirmed in the downgradient wells will be added to the routine groundwater monitoring parameter list.
- Within 90 days of initiating evaluation monitoring compliance monitoring wells will be installed at the compliance line of the zone of discharge and downgradient of the affected detection wells. The compliance wells will be installed in accordance with 62-701.510(3)(d), F.A.C. Compliance wells and affected detection wells shall be sampled quarterly for analysis of the parameters listed in Rule 62-701.510(7)(a), F.A.C. and any other parameters detected in the affected detection and downgradient wells sampled in accordance with Rule 62-701.510(6)(a)2, F.A.C. Compliance wells and affected detection wells shall be sampled annually for analysis of the parameters listed in Rule 62-701.510(7)(c), F.A.C.
- Within 180 days of initiating evaluation monitoring, a contamination evaluation plan will be submitted to the FDEP. The contamination evaluation plan will be designed to delineate the extent and cause contamination and to predict the probability that FDEP water quality standards are not violated outside the zone of discharge and to evaluate methods to prevent any violations. Upon agreement with the FDEP that the plan is so designed, the plan shall be implemented and a contamination evaluation report will be submitted to the FDEP. All reasonable efforts will be made to prevent further degradation of water quality from the landfill activities.
- If the contamination evaluation report indicates that water quality standards or criteria are likely to be violated outside the zone of discharge, a prevention measures plan shall be submitted to the Department. Upon approval, the prevention measures shall be initiated.
- Evaluation monitoring shall not be discontinued until authorization to return to routine monitoring only is received from the Department.
- i. Water Quality Monitoring Report Requirements

(1) All representative water quality monitoring results shall be reported to the Department within 60 days from completion of laboratory analyses. In accordance with subsections 62-160.240(3) and 62-160.340(4), F.A.C., water quality data contained in the report shall be provided to the Department in an electronic format consistent with requirements for importing into Department databases.

At a minimum the semiannual report shall include the following:

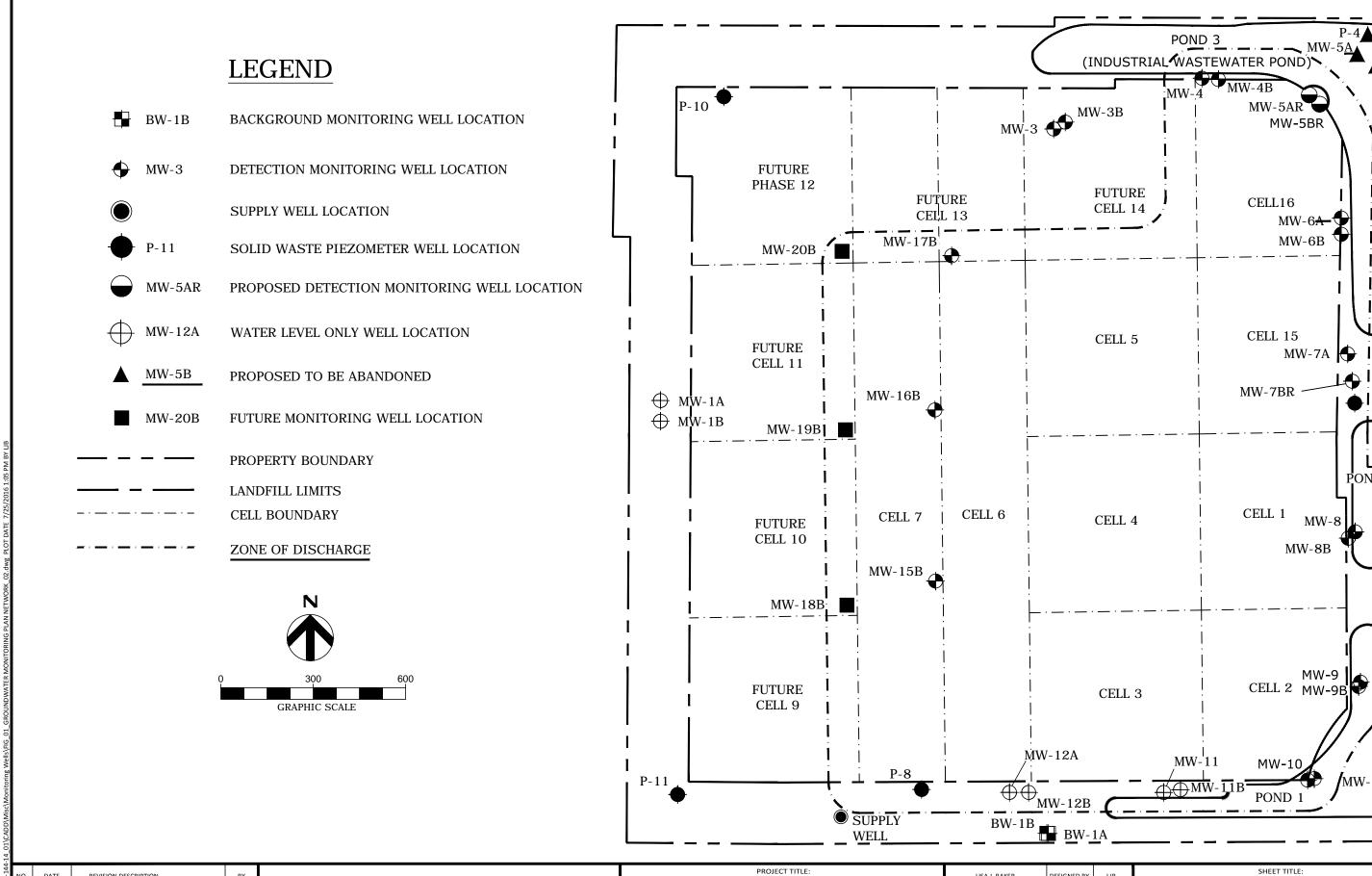
- The facility name and identification number, sample collection dates, and analysis dates;
- All analytical results, including all peaks even if below maximum contaminant levels;
- Identification number and designation of all groundwater monitoring points;
- Applicable water quality standards;
- Quality assurance, quality control notations;
- Method detection limits:
- STORET code numbers for all parameters;
- Water levels recorded prior to evaluating wells or sample collection. Elevation reference shall include the top of well casing and the land surface at each well site at a precision of plus or minus 0.01 foot, National Geodetic Vertical Datum (NGVD);
- Department Form 62-701.900(31);
- An updated groundwater table contour map signed and sealed by a professional geologist or professional engineer with experience in hydrogeologic investigations, with contours at no greater than one-foot intervals unless site-specific conditions dictate otherwise, which indicates groundwater elevations and flow directions; and
- A summary of any water quality standards or criteria that are exceeded.
- (2) A technical report will be submitted every two and one-half years summarizing and interpreting the water quality monitoring results and water level measurements collected during that period. The report will be in accordance with Rule 62-701.510(8)(b) and signed and sealed by Florida licensed Professional Geologist or Professional Engineer. The report shall contain, at a minimum, the following:
 - Tabular displays of any data which shows that a monitoring parameter has been detected, and graphical displays of any leachate key indicator parameters detected (such as pH, specific

- conductance, TDS, TOC, sulfate, chloride, sodium and iron), including hydrographs for all monitoring wells;
- Trend analyses of any monitoring parameters consistently detected;
- Comparison among shallow, middle, and deep zone wells;
- Comparisons between background water quality and the water quality in detection and compliance wells;
- Correlations between related parameters such as total dissolved solids and specific conductance;
- Discussion of erratic and/or poorly correlated data;
- An interpretation of the groundwater contour maps, including an evaluation of groundwater flow rates; and
- An evaluation of the adequacy of the water quality monitoring frequency and sampling locations based on site conditions.

TABLE 1

Well ID	Well Type	Aquifer	Existing or Future	Notes
BW-1A	Background	Surficial	Existing	
BW-1B	Background	Floridan	Existing	
MW-1A	Water Level	Surficial	Existing	
MW-1B	Water Level	Floridan	Existing	
MW-3	Detection	Surficial	Existing	
MW-3B	Detection	Floridan	Existing	
MW-4	Detection	Surficial	Existing	
MW-4B	Detection	Floridan	Existing	
MW-5A	Detection	Surficial	Existing	To be abandoned 60 days prior to placement of waste in Cell 16
MW-5AR	Detection	Surficial	Future	To be installed 60 days prior to placement of waste in Cell 16
MW-5B	Detection	Floridan	Existing	To be abandoned 60 days prior to placement of waste in Cell 16
MW-5BR	Detection	Floridan	Future	To be installed 60 days prior to placement of waste in Cell 16
MW-6	Detection	Surficial	Existing	
MW-6B	Detection	Floridan	Existing	
MW-7A	Detection	Surficial	Existing	
MW-7BR	Detection	Floridan	Existing	
MW-8	Detection	Surficial	Existing	
MW-8B	Detection	Floridan	Existing	
MW-9	Detection	Surficial	Existing	
MW-9B	Detection	Floridan	Existing	
MW-10	Detection	Surficial	Existing	
MW-10B	Detection	Floridan	Existing	
MW-11	Water Level	Surficial	Existing	
MW-11B	Water Level	Floridan	Existing	
MW-12A	Water Level	Surficial	Existing	
MW-12B	Water Level	Floridan	Existing	
MW-15B	Detection	Floridan	Existing	To be abandoned in conjunction with Cell 7 construction
MW-16B	Detection	Floridan	Existing	To be abandoned in conjunction with Cell 7 construction
MW-17B	Detection	Floridan	Existing	
Water	Supply	Floridan	Existing	
Supply	Supply	Tioridan	LXISTING	
MW-18A*	Detection	Surficial	Future	To be installed in conjunction with Cell 7 construction
MW-18B	Detection	Floridan	Future	To be installed in conjunction with Cell 7 construction
MW-19A*	Detection	Surficial	Future	To be installed in conjunction with Cell 7 construction
MW-19B	Detection	Floridan	Future	To be installed in conjunction with Cell 7 construction
MW-20A*	Detection	Surficial	Future	To be installed in conjunction with Cell 7 construction
MW-20B	Detection	Floridan	Future	To be installed in conjunction with Cell 7 construction
P-4	Piezometer	Surficial	Existing	To be abandoned within 60 days of permit modification issuance
P-6	Piezometer	Surficial	Existing	
P-8	Piezometer	Floridan	Existing	
P-10	Piezometer	Floridan	Existing	
P-11	Piezometer	Surficial	Existing	

^{*} To be installed only if water bearing sediments are encountered above the clay units confining the Floridan aquifer system.



REVISION DESCRIPTION DATE

Phone: 352.672.6867 Fax: 352.692.5390 Certificate of Authorization No. 30066

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY DADE CITY, FLORIDA

LISA J. BAKER	DESIGNED BY	LJB	
	DRAWN BY	LJB	
	CHECKED BY	JDL	
FL PE NO. 74652	APPROVED BY	ЫB	

REV GROUNDWATER MONITORING NETWORK

MW-6B

MW-7A

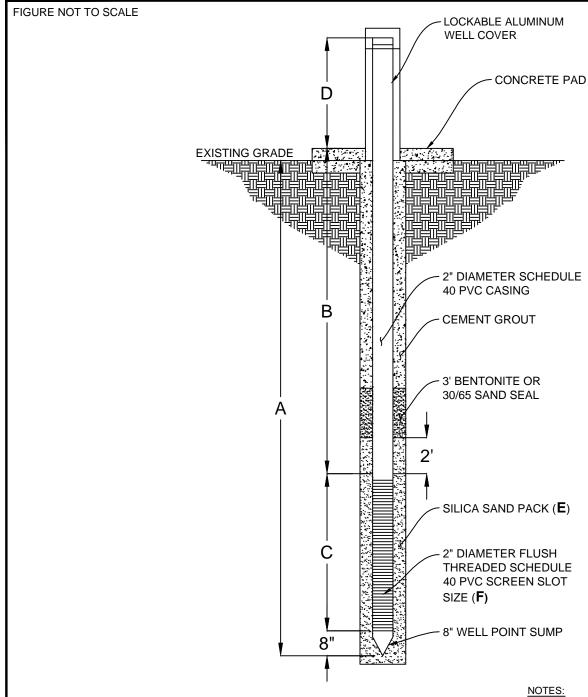
MW-8

MW-9

MW-10B

MW-8B

02000-144-14 AS SHOWN ATE: MAY 2016 FIGURE 1



WELL	A	В	O	D	Ш	F	TOP OF WELL SCREEN ELEVATION FT, NGVD	BOTTOM OF WELL SCREEN ELEVATION FT, NGVD	ASSUMED GROUND SURFACE ELEVATION FT, NGVD	ASSUMED LIMESTONE SURFACE ELEVATION FT, NGVD
MW-18A	25'	5'	20'	3'	20/30	0.010"	<u>143' (8)</u>	<u>123' (8)</u>	148' (2)	116' (5)
MW-19A	<u>25 70'</u>	<u>5</u> 50 ′	20'	3'	20/30	0.010"	<u>133' (8)</u>	<u>113' (8)</u>	138' (3)	61' (5)
MW-20A	25 50 ′	<u>5</u> 30 ′	20'	3'	20/30	0.010"	<u>82' ₍₈₎</u>	<u>62' (8)</u>	87' (4)	31' (5)
MW-5AR	28'	8'	20'	3'	20/30	0.010"	<u>79' (8)</u>	<u>59' 🙉</u>	87' (6)	60' (7)

- (1) Wells to be installed only if water bearing sediments are encountered above the Floridan aquifer confining layer.
- (2) From MW-15B elevation
- (3) From MW-16B elevation
- (4) From MW-17B elevation
- (5) From Cell 6 well lithologies
- (6) From MW-5A elevation
- (7) From MW-5A lithology
- (8) Based on site-specific lithology and water level. Subject to change per field findings during well installation.



ENTERPRISE ROAD RECYCLING AND DISPOSAL FACILITY DADE CITY, FLORIDA

PROPOSED SURFICIAL AQUIFER MONITOR WELL DETAIL <u>REV</u> FIGURE

REVISED MAY FEBRUARY 2016

2

		THREADED SCHEDULE 40 PVC SCREEN SLOT SIZE (F)
8"		— 8" WELL POINT SUMP
Å	7.0 N. 10/47	

3' BENTONITE OR 30/65 SAND SEAL

· SILICA SAND PACK (**E**)

2" DIAMETER FLUSH

WELL	А	В	С	D	Ш	F	TOP OF SCREEN ELEVATION FT. NGVD	BOTTOM OF SCREEN ELEVATION FT. NGVD	ASSUMED GROUND SURFACE ELEVATION FT, NGVD	ASSUMED LIMESTONE SURFACE ELEVATION FT, NGVD
MW-18B	<u>103</u> ' 100'	<u>83'</u> 80'	20'	3'	20/30	0.010"	<u>65' 🙉</u>	<u>45' (9)</u>	148' (1)	118' (<u>5</u> +)
MW-19B	100'	80'	20'	3'	20/30	0.010"	<u>58' (9)</u>	<u>38' (9)</u>	138' (2)	63' <u>6</u> =)
MW-20B	<u>72'</u> 80'	<u>52</u> ' 60'	20'	3'	20/30	0.010"	<u>35' (9)</u>	<u>15' (9)</u>	87' (3)	32' (Ze)
MW-5BR	<u>51'</u> 48'	<u>31'</u> 38'	<u>20'</u> 10'	3'	20/30	0.010"	<u>55' (9)</u>	<u>35' (9)</u>	86' (4)	60' <u>&</u>

NOTES:

- (1) From MW-15B ground elevation
- (2) From MW-16B ground elevation
- (3) From MW-17B ground elevation
- (4) From MW-5B ground elevation
- (5) From MW-15B lithology
- (6) From MW-16B lithology
- (7) From MW-17B lithology
- (8) From MW-5B lithology
- gased on site-specific lithology and water level data. Subject to change per field findings during well installation.



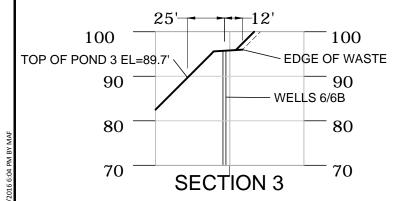
ENTERPRISE ROAD RECYCLING AND DISPOSAL FACILITY DADE CITY, FLORIDA

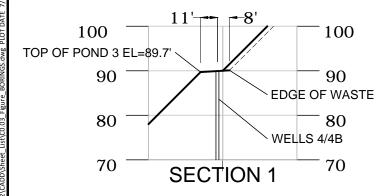
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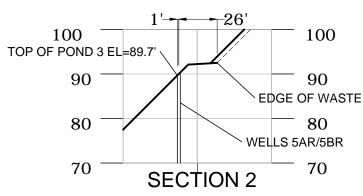
PROPOSED FLORIDAN AQUIFER MONITOR WELL DETAIL $\underline{\mathsf{REV}}$ FIGURE

3

REVISED MAY FEBRUARY-2016









BORING CROSS SECTIONS FOR
ENTERPRISE ROAD CLASS III
RECYCLING & DISPOSAL FACILITY
2016 PERMIT MODIFICATION
DADE CITY, PASCO COUNTY, FLORIDA

SECTION 6

WATER QUALITY MONITORING PLAN EVALUATION

(Water Quality Monitoring Plan Evaluation located in Section 2, Part G-1, Liner System Requirements Evaluation)

SECTION 7

CLOSURE AND RECLAMATION PLAN

Appendix 7-A Financial Assurance Cost Estimate

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY MAJOR PERMIT MODIFICATION CLOSURE AND RECLAMATION PLAN

Prepared for:

ANGELO'S AGGREGATE MATERIALS, LTD

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Presented to:

FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION SOUTHWEST DISTRICT – SOLID WASTE DIVISION

13051 N. Telecom Parkway Temple Terrace, Florida 33637

Prepared by:

LOCKLEAR & ASSOCIATES, INC.

4140 NW 37 Place, Suite A Gainesville, Florida 32606 Certificate of Authorization #30066

Project No.: 02000-144-15

March 2016

Revised July 2016 RAI 1 Response

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1.0 RECLAMATION AND CLOSURE STANDARDS

This Closure Plan is designed to comply with the Florida Department of Environmental Protection (FDEP) requirements of Rule 62-701.600, F.A.C. and the Pasco County Land Development Code (LDC) for Class I Mine reclamation and Class III landfill closure. The landfill will be used to reclaim the borrow pit excavation as phases are completed.

1.1 TIMING

Mine reclamation and landfill closure will commence when all cells have been filled. Reclamation and closure will be completed within four (4) months of commencement. An intermediate soil cover of at least one (1) foot in depth will be applied and maintained within seven (7) days of lift completion. If the landfill operator (Operator) wishes to deposit additional solid waste in the completed cell, all or part of the intermediate cover may be removed to place the waste or to install the final cover. Intermediate cover will be placed on completed landfill cells and sideslopes as filling progresses. Final cover will be installed upon each completed landfill cell within 180 days after attaining final elevation. The remaining Facility life is provided in Section 3.8.3 of the Engineering Report in Section 3.

1.2 STORMWATER MANAGEMENT

The Conceptual Closure Plan (Drawing Sheet C2.00 of the 2016 Plan Set provided in Section 4 Appendix A) includes a site stormwater system comprised of three dry retention ponds. Stormwater runoff will sheetflow down the sideslopes of the landfill into the retention ponds. The Facility's overall stormwater management system is governed by the Mining Operations and ERP Permits. Grades and elevations vary based on the current mining operations and topography. As required by the Florida Department of Environmental Protection (FDEP), a detailed Closure Permit Application with stormwater conveyance systems will be submitted at the time of closure. The stormwater facilities will be constructed in accordance to the approved Closure Permit to prevent the offsite runoff of stormwater.

1.3 FINAL COVER SPECIFICATIONS

The construction of the final cover will consist of three main operations. First, on-site clayey sand and sandy clay soils will be utilized to construct a barrier layer. Secondly, a layer of soil capable of sustaining vegetation will be constructed. Finally, seeding and mulching, or sodding with "Argentine" Bahia grass, or equivalent, will then be performed to establish a permanent ground cover. Detailed specifications for each of these operations are described as follows:

1.3.1 Final Cover Design

All areas filled with waste will have a final cover of soil designed to minimize infiltration of rainfall. Final cover will be initiated with 30 days of reaching final grade and will be placed and completed over each cell within 180 days after final waste deposit. The final cover will consist of a 3-foot thick layer of soil, of which the bottom 18 inches is barrier layer and the top 18 inches will sustain vegetative growth. A detail is provided on Sheet C3.00 of the 2016 Plan Set provided in Section 4 Appendix A.

1.3.2 Barrier Layer

The 18-inch barrier layer will have a permeability of 1 x 10⁻⁷ cm/sec or less. On site clayey sands will be used to construct the barrier layer. Once these soils have been placed and compacted in 6-inch lifts to 95% standard proctor, a series of *insitu* thickness tests and permeability tests will be completed prior to placement to of the vegetative soil layer.

1.3.3 <u>Vegetative Soil Cover</u>

An 18-inch layer of soil from the onsite borrow operation may be used, as the vegetative soil layer. These soils will sustain vegetative growth (grasses).

1.3.4 Grading and Compaction

Grading work will be performed as shown and specified on the construction plans, (Sheet C1.00 through C2.10 of the 2016 Plan Set provided in Section 4 Appendix A). Final slopes will not exceed a 3:1 slope.

The Applicant will be responsible for grading within the landfill limits. All irregularities and low areas will be fine graded with onsite soil material. The Applicant will maintain grades, profiles and contours as indicated on the approved final grading plan. The Applicant will protect and maintain finish graded areas from traffic and erosion. In the event that the site grading is eroded and/or damaged prior to final acceptance, the Applicant will repair and reestablish the grades in accordance with the construction plans.

1.3.5 Construction Quality Assurance Plan

To assure that the landfill's final cover meets the design parameters, the following Construction Quality Assurance Plan (CQA) plan has been developed. This CQA plan will be under the direction of a Florida registered professional engineer experienced in geotechnical engineering or landfill cover construction. The engineer or his designee will be on-site at all times during

construction of the cover to monitor construction activities. Field and laboratory testing during final cover construction will be by a qualified soil testing laboratory.

Prior to final cover construction, a suitable borrow source meeting the project specifications for the barrier layer will be determined. The Applicant plans to use on-site soils to meet these specifications. A minimum of three (3) representative samples from on-site soils will be submitted to a laboratory for index testing to quantify the variability of the borrow materials. The index tests will consist of percent fines (ASTM D-1140), Atterburg limits (ASTM D-4318), and moisture content (ASTM D-2216).

In addition, a minimum of three (3) laboratory hydraulic conductivity tests will be conducted on the barrier layer borrow source by ASTM D-5084 under a consolidation stress no greater than 10 pounds per square inch. The borrow source will only be considered suitable if the laboratory reports document a hydraulic conductivity of 1 x 10⁻⁷ cm/sec or less at the 95 percent confidence level.

The following field tests will be performed during final cover construction:

- 1. Density tests at a minimum of two tests per acre per 6-inch lift, of the compacted cover material;
- 2. Thickness measurements at a minimum of three tests per acre;
- 3. Index testing as previously discussed at a minimum of one sample per acre;
- 4. Hydraulic conductivity testing of Shelby tube samples (ASTM D-2937) of compacted barrier layer by laboratory test method ASTM D-5084 at a minimum frequency of one test every two acres. The barrier layers' hydraulic conductivity will be considered acceptable if laboratory reports meet the project specifications of 1 x 10⁻⁷ cm/sec or less at the 95 percent confidence level.

If laboratory test data for a cover section does not meet these requirements, additional random sample testing may be conducted to determine if the cover is acceptable to the Project Engineer, the cover section must be reworked or reconstructed to meet these requirements.

CQA reporting requirements will include: daily summary reports during cover construction; observation data sheets; problem identification and corrective actions taken; and final documentation, laboratory reports and construction record drawings. A final report with all such documents will be submitted to the Pasco County and the FDEP.

1.3.6 Seeding and Mulching

Seeding and mulching will consist of establishing a dense stand of grass throughout each closed cell. Included with this task are fertilizing, watering, and periodic maintenance mowing as

required to produce a healthy stand of grass. Seeding work will be performed only after planting and other work affecting ground surface has been completed unless the Applicant is specifically requested to do otherwise for purposes of stabilization, etc., prior to project completion. The vegetation species recommended are drought resistant and their roots will not penetrate the final cover to provide a channel for moisture infiltration.

1.3.7 Materials

Seeds and mulch materials will conform to the following:

1. Seed - Fresh, clean new crop mixture composed of the following variety and proportions:

<u>Blend</u>	<u>Parts</u>	<u>Purity</u>	Min. Germination
Argentine Bahia (or equivalent)	100 Percent	80 Percent	90 Percent

Rate will be 120 pounds per acre (Refer to Index No.104, *Roadway and Traffic Design Standards*, Florida Department of Transportation, 1992).

- 2. Mulch Dry mulch, free from mature seed bearings stalks or roots of noxious weeds. Dry mulch will be straw or hay consisting of oat, rye or wheat straw. Approximately two (2) inches of the mulch material will be applied uniformly over the seeded area
- 3. Fertilizer Granular, non-burning product containing 6 percent nitrogen, 6 percent phosphoric acid, and 6 percent potash by weight, and spread uniformly at a rate of 220 pounds per acre. Fertilizer will be mixed with the soil to a depth of \pm four (4) inches.
- 4. Watering The seeded area will be watered so as to provide optimum growth conditions for the establishment of grass. The water used in the grassing operations may be obtained from any approved supply well, like Larkin's well on the adjacent property to the west. The water will be free of excess and harmful chemicals, acids, alkalis, or any substance which might be harmful to plant growth or obnoxious odors to traffic. Salt water will not be used.

The Applicant will provide a uniform dense stand of grass by watering, mowing and maintaining seeded areas for a thirty (30) year period after closure or until final acceptance by FDEP and the County, whichever is less. Sodding may be used as an alternative to seeding and mulching.

1.4 RECLAMATION APPROVAL

Approval of reclaimed areas (final cover) may be requested at any time by submitting such request to the County and the FDEP. The request will include a map specifying reclamation areas (final cover) for which approval is sought and a general description of how reclamation has been accomplished. The Applicant will coordinate and schedule the review of the reclaimed areas with the appropriate departments, divisions or agencies. Reclamation of the site will be deemed completed upon demonstration and agency approval that the site has been reclaimed in accordance with the approved reclamation plan.

1.5 INSPECTIONS

County and FDEP staff will have access to the project to inspect and observe permitted activities in order to determine compliance with the terms of the Closure Permit. The County and FDEP will also have access to the site during the post-closure phase of the project.

1.6 SURVEY MONUMENTS

Permanent concrete monuments will be installed to mark the boundaries of the landfill property. Where the final grade of the landfill is 20 feet or less above grade, permanent markers will be installed to outline the general waste filled area. The location and elevation of all markers will be tied to boundary markers by the professional performing the final survey and will be submitted on a site plan filed with the "Declaration to the Public."

1.7 FINAL SURVEY AND AS BUILT REPORTS

A final topographic survey will be performed by a Florida registered land surveyor to verify the final contours and elevations of the facility are in accordance with the plans as approved in the permit within 180 days after closure. This survey will be submitted to the FDEP along with the Certification of Closure Construction Completion on Form 62-701.900(2), F.A.C..

1.8 OFFICIAL DATE OF CLOSING

Upon receipt and approval of the Certification of Closure Construction Completion and the "Declaration to the Public", FDEP and the County will, within 30 days, acknowledge by letter to the facility operator, that notice of termination of operations and closing of the facility has been completed. The date of the letter will be the official Date of Landfill Closing for purposes of determining the Long Term Care Period.

1.9 CLOSURE SCHEDULE

The schedule for closure activities will be based on the time required to fill each cell to the final grades. Please refer to Sections 1.10 through 1.12 for closure milestones.

1.10 NOTICE AND ADVICE TO USERS

At least 90 days prior to the date when wastes will no longer be accepted at the landfill, the owner or operator will submit an application to advise users of the intent to close the facility by posting signs at the entrance of the facility giving the date of closing, the location of alternative disposal facilities and name of the entity responsible for closing the landfill. These signs will be maintained throughout the closing period. If unforeseen circumstances do not allow the 120 day notice to users, notice will be provided as soon as the need to close the facility becomes apparent.

1.11 NOTICE TO THE PUBLIC

Once closure construction has been completed, a Declaration to the Public will be filed in the deed records in the office of the Pasco County Clerk of Courts. The Declaration to the Public will include a legal description of the Class III Landfill property and a site plan showing the limits of waste. The Declaration to the Public will also include a notice that any future owner or user of the site should consult with the Department prior to planning or initiating any activity involving disturbing the landfill, monitoring system, or control structures. A certified copy of this notice will be filed with the FDEP.

1.12 CLOSURE PERMIT APPLICATION SUBMITTAL

A Closure Permit application will be submitted to Pasco County and the FDEP no less than 90 days prior to the scheduled closing day in accordance with the requirements of Rule 62-701.600, F.A.C..

The Closure Permit application will include the following: Closure Design Plan, Closure Operation Plan, Long-Term Care Plan, and proof of financial responsibility for long-term care period.

2.0 FINAL USE AND LONG TERM CARE

The proposed final use of the closed landfill will be as pastureland. The final use for the landfill site will exclude any buildings or other structures, unless such buildings and structures are specifically designed to address gas venting and settlement considerations associated with construction over a landfill. Long term care for the site will include maintaining the landscaping,

Page 6 of 10

ENTERPRISE ROAD CLASS III RECYCLING AND DISPOSAL FACILITY
March 2016 MODIFICATION APPLICATION (July 2016 RAI 1 Response)

CLOSURE AND RECLAMATION PLAN

security facilities, erosion control, filling subsidence areas, and maintaining the stormwater system for a period of thirty (30) years and maintaining the groundwater monitoring plan for a period of time established by the County or the FDEP. The Long-Term Care period may be extended if the closure design or operation plan is found to be ineffective, per Rule 62-701.620 F.A.C..

2.1 REPLACEMENT OF MONITORING DEVICES

If the monitoring wells or other devices required by the Groundwater Monitoring Plan are destroyed or fail to operate for any reason, the landfill Owner or Operator will, upon discovery, notify the FDEP and County in writing. All inoperative monitoring devices will be repaired or replaced with functioning devices within 60 days of the discovery of the malfunctioning unit.

2.2 LONG TERM MONITORING

Once the proposed Landfill facility is closed, groundwater and gas monitoring will continue for a period of up to 30 years with reports submitted to the County and the FDEP. Groundwater reports will be submitted semi-annually and gas monitoring reports will be submitted on a quarterly basis.

A Stabilization Report will be submitted to the Department every 5 years after the long-term care permit is issued. The Stabilization Report will include or address the following:

- Water quality technical report
- Waste subsidence
- Barrier layer effectiveness
- Stormwater management
- Gas production and management

2.3 FINAL COVER SYSTEM MAINTENANCE

Regular maintenance of all reclaimed areas will be performed by the Operator or a designated agent in order to assure that the reclamation standards are achieved and the approved reclamation plan is accomplished. The maintenance will include monitoring for a minimum of thirty (30) years after planting, replacement of any planted areas that fail to survive in accordance with the established standards, the removal of non-native species that have not been approved by the County, and the maintenance of all required slopes, final cover, embankments, ponds, fences, gates, signs, monitoring systems and stormwater facilities. The operator will maintain a stockpile on-site of approximately 60,000 cyds of cover material to be used for final cover maintenance.

The Operator will conduct monthly inspections of the facility. The site inspection will include the verification that the final cover system retains its integrity and effectiveness. The final cover will be routinely evaluated and inspected for any evidence of soil erosion, settlement and subsidence, exposed waste, cracks, ponded water, vegetation stress, slope failure, and seeps.

Deficiencies such as cracks, erosion damage, or settlement in the final cover will be evaluated regarding its extent and depth. Repairs and restoration will be consistent with the final cover construction specifications. Location of areas repaired will be identified on a site map for future reference. Areas requiring repeated repairs will be evaluated and considered for special or expanded improvements to retain the integrity and performance of the final cover system. If necessary, temporary berms, ditches, and erosion materials will be used to prevent further erosion damage or ponding on damaged soil cover areas until the site conditions permit the final cover areas and vegetation to be re-established. Preventative maintenance of the final cover should preclude problems arising from potential seeps from infiltration of surface water.

2.4 REVEGETATION

- 1. Revegetation of all disturbed areas will be conducted in a manner so as to achieve permanent revegetation which will minimize soil erosion and surface water runoff, conceal the effects of surface mining and recognize the requirements for appropriate habitat for fish and wildlife. Should washes, rills, gullies, or the like, develop after revegetation and before a thirty (30) year maintenance period, such eroded areas will be repaired, the slopes stabilized and revegetated, within thirty (30) days.
- 2. Good quality topsoil will be applied as the soil cover material for all reclaimed areas. Alternate growing media must be approved by the County prior to commencement of revegetation.
- 3. Revegetation efforts will commence within thirty (30) days after completion of regrading and will be completed within one hundred and twenty (120) days.

2.5 LANDFILL GAS MANAGEMENT SYSTEM

If the gas probes or other devices required by the landfill gas management system are destroyed or fail to operate for any reason, the landfill Operator will, upon discovery, notify the FDEP and County in writing. All inoperative monitoring devices will be repaired or replaced with functioning devices within 60 days of the discovery of the malfunctioning unit.

2.6 STORMWATER DRAINAGE SYSTEMS

Drainage control system problems can result in accelerated erosion of the final cover system and differential settlement of drainage control structures can limit their usefulness and may result in

failure of the drainage structure. It is expected that the drainage facilities at the Facility will require a greater amount of maintenance in the period immediately following construction than in later periods. This is due to greater potential for differential settlement early in the post closure period and the lack of mature vegetation.

The Operator will inspect the drainage facilities for the following:

- Evidence of erosion
- Standing water
- Formation of gullies
- Settlement, blockage, and damage to drainage channels, structures, swales and culverts

Inspection of the drainage facilities will occur prior to and during the rainy season to ensure proper functioning. Surface areas will be inspected during dry periods and necessary repairs made prior to the rainy season. Inspections will include checking for erosional ruts and settlement cracks. In addition, inspections will be made after each major storm to ensure that all swales are functioning properly and that there is no ponding water. All swales, drainage channels, and retention ponds will be inspected on a regular basis for silt or debris build-up. Damage to the drainage system will be addressed immediately after finding a problem. Permanent repairs and restoration will be made consistent with final closure construction specifications. Temporary repairs may be utilized until permanent repairs can be scheduled.

2.7 REDUCED LONG-TERM CARE PERIOD

The owner of the landfill may apply to Pasco County and FDEP for a permit modification to reduce the long-term care schedule after a 10-year history after closure in accordance with Rule 62-701.620 (2), F.A.C..

2.8 RIGHT OF ACCESS AND ACCESS CONTROL

The Owner currently poses a right of access to the subject site. Any future owner or operator will maintain this right of access to the access route and the property for the life of the landfill and throughout the long-term care period. All owners/operators will maintain all security barriers (fencing, signage, gates) for the design life and long-term care period of the landfill.

2.9 CONTINGENCY PLAN FOR EMERGENCIES

If fires or severe weather events occur, the Operator will follow the procedures discussed in the Contingency Plan, Section 3, Appendix 3-B Appendix H of the Engineering Report.

2.10 SUCCESSORS OF INTEREST

Any person or corporation acquiring rights or ownership, possession or operation of the proposed Class III landfill will be subject to all the requirements of the permit for the proposed facility. Any lease or transfer of property will include the following conditions:

- 1. The previous owner or operator responsible for closure will maintain proof of financial responsibility with the FDEP and Pasco County.
- 2. State the party responsible for continuance of monitoring, maintenance, and correction of problems.
- 3. Mineral rights to any recoverable materials buried at the landfill. Disturbance of a closed landfill will require a Department permit.

2.11 COMPLETION OF LONG-TERM CARE

Upon completion of the landfill's long-term care period, the Operator will notify the FDEP and Pasco County that a Professional Engineer certification has been placed in the landfill's operating record verifying that long-term care has been completed in accordance with the approved Closure and Long-term Care Plans.

3.0 FINANCIAL RESPONSIBILITY

Upon approval of the application, the owner or operator will provide financial assurance documentation for closure and post-closure costs. This financial assurance documents will be submitted prior to permit being issued. See <u>Section 7</u>, <u>Appendix 7-A Appendix F-1</u> for the Financial Assurance Cost estimates for the Class III landfill. Third party estimates for selected portions of the proposed work were used for the estimates. A financial assurance mechanism will be fully funded prior to the acceptance of any solid wastes at the proposed landfill.

3.1 ANNUAL COST ADJUSTMENTS

The Operator of the landfill will submit an annual cost adjustment statement of closure and long-term care costs certified by a Professional Engineer to the FDEP and Pasco County. These cost estimates will be revised for inflation and any changes in closure or corrective action plans.

Appendix 7-A FINANCIAL ASSURANCE COST ESTIMATE



Florida Department of Environmental Protection

Bob Martinez Center 2600 Blair Stone Road Tallahassee, Florida 32399-2400 DEP Form # 62-701.900(28), F.A.C.

Form Title: Closure Cost Estimating Form For Solid Waste Facilities

Effective Date: January 6, 2010

Date of DEP Approval:

Incorporated in Rule 62-701.630(3), F.A.C.

CLOSURE COST ESTIMATING FORM FOR SOLID WASTE FACILITIES

I. GENERA	AL INFORMATI	ON:					
Facility Na	me: <u>Enterpri</u>	se Class III Rec	ycling and Dis _l	oosal Facility		WACS ID: 87895	
Permit App	olication or Cons	sent Order No.:	177982-020	-SO/T3	Expira	tion Date: <u>7/9/</u>	2018
Facility Ad	dress: <u>41111</u>	Enterprise Roa	ıd, Dade City, I	Florida 33525			
Permittee of	or Owner/Opera	ator: <u>Angelo'</u>	s Aggregate M	aterials, LTD.			
Mailing Ad	dress: <u>855 28</u>	8th Street, Sout	h, St. Petersbu	rg, Florida 33712			
Latitude:	28	° 19'	53 "	Longitude:	82°	08'	06 "
Coordinate	Method: Sta	ate Plan		atum: NGVD 29			
Collected b	oy:			Company/Affiliation	Pickett Survey	ing	
Solid Wast	e Disposal Unit	s Included in Es	stimate:				
			Date Unit	Active Life of		If closed:	If closed:
			Began Accepting	Unit From Date of Initial Receipt	If active: Remaining	Date last waste	Official date of
F	Phase / Cell	Acres	Waste	of Waste	life of unit	received	closing
	7, 15 and 16	67.0	2004	22	13	N/A	N/A
	,				-		
Tatal diama	and weith a suppose	- :		Clasuma	1		
rotal dispo	isai unii acreage	e included in thi	s estimate:	Closure:		ng-Term Care:	
E.	acility type:	□ Class I	č C	Class III	C D Debris	Dienocal	
	k all that apply)			//a55 III	C D Debits	о Бізрозаі	
(000.		U Other					
II TYPE (OF FINANCIAL	ASSURANCE		Check type)			
· · · · <u> </u>	Letter of Cred		•	ce Certificate	□ Fsn	row Account	
	Performance		□ Financi			m 29 (FA Defe	erral)
	Guarantee Bo			und Agreement	01	20 (1712010	
J				by Trust Fund Agreemen	t		
	maioatoo moor	omo anacroquito	add of a otalial	o, . racer and rigitation	•		

III. ESTIMATE ADJUSTMENT 40 CFR Part 264 Subpart H as adopted by reference in Rule 62-701.630, Florida Administrative Code, (F.A.C.) sets forth the method of annual cost estimate adjustment. Cost estimates may be adjusted by using an inflation factor or by recalculating the maximum costs of closure in current dollars. Select one of the methods of cost estimate ajustment below. □ (a) Inflation Factor Adjustment □ (b) Recalculated or New Cost Estimates Inflation adjustment using an inflation factor may only be made when a Department approved closure cost estimate exists and no changes have occurred in the facility operation which would necessitate modification to the closure plan. The inflation factor is derived from the most recent Implicit Price Deflator for Gross National Product published by the U.S. Department of Commerce in its survey of Current Business. The inflation factor is the result of dividing the latest published annual Deflatory by the Deflator for the previous year. The inflation factor may also be obtained from the Solid Waste website www.dep.state.fl.us/waste/categories/swfr or call the Financial Coordinator at (850) 245-8706. This adjustment is based on the Department approved closing cost estimate dated: Latest Department Approved **Current Year Inflation** Inflation Adjusted Closing **Closing Cost** Estimate: Factor, e.g. 1.02 Cost Estimate: This adjustment is based on the Department approved long-term care cost estimate dated: Inflation Adjusted Annual Latest Department Approved Current Year Inflation Long-Term Care Cost Annual Long-Term Care Cost Estimate: Factor, e.g. 1.02 Estimate: Number of Years of Long Term Care Remaining: 30 **Inflation Adjusted Long-Term Care Cost Estimate:** Signature by: □ Owner/Operator □ Engineer (check what applies) Signature Address City, State, Zip Code Name Title Date E-Mail Address

Telephone Number

IV. ESTIMATED CLOSING COST (check what applies)

Notes: 1. Cost estimates for the time period when the extent and manner of landfill operation makes closing most exp

- 2. Cost estimate must be certified by a professional engineer.
- 3. Cost estimates based on third party suppliers of material, equipment and labor at fair market value.
- 4. In some cases, a price quote in support of individual item estimates may be required.

Number							
Description	Unit	of Units	Cost / Unit	Total Cost			
1. Proposed Monitoring Wells	(Do not include	wells alread	dy in existence.)				
	EA						
		Subtotal	Proposed Monitoring Wells:				
2. Slope and Fill (bedding layer l	between waste a	nd barrier la	yer):				
Excavation	CY						
Placement and Spreading	-CY- AC.	67	\$1,235.05	\$82,748.35			
Compaction	CY						
Off-Site Material	CY						
Delivery	CY						
			Subtotal Slope and Fill:	\$82,748.35			
B. Cover Material (Barrier Layer)	:		_				
Off-Site Clay	CY	160,755	\$9.26	\$1,488,591.30			
Synthetics - 40 mil	SY						
Synthetics - GCL	SY						
Synthetics - Geonet	SY						
Synthetics - Other (explain)			 -				
			Subtotal Cover Material:	\$1,488,591.30			
. Top Soil Cover:	-		_	+ 1, 100,000 1100			
Off-Site Material	CY	160,755	\$4.37	\$702,499.35			
Delivery	CY			ψ. σΞ, ισσίσσ			
Spread	CY		 -				
			Subtotal Top Soil Cover:	\$702,499.35			
i. Vegetative Layer				ψ1 02,433.33			
Sodding	SY	3,000	\$1.29	\$3,870.00			
Hydroseeding	AC	67	\$10.03	\$672.01			
Fertilizer	AC		Ψ10.03	ψ012.01			
Mulch	AC						
Other (explain) Return trips to	EA	4	\$514.61	\$2,058.44			
			Subtotal Vegetative Layer:				
irrigate, establish vegetation 5. Stormwater Control System:	-		Cubicial vegetative Layer	\$6,600.45			
Earthwork	CY						
Grading	SY						
· ·	LF	3,119	ФЭЭ 47	\$70,002,02			
Piping Ditches	LF LF	2,000	\$22.47	\$70,083.93			
Berms	LF LF	12,114	\$2.06	\$4,120.00			
Control Structures		11	\$4.01	\$48,577.14			
Other (explain)Drop Inlets	EΑ	12	\$2,161.34	\$23,774.74			
Other (exhiairi)	<u>EA</u>		\$2,158.17	\$25,898.04			
	_	Subiolai	Stormwater Control System: _	\$172,453.85			

Description	Unit	Number of Units	Cost / Unit	Total Cos
7. Passive Gas Control:				
Wells	EA LF	550	\$95.72	\$52,646.00
Pipe and Fittings	LF			
Monitoring Probes	EA	9	\$1,629.24	\$14,663.16
NSPS/Title V requirements	LS	1		
8. Active Gas Extraction Control		S	Subtotal Passive Gas Cont	rol: \$67,309.16
Traps	EA			
Sumps	EA			
Flare Assembly	EA			
Flame Arrestor	EA			
Mist Eliminator	EA			
Flow Meter	EA		<u> </u>	
Blowers	EA			
Collection System	LF			
Other (explain)	LI			
		Subtotal A	active Gas Extraction Cont	rol:
9. Security System:	•			
Fencing	LF			
Gate(s)	EA			
Sign(s)	EA			
5 ()			Subtotal Security Syste	 em:
10. Engineering:				
Closure Plan Report	LS	1	\$25,730.25	\$25,730.25
Certified Engineering Drawings	LS	1	\$15,438.15	\$15,438.15
NSPS/Title V Air Permit	LS	1		
Final Survey	LS	1	\$4,837.29	\$4,837.29
Certification of Closure	LS	1	\$18,525.78	\$18,525.78
Other (explain)	·			
			Subtotal Engineeri	ng: \$64,531.47
Description Hours	Cost /	Hour I	Hours Cost / Hour	Total Cos
11. Professional Services				
	t Management		Quality Assurance	
P.E. Supervisor				
On-Site Engineer				
Office Engineer				
On-Site Technician	 			
Other (explain) 1	\$102	<u>.,9(</u>	1 \$180,09	\$282,999.00
See explanations				
		Number		
Description	Unit	of Units	Cost / Unit	Total Cos
Quality Assurance Testing	LS	1	\$30,447.89	\$30,447.89
			ıbtotal Professional Servic	

		Subtotal of 1-11 Above:	\$2,898,180.82
		_	
12.	Contingency 10 % of	f Subtotal of 1-11 Above	\$289,818.08
		Subtotal Contingency:	\$289,818.08
		Estimated Closing Cost Subtotal: _	\$3,187,998.90
	Description		Total Cost
13.	Site Specific Costs		
	Mobilization	_	\$133,797.30
	Waste Tire Facility		
	Materials Recovery Facility		
	Special Wastes	_	\$18,525.78
	Leachate Management System I	Modification	
	Other (explain)	_	
		Subtotal Site Specific Costs:	\$152,323.08
		TOTAL ESTIMATED CLOSING COSTS (\$):	\$3,340,321.98

V. ANNUAL COST FOR L	ONG-TERM CARE			
See 62-701.600(1)a.1., 62-701				
certified closed and Departme	· · · · · · · · · · · · · · · · · · ·			years remaining.
(Check Term Length) 5 Year				
	timates must be certified by			
2. Cost es	timates based on third party	suppliers of material, e	equipment and labor at fair r	narket value.
3. In some	cases, a price quote in sup	port of individual item e	estimates may be required.	
All items must be address	sed. Attach a detailed ex	planation for all entri	es left blank.	
	Sampling			
	Frequency	Number of	(Cost / Well) /	
Description	(Events / Year)	Wells	Event	Annual Cost
1. Groundwater Monitorin		3)(a)]		
Monthly	12			
Quarterly	4			
Semi-Annually	2		\$661.63	\$34,404.76
Annually	1			
			Groundwater Monitoring:	\$34,404.76
2. Surface Water Monitor	• • • • • • • • • • • • • • • • • • • •	(8)(b)]		
Monthly	12			
Quarterly	4			
Semi-Annually	2			
Annually	1			
		Subtotal S	urface Water Monitoring:	
3. Gas Monitoring [62-701	·			
Monthly	12			
Quarterly	4	16	\$64.33	\$4,117.12
Semi-Annually	2			
Annually	1			
			Subtotal Gas Monitoring:	\$4,117.12
4. Leachate Monitoring [6		62-701.510(8)c]		
Monthly	12			
Quarterly	4			
Semi-Annually	2			
Annually	1			
Other (explain)				
		Subto	otal Leachate Monitoring:	
		Number of		
Description	Unit	Units / Year	Cost / Unit	Annual Cost
5. Leachate Collection/Tr	eatment Systems Maint	enance		
<u>Maintenance</u>				
Collection Pipes	LF			
Sumps, Traps	EA			

Lift Stations

Cleaning

Tanks

EΑ

LS

EΑ

		Number of		
Description	Unit	Units / Year	Cost / Unit	Annual Cost
5. (continued)				
<u>Impoundments</u>				
Liner Repair	SY			
Sludge Removal	CY			
Aeration Systems				
Floating Aerators	EA			
Spray Aerators	EA			
<u>Disposal</u>				
Off-site (Includes	1000 gallon			
ransportation and disposal)		Subtotal Leacha	te Collection / Treatment Systems Maintenance:	
6. Groundwater Monitoring We	ell Maintenance		e joterne mannenance.	
Monitoring Wells	LF			
Replacement	EA	1	\$3,602.24	\$3,602.24
Abandonment	EA		\$3,002.24	\$3,002.24
, is all actions of		tal Groundwater Moni	toring Well Maintenance:	¢2.000.04
7. Gas System Maintenance	Gusto	tar Greatianater meni	ioning Wom Mamilenance.	\$3,602.24
Piping, Vents	LF			
Blowers	EA			
Flaring Units	EA			
Meters, Valves	EA			
Compressors	EA			
Flame Arrestors	EA			
Operation	LS	1	\$2,573.03	ΦΩ 57 2 Ω2
o p s s s s s s s s s s s s s s s s s s			as System Maintenance:	\$2,573.03 \$2,573.03
8. Landscape Maintenance				\$2,573.03
Mowing	AC	_268	\$42.29	\$11,333.72
Fertilizer	AC		φ42.29	ψ11,555.72
	,	Subtotal I	_andscape Maintenance:	\$11,333.72
9. Erosion Control and Cover	Maintenance			\$11,333.72
Sodding	SY			
Regrading	AC			
Liner Repair	SY	1	\$7,719.08	\$7,719.08
Clay	CY		φι,ι 19.00	φ1,119.00
,		ototal Erosion Control	and Cover Maintenance:	\$7,719.08
10. Storm Water Management				ψι,ι 13.00
Conveyance Maintenance	LS	1	\$3,602.24	\$3,602.24
, ,		orm Water Manageme	nt System Maintenance:	\$3,602.24
11. Security System Maintena		2	,	φ3,002.24
Fences	LS	1	\$3,087.63	\$3,087.63
Gate(s)	EA		φυ,υοι.υυ	φ3,007.03
Sign(s)	EA			
<u> </u>	_, ,	Subtotal Secur	ity System Maintenance:	Ф0 00= 00
		Guntotal Gecul	ity System Maintenance.	\$3.087.63

		Number of			
Description	Unit	Units / Year	Cost / Unit	Annual Cost	
12. Utilities	LS	1	\$1,235.05	\$1,235.05	
			Subtotal Utilities:	\$1,235.05	
Leachate Collection/Trea	atment Systems C	peration			
<u>Operation</u>					
P.E. Supervisor	HR				
On-Site Engineer	HR				
Office Engineer	HR				
OnSite Technician	HR				
Materials	LS	1			
	Subtotal Le	achate Collection/Treatn	nent Systems Operation:		
14. Administrative			•		
P.E. Supervisor	HR				
On-Site Engineer	HR				
Office Engineer	HR	112	\$72.04	\$8,068.48	
OnSite Technician	HR				
Other 1 - 5 year Report	LS	1	\$4,631.45	\$4,631.45	
			Subtotal Administrative:	\$12,699.93	
	-		- -		
		S	Subtotal of 1-14 Above:	\$84,374.80	
15. Contingency	10 % of Subtotal of 1-14 Above			\$8,437.48	
			Subtotal Contingency:	\$8,437.48	
		Number of			
Description	Unit	Units / Year	Cost / Unit	Annual Cost	
16. Site Specific Costs					
	-	Sub	total Site Specific Costs:		
	ANNUAL LONG-TERM CARE COST (\$ / YEAR):_			\$92,812.28	
		30			
	TOTAL LONG-TERM CARE COST (\$):				

VI. CERTIFICATION BY ENGINEER

This is to certify that the Cost Estimates pertaining to the engineering features of this solid waste management facility have been examined by me and found to conform to engineering principles applicable to such facilities. In my professional judgment, the Cost Estimates are a true, correct and complete representation of the financial liabilities for closing and/or long-term care of the facility and comply with the requirements of Rule 62-701.630 F.A.C. and all other Department of Environmental Protection rules, and statutes of the State of Florida. It is understood that the Cost Estimates shall be submitted to the Department annually, revised or adjusted as required by Rule 62-701.630(4), F.A.C.

No. 74652

Baker, P.E.

Name and Title (please type)

ORIDA

Plorida Registration Number

(please affix seal)

4140 NW 37th Place, Suite A

Mailing Address

Gainesville, Florida 32606

City, State, Zip Code

lisa@locklearconsulting.com

E-Mail address (if available)

352-672-6867

Telephone Number

VII. SIGNATURE BY OWNER/OPERATOR

Signature of Applicant

Mailing Address

John Arnold, P.E.

Name and Title (please type)

St. Petersburg, Florida 33712

City, State, Zip Code

Mailing Address

St. Petersburg, Florida 33712

St. Petersburg, Florida 33712

City, State, Zip Code

813-477-1719

E-Mail address (if available)

Telephone Number